



**FATİH SULTAN MEHMET VAKIF ÜNİVERSİTESİ
LİSANSÜSTÜ EĞİTİM ENSTİTÜSÜ
İNŞAAT MÜHENDİSLİĞİ ANABİLİM DALI
İNŞAAT MÜHENDİSLİĞİ PROGRAMI**

**BETONARME ÇERÇEVELİ VE ÇERÇEVELİ PERDELİ
TAŞIYICI SİSTEMLİ HASTANE BİNALARINDA DEPREM
VE DÜŞEY YÜKLERDEN MEYDANA GELEN KOLON
EKSENEL KUVVET ORANLARININ TESPİTİ**

YÜKSEK LİSANS TEZİ

MOHAMMAD NABİ MORAD ZADEH

İSTANBUL, 2024



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İSTANBUL, 2024

02/07/2024

LİSANSÜSTÜ EĞİTİM ENSTİTÜSÜ MÜDÜRLÜĞÜNE

İnşaat Mühendisliği Anabilim Dalı İnşaat Mühendisliği Tezli Yüksek Lisans programı öğrencisi 210241101 numaralı Mohammad Nabi Morad Zadeh'in hazırladığı "Betonarme Çerçeve ve Çerçeve Perdeli Taşıyıcı Sistemli Hastahane Binalarında Deprem ve Düşey Yüklerden Meydana Gelen Kolon Eksenel Kuvvet Oranlarının Tespiti" konulu Yüksek Lisans tezi ile ilgili Tez Savunma Sınavı, 02/07/2024 Salı günü saat 14:00'da yapılmış, sorulara alınan cevaplar sonunda adayın tezinin **Kabulüne Oy Birliği** ile karar verilmiştir.

Tez adı değişikliği yapılması halinde: Tez adının
.....
şeklinde değiştirilmesi uygundur.

Jüri Üyesi	Karar
1. Prof. İbrahim EKİZ (Danışman)	KABUL
2. Prof. Dr. Bilge DORAN	KABUL
3. Dr. Öğr. Üyesi Cenk AKSOYLAR	KABUL
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5.	
6. (İkinci Danışman)*.....	

*2. Danışman varsa doldurulması gerekmektedir.

ETİK BİLDİRİM

Bu tezin yazılmasında bilimsel ahlak kurallarına uyulduğunu, başkalarının eserlerinden yararlanılması durumunda bilimsel normlara uygun olarak atıfta bulunulduğunu, kullanılan verilerde herhangi bir tahrifat yapılmadığını, tezin herhangi bir kısmının bağlı olduğum üniversite veya bir başka üniversitedeki başka bir çalışma olarak sunulmadığını beyan ederim.

Mohammad Nabi Morad Zadeh

Aileme

Mohammad Nabi Morad Zadeh

BETONARME ÇERÇEVELİ VE ÇERÇEVELİ PERDELİ TAŞIYICI SİSTEMLİ HASTANE BİNALARINDA DEPREM VE DÜŞEY YÜKLERDEN MEYDANA GELEN KOLON EKSENEL KUVVET ORANLARININ TESPİTİ

Mohammad Nabi Morad Zadeh

ÖZET

Kolonların brüt en kesit alanı, TBDY 2018'e göre, $A_c \geq N_{dm}/0,4f_{ck}$ koşulunu sağlayacak şekilde hesaplanmaktadır. Bu hesaplamada kullanılan N_{dm} eksenel basınç kuvveti, sabit yük G ve azaltılmış hareketli yük Q 'un dikey etkileriyle, deprem etkisi E 'nin birleşiminden kaynaklanan en büyük eksenel basınç kuvveti olarak tanımlanır, yani $G + Q + E$ altında hesaplanır. Düşey yüklerin neden olduğu eksenel basınç kuvveti kolaylıkla hesaplanabilirken, deprem etkisinin neden olduğu eksenel kuvvet ancak sistem boyutlandırıldıktan sonra hesaplanır.

Bu tezde, perdesiz ve farklı perdeli betonarme kolonlarda düşey yüklerden ve deprem yüklerinden kaynaklanan eksenel kuvvetleri belirlemek için, boyutlandırma hesaplarına girmeden önce yaklaşık değerler belirlenmiştir. Bu amaçla, düşey yükler için belirli oranlar (k_p , k_E) tespit edilmiştir. Bu oranlar ve düşey yüklerin birleşik etkisi $G + Q$ ile çarpılarak, kolonlarda meydana gelen eksenel kuvvetlerin deprem etkisi altında yaklaşık olarak hesaplanması ve boyutlandırma çalışmalarında kolaylık sağlanmıştır.

Tez dört bölümden oluşmaktadır. Birinci bölümde, konunun tanıtımı yapılarak çalışmanın amacı ve kapsamı hakkında bilgi verilmiştir.

Birinci bölümde, güncellenen deprem yönetmeliğine uygun olarak Eşdeğer Deprem Yüğü Yöntemi kullanılarak taban kesme kuvvetinin hesaplanması için gerekli parametrelerin detaylı bir şekilde nasıl bulunduğu anlatılmıştır.

İkinci ve üçüncü bölümde, tezin amacı olan oranların belirlenmesi için üç farklı deprem noktasında beş farklı zemin sınıfı için 6 katlı, 9 katlı ve 12 katlı olduğu varsayılan bir hastane binasının tasarımı yapılmıştır. Bu süreçte, ön boyutlandırma, deprem parametrelerinin belirlenmesi ve taban kesme kuvvetinin hesaplanması gibi çalışmalar yürütülmüştür. Ayrıca, verilen bilgilere göre kolonlarda düşey yüklerden ve deprem yüklerinden kaynaklanan eksenel kuvvetler hesaplanmıştır.

Sonuç kısmında ise yapılan hesaplar sonucunda elde edilen katsayılar (düşey yükler için k_p , deprem yükleri için k_E) değerleri üç farklı deprem noktası ve beş farklı zemin sınıfı için perdesiz ve perdeli 6 katlı, 9 katlı ve 12 katlı hastane binaları için sunulmuştur.

Anahtar Kelimeler: Yapı Periyodu, Taban Kesme Kuvveti, Yapı Kütlesi, Eksenel Kuvvet, Eşdeğer Deprem Yüğü

DETERMINATION OF COLUMN AXIAL FORCE RATIOS CAUSED BY EARTHQUAKES AND VERTICAL LOADS IN HOSPITAL BUILDINGS WITH REINFORCED CONCRETE FRAME AND FRAME CURTAIN CARRIER SYSTEM

Mohammad Nabi Morad Zadeh

ABSTRACT

The gross cross-sectional area of the columns is calculated according to TBDY 2018, satisfying the condition $A_c \geq N_{dm}/0.4f_{ck}$. The axial compressive force N_{dm} used in this calculation is defined as the maximum axial compressive force resulting from the combined effect of the dead load G , the reduced live load Q , and the earthquake effect E , calculated under the combination of $G + Q + E$. While the axial compressive force caused by vertical loads can be easily calculated, the axial force caused by the earthquake effect is calculated only after the system is sized.

In this thesis, approximate values have been determined before entering into the sizing calculations to determine the axial forces arising from vertical loads and earthquake loads in non-shear and different shear reinforced concrete columns. For this purpose, specific ratios (k_P , k_E) have been determined for vertical loads. These ratios, multiplied by the combined effect of vertical loads $G + Q$, provide an approximate calculation of the axial forces in the columns under earthquake effect, thus facilitating the sizing calculations.

The thesis consists of four chapters. In the first chapter, an introduction to the subject is provided, along with information about the purpose and scope of the study. The First chapter explains in detail how the necessary parameters for calculating the base shear force using the Equivalent Seismic Load Method in accordance with the updated seismic regulation are obtained.

In the second and third chapter, the design of a hospital building, assumed to be 6, 9, and 12 storeys high, without shear walls and with different shear walls, is

carried out to determine the ratios aimed at the objective of the thesis for three different seismic points and five different soil classes. In this process, tasks such as preliminary sizing, determining earthquake parameters, and calculating base shear force were carried out. Additionally, axial forces caused by vertical loads and earthquake loads in the columns were calculated based on the given information.

In the Result chapter presents the coefficients obtained from the calculations (k_P for vertical loads, k_E for earthquake loads) for 6, 9, and 12-story hospital buildings without and with shear walls for three different seismic points and five different soil classes.

Keywords: Building Period, Base Shear Force, Building Mass, Axial Force, Equivalent Seismic Load

ÖN SÖZ

Bu çalışmanın gerçekleştirilmesinde, iki yıl boyunca değerli bilgilerini bizlerle paylaşan, kullandığı her kelimenin hayatıma kattığı önemini asla unutmayacağım saygıdeğer danışman hocam; Prof. İbrahim Ekiz'e, çalışmam boyunca yardımlarını esirgemeyen Arş. Gör. Dr. Sezer Öztürk'e sonsuz teşekkürlerimi sunarım.

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SEMBOLLER

A_c	: KOLON brüt enkesit alanı
A_t	: Amprik doğal titreşim periyodu hesabında kullanılan eşdeğer alan
A_{wj}	: j'inci perdenin gövde enkesit alanı
C_t	: Amprik doğal titreşim periyodu hesabında kullanılan katsayı
D	: Dayanım fazlalığı katsayısı
D_{fi}	: Binanın i'inci katında F_{fi} fiktif yüklerine göre hesaplanan yer değiştirme
$d_{fi}^{(X)}$	: (X) deprem doğrultusunda binanın hâkim doğal titreşim periyodunun hesabında i' inci kata etki ettirilen fiktif yükten oluşan yer değiştirme
$E_d^{(H)}$	: Doğrultu birleştirilmesi uygulanmış tasarıma esas yatay deprem etkisi
$E_d^{(X)}$	: (X) doğrultusundaki depremin etkisi altında tasarıma esas deprem etkisi
$E_d^{(Y)}$	: (Y) doğrultusundaki depremin etkisi altında tasarıma esas deprem etkisi
$E_d^{(Z)}$	: (Z) doğrultusundaki depremin etkisi altında tasarıma esas deprem etkisi
F_{ck}	: Beton karakteristik dayanımı
F_{fi}	: Binanın hâkim doğal titreşim periyodunun hesabında i'inci kata etki ettirilen fiktif yük
F_i	: Eşdeğer deprem yükü yönteminde i'inci kata etkiyen eşdeğer deprem yükü
$F_{iE}^{(X)}$	: (X) deprem doğrultusunda i'inci kat kütle merkezine etkiyen eşdeğer deprem yükü
F_s	: Kısa periyot bölgesi için yerel zemin etki katsayıları
F_1	: 1,0 saniye periyot için yerel zemin etki katsayısı
G	: Sabit yük etkisi

g	: Yerçekimi ivmesi
H_N	: Binanın toplam yüksekliği
I	: Bina önem katsayısı
I_{wj}	: j'inci perdenin planda uzunluğu
m_j^(s)	: Tipik sonlu elemanlar düğüm noktası j'ye etkileyen tekil kütle
m_i	: i'inci katın toplam kütlesi
m_t	: Binanın bodrum katlarının üstündeki üst bölümünün toplam kütlesi
n	: Hareketli yük katılım katsayısı
N_{dm}	: Düşey yükler ve deprem yüklerinin ortak etkisi altında hesaplanan eksenel basınç kuvvetlerinin en büyüğü
R	: Taşıyıcı sistem davranış katsayısı
R_a(T)	: Deprem yükü azaltma katsayısı
S_s	: Kısa periyot harita spektral ivme katsayısı
S₁	: 1.0 saniye periyot için harita spektral ivme katsayısı
S_{DS}	: Kısa periyot tasarım spektral ivme katsayısı
S_{D1}	: 1.0 saniye periyot için tasarım spektral ivme katsayısı
S_{ae}(T)	: Elastik spektral ivme
S_{aR}(T)	: Azaltılmış tasarım spektral ivmesi
T	: Bina doğal titreşim periyodu
T_A, T_B	: Yatay elastik tasarım ivme spektrumu köşe periyodu
T_L	: Yatay elastik tasarım spektrumunda sabit yer değiştirme bölgesine geçiş periyodu
T_P^(X)	: (X) deprem doğrultusunda binanın hâkim doğal titreşim periyodu
T_{PA}	: Amprik olarak hesaplanan hâkim doğal titreşim periyodu
V_T	: Taban kesme kuvveti
ΔF_N	: Binanın N'inci katına (tepesine) etkileyen ek eşdeğer deprem yükü
w_i	: Binanın i'inci katının, hareketli yük katılım katsayısı kullanılarak hesaplanan ağırlığı
w_j^(s)	: Tipik sonlu elemanlar düğüm noktası j'ye etkileyen tekil ağırlık

$w_{G,j}^{(s)}$	: Tipik sonlu elemanlar düğüm noktası j'ye etkiyen tekil sabit ağırlık
$w_{Q,j}^{(s)}$	:Tipik sonlu elemanlar düğüm noktası j'ye etkiyen tekil ek (hareketli) ağırlık
Q	: Hareketli yük etkisi
β	: Hareketli yük azaltma sayısı
γ	: % eksiltme değeri

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KISALTMALAR

BKS	Bina kullanım sınıfı
BYS	Bina yükseklik sınıfı
DD-1	Deprem Yer Hareketi Düzeyi-1
DD-2	Deprem Yer Hareketi Düzeyi-2
DD-3	Deprem Yer Hareketi Düzeyi-3
DD-4	Deprem Yer Hareketi Düzeyi-4
DGT	Dayanıma Göre Tasarım
DTS	Deprem tasarım sınıfı
TDBYBHY 2007 Yönetmelik	Deprem Bölgelerinde Yapılacak binalar Hakkında
TBDY 2018	Türkiye Bina Deprem Yönetmeliği
TS 498	Yapı Elemanlarının Boyutlandırılmasında Alınacak
Yüklerin Hesap Değerleri	
TS 500	Betonarme Yapıların Tasarım ve Yapım Kuralları

GİRİŞ

Depremeler dünya genelinde insanları maddi, manevi ve psikolojik açıdan kitlesel olarak olumsuz etkiler. Türkiye, coğrafi konumu itibarıyla aktif fay hatlarına sahip bir deprem kuşağında yer alır. Bu nedenle Türkiye tarih boyunca birçok büyük depremle karşılaşmış ve bu depremler sonucunda ciddi can ve mal kayıpları yaşanmıştır. Bu kayıpları minimize etmek amacıyla, yapıların depreme dayanıklı bir şekilde tasarlanması ve inşa edilmesi için belirli kurallar konmuştur. Bu kurallar, daha anlaşılır ve bir arada bulunabilir olması amacıyla deprem yönetmeliği adı altında düzenlenmiştir.

Yapı mühendisliği, diğer mühendislik ve bilim dalları gibi sürekli bir gelişim sürecindedir. Bu alanda bilgi birikimi ve teknolojik ilerlemeler sayesinde yapı çözümleri konusunda sürekli olarak yeni yöntemler ve hesap esasları gelişmektedir. Bu ilerlemelerle birlikte, yapı tasarımı ve yapımına yönelik hazırlanan yönetmelikler de zaman içinde yenilenmektedir. Türkiye’de, geçmişten günümüze kadar bir dizi yönetmelik ve talimatname uygulanmıştır. Bu belgeler arasında 1940 İtalyan Yapı Talimatnamesi, 1944 Zelzele Mıntıkları Muvakkat Yapı Talimatnamesi, 1949 Türkiye Yersarsıntısı Bölgeleri Yapı Yönetmeliği, 1953 Yersarsıntısı Bölgelerinde Yapılacak Yapılar Hakkında Yönetmelik, 1962 Afet Bölgelerinde Yapılacak Yapılar Hakkında Yönetmelik, 1968 Afet Bölgelerinde Yapılacak Yapılar Hakkında Yönetmelik, 1975 Afet Bölgelerinde Yapılacak Yapılar Hakkında Yönetmelik, 1997 Afet Bölgelerinde Yapılacak Yapılar Hakkında Yönetmelik, 2007 Deprem Bölgelerinde Yapılacak Binalar Hakkında Yönetmelik ve en son olarak 18 Mart 2018’de yürürlüğe giren Türkiye Bina Deprem Yönetmeliği (TBDY 2018) bulunmaktadır. Yeni yönetmelikte birçok konuda revizyon yapılmıştır, bu da yapı sektöründe güvenli ve dayanıklı binaların inşası için güncel standartların takip edilmesine olanak sağlamaktadır.

TEZİN AMACI

TBDY 2018'e göre kolon brüt enkesit alanı (A_c), $N_{dm}/0,4f_{ck}$ formülüyle hesaplanmaktadır. Bu hesaplama için kullanılan N_{dm} ; sabit yükler (G), hareketli yükler için TS 498'de tanımlanan hareketli yük azaltma katsayıları dikkate alınarak hesaplanan hareketli yükler (Q) ve E deprem etkisinin ortak etkisi $G + Q + E$ altında hesaplanan eksenel basınç kuvvetlerinin en büyüğüdür. Ancak, bu ortak etki kolon boyutlandırma işlemlerini karmaşık hale getirebilmektedir.

Bu bağlamda, bir tez çalışmasında deprem kuvveti etkisi altında kolonlarda oluşan eksenel basınç kuvvetinin daha hızlı hesaplanabilmesi üzerinde durulmuştur. Bu amaç doğrultusunda, kolonlarda oluşan eksenel basınç kuvvetinin yapının düşey yükleri etkisi altında ($NG + Q$) ve buna bağlı olarak eksenel basınç kuvvetinin hesaplanmasında kullanılabilecek k_P ve k_E oranları belirlenmeye çalışılmıştır. Bu oranlar ve yapıların düşey yükleri kullanılarak doğrudan yapının deprem kuvveti altında kolonlarda oluşacak eksenel basınç kuvveti bulunması ve hesaplamalarda basitlik sağlanması amaçlanmıştır.

Esin Dincel 2020 tarihli yüksek lisan tezinde okul binalarında ve Veli Tosun 2022 tarihli yüksek lisans tezinde Büro ve konut binalarında deprem ve düşey yüklerden meydana gelen kolon eksenel kuvvet oranlarının belirlenmesi ile ilgili çalışma yapmıştır.[6],[7].

Araştırma kapsamında, perdesiz ve perdeli betonarme çerçeveden oluşan bir hastane binası, İzmir, İstanbul, Ankara illerinde ve her il için farklı zemin sınıflarında 6 katlı, 9 katlı ve 12 katlı olarak kabul edilmiştir. Her durum için ayrı ayrı oran hesaplamaları yapılmıştır.

Tezde, perdesiz binalar Model 1, 1. Perdeli sistemleri Model 2, 2. Perdeli sistemleri Model 3 ve 3. Perdeli sistemleri ise Model 4 olarak tanımlanmıştır.

BİRİNCİ BÖLÜM

1. EŞDEĞER DEPREM YÜKÜ YÖNTEMİ

TBDY 2018'in 4. Bölümü, "Deprem Etkisi Altında Dayanıma Göre Tasarım Hesap Esasları" başlığını içerir ve eşdeğer deprem yükü yöntemini detaylı bir şekilde açıklar. 2. Bölüm "Deprem Yer Hareketi" ve 3. Bölüm "Deprem Etkisi Altında Binaların Değerlendirilmesi ve Tasarımı İçin Genel Esaslar" ise ilgili parametreleri detaylı olarak ele alır.

1.1. DOĞRUSAL HESAP YÖNTEMİNİN SEÇİMİ

Dayanıma göre tasarım yöntemlerinden biri olan Eşdeğer Deprem Yükü Yöntemi, tasarım esnasında Modal Hesap Yöntemi (Mod Birleştirme ve Mod Toplama) yerine kullanılabilir. Ancak, bu tez çalışmasında Modal Hesap Yöntemi tercih edilmeyecek ve sadece Eşdeğer Deprem Yükü Yöntemi üzerinde durulacaktır. Eşdeğer Deprem Yükü Yönteminin uygulanabileceği bina türleri ve yükseklik sınıfları sınırlıdır, bu kısıtlamalar Çizelge 1.1'de detaylı olarak açıklanmıştır. Bu bağlamda, tezde Modal Hesap Yöntemi üzerine detaylı bir anlatım bulunmamaktadır.

Çizelge 1.1: Eşdeğer Deprem Yöntemini Uygulanabileceği Binalar [1].

Bina Türü	İzin Verilen Bina Yükseklik Sınıfı	
	DTS = 1, 1a, 2, 2a	DTS = 3, 3a, 4, 4a
Her bir katta burulma düzensizliği katsayısının $\eta_{bi} \leq 2.0$ koşulunu sağladığı ve ayrıca B2 türü düzensizliğinin olmadığı binalar	BYS ≥ 4	BYS ≥ 5
Diğer tüm binalar	BYS ≥ 5	BYS ≥ 6

Çizelge (1.1)'de DTS ifadesi deprem tasarım sınıfını ifade etmektedir. BYS ifadesi ise bina yükseklik sınıfını ifade etmektedir. İlerleyen bölümlerde bu ifadelerin tanım ve hesapları ayrıntılı olarak anlatılmaktadır.

1.2. BİNA YÜKSEKLİĞİ VE BİNA YÜKSEKLİK SINIFLARI

1.2.1. Bina Tabanı ve Bina Yüksekliği

Rijit bodrum perdelerinin binayı her taraftan ya da minimum üç taraftan çevrelemesi veya birbirine dik bina eksenlerinin her biri doğrultusundaki hakim titreşim modunda bodrum katlar dahil binanın tamamı için hesaplanan doğal titreşim periyodunun zemin kat döşemesi de dahil bodrum katlarının kütlelerini hesaba dahil etmeksizin aynı doğrultuda hesaplanan doğal titreşim periyoduna oranının 1.1' den küçük olması ($T_{p,tüm} \leq 1.1 T_{p,üst}$) halinde bu iki koşulu da sağlayan bodrumlu binalarda bina tabanı; bodrum perdelerinin üst kotundaki kat döşemesindeki seviyesi kabul edilir. Bu koşullardan birini sağlamayan bodrumlu binalarda ve bodrumsuz binalarda bina tabanı temel üst kotunda kabul edilmektedir [1].

1.2.2. Bina Yükseklik Sınıfları

Yönetmelik, deprem etkisi altında tasarımda binaları yüksekliklerine göre sekiz sınıfa ayırmıştır. Bina yüksekliği, daha önce belirlenen bina tabanından itibaren ölçülen H_N olarak tanımlanmıştır [1]. Bina yükseklik sınıfı, hesaplanan bu H_N ve deprem tasarım sınıfı (DTS)'ye bağlı olarak Çizelge 1.2'ye göre belirlenir.

Çizelge 1.2: Bina Yükseklik Sınıfları ve Deprem Tasarım Sınıflarına Göre Tanımlanan Bina Yükseklik Aralıkları [1].

Bina Yükseklik Sınıfı	Bina Yükseklik Sınıfları ve Deprem Tasarım Sınıflarına Göre Tanımlanan Bina Yükseklik Aralıkları [m]		
	DTS = 1, 1a, 2, 2a	DTS = 3, 3a	DTS = 4, 4a
BYS = 1	$H_N > 70$	$H_N > 91$	$H_N > 105$
BYS = 2	$56 < H_N \leq 70$	$70 < H_N \leq 91$	$91 < H_N \leq 105$
BYS = 3	$42 < H_N \leq 56$	$56 < H_N \leq 70$	$56 < H_N \leq 91$
BYS = 4	$28 < H_N \leq 42$	$42 < H_N \leq 56$	
BYS = 5	$17.5 < H_N \leq 28$	$28 < H_N \leq 42$	
BYS = 6	$10.5 < H_N \leq 17.5$	$17.5 < H_N \leq 28$	
BYS = 7	$7 < H_N \leq 10.5$	$10.5 < H_N \leq 17.5$	
BYS = 8	$H_N \leq 7$	$H_N \leq 10.5$	

1.3. DEPREM TASARIM SINIFININ BELİRLENMESİ

Deprem etkisi altında tasarımda esas alınacak Deprem Tasarım sınıfı (DTS); kısa periyot tasarım spektral ivme katsayısı S_{DS} ve bina kullanım sınıfına (BKS) bağlı olarak Çizelge 1.3'e göre belirlenmektedir. S_{DS} ifadesinin hesabı ilerleyen bölümlerde detaylı olarak anlatılmıştır.

Çizelge 1.3: Deprem Tasarım sınıfları [1].

DD-2 Deprem Yer Hareketi Düzeyinde Kısa Periyot Tasarım Spektral İvme Katsayısı (S_{DS})	Bina Kullanım Sınıfı	
	BKS = 1	BKS = 2, 3
$S_{DS} < 0.33$	DTS = 4a	DTS = 4
$0.33 \leq S_{DS} < 0.50$	DTS = 3a	DTS = 3
$0.50 \leq S_{DS} < 0.75$	DTS = 2a	DTS = 2
$0.75 \leq S_{DS}$	DTS = 1a	DTS = 1

1.4. BİNA KULLANIM SINIFI VE BİNA ÖNEM KATSAYILARI

Deprem tasarım sınıfını belirlemek için kullanılan bina kullanım sınıfı ise Çizelge 1.4'te bina kullanım amacına bağlı olarak belirlenmektedir. Ayrıca bina önem katsayıları da aynı çizelgeden bina kullanım sınıflarına göre belirlenmektedir.

Çizelge 1.4: Bina Kullanım Sınıfları ve Bina Önem katsayıları [1].

Bina Kullanım Sınıfı	Binanın Kullanım Amacı	Bina Önem Katsayısı (I)
BKS = 1	Deprem sonrası kullanımı gereken binalar, insanların uzun süreli ve yoğun olarak bulunduğu binalar, değerli eşyanın saklandığı binalar ve tehlikeli madde içeren binalar a) Deprem sonrasında hemen kullanılması gerekli binalar (Hastaneler, dispanserler, sağlık ocakları, itfaiye bina ve tesisleri, PTT ve diğer haberleşme tesisleri, ulaşım istasyonları ve terminalleri, enerji üretim ve dağıtım tesisleri, vilayet, kaymakamlık ve belediye yönetim binaları, ilk yardım ve afet planlama istasyonları) b) Okullar, diğer eğitim bina ve tesisleri, yurt ve yatakhaneler, askeri kışlalar, cezaevleri, vb. c) Müzeler d) Toksik, patlayıcı, parlayıcı, vb. özellikleri olan maddelerin bulunduğu veya depolandığı binalar	1.5
BKS = 2	İnsanların kısa süreli ve yoğun olarak bulunduğu binalar Alışveriş merkezleri, spor tesisleri, sinema, tiyatro, konser salonları, ibadethaneler, vb.	1.2
BKS = 3	Diğer binalar BKS = 1 ve BKS = 2 için verilen tanımlara girmeyen diğer binalar (Konutlar, işyerleri, oteller, bina türü endüstri yapıları, vb.)	1.0

1.5. KÜTLENİN MODELLENMESİ

Taşıyıcı sistem elemanlarının çubuk, levha (membran) veya kabuk sonlu eleman şeklinde Modellendiğinde tekil düğüm noktası kütleleri, bağlı sonlu elemanların kapsama alanlarındaki yayılı kütlelerin bileşkeleri olarak tanımlanırlar. Sonlu eleman düğüm noktalarındaki tekil kütleler, sadece iki yatay veya ek olarak düşey öteleme serbestlik derecelerine karşılık gelecek şekilde tanımlanır [1].

Sonlu eleman düğüm noktası j ' ye etkiyen tekil kütle $m^{(s)}$ değeri Denklem (1.1) ile bulunur. Denklemdeki $w_{G,j}^{(s)}$ ve $w_{Q,j}^{(s)}$ sonlu eleman düğüm noktası j 'ye etki eden sabit ve hareketli yük bileşkesini gösterir [1].

$$W_j^{(s)} = W_{G,j}^{(s)} + nW_{Q,j}^{(s)} \quad m_j^{(s)} = \frac{w_j}{g} \quad (1.1)$$

Denklem (1.1)'deki n hareketli yük kütle katılım sayısını ifade etmektedir. Hareketli yük katılım sayısı Çizelge (1.5)'te tanımlanan bina kullanım amacına göre belirlenmektedir.

Çizelge 1.5: Hareketli Yük Kütle Katılım Sayısı [1].

Binanın Kullanım Amacı	n
Depo, antrepo, vb.	0.80
Okul, öğrenci yurdu, spor tesisi, sinema, tiyatro, konser salonu, ibadethane, lokanta, mağaza, vb.	0.60
Konut, işyeri, otel, hastane, otopark, vb.	0.30

Binanın toplam eşdeğer deprem yükü hesabı için kullanılacak olan binanın toplam kütlesi m_t Denklem (1.2) ile belirlenmektedir.

$$m_t = \sum_i^N m_i \quad (1.2)$$

m_i i ' inci kat döşemesinin toplam kütlesidir. Kat kütlelerinin hesabı da Denklem (1.1) esas alınarak yapılır [1].

1.6. BİNANIN DOĞAL TİTREŞİM PERİYODUNUN BELİRLENMESİ

Binanın hâkim doğal titreşim periyodu $T_p^{(X)}$ daha kesin bir hesap yapılmadıkça Eşdeğer Deprem Yüğü Yöntemi uygulanan tüm binalarda X deprem doğrultusundaki binanın hâkim doğal titreşim periyodu Denklem (1.3) ile bulunacaktır [1].

$$T_p^{(X)} = 2\pi \left[\frac{\sum_{i=1}^N m_i d_{fi}^{(X)2}}{\sum_{i=1}^N F_{fi}^{(X)} d_{fi}^{(X)}} \right]^{1/2} \quad (1.3)$$

i' inci kata etkiyen fiktif yük $F_{fi}^{(X)}$ Denklem (1.10)' de $(V_{te}^{(X)} - \Delta F_{NE}^{(X)})$ yerine Örneğin 100 gibi herhangi bir değer konularak hesaplanacaktır [1].

Binanın hâkim doğal titreşim periyodu $DTS = 1, 1a, 2, 2a, BYS \geq 6$ olan binalarda ve $DTS = 3, 3a, 4, 4a$ olan tüm binalarda Denklem (1.3) hesaplanmadan Denklem (1.4) ile hesaplanan ampirik doğal titreşim periyodu T_{pA} alınabilir [1].

$$T_{pA} = C_t H_N^{3/4} \quad (1.4)$$

Binanın Denklem (1.3)'de hesaplanan hakim doğal titreşim periyodu $T_p^{(X)}$ 'in deprem hesabında kullanılacak en büyük değeri Denklem (1.6)'da hesaplanan T_{pA} periyodunun 1.4 katından daha büyük olmamalıdır [1].

Denklem (1.4)'te verilen C_t , taşıyıcı sistemi sadece betonarme çerçevelerden oluşan binalarda 0.1, çelik çerçevelerden veya çaprazlı çelik çerçevelerden oluşan binalarda 0.08, diğer tüm binalarda 0.07 alınacaktır. Deprem etkilerinin tamamının ise C_t Denklem (1.5) ile bulunacaktır [1].

$$C_t = \frac{0.1}{\sqrt{A_t}} \leq 0,07 \quad (1.5)$$

Denklem (1.5)'teki eşdeğer alanı olan A_t Denklem (1.8)'teki ifade ile bulunmaktadır.

$$A_t = \sum_j A_{WJ} \left[0.2 + \left(\frac{L_{WJ}}{H_N} \right)^2 \right] \leq \sum_j A_{WJ} \quad (1.6)$$

1.7. AZALTILMIŞ TASARIM SPEKTRAL İVMESİ

Yatay doğrultuda azaltılmış deprem yüklerinin belirlenmesinde de kullanılacak olan azaltılmış tasarım ivme spektrumunun belirli bir T doğal titreşim periyodu için

ordinatı olan azaltılmış tasarım spektral ivmesi $S_{aR}(T)$ Denklem (1.7) ile belirlenmektedir [1].

$$S_{aR}(T) = \frac{S_{ae}(T)}{R_a(T)} \quad (1.7)$$

Denklem (1.7)'de $S_{ae}(T)$ DD-2 deprem yer hareketi için Yatay Elastik Tasarım Spektral İvmesini, $R_a(T)$ Deprem Yüğü Azaltma Katsayısını ifade etmektedir.

1.8. YATAY ELASTİK SPEKTRUMU

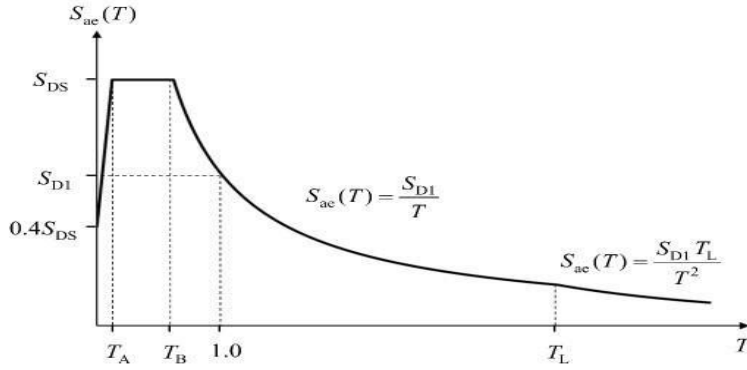
Herhangi bir yer hareketi düzeyi için yatay elastik tasarım spektral ivmeleri $S_{ae}(T)$, doğal titreşim periyodu T 'ye bağlı olarak g cinsinden tanımlanmaktadır [1].

Yani Denklem (1.8) ile bulunan $S_{ae}(T)$, g yerçekimi ivmesi değerine bölünerek Denklem (1.7)'de kullanılmaktadır.

$$\begin{aligned} S_{ae}(T) &= (0.4 + 0.6 \frac{T}{T_A}) S_{DS} & (0 \leq T \leq T_A) \\ S_{ae}(T) &= S_{DS} & (T_A \leq T \leq T_B) \\ S_{ae}(T) &= \frac{S_{D1} \cdot T_L}{T^2} & (T_L \leq T) \\ S_{ae}(T) &= \frac{S_{D1}}{T} & (T_B \leq T \leq T_L) \end{aligned} \quad (1.8)$$

Denklem (1.8)'de S_{DS} ve S_{D1} tasarım spektral ivme katsayısını ifade etmektedir ve Denklem (1.10) ile belirlenmektedir.

T ise doğal titreşim periyodunu ifade etmektedir. Şekil 1.1 'de verilen grafiğe göre yatay tasarım spektrumunun köşe periyotları olan T_A ve T_B ise Denklem (1.9)'da belirtildiği üzere tasarım spektral ivme katsayılarına bağlı olarak bulunmaktadır. Sabit yer değiştirme bölgesine geçiş periyodu $T_L = 6$ sn olarak alınmaktadır [1].



Şekil 1.1: Yatay elastik tasarım spektrumu [1].

$$T_A = 0.2 \frac{S_{D1}}{S_{DS}} \quad T_B = \frac{S_{D1}}{S_{DS}} \quad (1.9)$$

1.9. DEPREM YER HAREKET DÜZEYLERİ

TBDY 2018'de DD-1, DD-2, DD-3, DD-4 olmak üzere dört farklı deprem yer hareket düzeyi tanımlanmıştır.

1.9.1. Deprem Yer Hareket Düzeyi-1 (DD-1)

Spektral büyüklüklerin 50 yılda aşılma olasılığının %2 ve buna bağlı ve buna karşı gelen tekrarlanma periyodunun 2475 yıl olduğu çok seyrek deprem yer hareketini nitelemektedir. Bu deprem yer hareketi, göz önüne alınan en büyük deprem yer hareketi olarak da adlandırılmaktadır [1].

1.9.2. Deprem Yer Hareketi Düzeyi-2 (DD-2)

Spektral büyüklüklerin 50 yılda aşılma olasılığının %10 ve buna karşı gelen tekrarlanma periyodunun 475 yıl olduğu seyrek deprem yer hareketini nitelemektedir. Bu deprem yer hareketi, standart tasarım deprem yer hareketi olarak da adlandırılmaktadır [1].

1.9.3. Deprem Yer Hareketi Düzeyi-3 (DD-3)

Spektral büyüklüklerin 50 yılda aşılma olasılığının %50 ve buna karşı gelen tekrarlanma periyodunun 72 yıl olduğu sık deprem yer hareketini nitelemektedir [1].

1.9.4. Deprem Yer Hareketi Düzeyi-4 (DD-4)

Spektral büyüklüklerin 50 yılda aşılma olasılığının %68 (30 yılda aşılma olasılığı %50) ve buna karşı gelen tekrarlanma periyodunun 43 yıl olduğu çok sık deprem yer hareketini nitelemektedir. Bu deprem yer hareketi, servis deprem yer hareketi olarak da adlandırılmaktadır [1].

1.10. TASARIM SPEKTRAL İVME KATSAYISI

Birbirine dik iki yatay doğrultudaki deprem etkilerinin geometrik ortalamasına karşı gelen harita spektral ivme katsayıları, belirli bir deprem yer hareketi düzeyi için referans zemin koşulu $((V_s)_{30} = 760 \text{ m/s})$ göz önüne alınarak %5 sönüm oranı için boyutsuz harita spektral ivme katsayıları tanımlanmıştır. Bu boyutsuz harita spektral ivme katsayıları S_S , kısa periyot harita spektral ivme katsayısı, S_1 1,0 saniye için harita spektral ivme katsayısı şeklindedir [1].

Yönetmelikte DD-1, DD-2, DD-3, DD-4 olarak tanımlanan dört farklı deprem yer hareketi düzeyi için Türkiye deprem Haritalarından ([httpModel 1://tdth.afad.gov.tr/](http://tdth.afad.gov.tr/)) yararlanılarak yapının inşa edileceği yere ait harita spektral ivme katsayıları (S_S , S_1) bulunur.

$$S_{D1} = S_1 F_1 \quad S_{DS} = S_S F_S \quad (1.10)$$

F_S ve F_1 ise yerel zemin etki katsayılarını ifade etmektedir ve Çizelge (1.6), Çizelge (1.7)'de verilen harita spektral ivme katsayı değerlerine ve binanın uygulanacağı alanın yerel zemin sınıfına bağlı olarak belirlenmektedir. Çizelgelerde yer alan Yerel zemin sınıflarının tanımları ise Çizelge (1.8)'de verilmiştir.

Çizelge 1.6: Kısa Periyot Bölgesi için Yerel Zemin Etki Katsayıları [1].

Yerel Zemin Sınıfı	1.0 saniye periyot için Yerel Zemin Etki Katsayısı F1					
	$S_1 \leq 0.10$	$S_1 \leq 0.20$	$S_1 \leq 0.30$	$S_1 \leq 0.40$	$S_1 \leq 0.50$	$S_1 \leq 0.60$
ZA	0.8	0.8	0.8	0.8	0.8	0.8
ZB	0.8	0.8	0.8	0.8	0.8	0.8
ZC	1.5	1.5	1.5	1.5	1.5	1.4
ZD	2.4	2.2	2.0	1.9	1.8	1.7
ZE	4.2	3.3	2.8	2.4	2.2	2.0
ZF	Sahaya özel zemin davranış analizi yapılacaktır.					

Çizelge 1.7: 1.0 Saniye Periyot için Yerel Zemin Etki Katsayıları [1].

Yerel Zemin Sınıfı	1.0 saniye periyot için Yerel Zemin Etki Katsayısı F1					
	$S_1 \leq 0.10$	$S_1 = 0.20$	$S_1 = 0.30$	$S_1 = 0.40$	$S_1 = 0.50$	$S_1 \geq 0.60$
ZA	0.8	0.8	0.8	0.8	0.9	0.8
ZB	0.8	0.8	0.8	0.8	0.9	0.8
ZC	1.5	1.5	1.5	1.5	1.5	1.4
ZD	2.4	2.2	2.0	1.9	1.8	1.7
ZE	4.2	3.3	2.8	2.4	2.2	2.0
ZF	Sahaya özel zemin davranış analizi yapılacaktır.					

Çizelge 1.8: Yerel Zemin Sınıfları [1].

Yerel Zemin Sınıfı	Zemin Cinsi	Üst 30 metrede ortalama		
		$(V_s)_{30}$ [m/s]	$(N_{60})_{30}$ [darbe/30cm]	$(C_u)_{30}$ [Kpa]
ZA	Sağlam, sert kayalar	> 1500	–	–
ZB	Az ayrılmış, orta sağlam kayalar	760 – 1500	–	–
ZC	Çok sıkı kum, çakıl ve sert kil tabakaları veya ayrılmış, çok çatlaklı zayıf kayalar	360 – 760	> 50	> 250
ZD	Orta sıkı – sıkı kum, çakıl veya çok katı kil tabakaları	180 – 360	15 – 50	70 – 250
ZE	Gevşek kum, çakıl veya yumuşak – katı kil tabakaları veya $PI > 20$ ve $w > \% 40$ koşullarını sağlayan toplamda 3 metreden daha kalın yumuşak kil tabakası ($C_u < 25$ kPa) içeren profiller	< 180	< 15	< 70
ZF	Sahaya özel araştırma ve değerlendirme gerektiren zeminler: 1) Deprem etkisi altında çökme ve potansiyel göçme riskine sahip zeminler (sıvılaşabilir zeminler, yüksek derecede hassas killer, göçebilir zayıf çimentolu zeminler vb.), 2) Toplam kalınlığı 3 metreden fazla turba ve/veya organik içeriği yüksek killer, 3) Toplam kalınlığı 8 metreden fazla olan yüksek plastisiteli ($PI > 50$) killer, 4) Çok kalın (> 35 m) yumuşak veya orta katıkiller.			

1.11. DEPREM YÜKÜ AZALTMA KATSAYISI

Denklem (1.7)'de azaltılmış tasarım spektral ivme katsayısının hesabında kullanılan Deprem yükü azaltma katsayısı $R_a(T)$ yapının doğal titreşim periyodu T ve spektrum köşe periyodu değerlerine bağlı olarak seçilecek Denklem (1.11) veya Denklem (1.12)'e göre hesaplanmaktadır.

$$R_a(T) = \frac{R}{T} \quad (T > T_B) \quad (1.11)$$

$$R_a(T) = D + \left(\frac{R}{I} - D\right) \frac{T}{T_B} \quad (T < T_B) \quad (1.12)$$

Bu denklemlerde I Bina Önem Katsayısını ifade etmektedir ve Çizelge (1.4)'te verilen bina kullanım amacına göre belirlenmektedir. R Taşıyıcı Sistem Davranış Katsayısı, D Dayanım Fazlalığı katsayısı olup TBDY 2018'de bulunan Tablo 4.1'e göre belirlenmektedir.

1.12. TOPLAM EŞDEĞER DEPREM YÜKÜNÜN BELİRLENMESİ

Eşdeğer Deprem Yüğü Yöntemi; birbirine dik X ve Y deprem doğrultusunda binaya etki eden depremler için her doğrultuda ayrı ayrı uygulanır. Buradaki bağıntılar (X) deprem doğrultusu için verilmiştir [1].

Göz önüne alınan X deprem doğrultusunda binanın tümüne etkiyen Toplam Eşdeğer Deprem Yüğü (Taban Kesme Kuvveti), $V_{tE}^{(X)}$ Denklem (1.13) ile belirlenmektedir.

$$V_{tE}^{(X)} = m_t S_{aR}(T_p^{(X)}) \geq 0.04 m_t I S_{DS} g \quad (1.13)$$

Bu denklemde eşitliğin hangi tarafındaki değer büyük ise yapı için taban kesme kuvveti olarak o değer alınmaktadır. Denklemde bulunan I ifadesi bina önem katsayısı olup Çizelge (1.4)'ten elde edilmektedir. Denklemdeki diğer ifadeler ise m_t binanın toplam kütesini, $S_{aR}(T_p^{(X)})$ (X) deprem doğrultusunda binanın hakim doğal titreşim periyodu $T_p^{(X)}$ göz önüne alınarak hesaplanan azaltılmış tasarım spektral ivmesini, S_{DS} kısa periyot tasarım spektral ivme katsayısını ifade etmektedir. Bu ifadelerin hesabı ayrıntılı olarak yukarıdaki kısımlarda anlatılmıştır.

1.13. KATLARA ETKİYEN EŞDEĞER DEPREM YÜKLERİNİN BELİRLENMESİ

Toplam eşdeğer deprem yükü bina katlarına etkiyen eşdeğer deprem yüklerinin toplamı olarak Denklem (1.14) ile belirlenmektedir [1].

$$V_{tE}^{(X)} = \Delta F_{NE}^{(X)} + \sum_{i=1}^N F_{iE}^{(X)} \quad (1.14)$$

Binanın N'inci katına (tepesine) etkiyen ek eşdeğer deprem yükü $\Delta F_{NE}^{(X)}$ Denklem (1.15) ile belirlenmektedir [1].

$$\Delta F_{NE}^{(X)} = 0.0075 N V_{tE}^{(X)} \quad (1.15)$$

Toplam eşdeğer deprem yükü $\Delta F_{NE}^{(X)}$ dışında kalan kısım N'inci kat dahil olmak üzere bina katlarına Denklem (1.16) ile dağıtılmaktadır.

$$F_{iE}^{(X)} = (V_{tE}^{(X)} - \Delta F_{NE}^{(X)}) \frac{m_i H_i}{\sum_{j=1}^N m_j H_j} \quad (1.16)$$

Kat döşemelerinin rijit diyafram olarak Modellenmesi halinde eşdeğer deprem yükü $F_{iE}^{(X)}$ i'inci kattaki ana düğüm noktasına göz önüne alınan deprem doğrultusunda etki ettirilir. Kat döşemeleri levha (membran) şeklinde sonlu elemanlarla Modellendiğinde i' inci katta j'inci düğüm noktasına etki eden eşdeğer deprem yükü Denklem (1.17) ile hesaplanır [1].

$$f_{jE}^{(S)} = \frac{F_{jE}^{(X)}}{m_i} m_j^{(S)} \quad (1.17)$$

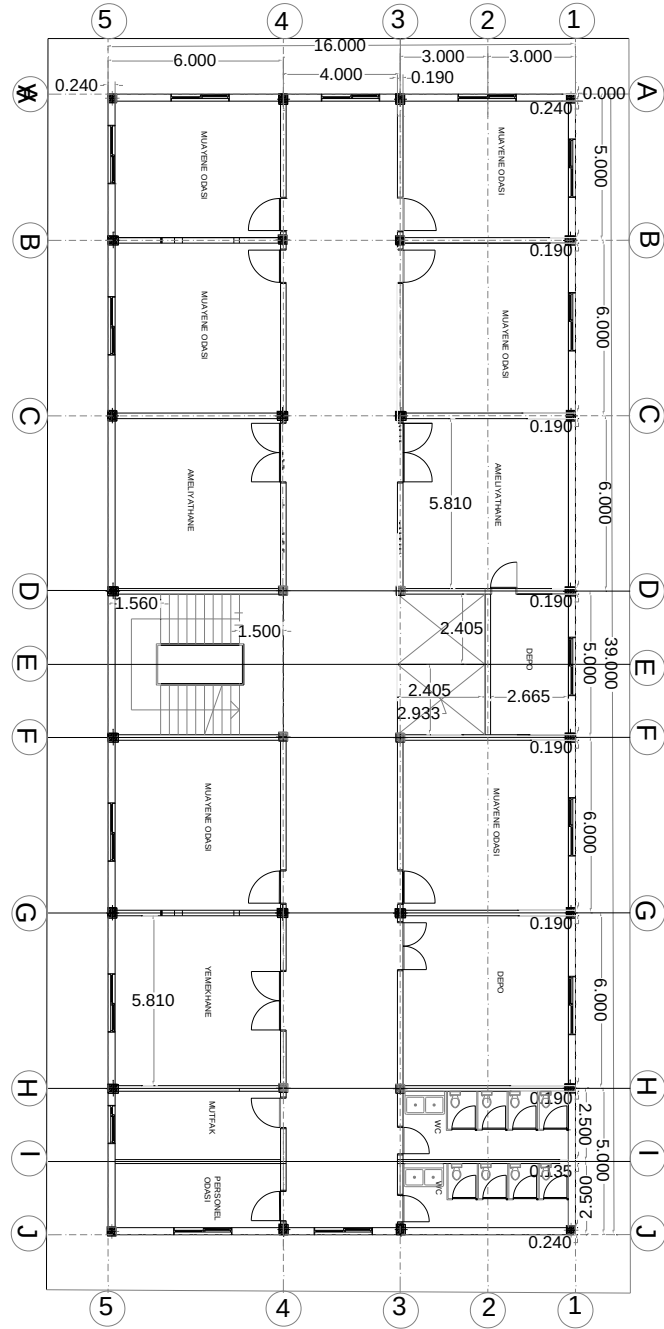
İKİNCİ BÖLÜM

2. BETONARME HASTANE BİNASININ TASARIMI

2.1. BİNA BİLGİLERİ

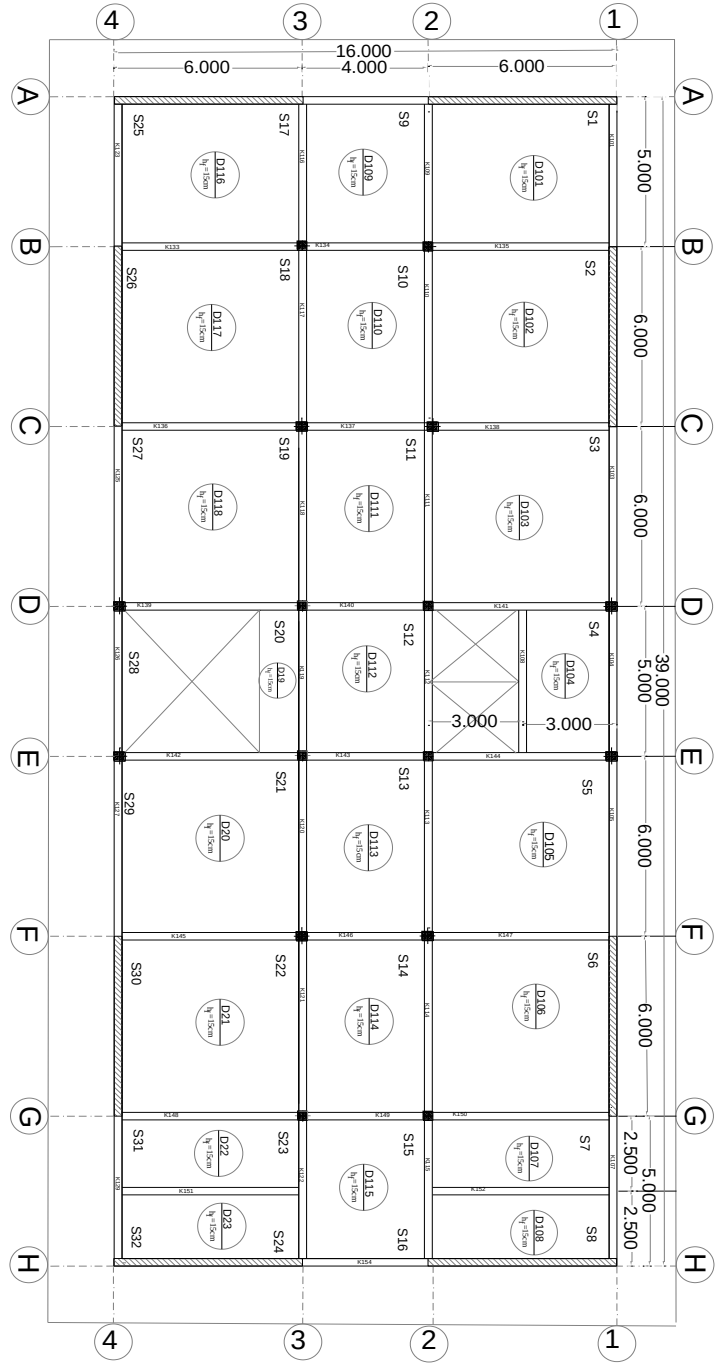
Bu çalışmada, simetrik betonarme çerçevelerden oluşan 6 katlı, 9 katlı ve 12 katlı bir hastane binasının detaylı tasarımı ve deprem hesabı gerçekleştirilmiştir. TS 498, TS 500 ve Türkiye Bina Deprem Yönetmeliği 2018 standartlarına göre yapılan bu tasarım, bina taşıyıcı sisteminde perde kullanılmadan, sadece betonarme çerçeveler ve perdeli sistem kullanılarak gerçekleştirilmiştir.

Hastane binasının her kat yüksekliği 3,10 m olarak belirlenmiş olup, C30 betonu kullanılmıştır. Döşeme kalınlıkları ise 15 cm olarak seçilmiştir. Kolon boyutları, yönetmeliklere uygun olarak hesaplanmış ve detayları ilerleyen bölümlerde açıklanmıştır. Toplam kat planı boyutları 39 m x 16 m'dir ve X yönlü aks aralıkları 5 m, 6 m, 6 m, 5 m, 6 m, 6 m, 5 m; Y yönlü aks aralıkları ise 6 m, 4 m, 6 m olarak düzenlenmiştir. Her iki yönde simetrik kat planı kullanılmıştır. Kat planı ve boyutları her katta aynı olup, tipik kat planı Şekil 3.1'de, tipik kat kalıp planı Şekil 2.2, 2.3, 2.4, 2.5'te gösterilmiştir.

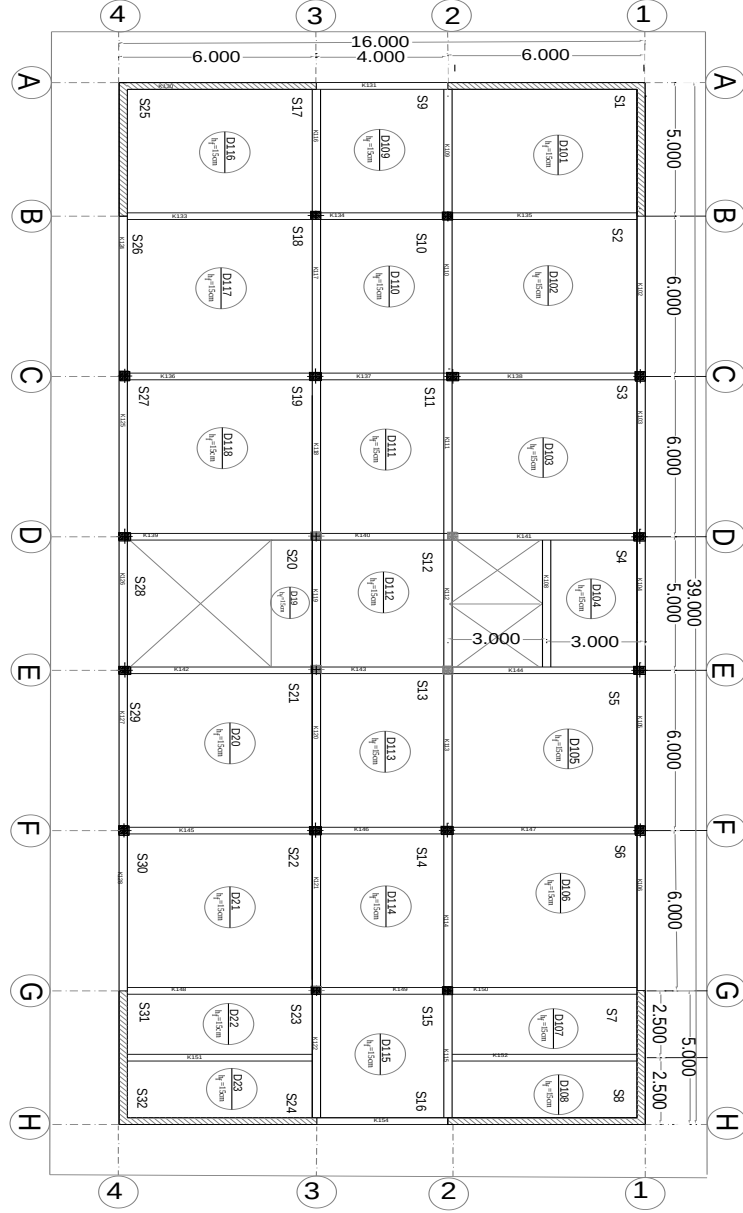


Şekil 2.1:Yapıya Ait Tipik Mimari Kat Planı.

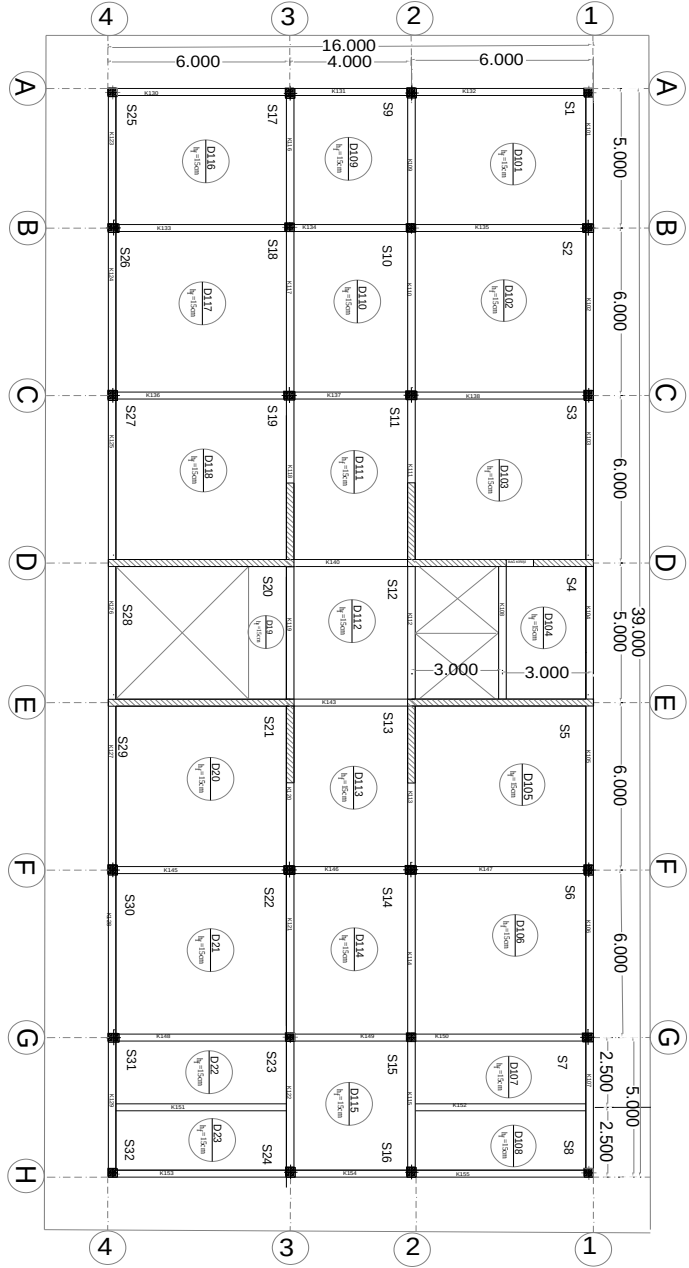




Şekil 2.3: Yapıya Ait Tipik Kat Kalıp Planı (Model 2).



Şekil 2.4: Yapıya Ait Tipik Kat Kalıp Planı (Model 3).



Şekil 2.5: Yapıya Ait Tipik Kat Kalıp Planı (Model 4).

2.2. ÖN BOYUTLANDIRMA

Hastane binasının TS 498, TS 500 ve Türkiye Bina Deprem Yönetmeliği 2018'e göre detaylı olarak tasarımı ve deprem hesabı yapılmıştır. Yapının taşıyıcı sisteminde önce çerçeve daha sonra da değişik konularda yerleştirilen perdeler ile çerçeve perde sistemler oluşturulmuştur.

2.2.1. Döşeme Hesap ve Tasarımı

2.2.1.1. Döşeme Kalınlığının Belirlenmesi

TS 500'de döşemeler düzgün yayılı yük taşıyan, dörtkenarı boyunca mesnetlenmiş ve uzun kenarının kısa kenarına oranı 2'den büyük olan ($l_1/l_s > 2$) betonarme plaklar tek doğrultuda çalışan plaklar, uzun kenarının kısa kenarına oranına oranı 2'den küçük olan döşemeler ($l_1/l_s < 2$) iki doğrultuda çalışan plaklar olarak tanımlanmaktadır.

Yapıda bulunan çift doğrultuda çalışan döşeme kalınlıklarının hesabı Denklem (2.1), tek doğrultuda çalışan döşeme kalınlıklarının hesabı Denklem (2.2) kullanılarak yapılmıştır.

$$h_f = \frac{l_{sn}}{15 + \frac{20}{m}} \times \left(1 - \frac{\alpha}{4}\right) \quad (2.1)$$

$$h_f = \frac{l_n}{30} \quad (2.2)$$

l_{sn} : Kısa kenar doğrultusundaki serbest açıklık

l_n : Döşeme serbest açıklığı m: Döşemenin uzun kenar açıklığının kısa kenar açıklığına oranı (l_1/l_{sn})

α : Sürekli kenar uzunluğunun toplam kenar uzunluğuna oranıdır.

Verilen denklemler kullanılarak yapılan hesaplamalar sonucunda döşeme kalınlığı $h_f = 15$ cm seçilmiştir.

2.2.1.2. Döşeme Yüklerinin Belirlenmesi

Döşemelerde kaplama malzemesi olarak karo mozaik kullanıldığı kabul edilmiştir. Döşemeler için hareketli yük TS 498'den alınmıştır.

Sabit Yükler (G):

$$\text{Döşeme öz ağırlığı: } 0,15 \times 25 = 3,75 \text{ kN/m}^2$$

$$\text{Kaplama + sıva toplam ağırlığı} = 1,51 \text{ kN/m}^2$$

$$\text{Toplam Sabit yük} = 5,26 \text{ kN/ m}^2$$

Hareketli yükler(Q):

$$\text{Muayene odaları: } 3,5 \text{ kN/m}^2, \text{ Ameliyathane odaları: } 3,5 \text{ kN/m}^2$$

$$\text{Depo döşemeleri: } 5 \text{ kN/m}^2, \text{ Koridor döşemeleri: } 5 \text{ kN/m}^2$$

$$\text{Yemekhane döşemeleri: } 5 \text{ kN/m}^2, \text{ Mutfaklar: } 3,5 \text{ kN/m}^2$$

$$\text{Personel odaları: } 3,5 \text{ kN/m}^2, \text{ Giriş: } 5 \text{ kN/m}^2, \text{ wc: } 5 \text{ kN/m}^2$$

2.2.2. Kiriş Boyutlarının ve Yüklerinin Belirlenmesi

2.2.2.1. Kiriş Boyutlarının Belirlenmesi

Kiriş ön boyutları TBDY 2018 ve TS500'de belirtilen koşullara bağlı alınarak seçilmiştir. Kiriş boyutları olan kiriş toplam yüksekliği ($h_{\text{kiriş}}$) ve kiriş gövde genişliği (b_w) ile ilgili olarak yönetmeliklerde aşağıdaki koşullar verilmiştir.

$$b_w \geq 250 \text{ mm (TBDY 2018)}$$

$$h_{\text{kiriş}} \geq 300 \text{ mm}, h_{\text{kiriş}} \geq 3 \times h_f$$

$$h_{\text{kiriş}} \leq 3,5 \times b_w$$

$$h_{\text{kiriş}} < 10 / 4$$

Bu koşullar göz önünde bulundurularak yapının kiriş boyutları X ve Y yönünde tüm açıklıklarda 25/60 cm olarak seçilmiştir.

2.2.2.2. Kirişlere gelen yüklerin belirlenmesi

Yapıdaki tüm kat kirişlerine, kendi ağırlıkları dışında döşeme ve duvarlardan gelen yükler bulunmaktadır. Döşemelerden kirişlere sabit yük (G) ve hareketli yük (Q) aktarımı mevcuttur. Döşemelerden kirişlere iletilen yükler, uzun kenar doğrultusunda trapez yaylı yük ve kısa kenar doğrultusunda üçgen yaylı yük olarak aktarılmıştır.

Kirişler üzerinde, dış duvarlarda 24 cm kalınlığındaki tuğla duvar ve iç duvarlarda 19 cm kalınlığındaki tuğla duvar bulunmaktadır. Tuvalet, personel ve mutfak arasındaki duvarlar ise 13,5 cm kalınlığındadır. Hastane binasının bir katında toplam 55 adet kiriş bulunmaktadır, ancak yapı her iki doğrultuda simetrik olduğu için sadece 24 adet kiriş için hesap yapılmıştır. Kirişlere gelen yüklerin hesabı detaylı olarak açıklanmış olup, bu hesaplamaların sonuçları Çizelge (2.1)'de belirtilmiştir.

Duvar ağırlıkları:

$$19 \text{ cm'lik tuğla duvar: } 2,9 \times (3,10 - 0,60) = 7,25 \text{ kN/m}$$

$$24 \text{ cm'lik tuğla duvar: } 3,35 \times (3,10 - 0,60) = 8,375 \text{ kN/m}$$

24 cm'lik tuğla duvar (60cm yükseklikli kiriş altında, pencere olması durumunda):

$$3,35 \times (3,10 - (0,60 + 0,90)) = 5,36 \text{ kN/m}$$

$$13,5 \text{ cm'lik tuğla duvar: } 2,45 \times (3,10 - 0,60) = 6,125 \text{ kN/m}$$

Kiriş Zati Ağırlığı:

25/60 cm boyutundaki kiriş:

$$0,25 \times (0,60-0,15) \times 25 = 2,81 \text{ kN/m}$$

- **K101 Kirişi:**

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D101 döşemesinden: $5,26 \times (5/2) = 13,15 \text{ kN/m}$ (üçgen yayılı)

Hareketli yükler:

D101 döşemesinden: $3,5 \times (5/2) = 8,75 \text{ kN/m}$ (üçgen yayılı)

- **K102 Kirişi:**

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D102 döşemesinden: $5,26 \times (6/2) = 15,78 \text{ kN/m}$ (üçgen yayılı)

Hareketli yükler:

D102 döşemesinden: $3,5 \times (6/2) = 10,5 \text{ kN/m}$ (üçgen yayılı)

- **K103 Kirişi:**

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D103 döşemesinden: $5,26 \times (6/2) = 15,78 \text{ kN/m}$ (üçgen yayılı)

Hareketli yükler:

D103 döşemesinden: $3,5 \times (6/2) = 10,5 \text{ kN/m}$ (üçgen yayılı)

- K104 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D104 d řemesinden: $5,26 \times (3/2) = 7,89$ kN/m ( çgen yayılı)

Hareketli y kler:

D104 d řemesinden: $5 \times (3/2) = 7,5$ kN/m ( çgen yayılı)

- K108 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D104 d řemesinden: $5,26 \times (3/2) = 7,89$ kN/m (trapez yayılı)

Hareketli y kler:

D104 d řemesinden: $5 \times (3/2) = 7,5$ kN/m (trapez yayılı)

- K109 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D101 d řemesinden: 13,15 kN/m ( çgen yayılı)

D109 d řemesinden: $5,26 \times (4/2) = 10,52$ kN/m (trapez yayılı)

Hareketli y kler:

D101 d řemesinden: 8,75 kN/m ( çgen yayılı)

D109 d řemesinden: $5 \times (4/2) = 10$ kN/m (trapez yayılı)

- K110 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D102 döşemesinden: $5,26 \times (6/2) = 15,78$ kN/m (üçgen yayılı)

D110 döşemesinden: $5,26 \times (4/2) = 10,52$ kN/m (trapez yayılı)

Hareketli yükler:

D102 döşemesinden: $3,5 \times (6/2) = 10,50$ kN/m (üçgen yayılı)

D110 döşemesinden: $5 \times (4/2) = 10$ kN/m (trapez yayılı)

- K111 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D103 döşemesinden: $5,26 \times (6/2) = 15,78$ kN/m (üçgen yayılı)

D111 döşemesinden: $5,26 \times (4/2) = 10,52$ kN/m (trapez yayılı)

Hareketli yükler:

D103 döşemesinden: 10,50 kN/m (üçgen yayılı)

D111 döşemesinden: $5 \times (4/2) = 10$ kN/m (trapez yayılı)

- K112 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D112 döşemesinden: $5,26 \times (4/2) = 10,52$ kN/m (trapez yayılı)

Hareketli yükler:

D112 döşemesinden: $5 \times (4/2) = 10$ kN/m (trapez yayılı)

- K131 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 5,36 kN/m

D109 d řemesinden: $5,26 \times (4/2) = 10,52$ kN/m ( çgen yayılı)

Hareketli y kler:

D109 d řemesinden: $5 \times (4/2) = 10$ kN/m ( çgen yayılı)

- K132 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 5,36 kN/m

D101 d řemesinden: $5,26 \times (5/2) = 13,15$ kN/m (trapez yayılı)

Hareketli y kler:

D101 d řemesinden: $3,5 \times (5/2) = 8,75$ kN/m (trapez yayılı)

- K134 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D109 d řemesinden: 10,52 kN/m ( çgen yayılı)

D110 d řemesinden: $5,26 \times (4/2) = 10,52$ kN/m ( çgen yayılı)

Hareketli y kler:

D109 d řemesinden: 10 kN/m ( çgen yayılı)

D110 d řemesinden: $5 \times (4/2) = 10$ kN/m ( çgen yayılı)

- K135 Kirişı:

Sabit Y kler:

Kiriř Kendi aęırlıęı: 2,81 kN/m

Duvar aęırlıęı: 7,25 kN/m

D101 d řemesinden: 13,15 kN/m (trapez yayılı)

D102 d řemesinden: $5,26 \times (6/2) = 15,78$ kN/m ( çgen yayılı)

Hareketli y kler:

D101 d řemesinden: 8,75 kN/m (trapez yayılı)

D102 d řemesinden: $3,5 \times (6/2) = 10,5$ kN/m ( çgen yayılı)

- K137 Kirişı:

Sabit Y kler:

Kiriř Kendi aęırlıęı: 2,81 kN/m

Duvar aęırlıęı: 7,25 kN/m

D110 d řemesinden: 10,52 kN/m ( çgen yayılı)

D111 d řemesinden: 10,52 kN/m ( çgen yayılı)

Hareketli y kler:

D110 d řemesinden: 10 kN/m ( çgen yayılı)

D111 d řemesinden: 10 kN/m ( çgen yayılı)

- K138 Kirişı:

Sabit Y kler:

Kiriř Kendi aęırlıęı: 2,81 kN/m

Duvar aęırlıęı: 7,25 kN/m

D102 d řemesinden: 15,78 kN/m ( çgen yayılı)

D103 d řemesinden: 15,78 kN/m ( çgen yayılı)

Hareketli y kler:

D102 d řemesinden: 10,50 kN/m ( çgen yayılı)

D103 d řemesinden: 10,50 kN/m ( çgen yayılı)

- K140 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D111 döşemesinden: 10,52 kN/m (üçgen yayılı)

D112 döşemesinden: 10,52 kN/m (üçgen yayılı)

Hareketli yükler:

D111 döşemesinden: 10 kN/m (üçgen yayılı)

D112 döşemesinden: 10 kN/m (üçgen yayılı)

- K141 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D103 döşemesinden: 15,78 kN/m (üçgen yayılı)

D104 döşemesinden: $5,26 \times (3/2) = 7,89$ kN/m (trapez yayılı)

Hareketli yükler:

D103 döşemesinden: 10,50 kN/m (üçgen yayılı)

D104 döşemesinden: $3,5 \times (3/2) = 5,25$ kN/m (trapez yayılı)

- K147 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D105 döşemesinden: $5,26 \times (6/2) = 15,78$ kN/m (üçgen yayılı)

D106 döşemesinden: $5,26 \times (6/2) = 15,78$ kN/m (üçgen yayılı)

Hareketli yükler:

D105 döşemesinden: $3,5 \times (6/2) = 10,5$ kN/m (üçgen yayılı)

D106 döşemesinden: $5 \times (6/2) = 15$ kN/m (üçgen yayılı)

- K148 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D121 d řemesinden: $5,26 \times (6/2) = 15,78$ kN/m ( çgen yayılı)

D122 d řemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

Hareketli y kler:

D121 d řemesinden: $5 \times (6/2) = 15$ kN/m ( çgen yayılı)

D122 d řemesinden: $3,5 \times (2,5/2) = 4,375$ kN/m (trapez yayılı)

- K150 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 7,25 kN/m

D106 d řemesinden: $5,26 \times (6/2) = 15,78$ kN/m ( çgen yayılı)

D107 d řemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

Hareketli y kler:

D106 d řemesinden: $5 \times (6/2) = 15$ kN/m ( çgen yayılı)

D107 d řemesinden: $5 \times (2,5/2) = 6,25$ kN/m (trapez yayılı)

- K151 Kirişı:

Sabit Y kler:

Kiriř Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 6,125 kN/m

D122 d řemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

D123 d řemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

Hareketli y kler:

D122 d řemesinden: $3,5 \times (2,5/2) = 4,375$ kN/m (trapez yayılı)

D123 d řemesinden: $3,5 \times (2,5/2) = 4,375$ kN/m (trapez yayılı)

- K152 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 6,125 kN/m

D107 döşemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

D108 döşemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

Hareketli yükler:

D107 döşemesinden: $5 \times (2,5/2) = 6,25$ kN/m (trapez yayılı)

D108 döşemesinden: $5 \times (2,5/2) = 6,25$ kN/m (trapez yayılı)

- K153 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D123 döşemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

Hareketli yükler:

D123 döşemesinden: $5 \times (2,5/2) = 6,25$ kN/m (trapez yayılı)

- K155 Kirişi:

Sabit Yükler:

Kiriş Kendi ağırlığı: 2,81 kN/m

Duvar ağırlığı: 8,375 kN/m

D108 döşemesinden: $5,26 \times (2,5/2) = 6,575$ kN/m (trapez yayılı)

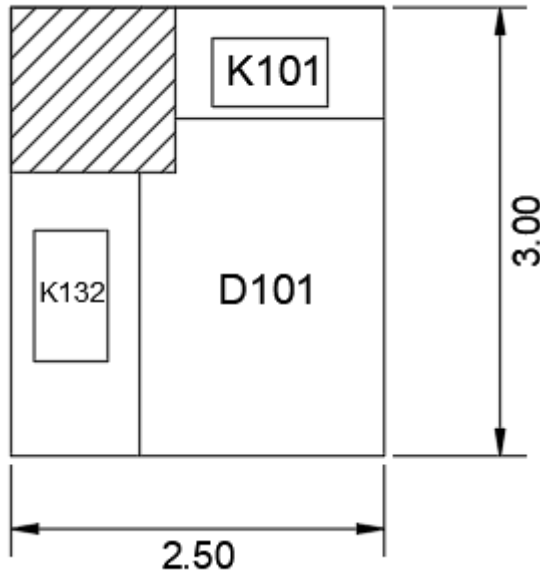
Hareketli yükler:

D108 döşemesinden: $3,5 \times (2,5/2) = 4,375$ kN/m (trapez yayılı)

2.2.2.3. Kolonlara Gelen Yüklerin Belirlenmesi

Kolonlara gelen sabit ve hareketli yükler 6 katlı, 9 katlı ve 12 katlı hastane yapısının kat planı simetrik olduğu ve her bir katta kat planı aynı olduğu için yalnızca gelen yüklerin değiştiği kolonlar için yük alma bölgesi ve hesaplar ayrıntılı olarak gösterilmiştir.

S1 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.6)



Şekil 2.6: S1 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D101 Döşemesi: $5,26 \times 2,5 \times 3 = 39,45$ kN

K101 Kirişi: $2,81 \times 2,5 = 7,025$ kN

K132 Kirişi: $2,81 \times 3 = 8,43$ kN

Duvardan Gelen Yük (K101): $5,36 \times 2,5 = 13,4$ kN

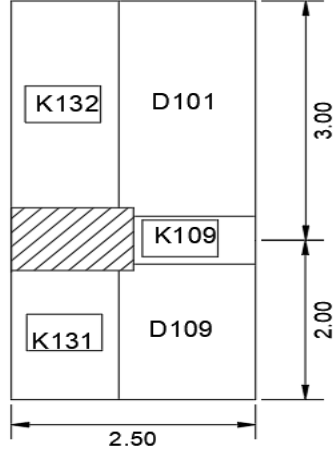
Duvardan Gelen Yük (K132): $5,36 \times 3 = 16,08$ kN

Kolon öz Ağırlığı: 6,975 kN

Hareketli Yükler

D101 Döşemesi: $3,50 \times 3 \times 2,5 = 26,25$ kN

S9 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.7)



Şekil 2.7: S9 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D101 Döşemesi: $5,26 \times 2,5 \times 3 = 39,45$ kN

D109 Döşemesi: $5,26 \times 2,5 \times 2 = 26,3$ kN

K131 Kirişi: $2,81 \times 2 = 5,62$ kN

K132 Kirişi: $2,81 \times 3 = 8,43$ kN

K109 Kirişi: $2,81 \times 2,5 = 7,025$ kN

Duvardan Gelen Yük (K131): $5,36 \times 2 = 10,72$ kN

Duvardan Gelen Yük (K132): $5,36 \times 3 = 16,08$ kN

Duvardan Gelen Yük (K109): $5,36 \times 2,5 = 13,4$ kN

Kolon öz Ağırlığı: 8,138 kN

Hareketli Yükler

D101 Döşemesi: $3,50 \times 3 \times 2,5 = 26,25$ kN

D109 Döşemesi: $5 \times 2 \times 2,5 = 25$ kN

S2 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.8)



Şekil 2.8: S2 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D101 Döşemesi: $5,26 \times 2,5 \times 3 = 39,45 \text{ kN}$

D102 Döşemesi: $5,26 \times 3 \times 3 = 47,34 \text{ kN}$

K101 Kirişi: $2,81 \times 2,5 = 7,025 \text{ kN}$

K102 Kirişi: $2,81 \times 3 = 8,43 \text{ kN}$

K135 Kirişi: $2,81 \times 3 = 8,43 \text{ kN}$

Duvardan Gelen Yük (K101): $5,36 \times 2,5 = 13,4 \text{ kN}$

Duvardan Gelen Yük (K102): $5,36 \times 3 = 16,08 \text{ kN}$

Duvardan Gelen Yük (K135): $7,25 \times 3 = 21,75 \text{ kN}$

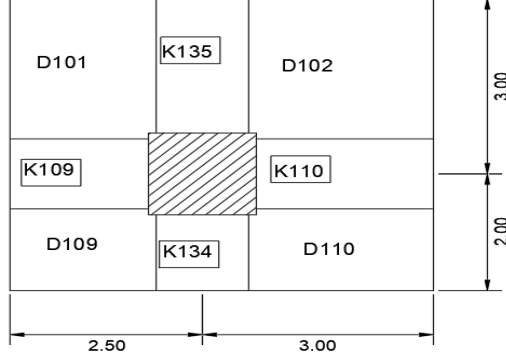
Kolon öz Ağırlığı: $8,138 \text{ kN}$

Hareketli Yükler

D101 Döşemesi: $3,50 \times 3 \times 2,5 = 26,25 \text{ kN}$

D102 Döşemesi: $3,50 \times 3 \times 3 = 31,5 \text{ kN}$

S10 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.9)



Şekil 2.9: S10 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D101 Döşemesi: $5,26 \times 2,5 \times 3 = 39,45 \text{ kN}$

D109 Döşemesi: $5,26 \times 2 \times 2,5 = 26,3 \text{ kN}$

D102 Döşemesi: $5,26 \times 3 \times 3 = 47,34 \text{ kN}$

D110 Döşemesi: $5,26 \times 3 \times 2 = 31,56 \text{ kN}$

K109 Kirişi: $2,81 \times 2,5 = 7,025 \text{ kN}$

K110 Kirişi: $2,81 \times 3 = 8,43 \text{ kN}$

K134 Kirişi: $2,81 \times 2 = 5,62 \text{ kN}$

K135 Kirişi: $2,81 \times 3 = 8,43 \text{ kN}$

Duvardan Gelen Yük (K109): $5,36 \times 2,5 = 13,4 \text{ kN}$

Duvardan Gelen Yük (K110): $5,36 \times 3 = 16,08 \text{ kN}$

Duvardan Gelen Yük (K135): $7,25 \times 3 = 21,75 \text{ kN}$

Kolon öz Ağırlığı: $6,975 \text{ kN}$

Hareketli Yükler

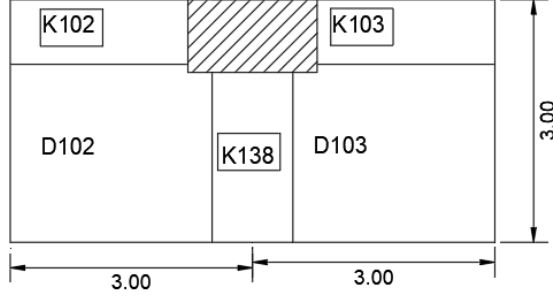
D101 Döşemesi: $3,50 \times 3 \times 2,5 = 26,25 \text{ kN}$

D109 Döşemesi: $5 \times 2 \times 2,5 = 25 \text{ kN}$

D102 Döşemesi: $3,50 \times 3 \times 3 = 31,5 \text{ kN}$

D110 Döşemesi: $5 \times 3 \times 2 = 30 \text{ kN}$

S3 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.10)



Şekil 2.10: S3 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D102 Döşemesi: $5,26 \times 3 \times 3 = 47,34$ kN

D103 Döşemesi: $5,26 \times 3 \times 3 = 47,34$ kN

K102 Kirişi: $2,81 \times 3 = 8,43$ kN

K103 Kirişi: $2,81 \times 3 = 8,43$ kN

K138 Kirişi: $2,81 \times 3 = 8,43$ kN

Duvarдан Gelen Yük (K102): $5,36 \times 3 = 16,08$ kN

Duvarдан Gelen Yük (K103): $8,375 \times 3 = 25,125$ kN

Duvarдан Gelen Yük (K138): $7,25 \times 3 = 21,75$ kN

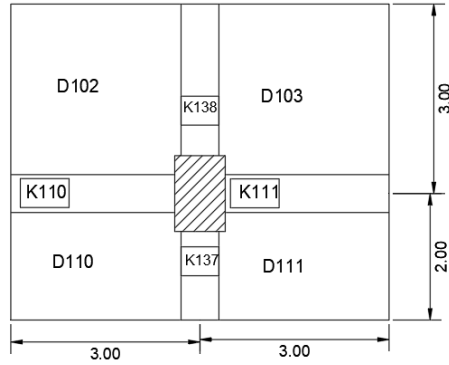
Kolon öz Ağırlığı: 8,138 kN

Hareketli Yükler

D102 Döşemesi: $3,50 \times 3 \times 3 = 31,5$ kN

D103 Döşemesi: $3,50 \times 3 \times 3 = 31,5$ kN

S11 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.11)



Şekil 2.11: S11 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D102 Döşemesi: $5,26 \times 3 \times 3 = 47,34 \text{ kN}$

D110 Döşemesi: $5,26 \times 3 \times 2 = 31,56 \text{ kN}$

D103 Döşemesi: $5,26 \times 3 \times 3 = 47,34 \text{ kN}$

D111 Döşemesi: $5,26 \times 3 \times 2 = 31,56 \text{ kN}$

K110 Kirişı: $2,81 \times 3 = 8,43 \text{ kN}$

K111 Kirişı: $2,81 \times 3 = 8,43 \text{ kN}$

K137 Kirişı: $2,81 \times 2 = 5,62 \text{ kN}$

K138 Kirişı: $2,81 \times 3 = 8,43 \text{ kN}$

Duvar dan Gelen Yü k (K110): $7,25 \times 3 = 21,75 \text{ kN}$

Duvarдан Gelen Yüк (K111): $7,25 \times 3 = 21,75 \text{ kN}$

Duvar dan Gelen Yü k (K138): $7,25 \times 3 = 21,75 \text{ kN}$

Kolon öz Ağırlığı: 8,138 kN

Hareketli Yükler

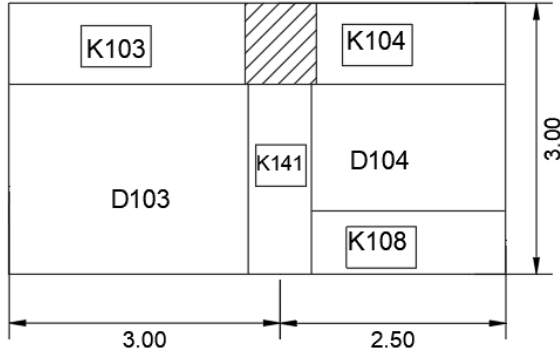
D102 Döşemesi: $3,50 \times 3 \times 3 = 31,5 \text{ kN}$

D110 Döşemesi: $5 \times 3 \times 2 = 30 \text{ kN}$

D103 Döşemesi: $3,50 \times 3 \times 3 = 31,5 \text{ kN}$

D111 Döşemesi: $5 \times 3 \times 2 = 30 \text{ kN}$

S4 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.12)



Şekil 2.12: S4 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D103 Döşemesi: $5,26 \times 3 \times 3 = 47,34 \text{ kN}$

D104 Döşemesi: $5,26 \times 3 \times 5 \times (0,75/2) = 29,59 \text{ kN}$

K103 Kirişı: $2,81 \times 3 = 8,43 \text{ kN}$

K104 Kirişi: $2,81 \times 2.5 = 7,025 \text{ kN}$

K141 Kirişı: $2,81 \times 3 = 8,43 \text{ kN}$

K108 Kirişi: $2,81 \times 5 \times 0,25 = 3,5125 \text{ kN}$

Duvardan Gelen Yük (K103): $8,375 \times 3 = 21,75 \text{ kN}$

Duvardan Gelen Yük (K104): $5,36 \times 2,5 = 21,75 \text{ kN}$

Duvarдан Gelen Yüк (K141): $7,25 \times 3 = 21,75 \text{ kN}$

Duvar dan Gelen Yü k (K108): $7,25 \times 5 \times 0,25 = 9,0625 \text{ kN}$

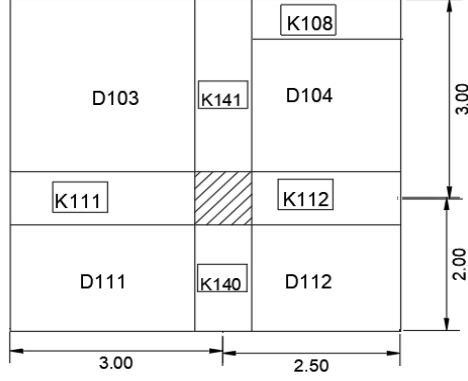
Kolon öz Ağırlığı: 8,138 kN

Hareketli Yükler

D103 Döşemesi: $3,50 \times 3 \times 3 = 31,5 \text{ kN}$

D104 Döşemesi: $5 \times 3 \times 5 \times (0,75/2) = 28,125 \text{ kN}$

S12 Kolonuna Gelen Eksenel Kuvvet (Şekil 2.13)



Şekil 2.13: S12 Kolonu Yük Alma Bölgesi.

Sabit Yükler

D103 Döşemesi: $5,26 \times 3 \times 3 = 47,34 \text{ kN}$

D111 Döşemesi: $5,26 \times 2 \times 3 = 31,56 \text{ kN}$

D104 Döşemesi: $5,26 \times 3 \times 5 \times (0,25/2) = 9,8625 \text{ kN}$

D112 Döşemesi: $5,26 \times 2,5 \times 2 = 26,3 \text{ kN}$

K111 Kirişi: $2,81 \times 3 = 8,43 \text{ kN}$

K112 Kirişi: $2,81 \times 2,5 = 7,025 \text{ kN}$

K140 Kirişi: $2,81 \times 2 = 5,62 \text{ kN}$

K141 Kirişi: $2,81 \times 3 = 8,43 \text{ kN}$

K108 Kirişi: $2,81 \times 5 \times 0,25 = 3,5125 \text{ kN}$

Duvarдан Gelen Yük (K111): $7,25 \times 3 = 21,75 \text{ kN}$

Duvarдан Gelen Yük (K141): $7,25 \times 3 = 21,75 \text{ kN}$

Duvarдан Gelen Yük (K108): $7,25 \times 5 \times 0,25 = 9,0625 \text{ kN}$

Kolon öz Ağırlığı: $6,975 \text{ kN}$

Hareketli Yükler

D103 Döşemesi: $3,50 \times 3 \times 3 = 31,5 \text{ kN}$

D111 Döşemesi: $5 \times 2 \times 3 = 30 \text{ kN}$

D104 Döşemesi: $5 \times 3 \times 5 \times (0,25/2) = 9,375 \text{ kN}$

D112 Döşemesi: $5 \times 2 \times 2,5 = 25 \text{ kN}$

ÜÇÜNCÜ BÖLÜM

3. DEPREM PARAMETRELERİNİN BELİRLENMESİ

TBDY 2018, spektrum tanımı ve deprem parametrelerini belirleyen katsayıları değiştirerek, spektrumları yapının konumuna özel olarak tanımlamıştır. Bu yönetmelikte, spektrumlar harita spektral katsayıları ve yerel zemin etki katsayılarına bağlı olarak özelleştirilmiştir. Harita spektral ivme katsayısı, kısa periyot bölgesi ve 1.0 saniye periyot için iki ayrı değer üzerinden elde edilmektedir. Bu düzenlemeler, binaların coğrafi konumlarına ve yerel zemin koşullarına göre daha hassas bir şekilde deprem etkilerini değerlendirmeyi amaçlamaktadır.

Tasarlanan hastane binasının İzmir (38.385957° N, 27.174401° E), İstanbul (41.041455° N, 29.15173° E) ve Ankara (39.885507° N, 32.852896° E) koordinatlarında yer aldığı kabul edilmektedir. Bina tasarımında, deprem yer hareket düzeyi DD-2 olarak belirlenmiş, spektral büyüklüklerin 50 yılda aşılma olasılığı %10 ve buna karşılık gelen tekrarlanma periyodu 457 yıl olarak seçilmiştir.

TBDY 2018'de yerel zemin sınıf tanımları değiştirilerek beş farklı zemin sınıfı tanımlanmıştır. TBDY 2018'de tanımlanan zemin sınıfları Çizelge 1.8'de verilmiştir. Bu çalışmada tasarımı yapılan Hastane binasının farklı kat sayılarına ait yapıları ZA, ZB, ZC, ZD ve ZE yerel zemin sınıfları üzerinde projelendirildiği kabul edilmiştir.

Hastane binasının kabul edilen bu değerlerine ait harita spektral ivme katsayıları, tasarım spektrum değerleri, tasarım spektral ivme katsayıları, yerel zemin etki katsayıları, tasarım spektrum değerleri <http://tdth.afad.gov.tr/> adresindeki Deprem Tehlike Haritalarından alınmıştır. Bu değerler Çizelge 3.1 ile 3.9 arasındaki çizelgelerde verilmiştir.

3.1. PERİYOT HESABI

Bu çalışmanın amacı, yapıların gerçek periyotlarını belirlemeden önce, 3 boyutlu Modelleme programları kullanılmadan yapıların hızlı ve yaklaşık bir ön tasarımının gerçekleştirilebilmesini sağlamaktır. Türkiye Bina Deprem Yönetmeliği 2018'de, deprem hesaplamalarında kullanılacak bina ampirik doğal titreşim periyodu (T_{pA}) değerinin 1,4 katından daha büyük olamayacağı belirtilmektedir. Bu bağlamda,

Hastane binasının periyodu, Denklem (3.1) kullanılarak hesaplanan ampirik doğal titreşim periyodu değerinin 1,4 katı olarak alınmıştır. Bu yaklaşım, yapıların hızlı bir ön tasarım sürecinde kullanılarak, daha detaylı analizlere geçilmeden önce genel bir değerlendirme sağlamayı hedeflemektedir.

$$T_{PA} = C_t H_N^{3/4} \quad (3.1)$$

Hastane binası sadece betonarme çerçeveden oluştuğu için $C_t = 0,1$ olarak alınmıştır.

6 Katlı Yapı için Periyot Hesabı

$$C_t = 0,1, H_N = 6 \times 3,10 = 18,60 \text{ m}$$

$$T_{pA} = 0,1 \times 18,60^{3/4} = 0,896 \text{ sn}$$

$$T_p \leq 1,4 \times T_{pA} \text{ olması gerektiği için;}$$

$$T_p = 1,4 \times 0,896 = 1,254 \text{ sn}$$

9 Katlı Yapı için Periyot Hesabı

$$C_t = 0,1, H_N = 9 \times 3,10 = 27,90 \text{ m}$$

$$T_{pA} = 0,1 \times 27,9^{3/4} = 1,21 \text{ sn}$$

$$T_p \leq 1,4 \times T_{pA} \text{ olması gerektiği için;}$$

$$T_p = 1,4 \times 1,21 = 1,694 \text{ sn}$$

12 Katlı Yapı için Periyot Hesabı

$$C_t = 0,1, H_N = 12 \times 3,10 = 37,20 \text{ m}$$

$$T_{pA} = 0,1 \times 37,20^{3/4} = 1,506 \text{ sn}$$

$$T_p \leq 1,4 \times T_{pA} \text{ olması gerektiği için;}$$

$$T_p = 1,4 \times 1,506 = 2,1084 \text{ sn}$$

3.2. EŞDEĞER DEPREM YÜKÜ VE TABAN KESME KUVVETİNİN BELİRLENMESİ

Bu çalışmada, Türkiye Bina Deprem Yönetmeliği 2018'e (TBDY 2018) uygun olarak, taban kesme kuvveti, yapının azaltılmış tasarım spektral ivmesine, tasarım spektral ivme kat sayısına ve binanın toplam kütesine bağlı olarak hesaplanmıştır. Hesaplamalar, yapının farklı kat sayılarına (6 katlı, 9 katlı ve 12 katlı), her zemin sınıfı üzerinde ve belirli koordinatlarda detaylı bir şekilde yapılmıştır. Bu hesaplamalar, Bölüm 1'de detaylı olarak anlatılan eşdeğer deprem yükü yöntemi kullanılarak gerçekleştirilmiştir.

3.2.1. Seçilen İllere Göre Taban Kesme kuvvetinin hesabı

Bu çalışmada, İzmir, İstanbul ve Ankara illerinde bulunan ZA, ZB, ZC, ZD ve ZE zemin sınıfları üzerinde yer aldığı kabul edilen 6 katlı, 9 katlı ve 12 katlı hastane binalarının taban kesme kuvveti hesaplamaları detaylı olarak anlatılmıştır. Hesaplamalarda kullanılan periyot değerleri, daha önce verilmiş olan bina yüksekliğine bağlı olarak bulunan periyot T_{pA} ve hastane binasının periyodu $1.4 \times T_{pA}$ olarak kabul edilmiştir.

Taban kesme kuvvetinin hesaplanmasında kullanılan bina önem katsayısı, Çizelge 1.4'te hastane için $I = 1,5$ olarak alınmıştır. Ayrıca, bina taşıyıcı sistem davranış katsayısı TBDY 2018'de bulunan Tablo 4.1'e göre beton arme çerçeve sistemlerde $R = 8$ perdeli çerçeve sistemlerde 7 olarak belirlenmiştir. Hastane binasının taban kesme kuvveti Denklem (3.2) kullanılarak hesaplanmıştır.

$$V_{tE}^{(X)} = m_t S_{aR}(T_p^{(X)}) \geq 0,04 m_t I S_{DS} g \quad (3.2)$$

Taban kesme kuvveti hesapları için İstanbul ilinde ZA ve ZB zemin sınıflarında bulunan 6 katlı hastane binası için T_{pA} ve $1.4 \times T_{pA}$ periyot değerleri kullanılarak detaylı hesaplamalar aşağıda verilmiştir.

İstanbul ZA

Çizelge 1.6 ve Çizelge 1.7 'ye göre:

$$S_S = 0.933 \quad S_1 = 0.260$$

Yerel Zemin Sınıfı ZA ve $SS = 1.061$ için $FS = 0.800$

Tasarım Spektral İvme Katsayıları:

$$S_{DS} = S_S \cdot F_S = 0.933 \times 0.800 = 0.746$$

$$S_{D1} = S_1 \cdot F_1 = 0.260 \times 0.800 = 0.208$$

İstanbul ZE

$$S_S = 0.933 \quad S_1 = 0.260$$

Yerel Zemin Sınıfı ZE ve $SS = 0.933$ için $FS = 1.154$

Tasarım Spektral İvme Katsayıları:

$$S_{DS} = S_S \cdot F_S = 0.933 \times 1.154 = 1.076$$

$$S_{D1} = S_1 \cdot F_1 = 0.260 \times 3.000 = 0.780$$

ZA zemin sınıfı için taban kesme kuvveti hesabı

$$m_t = 4117.655, \quad g = 9,81 \text{ m/s}^2, \quad S_{DS} = 0,746, \quad S_{D1} = 0,208, \quad T_L = 6 \text{ s}$$

$$T_A = 0.2 \frac{S_{D1}}{S_{DS}} = 0.2 \frac{0,208}{0,746} = 0,056 \text{ sn}$$

$$T_B = \frac{S_{D1}}{S_{DS}} = \frac{0,208}{0,746} = 0,279 \text{ sn}$$

$$R_a = \frac{R}{I} = \frac{8}{1,5} = 5,33 \quad (T > T_B)$$

Yapı Periyodunun T_{pA} olması durumunda taban kesme kuvveti değeri:

$$T = 0,896 \text{ sn}$$

$$S_{ae}(T) = \frac{S_{D1}}{T} = \frac{0,208}{0,896} = 0,232 \quad (T_B \leq T \leq T_L)$$

$$S_{aR}(T) = \frac{S_{ae}(T)}{R_a(T)} = \frac{0,232}{5,33} g = 0,427 \text{ m/s}^2$$

$$V_{tE,min} = m_t \times S_{aR} = 4117.655 \times 0,427 = 1759.329 \text{ kN}$$

$$0.04 \times m_t \times I \times S_{DS} \times g = 0,04 \times 1,5 \times 0,746 \times 9,81 = 1808.044 \text{ kN}$$

$$V_{tE,min} \geq 0.04 \times m_t \times I \times S_{DS} \times g \text{ olmalı}$$

$$1759.329 \geq 1808.044 \text{ koşulu sağlanmadığı için}$$

$$V_{tE} = 1808.044 \text{ kN olarak alınır.}$$

Yapı Periyodunun $1.4 \times T_{pA}$ olması durumunda taban kesme kuvveti değeri:

$$T = 1,254 \text{ sn}$$

$$S_{ae}(T) = \frac{S_{D1}}{T} = \frac{0,208}{1,254} = 0,166 \quad (T_B \leq T \leq T_L)$$

$$S_{aR}(T) = \frac{S_{ae}(T)}{R_a(T)} = \frac{0,166}{5,33} g = 0,305 \text{ m/s}^2$$

$$V_{tE,min} = m_t \times S_{aR} = 4117.655 \times 0,305 = 1257.064 \text{ kN}$$

$$0.04 \times m_t \times I \times S_{DS} \times g = 0,04 \times 1,5 \times 0,746 \times 9,81 = 1808.044 \text{ kN}$$

$$V_{tE,min} \geq 0.04 \times m_t \times I \times S_{DS} \times g \text{ olmalı}$$

$$1257.064 \geq 1808.044 \text{ koşulu sağlanmadığı için}$$

$$V_{tE} = 1808.044 \text{ kN olarak alınır.}$$

ZB zemin sınıfı için taban kesme kuvveti hesabı

$$m_t = 4117.655, g = 9,81 \text{ m/s}^2, S_{DS} = 0,840, S_{D1} = 0,208, T_L = 6 \text{ s}$$

$$T_A = 0.2 \frac{S_{D1}}{S_{DS}} = 0.2 \frac{0,208}{0,840} = 0,050 \text{ sn}$$

$$T_B = \frac{S_{D1}}{S_{DS}} = \frac{0,208}{0,840} = 0,248 \text{ sn}$$

$$R_a = \frac{R}{I} = \frac{8}{1,5} = 5,33 \quad (T > T_B)$$

Yapı Periyodunun T_{pA} olması durumunda taban kesme kuvveti değeri:

$$T = 0,896 \text{ sn}$$

$$S_{ae}(T) = \frac{S_{D1}}{T} = \frac{0,208}{0,896} = 0,232 \quad T_B \leq T \leq T_L$$

$$S_{aR}(T) = \frac{S_{ae}(T)}{R_a(T)} = \frac{0,232}{5,33} g = 0,427 \text{ m/s}^2$$

$$V_{tE, \min} = m_t \times S_{aR} = 4117.655 \times 0,427 = 1759.329 \text{ kN}$$

$$0.04 \times m_t \times I \times S_{DS} \times g = 0,04 \times 1,5 \times 0,840 \times 9,81 = 2035.867 \text{ kN}$$

$$V_{tE, \min} \geq 0.04 \times m_t \times I \times S_{DS} \times g \text{ olmalı}$$

$$1759.329 \geq 2035.867 \text{ koşulu sağlanmadığı için}$$

$$V_{tE} = 2035.867 \text{ kN olarak alınır.}$$

Yapı Periyodunun $1.4 \times T_{pA}$ olması durumunda taban kesme kuvveti değeri:

$$T = 1,254 \text{ sn}$$

$$S_{ae}(T) = \frac{S_{D1}}{T} = \frac{0,208}{1,254} = 0,166 \quad T_B \leq T \leq T_L$$

$$S_{aR}(T) = \frac{S_{ae}(T)}{R_a(T)} = \frac{0,166}{5,33} g = 0,305 \text{ m/s}^2$$

$$V_{tE, \min} = m_t \times S_{aR} = 4117.655 \times 0,305 = 1257.064 \text{ kN}$$

$$0.04 \times m_t \times I \times S_{DS} \times g = 0,04 \times 1,5 \times 0,840 \times 9,81 = 2035.867 \text{ kN}$$

$$V_{tE, \min} \geq 0.04 \times m_t \times I \times S_{DS} \times g \text{ olmalı}$$

$$1257.064 \geq 2035.867 \text{ koşulu sağlanmadığı için}$$

$$V_{tE} = 2035.867 \text{ kN olarak alınır.}$$

İstanbul, Ankara ve İzmir’de Model 1 için 6, 9, 12 katlı binalara ait değişik Zemin sınıfları için yukarıda hesaplanan taban kesme kuvvetleri ve bunların ZA zemin sınıfındaki taban kesme kuvvetlerine oranları Çizelge 3.1 ila Çizelge 3.9 da verilmiştir.

Çizelge 3.1: İstanbul'daki 6 Katlı Hastane Binasının Taban Kesme Kuvveti.

$m_t = 4117.655$, $g = 9,81$ m/s ² , $T_L = 6$ s olarak alınmıştır.						$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$							
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	T (s)	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap}$ (kN)	V_{tz} / V_{tZA}
ZA	TPA	0.746	0.208	0.056	0.279	5.330	0.427	0.232	0.896	1759.329	1808.044	1808.044	1.000
	1.4 × TPA						0.305	0.166	1.254	1257.064	1808.044	1808.044	1.000
ZB	TPA	0.840	0.208	0.050	0.248	5.330	0.427	0.232	0.896	1759.329	2035.867	2035.867	1.126
	1.4 × TPA						0.305	0.166	1.254	1257.064	2035.867	2035.867	1.126
ZC	TPA	1.120	0.390	0.070	0.348	5.330	0.801	0.435	0.896	3298.742	2714.490	3298.742	1.824
	1.4 × TPA						0.572	0.311	1.254	2356.996	2714.490	2714.490	1.501
ZD	TPA	1.051	0.541	0.103	0.515	5.330	1.111	0.604	0.896	4575.947	2547.258	4575.947	2.531
	1.4 × TPA						0.794	0.431	1.254	3269.576	2547.258	3269.576	1.808
ZE	TPA	1.076	0.780	0.145	0.725	5.330	1.602	0.871	0.896	6597.484	2607.849	6597.484	3.649
	1.4 × TPA						1.145	0.622	1.254	4713.992	2607.849	4713.992	2.607

Çizelge 3.2: İzmir'deki 6 Katlı Hastane Binasının Taban Kesme Kuvveti.

$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$													
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	T (s)	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap}$ (kN)	
ZA	TPA	0.849	0.206	0.049	0.243	5.330	0.423	0.230	0.896	1742.412	2057.680	2057.680	
	1.4 × TPA						0.302	0.164	1.254	1244.977	2057.680	2057.680	
ZB	TPA	0.955	0.206	0.043	0.216	5.330	0.423	0.230	0.896	1742.412	2314.587	2314.587	
	1.4 × TPA						0.302	0.164	1.254	1244.977	2314.587	2314.587	
ZC	TPA	1.273	0.387	0.061	0.304	5.330	0.795	0.432	0.896	3273.367	3085.309	3273.367	
	1.4 × TPA						0.568	0.309	1.254	2338.865	3085.309	3085.309	
ZD	TPA	1.141	0.538	0.094	0.472	5.330	1.105	0.600	0.896	4550.572	2765.387	4550.572	
	1.4 × TPA						0.790	0.429	1.254	3251.446	2765.387	3251.446	
ZE	TPA	1.115	0.777	0.139	0.697	5.330	1.596	0.867	0.896	6572.109	2702.372	6572.109	
	1.4 × TPA						1.140	0.620	1.254	4695.861	2702.372	4695.861	

Çizelge 3.3: Ankara'daki 6 Katlı Hastane Binasının Taban Kesme Kuvveti.

$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$												
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	$T (s)$	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap} (kN)$
ZA	TPA	0.281	0.098	0.070	0.349	5.330	0.201	0.109	0.896	828.915	681.046	828.915
	1.4 × TPA						0.144	0.078	1.254	592.271	681.046	681.046
ZB	TPA	0.316	0.098	0.062	0.310	5.330	0.201	0.109	0.896	828.915	765.874	828.915
	1.4 × TPA						0.144	0.078	1.254	592.271	765.874	765.874
ZC	TPA	0.456	0.185	0.081	0.406	5.330	0.380	0.206	0.896	1564.788	1105.185	1564.788
	1.4 × TPA						0.272	0.148	1.254	1118.062	1105.185	1118.062
ZD	TPA	0.533	0.290	0.109	0.544	5.330	0.596	0.324	0.896	2452.911	1291.806	2452.911
	1.4 × TPA						0.426	0.231	1.254	1752.638	1291.806	1752.638
ZE	TPA	0.743	0.491	0.132	0.661	5.330	1.009	0.548	0.896	4153.032	1800.773	4153.032
	1.4 × TPA						0.721	0.392	1.254	2967.397	1800.773	2967.397

Çizelge 3.4: İstanbul'daki 9 Katlı Hastane Binasının Taban Kesme Kuvveti.

$m_t = 6176.4826, g = 9,81 \text{ m/s}^2, T_L = 6 \text{ s}$ olarak alınmıştır.										$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$			
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	$T \text{ (s)}$	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap} \text{ (kN)}$	V_{tz} / V_{tzA}
ZA	TPA	0.746	0.208	0.056	0.279	5.330	0.427	0.232	0.896	2638.994	2712.066	2712.066	1.000
	$1.4 \times TPA$						0.305	0.166	1.254	1885.597	2712.066	2712.066	1.000
ZB	TPA	0.840	0.208	0.050	0.248	5.330	0.427	0.232	0.896	2638.994	3053.801	3053.801	1.125
	$1.4 \times TPA$						0.305	0.166	1.254	1885.597	3053.801	3053.801	1.125
ZC	TPA	1.120	0.390	0.070	0.348	5.330	0.801	0.435	0.896	4948.113	4071.735	4948.113	1.822
	$1.4 \times TPA$						0.572	0.311	1.254	3535.494	4071.735	4071.735	1.499
ZD	TPA	1.051	0.541	0.103	0.515	5.330	1.111	0.604	0.896	6863.921	3820.887	6863.921	2.525
	$1.4 \times TPA$						0.794	0.431	1.254	4904.365	3820.887	4904.365	1.804
ZE	TPA	1.076	0.780	0.145	0.725	5.330	1.602	0.871	0.896	9896.226	3911.774	9896.226	3.638
	$1.4 \times TPA$						1.145	0.622	1.254	7070.988	3911.774	7070.988	2.599

Çizelge 3.5: İzmir’deki 9 Katlı Hastane Binasının Taban Kesme Kuvveti.

$m_t = 8235.3101$, $g = 9,81$ m/s ² , $T_L = 6$ s olarak alınmıştır.										$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$		
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	T (s)	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap}$ (kN)
ZA	TPA	0.849	0.206	0.049	0.243	5.330	0.423	0.230	0.896	2613.619	3086.521	3086.521
	1.4 × TPA						0.302	0.164	1.254	1867.466	3086.521	3086.521
ZB	TPA	0.955	0.206	0.043	0.216	5.330	0.423	0.230	0.896	2613.619	3471.881	3471.881
	1.4 × TPA						0.302	0.164	1.254	1867.466	3471.881	3471.881
ZC	TPA	1.273	0.387	0.061	0.304	5.330	0.795	0.432	0.896	4910.051	4627.963	4910.051
	1.4 × TPA						0.568	0.309	1.254	3508.298	4627.963	4627.963
ZD	TPA	1.141	0.538	0.094	0.472	5.330	1.105	0.600	0.896	6825.859	4148.080	6825.859
	1.4 × TPA						0.790	0.429	1.254	4877.168	4148.080	4877.168
ZE	TPA	1.115	0.777	0.139	0.697	5.330	1.596	0.867	0.896	9858.164	4053.558	9858.164
	1.4 × TPA						1.140	0.620	1.254	7043.792	4053.558	7043.792

Çizelge 3.6: Ankara’deki 9 Katlı Hastane Binasının Taban Kesme Kuvveti.

										$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$		
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	T (s)	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap}$ (kN)
ZA	TPA	0.281	0.098	0.070	0.349	5.330	0.201	0.109	0.896	1243.372	1021.569	1243.372
	1.4 × TPA						0.144	0.078	1.254	888.406	1021.569	1021.569
ZB	TPA	0.316	0.098	0.062	0.310	5.330	0.201	0.109	0.896	1243.372	1148.811	1243.372
	1.4 × TPA						0.144	0.078	1.254	888.406	1148.811	1148.811
ZC	TPA	0.456	0.185	0.081	0.406	5.330	0.380	0.206	0.896	2347.182	1657.778	2347.182
	1.4 × TPA						0.272	0.148	1.254	1677.093	1657.778	1677.093
ZD	TPA	0.533	0.290	0.109	0.544	5.330	0.596	0.324	0.896	3679.366	1937.710	3679.366
	1.4 × TPA						0.426	0.231	1.254	2628.957	1937.710	2628.957
ZE	TPA	0.743	0.491	0.132	0.661	5.330	1.009	0.548	0.896	6229.547	2701.160	6229.547
	1.4 × TPA						0.721	0.392	1.254	4451.096	2701.160	4451.096

Çizelge 3.7: İstanbul'daki 12 Katlı Hastane Binasının Taban Kesme Kuvveti.

$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$													
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	$T (s)$	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap} (kN)$	V_{tz} / V_{tzA}
ZA	TPA	0.746	0.208	0.056	0.279	5.330	0.427	0.232	0.896	3518.658	3616.088	3616.088	1.000
	1.4 × TPA						0.305	0.166	1.254	2514.129	3616.088	3616.088	1.000
ZB	TPA	0.840	0.208	0.050	0.248	5.330	0.427	0.232	0.896	3518.658	4071.735	4071.735	1.125
	1.4 × TPA						0.305	0.166	1.254	2514.129	4071.735	4071.735	1.125
ZC	TPA	1.120	0.390	0.070	0.348	5.330	0.801	0.435	0.896	6597.484	5428.980	6597.484	1.822
	1.4 × TPA						0.572	0.311	1.254	4713.992	5428.980	5428.980	1.499
ZD	TPA	1.051	0.541	0.103	0.515	5.330	1.111	0.604	0.896	9151.895	5094.516	9151.895	2.527
	1.4 × TPA						0.794	0.431	1.254	6539.153	5094.516	6539.153	1.805
ZE	TPA	1.076	0.780	0.145	0.725	5.330	1.602	0.871	0.896	13194.968	5215.699	13194.968	3.641
	1.4 × TPA						1.145	0.622	1.254	9427.984	5215.699	9427.984	2.601

Çizelge 3.8: İzmir'deki 12 Katlı Hastane Binasının Taban Kesme Kuvveti.

$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$												
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	$T (s)$	$V_{tE} = m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap} (kN)$
ZA	TPA	0.849	0.206	0.049	0.243	5.330	0.423	0.230	0.896	3484.825	4115.361	4115.361
	1.4 × TPA						0.302	0.164	1.254	2489.955	4115.361	4115.361
ZB	TPA	0.955	0.206	0.043	0.216	5.330	0.423	0.230	0.896	3484.825	4629.175	4629.175
	1.4 × TPA						0.302	0.164	1.254	2489.955	4629.175	4629.175
ZC	TPA	1.273	0.387	0.061	0.304	5.330	0.795	0.432	0.896	6546.734	6170.617	6546.734
	1.4 × TPA						0.568	0.309	1.254	4677.730	6170.617	6170.617
ZD	TPA	1.141	0.538	0.094	0.472	5.330	1.105	0.600	0.896	9101.145	5530.773	9101.145
	1.4 × TPA						0.790	0.429	1.254	6502.891	5530.773	6502.891
ZE	TPA	1.115	0.777	0.139	0.697	5.330	1.596	0.867	0.896	13144.218	5404.743	13144.218
	1.4 × TPA						1.140	0.620	1.254	9391.722	5404.743	9391.722

Çizelge 3.9: Ankara'daki 12 Katlı Hastane Binasının Taban Kesme Kuvveti.

										$V_{tE,min} > 0.04 \times m_t \times I \times S_{DS} \times g$		
Zemin Sınıfı		S_{DS}	S_{D1}	T_A	T_B	R_a	$S_{aR}(T)$	$S_{ae}(T)$	T (s)	$V_{tE}=m_t \times S_{aR}$	$0.04 \times m_t \times I \times S_{DS} \times g$	$V_{t,hesap}$ (kN)
ZA	TPA	0.281	0.098	0.070	0.349	5.330	0.201	0.109	0.896	1657.83	1362.09	1657.83
	1.4 × TPA								0.144	0.078	1.254	1184.54
ZB	TPA	0.316	0.098	0.062	0.310	5.330	0.201	0.109	0.896	1657.83	1531.75	1657.83
	1.4 × TPA								0.144	0.078	1.254	1184.54
ZC	TPA	0.456	0.185	0.081	0.406	5.330	0.380	0.206	0.896	3129.58	2210.37	3129.58
	1.4 × TPA								0.272	0.148	1.254	2236.12
ZD	TPA	0.533	0.290	0.109	0.544	5.330	0.596	0.324	0.896	4905.82	2583.61	4905.82
	1.4 × TPA								0.426	0.231	1.254	3505.28
ZE	TPA	0.743	0.491	0.132	0.661	5.330	1.009	0.548	0.896	8306.06	3601.55	8306.06
	1.4 × TPA								0.721	0.392	1.254	5934.79

3.3. KOLON ÖN BOYUTLANDIRMASI

Yapıdaki kolonların başlangıç enkesitlerinin belirlenmesi için kapsamı bir ön boyutlandırma çalışması gerçekleştirilmiştir. Kolon boyutları, Türkiye Bina Deprem Yönetmeliği (TBDY) 2018 standartları doğrultusunda kısmen dikdörtgen, kısmen kare en kesitli olarak belirlenmiş olup, minimum 30 cm'lik bir kolon enkesit alanı dikkate alınmıştır. Kolon boyutları, her birkaç katta bir değişecek şekilde seçilmiştir.

Ayrıca, tasarımı yapılan hastane binası için 6, 9 ve 12 kat gibi farklı kat sayılarına, değişen deprem bölgelerine ve zemin sınıflarına uygun olarak özel tasarım hesapları yapılmıştır. Bu çalışmalar, binanın sağlamlığı ve dayanıklılığı açısından kritik öneme sahiptir.

Kolonlara döşeme, kiriş, duvar ve üst kattaki kolondan etki eden sabit yükler (G), döşemelerden gelen hareketli yükler (Q) ve depremden gelen eksenel kuvvet N_E her kat kolonu için ayrı ayrı hesaplanmıştır.

Kolon boyutlandırılması başlangıçta yapının ETABS programında analizi yapılabilmesi için TS500'e göre $A_c \geq N_{dm} / 0,6 f_{ck}$ koşuluna göre en kesit alanları hesaplanarak yapılmıştır. C30 betonu için $f_{ck} = 3 \text{ kN/cm}^2$ alınmıştır. Bu değerler Çizelge 3.11, Çizelge 3.12 ve Çizelge 3.13'te verilmiştir. Kolon ön boyutlandırmasında eksenel kuvvetler dış cephelerde pencere boşlukları dikkate alınarak kiriş uçlarındaki momentleri etkisi göz önüne alınmadan hesaplanmıştır.

Kolonlarda oluşan eksenel basınç kuvveti N_{dm} hem $1,4G + 1,6Q$ hem de hareketli yük azaltma katsayısı hareketli yük (Q) ile çarpılarak $1,4G + 1,6\beta Q$ değerleri ile bulunarak arada oluşan değer fark çizelgede gösterilmeye çalışılmıştır. TBDY 2018'de kolon en kesit alanı $G + \beta Q$ kullanılarak hesaplanan N_{dm} 'nin $A_c \geq N_{dm} / 0,4 f_{ck}$ eşitliğinde kullanılmasıyla elde edilmektedir. Burada $G + \beta Q$ 'nun yaklaşık 1,5 katı $1,4G + 1,6Q$ verdiği için başlangıçta $A_c \geq N_{dm} / 0,6 f_{ck}$ eşitliği kullanılarak boyutlandırma yapılmıştır.

3.3.1. Hareketli Yük Azaltma Katsayı

Hareketli yük azaltma katsayısı en az üç kattan fazla yük taşıyan kolon, bağ kiriş, perde duvarı, temel duvarı gibi yapı elemanlarının hesaplanmasında ve buna eşdeğer zemin basıncının belirlenmesinde gerekli olan her kata gelen hareketli yük toplanarak sonucun bazı şartlar içinde azaltılması mümkündür. Yapının ilk üç katında en fazla hareketli yük değeri hesaba tam olarak katılır. Belirtilen yapı kısmındaki hareketli yük diğer katlara azalacak şekilde intikal ettirilir. Bu miktarlar yapıdaki hareketli yük toplamının belli bir kısmı kadardır [2].

Konutlarda, büro ve iş hanlarında % eksiltme değeri %20'den % 80'e kadar; hafif çalışma yapılan işyeri, atölye imalathane ve mağazalarda bu miktar %10'dan %40'a kadar olabilir [2].

Her kattan gelen hareketli yükün aynı olması durumunda TS 498'de yer alan bu miktarlar % eksiltme değeri ve toplam hareketli yüke bağlı azaltma değeri β (hesapla öngörülen toplam hareketli yükün toplam hareketli yüke oranı) Çizelge 3.10'da verilmiştir.

Çizelge 3.10: En Az Üç Tam Kattan Fazla Yük Taşıyan Elemanlar İçin % Eksiltme Değeri ve Azaltma Değeri, β (Her tam katta aynı hareketli yük olması halinde) [2].

a) Konut vs.													
Kat sayısı	1	2	3	4	5	6	7	8	9	10	11	12	
1 %eksiltme değeri	0	0	0	20	40	60	80	80	90	40	40	40	
2 Azaltma değeri (β)	1	1	1	0,95	0,88	0,8	0,71	0,65	0,6	0,6	0,6	0,6	
b) Atölye, işyeri, imalathane vs.													
3 %eksiltme değeri	0	0	0	10	20	30	40	40	40	20	20	20	
4 Azaltma değeri (β)	1	1	1	0,98	0,94	0,9	0,86	0,83	0,8	0,8	0,8	0,8	

Çizelge 3.11: 6 Katlı Hastane Binası Kolon Ön Boyutlandırması

KOLO N	KAT	N_{G0} (kN)	N_{Q0} (kN)	$N_{d1}=1,4$ $G_0 +$ $1,6Q_0$ (kN)	$N_{d2}=1,4G_0$ $+ 1,6\beta Q_0$ (kN)	$A_{c1}=N_{d1}/0,$ $6f_{ck}$ (cm ²)	$A_{c2}=N_{d2}/0,$ $6f_{ck}$ (cm ²)	BOY UT	cm ²
S1	6.KAT	91.36	26.25	169.9	161.5	94.39	89.72	30/30	900
	5.KAT	182.72	52.5	339.81	323.01	188.78	179.45	30/30	900
	4.KAT	274.08	78.75	509.71	484.51	283.17	269.17	30/30	900
	3.KAT	365.44	105	679.62	646.02	377.56	358.9	30/30	900
	2.KAT	456.8	131.25	849.52	807.52	471.96	448.62	30/30	900
	1.KAT	548.16	157.5	1019.42	969.02	566.35	538.35	30/30	900
S9	6.KAT	139.89	51.25	277.85	261.45	154.36	145.25	30/35	1050
	5.KAT	279.78	102.5	555.69	522.89	308.72	290.5	30/35	1050
	4.KAT	419.67	153.75	833.54	784.34	463.08	435.74	30/35	1050
	3.KAT	559.56	205	1111.38	1045.78	617.44	580.99	30/35	1050
	2.KAT	699.45	256.25	1389.23	1307.23	771.79	726.24	30/35	1050
	1.KAT	839.34	307.5	1667.08	1568.68	926.15	871.49	30/35	1050
S2	6.KAT	170.043	57.75	330.46	311.98	183.59	173.32	30/35	1050
	5.KAT	340.086	115.5	660.92	623.96	367.18	346.64	30/35	1050
	4.KAT	510.129	173.25	991.38	935.94	550.77	519.97	30/35	1050
	3.KAT	680.172	231	1321.84	1247.92	734.36	693.29	30/40	1200
	2.KAT	850.215	288.75	1652.3	1559.9	917.95	866.61	30/40	1200
	1.KAT	1020.258	346.5	1982.76	1871.88	1101.53	1039.93	30/40	1200
S10	6.KAT	242.76	112.75	520.26	484.18	289.04	268.99	35/35	1225
	5.KAT	485.52	225.5	1040.53	968.37	578.07	537.98	35/35	1225
	4.KAT	728.28	338.25	1560.79	1452.55	867.11	806.97	35/35	1225
	3.KAT	971.04	451	2081.06	1936.74	1156.14	1075.96	40/40	1600
	2.KAT	1213.8	563.75	2601.32	2420.92	1445.18	1344.96	40/40	1600
	1.KAT	1456.56	676.5	3121.58	2905.1	1734.21	1613.95	45/45	2025
S3	6.KAT	191.06	63	368.29	348.13	204.6	193.4	30/35	1050
	5.KAT	382.13	126	736.58	696.26	409.21	386.81	30/35	1050
	4.KAT	573.19	189	1104.86	1044.38	613.81	580.21	30/35	1050
	3.KAT	764.25	252	1473.15	1392.51	818.42	773.62	30/35	1050
	2.KAT	955.32	315	1841.44	1740.64	1023.02	967.02	30/35	1050
	1.KAT	1146.38	378	2209.73	2088.77	1227.63	1160.43	30/40	1200
S11	6.KAT	262.1	123	563.74	524.38	313.19	291.32	30/40	1200
	5.KAT	524.2	246	1127.47	1048.75	626.37	582.64	30/40	1200
	4.KAT	786.29	369	1691.21	1573.13	939.56	873.96	30/40	1200
	3.KAT	1048.39	492	2254.95	2097.51	1252.75	1165.28	35/45	1575
	2.KAT	1310.49	615	2818.69	2621.89	1565.94	1456.6	35/45	1575
	1.KAT	1572.59	738	3382.42	3146.26	1879.12	1747.92	40/50	2000
S4	6.KAT	181.84	59.69	350.08	330.98	194.49	183.88	30/35	1050
	5.KAT	363.68	119.38	700.16	661.96	388.98	367.75	30/35	1050
	4.KAT	545.52	179.07	1050.24	992.94	583.47	551.63	30/35	1050
	3.KAT	727.36	238.76	1400.32	1323.92	777.96	735.51	30/40	1200
	2.KAT	909.2	298.45	1750.4	1654.9	972.44	919.39	30/40	1200
	1.KAT	1091.04	358.14	2100.48	1985.88	1166.93	1103.26	30/40	1200
S12	6.KAT	207.62	95.88	444.07	413.39	246.7	229.66	35/35	1225
	5.KAT	415.24	191.75	888.13	826.77	493.41	459.32	35/35	1225
	4.KAT	622.85	287.63	1332.2	1240.16	740.11	688.98	35/35	1225
	3.KAT	830.47	383.5	1776.26	1653.54	986.81	918.63	40/40	1600
	2.KAT	1038.09	479.38	2220.33	2066.93	1233.51	1148.29	40/40	1600
	1.KAT	1245.71	575.25	2664.39	2480.31	1480.22	1377.95	45/45	2025

Çizelge 3.12: 9 Katlı Hastane Binası Kolon Ön Boyutlandırması

KOLON	KAT	N_{G0} (kN)	N_{Q0} (kN)	$N_{d1}=1,4G_0$ + $1,6Q_0$ (kN)	$N_{d2}=1,4G_0$ + $1,6\beta Q_0$ (kN)	$A_{c1}=N_{d1}/$ $0,6f_{ck}$ (cm ²)	$A_{c2}=N_{d2}/0,6f_{ck}$ (cm ²)	BOYUT	cm ²
S1	9.KAT	91.36	26.25	169.9	153.1	94.39	85.06	30/30	900
	8.KAT	182.72	52.5	339.81	306.21	188.78	170.12	30/30	900
	7.KAT	274.08	78.75	509.71	459.31	283.17	255.17	30/30	900
	6.KAT	365.44	105	679.62	612.42	377.56	340.23	30/30	900
	5.KAT	456.8	131.25	849.52	765.52	471.96	425.29	30/30	900
	4.KAT	548.16	157.5	1019.42	918.62	566.35	510.35	30/30	900
	3.KAT	639.52	183.75	1189.33	1071.73	660.74	595.4	30/30	900
	2.KAT	730.88	210	1359.23	1224.83	755.13	680.46	30/30	900
	1.KAT	822.24	236.25	1529.14	1377.94	849.52	765.52	30/30	900
S9	9.KAT	139.89	51.25	277.85	245.05	154.36	136.14	30/35	1050
	8.KAT	279.78	102.5	555.69	490.09	308.72	272.27	30/35	1050
	7.KAT	419.67	153.75	833.54	735.14	463.08	408.41	30/35	1050
	6.KAT	559.56	205	1111.38	980.18	617.44	544.55	30/35	1050
	5.KAT	699.45	256.25	1389.23	1225.23	771.79	680.68	30/35	1050
	4.KAT	839.34	307.5	1667.08	1470.28	926.15	816.82	30/35	1050
	3.KAT	979.23	358.75	1944.92	1715.32	1080.51	952.96	30/40	1200
	2.KAT	1119.12	410	2222.77	1960.37	1234.87	1089.09	35/40	1400
	1.KAT	1259.01	461.25	2500.61	2205.41	1389.23	1225.23	35/40	1400
S2	9.KAT	170.04	57.75	330.46	293.5	183.59	163.06	30/35	1050
	8.KAT	340.09	115.5	660.92	587	367.18	326.11	30/35	1050
	7.KAT	510.13	173.25	991.38	880.5	550.77	489.17	30/35	1050
	6.KAT	680.17	231	1321.84	1174	734.36	652.22	30/40	1200
	5.KAT	850.22	288.75	1652.3	1467.5	917.95	815.28	30/40	1200
	4.KAT	1020.26	346.5	1982.76	1761	1101.53	978.33	30/40	1200
	3.KAT	1190.3	404.25	2313.22	2054.5	1285.12	1141.39	35/45	1575
	2.KAT	1360.34	462	2643.68	2348	1468.71	1304.45	35/45	1575
	1.KAT	1530.39	519.75	2974.14	2641.5	1652.3	1467.5	40/45	1800
S10	9.KAT	242.76	112.75	520.26	448.1	289.04	248.95	35/35	1225
	8.KAT	485.52	225.5	1040.53	896.21	578.07	497.89	35/35	1225
	7.KAT	728.28	338.25	1560.79	1344.31	867.11	746.84	35/35	1225
	6.KAT	971.04	451	2081.06	1792.42	1156.14	995.79	40/40	1600
	5.KAT	1213.8	563.75	2601.32	2240.52	1445.18	1244.73	40/40	1600
	4.KAT	1456.56	676.5	3121.58	2688.62	1734.21	1493.68	45/45	2025
	3.KAT	1699.32	789.25	3641.85	3136.73	2023.25	1742.63	45/45	2025
	2.KAT	1942.08	902	4162.11	3584.83	2312.28	1991.57	50/50	2500
	1.KAT	2184.84	1014.75	4682.38	4032.94	2601.32	2240.52	50/50	2500
S3	9.KAT	191.06	63	368.29	327.97	204.6	182.2	30/35	1050
	8.KAT	382.13	126	736.58	655.94	409.21	364.41	30/35	1050
	7.KAT	573.19	189	1104.86	983.9	613.81	546.61	30/35	1050
	6.KAT	764.25	252	1473.15	1311.87	818.42	728.82	30/35	1050
	5.KAT	955.32	315	1841.44	1639.84	1023.02	911.02	30/35	1050
	4.KAT	1146.38	378	2209.73	1967.81	1227.63	1093.23	30/40	1200
	3.KAT	1337.44	441	2578.02	2295.78	1432.23	1275.43	35/40	1400
	2.KAT	1528.5	504	2946.31	2623.75	1636.84	1457.64	35/45	1575
	1.KAT	1719.57	567	3314.59	2951.71	1841.44	1639.84	40/45	1800
S11	9.KAT	262.1	123	563.74	485.02	313.19	269.45	30/40	1200
	8.KAT	524.2	246	1127.47	970.03	626.37	538.91	30/40	1200
	7.KAT	786.29	369	1691.21	1455.05	939.56	808.36	30/40	1200
	6.KAT	1048.39	492	2254.95	1940.07	1252.75	1077.82	35/45	1575
	5.KAT	1310.49	615	2818.69	2425.09	1565.94	1347.27	35/45	1575
	4.KAT	1572.59	738	3382.42	2910.1	1879.12	1616.72	40/50	2000
	3.KAT	1834.69	861	3946.16	3395.12	2192.31	1886.18	50/55	2750
	2.KAT	2096.78	984	4509.9	3880.14	2505.5	2155.63	50/55	2750
	1.KAT	2358.88	1107	5073.63	4365.15	2818.69	2425.09	50/60	3000
S4	9.KAT	181.84	59.69	350.08	311.88	194.49	173.27	30/35	1050
	8.KAT	363.68	119.38	700.16	623.76	388.98	346.53	30/35	1050
	7.KAT	545.52	179.07	1050.24	935.64	583.47	519.8	30/35	1050
	6.KAT	727.36	238.76	1400.32	1247.51	777.96	693.06	30/40	1200
	5.KAT	909.2	298.45	1750.4	1559.39	972.44	866.33	30/40	1200

	.4KAT	1091.04	358.14	2100.48	1871.27	1166.93	1039.59	30/40	1200
	3.KAT	1272.88	417.83	2450.56	2183.15	1361.42	1212.86	35/45	1575
	2.KAT	1454.72	477.52	2800.64	2495.03	1555.91	1386.13	35/45	1575
	1.KAT	1636.56	537.21	3150.72	2806.91	1750.4	1559.39	40/45	1800
S12	9.KAT	207.62	95.88	444.07	382.71	246.7	212.61	35/35	1225
	8.KAT	415.24	191.75	888.13	765.41	493.41	425.23	35/35	1225
	7.KAT	622.85	287.63	1332.2	1148.12	740.11	637.84	35/35	1225
	6.KAT	830.47	383.5	1776.26	1530.82	986.81	850.46	40/40	1600
	5.KAT	1038.09	479.38	2220.33	1913.53	1233.51	1063.07	40/40	1600
	4.KAT	1245.71	575.25	2664.39	2296.23	1480.22	1275.68	45/45	2025
	3.KAT	1453.33	671.13	3108.46	2678.94	1726.92	1488.3	45/45	2025
	2.KAT	1660.94	767	3552.52	3061.64	1973.62	1700.91	50/50	2500
	1.KAT	1868.56	862.88	3996.59	3444.35	2220.33	1913.53	50/50	2500

Çizelge 3.13: 12 Katlı Hastane Binası Kolon Ön Boyutlandırması

KOLO N	KAT	N_{G0} (kN)	N_{Q0} (kN)	$N_{d1}=1,4G_0$ $+1,6Q_0$ (kN)	$N_{d2}=1,4G_0+1,$ $6\beta Q_0$ (kN)	$A_{c1}=N_{d1}/0,6f_c$ k (cm ²)	$A_{c2}=N_{d2}/0,6$ fck (cm ²)	BOYUT	cm ²
S1	12.KAT	91.36	26.25	169.9	153.1	94.39	85.06	30/30	900
	11.KAT	182.72	52.5	339.81	306.21	188.78	170.12	30/30	900
	10.KAT	274.08	78.75	509.71	459.31	283.17	255.17	30/30	900
	9.KAT	365.44	105	679.62	612.42	377.56	340.23	30/30	900
	8.KAT	456.8	131.25	849.52	765.52	471.96	425.29	30/30	900
	7.KAT	548.16	157.5	1019.42	918.62	566.35	510.35	30/30	900
	6.KAT	639.52	183.75	1189.33	1071.73	660.74	595.4	30/30	900
	5.KAT	730.88	210	1359.23	1224.83	755.13	680.46	30/30	900
	4.KAT	822.24	236.25	1529.14	1377.94	849.52	765.52	30/30	900
	3.KAT	913.6	262.5	1699.04	1531.04	943.91	850.58	35/35	1225
	2.KAT	1004.96	288.75	1868.94	1684.14	1038.3	935.64	35/35	1225
	1.kat	1096.32	315	2038.85	1837.25	1132.69	1020.69	35/35	1225
S9	12.KAT	139.89	51.25	277.85	245.05	154.36	136.14	30/35	1050
	11.KAT	279.78	102.5	555.69	490.09	308.72	272.27	30/35	1050
	10.KAT	419.67	153.75	833.54	735.14	463.08	408.41	30/35	1050
	9.KAT	559.56	205	1111.38	980.18	617.44	544.55	30/35	1050
	8.KAT	699.45	256.25	1389.23	1225.23	771.79	680.68	30/35	1050
	7.KAT	839.34	307.5	1667.08	1470.28	926.15	816.82	30/35	1050
	6.KAT	979.23	358.75	1944.92	1715.32	1080.51	952.96	30/40	1200
	5.KAT	1119.12	410	2222.77	1960.37	1234.87	1089.09	35/40	1400
	4.KAT	1259.01	461.25	2500.61	2205.41	1389.23	1225.23	35/40	1400
	3.kat	1398.9	512.5	2778.46	2450.46	1543.59	1361.37	40/45	1800
	2.kat	1538.79	563.75	3056.31	2695.51	1697.95	1497.5	40/45	1800
	1.kat	1678.68	615	3334.15	2940.55	1852.31	1633.64	40/45	1800
S2	12.KAT	170.043	57.75	330.46	293.5	183.59	163.06	30/35	1050
	11.KAT	340.086	115.5	660.92	587	367.18	326.11	30/35	1050
	10.KAT	510.129	173.25	991.38	880.5	550.77	489.17	30/35	1050
	9.KAT	680.172	231	1321.84	1174	734.36	652.22	30/40	1200
	8.KAT	850.215	288.75	1652.3	1467.5	917.95	815.28	30/40	1200
	7.KAT	1020.258	346.5	1982.76	1761	1101.53	978.33	30/40	1200
	6.KAT	1190.301	404.25	2313.22	2054.5	1285.12	1141.39	35/45	1575

	5.KAT	1360.344	462	2643.68	2348	1468.71	1304.45	35/45	1575
	4.KAT	1530.387	519.75	2974.14	2641.5	1652.3	1467.5	40/45	1800
	3.KAT	1700.43	577.5	3304.6	2935	1835.89	1630.56	40/45	1800
	2.KAT	1870.473	635.25	3635.06	3228.5	2019.48	1793.61	45/50	2250
S10	1.KAT	2040.516	693	3965.52	3522	2203.07	1956.67	45/50	2250
	12.KAT	242.76	112.75	520.26	448.1	289.04	248.95	35/35	1225
	11.KAT	485.52	225.5	1040.53	896.21	578.07	497.89	35/35	1225
	10.KAT	728.28	338.25	1560.79	1344.31	867.11	746.84	35/35	1225
	9.KAT	971.04	451	2081.06	1792.42	1156.14	995.79	40/40	1600
	8.KAT	1213.8	563.75	2601.32	2240.52	1445.18	1244.73	40/40	1600
	7.KAT	1456.56	676.5	3121.58	2688.62	1734.21	1493.68	45/45	2025
	6.KAT	1699.32	789.25	3641.85	3136.73	2023.25	1742.63	45/45	2025
	5.KAT	1942.08	902	4162.11	3584.83	2312.28	1991.57	50/50	2500
	4.KAT	2184.84	1014.75	4682.38	4032.94	2601.32	2240.52	50/50	2500
	3.KAT	2427.6	1127.5	5202.64	4481.04	2890.36	2489.47	55/55	3025
	2.KAT	2670.36	1240.25	5722.9	4929.14	3179.39	2738.41	55/55	3025
	1.KAT	2913.12	1353	6243.17	5377.25	3468.43	2987.36	60/60	3600
S3	12.KAT	191.063	63.00	368.29	327.97	204.60	182.20	30/35	1050
	11.KAT	382.126	126.00	736.58	655.94	409.21	364.41	30/35	1050
	10.KAT	573.189	189.00	1104.86	983.90	613.81	546.61	30/35	1050
	9.KAT	764.252	252.00	1473.15	1311.87	818.42	728.82	30/35	1050
	8.KAT	955.315	315.00	1841.44	1639.84	1023.02	911.02	30/35	1050
	7.KAT	1146.378	378.00	2209.73	1967.81	1227.63	1093.23	30/40	1200
	6.KAT	1337.441	441.00	2578.02	2295.78	1432.23	1275.43	35/40	1400
	5.KAT	1528.504	504.00	2946.31	2623.75	1636.84	1457.64	35/45	1575
	4.KAT	1719.567	567.00	3314.59	2951.71	1841.44	1639.84	40/45	1800
	3.KAT	1910.63	630.00	3682.88	3279.68	2046.05	1822.05	40/50	2000
	2.KAT	2101.693	693.00	4051.17	3607.65	2250.65	2004.25	45/50	2250
	1.KAT	2292.756	756.00	4419.46	3935.62	2455.25	2186.45	45/55	2475
S11	12.KAT	262.098	123.00	563.74	485.02	313.19	269.45	30/40	1200
	11.KAT	524.196	246.00	1127.47	970.03	626.37	538.91	30/40	1200
	10.KAT	786.294	369.00	1691.21	1455.05	939.56	808.36	30/40	1200
	9.KAT	1048.392	492.00	2254.95	1940.07	1252.75	1077.82	35/45	1575
	8.KAT	1310.49	615.00	2818.69	2425.09	1565.94	1347.27	35/45	1575
	7.KAT	1572.588	738.00	3382.42	2910.10	1879.12	1616.72	40/50	2000
	6.KAT	1834.686	861.00	3946.16	3395.12	2192.31	1886.18	50/55	2750
	5.KAT	2096.784	984.00	4509.90	3880.14	2505.50	2155.63	50/55	2750
	4.KAT	2358.882	1107.00	5073.63	4365.15	2818.69	2425.09	50/60	3000
	3.KAT	2620.98	1230.00	5637.37	4850.17	3131.87	2694.54	55/65	3575
	2.KAT	2883.078	1353.00	6201.11	5335.19	3445.06	2963.99	55/65	3575
	1.KAT	3145.176	1476.00	6764.85	5820.21	3758.25	3233.45	55/70	3850
S4	12.KAT	181.84	59.69	350.08	311.88	194.49	173.27	30/35	1050
	11.KAT	363.68	119.38	700.16	623.76	388.98	346.53	30/35	1050
	10.KAT	545.52	179.07	1050.24	935.64	583.47	519.80	30/35	1050
	9.KAT	727.36	238.76	1400.32	1247.51	777.96	693.06	30/40	1200
	8.KAT	909.20	298.45	1750.40	1559.39	972.44	866.33	30/40	1200
	7.KAT	1091.04	358.14	2100.48	1871.27	1166.93	1039.59	30/40	1200
	6.KAT	1272.88	417.83	2450.56	2183.15	1361.42	1212.86	35/45	1575
	5.KAT	1454.72	477.52	2800.64	2495.03	1555.91	1386.13	35/45	1575
	4.KAT	1636.56	537.21	3150.72	2806.91	1750.40	1559.39	40/45	1800
	3.KAT	1818.40	596.90	3500.80	3118.78	1944.89	1732.66	40/45	1800
	2.KAT	2000.24	656.59	3850.88	3430.66	2139.38	1905.92	45/50	2250
	1.KAT	2182.08	716.28	4200.96	3742.54	2333.87	2079.19	45/50	2250
S12	12.KAT	207.62	95.88	444.07	382.71	246.70	212.61	35/35	1225
	11.KAT	415.24	191.75	888.13	765.41	493.41	425.23	35/35	1225
	10.KAT	622.85	287.63	1332.20	1148.12	740.11	637.84	35/35	1225
	9.KAT	830.47	383.50	1776.26	1530.82	986.81	850.46	40/40	1600
	8.KAT	1038.09	479.38	2220.33	1913.53	1233.51	1063.07	40/40	1600
	7.KAT	1245.71	575.25	2664.39	2296.23	1480.22	1275.68	45/45	2025
	6.KAT	1453.33	671.13	3108.46	2678.94	1726.92	1488.30	45/45	2025
	5.KAT	1660.94	767.00	3552.52	3061.64	1973.62	1700.91	50/50	2500
	4.KAT	1868.56	862.88	3996.59	3444.35	2220.33	1913.53	50/50	2500
	3.KAT	2076.18	958.75	4440.65	3827.05	2467.03	2126.14	55/55	3025
	2.KAT	2283.80	1054.63	4884.72	4209.76	2713.73	2338.75	55/55	3025
	1.KAT	2491.42	1150.50	5328.78	4592.46	2960.43	2551.37	60/60	3600

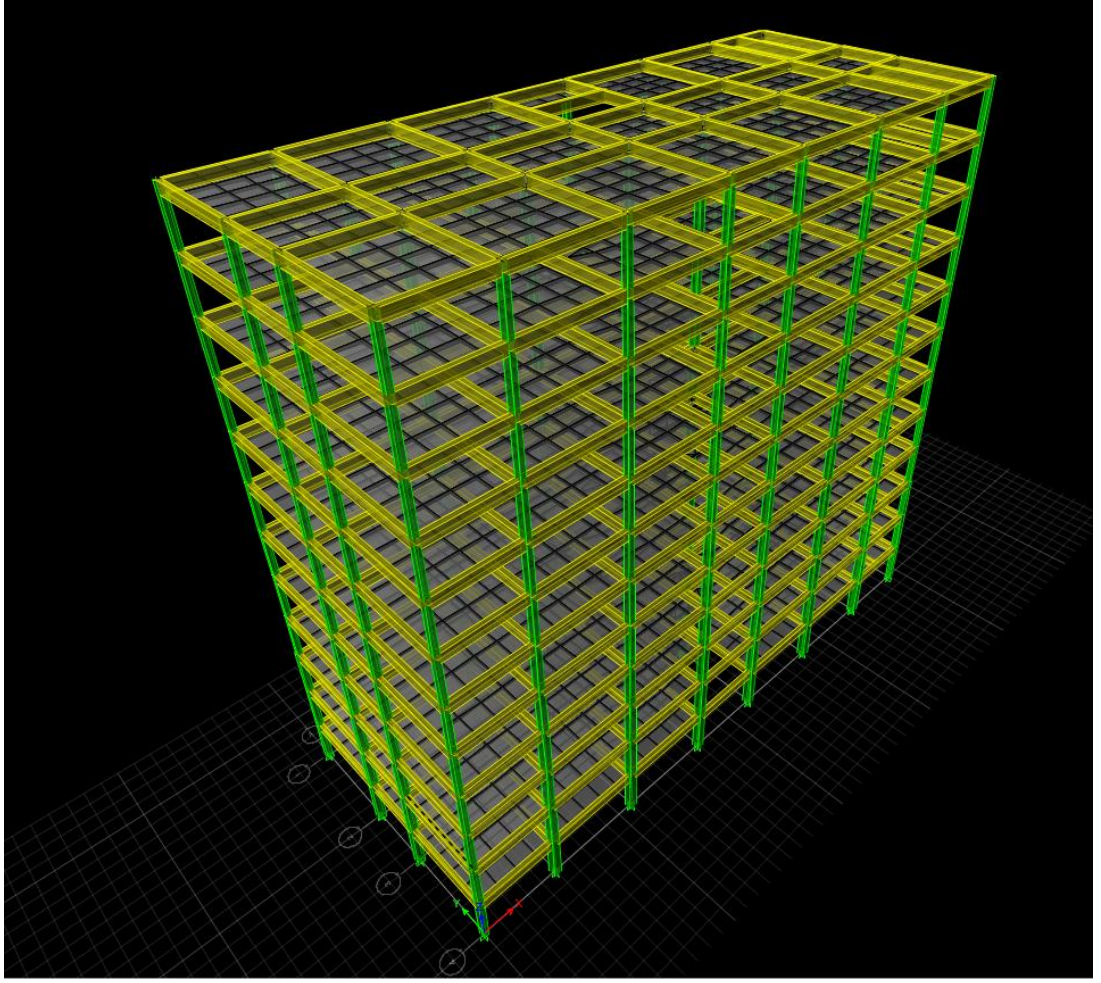
3.4. YAPISAL MODELLEME

Bu arařtırmada, hastane binasının analitik yapı Modeli oluşturulmuş ve bu Modelde 3 boyutlu yapısal analiz programı olan ETABS kullanılmıştır [5].

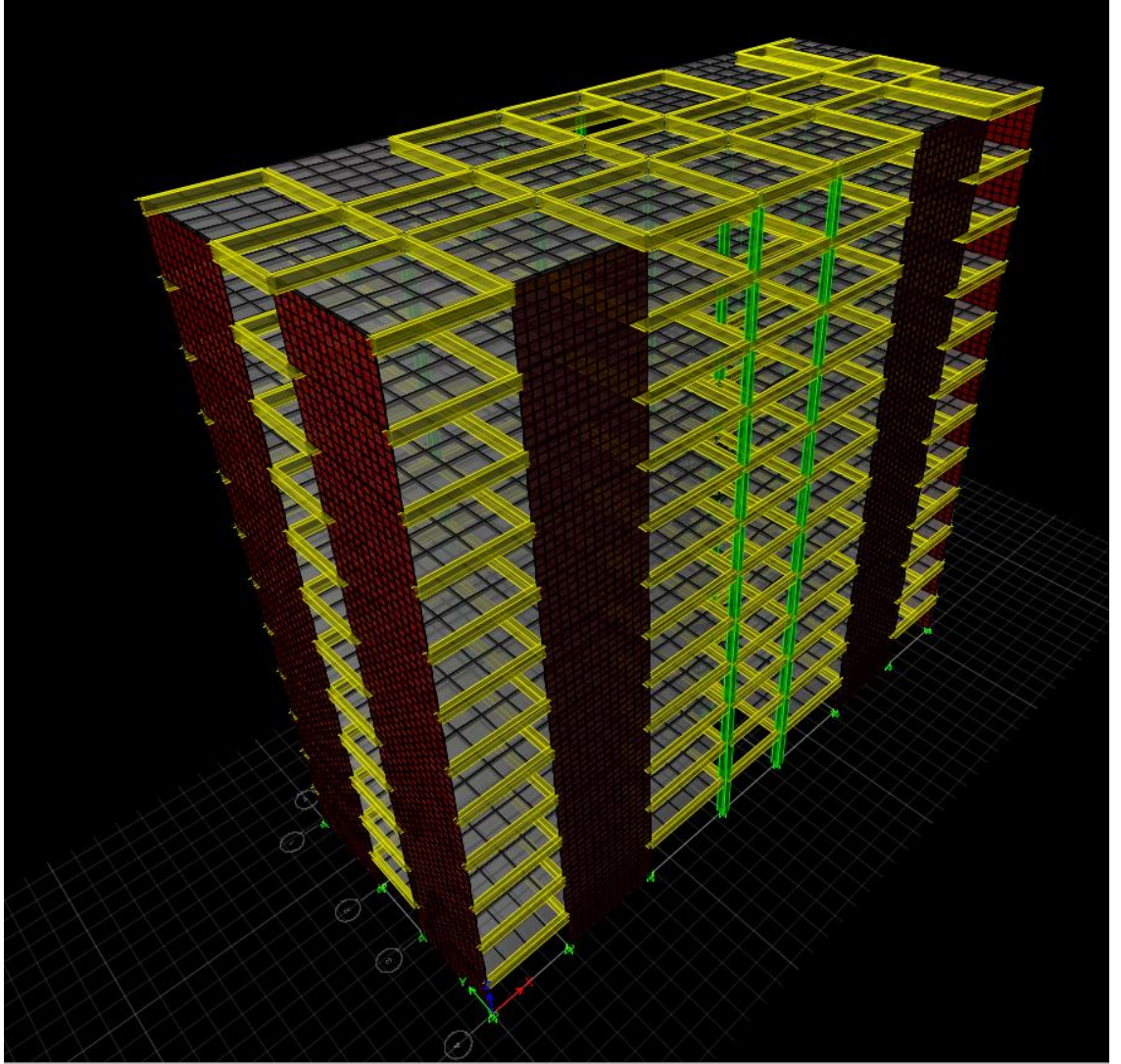
ETABS programı ile yapılan Modellemede, kolonlar ve kiriřler çubuk sonlu eleman (frame) olarak tanımlanmıştır. Döřemelerin kendi düzlemlerinde rijit diyafram olduđu ve kat kütlelerinin kat kütle merkezinde toplandıđı varsayılmıştır. Gerçek durumu daha dođru bir řekilde yansıtmak için, döřemelerden kiriřlere aktarılan yükler, kiriř uç momentlerinin dikkate alınmaması durumunda hesaplanan deđerler ETABS programında kiriř yüklerine eklenmiştir. Betonarme çerçeveden oluşan yapının taşıyıcı sistem elemanlarının etkin kesit rijitliđi çarpanları, TBDY 2018 standartlarından kiriřler için 0.35, kolonlar için ise 0.70 olarak alınmıştır. Modellemede, bu etkin kesit rijitliđi çarpanları, programda tanımlanarak taşıyıcı sistem elemanlarına uygulanmıştır.

Kat kesme kuvveti deđerleri, 1. Bölümde açıklanan Eřdeđer Deprem Yüğü Yöntemine göre hesaplanmıştır. Bu hesaplamalarda kat kesme kuvvetleri %5 eksantriklikle dikkate alınmış olup, ETABS programında her iki dođrultuda ayrı ayrı kat kütle merkezlerine etki ettirilmiştir. Analiz sürecinde yük kombinasyonları kullanılmamıştır.

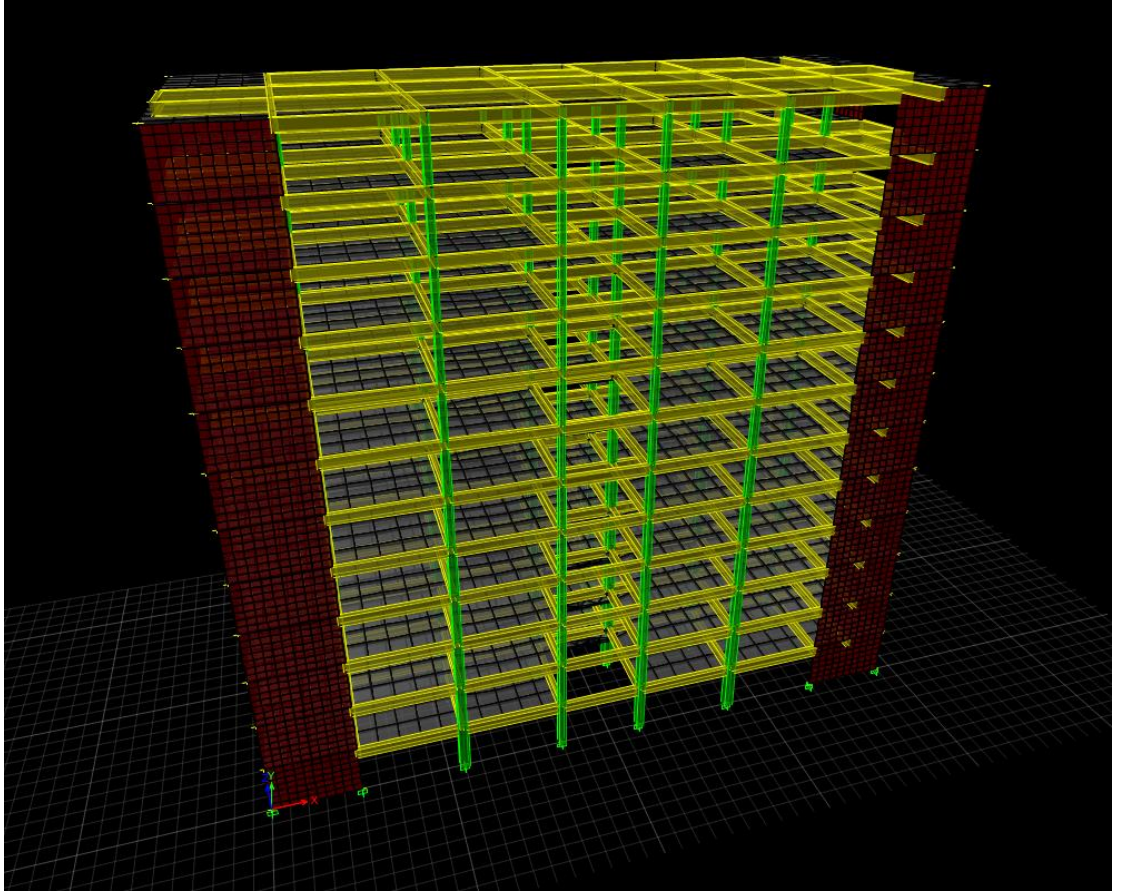
Hastane binasının 6, 9 ve 12 katlı projelerine ait yapı Modelleri aynı olup, ETABS programında oluşturulan 3 boyutlu tipik Modeli řekil 3.1, 3.2, 3.3 ve 3.4'te gösterilmiştir.



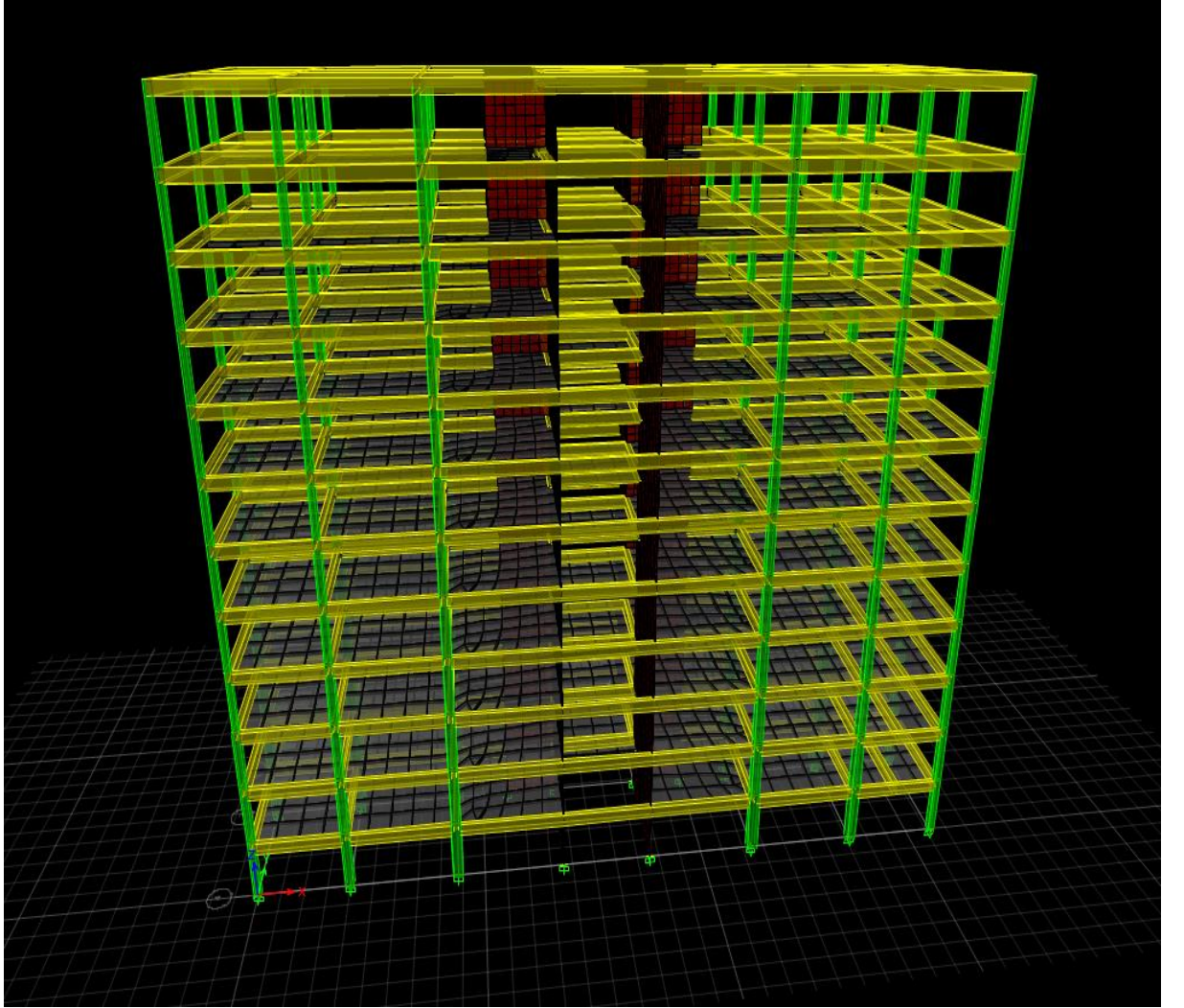
Şekil 3.1: Yapının 3 boyutlu Modeli (Model 1).



Şekil 3.2: Yapının 3 boyutlu Modeli (Model 2).



Şekil 3.3: Yapının 3 boyutlu Modeli (Model 3).



Şekil 3.4: Yapının 3 boyutlu Modeli (Model 4).

3.5. KOLONLARA GELEN EKSENEL KUVVETLERİN BELİRLENMESİ

Yapının kolonlarına, sabit yüklerden, hareketli yüklerden ve deprem yüklerinden gelen eksenel kuvvetlerin değerleri, yapının üç boyutlu Modellemesi ve yapıya ait önceki bölümlerde belirtilen yüklerin tanımlanmasıyla ETABS programında yapılan analizler sonucunda elde edilmiştir.

3.5.1. Düşey Yüklerin Etkisinde Oluşan Eksenel Kuvvetler

Hastane binasının 6, 9 ve 12 katlı durumları için ETABS programında yapıya etki eden sabit yükler (G) ve hareketli yükler (Q) ayrı ayrı tanımlanarak, bina özellikleri doğrultusunda kiriş uç momentlerinin göz önüne alınmaması durumuna göre hesaplanan düşey yüklerin etkisi altında kolonlarda oluşan eksenel kuvvetler belirlenmiştir. ETABS programında düşey yüklerden elde edilen eksenel kuvvetlerin toplam değeri (G + Q), kiriş uç momentlerinin göz önüne alınmaması durumuna göre hesaplanarak bulunan düşey yüklerden elde edilen eksenel kuvvetlerin ortak etkisi ($G_0 + Q_0$) olmak üzere bu değerler oranlanarak k_{P1} kat sayısı elde edilmiştir. Ayrıca hem ETABS'ten hem de kiriş uç momentlerinin göz önüne alınmaması durumuna göre hesaplanarak bulunan hareketli yük etkisinden elde edilen değerler, TS498'de bulunan hareketli yük azaltma katsayısı (β) ve yüzde eksiltme değerleri (γ) ile çarpılarak $G + \beta Q$, $G + \gamma Q$, $G_0 + \beta Q_0$ ve $G_0 + \gamma Q_0$ değerleri belirlenmiş ve bu değerler oranlanarak k_{P2} ve k_{P3} katsayıları da bulunmuştur. Hareketli yük azaltma katsayısı β , 6 katlı yapı için 0.80, 9 ve 12 katlı yapılar için 0.60 olarak alınmış olup, her kat kolonu bu değerlerle çarpılmıştır. 6 katlı Hastane binasına ait bulunan değerler Çizelge 3.14 ile Çizelge 3.25, 9 katlı ve 12 katlı hastane binasına ait çizelgeler ise Ek A'da verilmiştir. Dış kenarlardaki duvar ağırlıkları pencere boşluğu düşürmeden göz önüne alınmıştır.

Model 1 hastane binası için:

Çizelge 3.14: 6 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	$N_G + Q$ (kN)	N_{G0} (kN)	N_{Q0} (kN)	$N_{G0} + Q_0$ (kN)	$k_p = N_G + Q / N_{G0} + Q_0$
6	S1	97.217	20.654	117.872	101.95	26.25	128.2	0.919
	S9	153.023	47.497	200.520	154.96	51.25	206.21	0.972
	S2	192.629	56.574	249.203	186.63	57.75	244.38	1.020
	S10	272.354	121.828	394.182	242.76	112.75	355.51	1.109
	S3	197.677	58.413	256.090	200.11	63	263.11	0.973
	S11	285.699	130.066	415.765	262.098	123	385.098	1.080
	S4	187.451	55.984	243.435	185.97	59.69	245.66	0.991
	S12	218.403	92.896	311.299	207.618	95.875	303.493	1.026
5	S1	201.308	44.078	245.386	203.9	52.5	256.4	0.957
	S9	307.910	96.588	404.499	309.92	102.5	412.42	0.981
	S2	385.397	113.847	499.244	373.26	115.5	488.76	1.021
	S10	535.947	238.525	774.472	485.52	225.5	711.02	1.089
	S3	398.360	118.879	517.239	400.22	126	526.22	0.983
	S11	565.624	257.056	822.680	524.196	246	770.196	1.068
	S4	379.399	114.020	493.419	371.94	119.380	491.32	1.004
	S12	441.494	190.827	632.321	415.236	191.750	606.986	1.042
4	S1	304.099	66.939	371.038	305.85	78.75	384.6	0.965
	S9	462.330	145.247	607.576	464.88	153.75	618.63	0.982
	S2	578.079	170.837	748.915	559.89	173.25	733.14	1.022
	S10	801.308	356.414	1157.721	728.28	338.25	1066.53	1.086
	S3	598.374	178.793	777.167	600.33	189	789.33	0.985
	S11	846.674	384.690	1231.364	786.294	369	1155.294	1.066
	S4	570.613	171.683	742.296	557.91	179.07	736.98	1.007
	S12	662.983	287.470	950.452	622.854	287.625	910.479	1.044
3	S1	406.285	89.540	495.825	407.8	105	512.8	0.967
	S9	616.389	193.636	810.024	619.84	205	824.84	0.982
	S2	772.812	228.234	1001.045	746.52	231	977.52	1.024
	S10	1069.490	474.604	1544.094	971.04	451	1422.04	1.086
	S3	797.308	238.155	1035.463	800.44	252	1052.44	0.984
	S11	1130.501	512.457	1642.958	1048.392	492	1540.392	1.067
	S4	763.673	229.795	993.468	743.88	238.76	982.64	1.011
	S12	886.377	383.677	1270.053	830.472	383.5	1213.972	1.046
2	S1	507.915	111.849	619.764	509.75	131.25	641	0.967
	S9	770.510	241.871	1012.381	774.8	256.25	1031.05	0.982
	S2	968.369	285.964	1254.333	933.15	288.75	1221.9	1.027
	S10	1337.250	592.957	1930.207	1213.8	563.75	1777.55	1.086
	S3	996.244	297.267	1293.512	1000.55	315	1315.55	0.983
	S11	1414.433	640.403	2054.835	1310.49	615	1925.49	1.067
	S4	957.486	288.292	1245.778	929.85	298.45	1228.3	1.014
	S12	1108.415	479.100	1587.516	1038.09	479.375	1517.465	1.046
1	S1	607.281	133.203	740.483	611.7	157.5	769.2	0.963
	S9	924.357	289.574	1213.931	929.76	307.5	1237.26	0.981
	S2	1163.688	343.330	1507.018	1119.78	346.5	1466.28	1.028
	S10	1610.641	713.276	2323.917	1456.56	676.5	2133.06	1.089
	S3	1195.935	355.832	1551.768	1200.66	378	1578.66	0.983
	S11	1702.964	769.471	2472.436	1572.588	738	2310.588	1.070
	S4	1149.688	346.082	1495.770	1115.82	358.14	1473.96	1.015
	S12	1332.854	574.069	1906.923	1245.708	575.25	1820.958	1.047

Çizelge 3.15: 6 Katlı Hastane Binasına için $k_{p\beta}$ aksenal kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$ (kN)	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
6	S1	97.217	16.523	113.741	101.95	21	122.95	0.925
	S9	153.023	37.998	191.020	154.96	41	195.96	0.975
	S2	192.629	45.259	237.888	186.63	46.2	232.83	1.022
	S10	272.354	97.462	369.816	242.76	90.2	332.96	1.111
	S3	197.677	46.730	244.408	200.11	50.4	250.51	0.976
	S11	285.699	104.053	389.752	262.098	98.4	360.498	1.081
	S4	187.451	44.787	232.238	185.97	47.752	233.722	0.994
	S12	218.403	74.316	292.720	207.618	76.7	284.318	1.030
5	S1	201.308	35.262	236.571	203.9	42	245.9	0.962
	S9	307.910	77.271	385.181	309.92	82	391.92	0.983
	S2	385.397	91.078	476.475	373.26	92.4	465.66	1.023
	S10	535.947	190.820	726.767	485.52	180.4	665.92	1.091
	S3	398.360	95.103	493.464	400.22	100.8	501.02	0.985
	S11	565.624	205.645	771.268	524.196	196.8	720.996	1.070
	S4	379.399	91.216	470.615	371.94	95.504	467.444	1.007
	S12	441.494	152.662	594.156	415.236	153.4	568.636	1.045
4	S1	304.099	53.551	357.650	305.85	63	368.85	0.970
	S9	462.330	116.197	578.527	464.88	123	587.88	0.984
	S2	578.079	136.669	714.748	559.89	138.6	698.49	1.023
	S10	801.308	285.131	1086.439	728.28	270.6	998.88	1.088
	S3	598.374	143.034	741.408	600.33	151.2	751.53	0.987
	S11	846.674	307.752	1154.426	786.294	295.2	1081.494	1.067
	S4	570.613	137.346	707.959	557.91	143.256	701.166	1.010
	S12	662.983	229.976	892.958	622.854	230.1	852.954	1.047
3	S1	406.285	71.632	477.917	407.8	84	491.8	0.972
	S9	616.389	154.908	771.297	619.84	164	783.84	0.984
	S2	772.812	182.587	955.398	746.52	184.8	931.32	1.026
	S10	1069.490	379.683	1449.174	971.04	360.8	1331.84	1.088
	S3	797.308	190.524	987.832	800.44	201.6	1002.04	0.986
	S11	1130.501	409.966	1540.467	1048.392	393.6	1441.992	1.068

	S4	763.673	183.836	947.509	743.88	191.008	934.888	1.013
	S12	886.377	306.941	1193.318	830.472	306.8	1137.272	1.049
2	S1	507.915	89.479	597.394	509.75	105	614.75	0.972
	S9	770.510	193.496	964.006	774.8	205	979.8	0.984
	S2	968.369	228.771	1197.140	933.15	231	1164.15	1.028
	S10	1337.250	474.366	1811.616	1213.8	451	1664.8	1.088
	S3	996.244	237.814	1234.058	1000.55	252	1252.55	0.985
	S11	1414.433	512.322	1926.755	1310.49	492	1802.49	1.069
	S4	957.486	230.634	1188.119	929.85	238.76	1168.61	1.017
	S12	1108.415	383.280	1491.695	1038.09	383.5	1421.59	1.049
1	S1	607.281	106.562	713.843	611.7	126	737.7	0.968
	S9	924.357	231.659	1156.016	929.76	246	1175.76	0.983
	S2	1163.688	274.664	1438.352	1119.78	277.2	1396.98	1.030
	S10	1610.641	570.621	2181.262	1456.56	541.2	1997.76	1.092
	S3	1195.935	284.666	1480.601	1200.66	302.4	1503.06	0.985
	S11	1702.964	615.577	2318.541	1572.588	590.4	2162.988	1.072
	S4	1149.688	276.865	1426.553	1115.82	286.512	1402.332	1.017
	S12	1332.854	459.255	1792.109	1245.708	460.2	1705.908	1.051

Çizelge 3.16: 6 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	N_G (kN)	N_{YQ} (kN)	N_{G+YQ} (kN)	N_{G0} (kN)	N_{YQ0} (kN)	N_{G0+YQ0} (kN)	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
6	0.4	S1	97.217	8.262	105.479	101.95	10.5	112.45	0.938
	0.4	S9	153.023	18.999	172.022	154.96	20.500	175.46	0.980
	0.4	S2	192.629	22.630	215.259	186.63	23.1	209.73	1.026
	0.4	S10	272.354	48.731	321.085	242.76	45.1	287.86	1.115
	0.4	S3	197.677	23.365	221.043	200.11	25.2	225.31	0.981
	0.4	S11	285.699	52.026	337.725	262.098	49.2	311.298	1.085
	0.4	S4	187.451	22.393	209.845	185.97	23.876	209.846	1.000
	0.4	S12	218.403	37.158	255.561	207.618	38.35	245.968	1.039
5	0.6	S1	201.308	20.654	221.963	203.9	26.25	230.15	0.964
	0.6	S9	307.910	47.497	355.407	309.92	51.250	361.17	0.984
	0.6	S2	385.397	56.574	441.971	373.26	57.75	431.01	1.025
	0.6	S10	535.947	121.828	657.775	485.52	112.75	598.27	1.099
	0.6	S3	398.360	58.413	456.773	400.22	63	463.22	0.986
	0.6	S11	565.624	130.066	695.690	524.196	123	647.196	1.075
	0.6	S4	379.399	55.984	435.383	371.94	59.69	431.63	1.009
	0.6	S12	441.494	92.896	534.390	415.236	95.875	511.111	1.046
4	0.8	S1	304.099	37.178	341.277	305.85	47.25	353.1	0.967
	0.8	S9	462.330	85.495	547.825	464.88	92.250	557.13	0.983
	0.8	S2	578.079	101.833	679.911	559.89	103.95	663.84	1.024
	0.8	S10	801.308	219.290	1020.598	728.28	202.95	931.23	1.096
	0.8	S3	598.374	105.143	703.517	600.33	113.4	713.73	0.986
	0.8	S11	846.674	234.119	1080.792	786.294	221.4	1007.694	1.073
	0.8	S4	570.613	100.770	671.383	557.91	107.442	665.352	1.009
	0.8	S12	662.983	167.212	830.195	622.854	172.575	795.429	1.044
3	1	S1	406.285	57.832	464.117	407.8	73.5	481.3	0.964
	1	S9	616.389	132.992	749.381	619.84	143.500	763.34	0.982
	1	S2	772.812	158.407	931.218	746.52	161.7	908.22	1.025
	1	S10	1069.490	341.118	1410.609	971.04	315.7	1286.74	1.096
	1	S3	797.308	163.556	960.864	800.44	176.4	976.84	0.984
	1	S11	1130.501	364.185	1494.686	1048.392	344.4	1392.792	1.073
	1	S4	763.673	156.754	920.427	743.88	167.132	911.012	1.010
	1	S12	886.377	260.108	1146.484	830.472	268.45	1098.922	1.043
2	1	S1	507.915	78.486	586.401	509.75	99.75	609.5	0.962
	1	S9	770.510	180.489	950.999	774.8	194.750	969.55	0.981
	1	S2	968.369	214.980	1183.349	933.15	219.45	1152.6	1.027

	1	S10	1337.250	462.946	1800.196	1213.8	428.45	1642.25	1.096
	1	S3	996.244	221.969	1218.213	1000.55	239.4	1239.95	0.982
	1	S11	1414.433	494.250	1908.683	1310.49	467.4	1777.89	1.074
	1	S4	957.486	212.738	1170.223	929.85	226.822	1156.672	1.012
	1	S12	1108.415	353.003	1461.418	1038.09	364.325	1402.415	1.042
1	1	S1	607.281	99.140	706.421	611.7	126	737.7	0.958
	1	S9	924.357	227.986	1152.343	929.76	246.000	1175.76	0.980
	1	S2	1163.688	271.554	1435.242	1119.78	277.2	1396.98	1.027
	1	S10	1610.641	584.774	2195.415	1456.56	541.2	1997.76	1.099
	1	S3	1195.935	280.381	1476.317	1200.66	302.4	1503.06	0.982
	1	S11	1702.964	624.316	2327.281	1572.588	590.4	2162.988	1.076
	1	S4	1149.688	268.721	1418.409	1115.82	286.512	1402.332	1.011
	1	S12	1332.854	445.899	1778.753	1245.708	460.2	1705.908	1.043

Model 2:

Çizelge 3.17: 6 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_{G+Q}/N_{G0+Q0}$
6	S10	260.018	117.772	377.790	242.76	112.75	355.51	1.063
	S11	281.375	128.367	409.742	262.098	123	385.098	1.064
	S4	190.219	56.868	247.087	185.97	59.69	245.66	1.006
	S12	219.366	93.193	312.559	207.618	95.875	303.493	1.030
5	S10	512.203	231.007	743.210	485.52	225.5	711.02	1.045
	S11	556.620	253.740	810.360	524.196	246	770.196	1.052
	S4	382.374	115.139	497.513	371.94	119.38	491.32	1.013
	S12	443.194	191.436	634.630	415.236	191.75	606.986	1.046
4	S10	767.123	345.688	1112.811	728.28	338.25	1066.53	1.043
	S11	833.579	379.967	1213.546	786.294	369	1155.294	1.050
	S4	574.308	173.183	747.491	557.91	179.07	736.98	1.014
	S12	665.450	288.410	953.860	622.854	287.625	910.479	1.048
3	S10	1027.667	461.744	1489.410	971.04	451	1422.04	1.047
	S11	1113.916	506.539	1620.455	1048.392	492	1540.392	1.052
	S4	768.884	231.905	1000.789	743.88	238.76	982.64	1.018
	S12	889.597	384.965	1274.562	830.472	383.5	1213.972	1.050
2	S10	1291.092	579.163	1870.255	1213.8	563.75	1777.55	1.052
	S11	1395.271	633.580	2028.850	1310.49	615	1925.49	1.054
	S4	965.322	291.326	1256.647	929.85	298.45	1228.3	1.023
	S12	1112.346	480.733	1593.079	1038.09	479.375	1517.465	1.050
1	S10	1562.206	699.051	2261.257	1456.56	676.5	2133.06	1.060
	S11	1682.379	762.074	2444.453	1572.588	738	2310.588	1.058
	S4	1161.423	350.353	1511.775	1115.82	358.14	1473.96	1.026
	S12	1337.440	576.015	1913.455	1245.708	575.25	1820.958	1.051

Çizelge 3.18: 6 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$ (kN)	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
6	S10	260.018	94.217	354.235	242.76	90.2	332.96	1.064
	S11	281.375	102.694	384.069	262.098	98.4	360.498	1.065
	S4	190.219	45.495	235.714	185.97	47.752	233.722	1.009
	S12	219.366	74.554	293.920	207.618	76.7	284.318	1.034
5	S10	512.203	184.806	697.008	485.52	180.4	665.92	1.047
	S11	556.620	202.992	759.612	524.196	196.8	720.996	1.054
	S4	382.374	92.111	474.485	371.94	95.504	467.444	1.015
	S12	443.194	153.149	596.343	415.236	153.4	568.636	1.049
4	S10	767.123	276.550	1043.673	728.28	270.6	998.88	1.045
	S11	833.579	303.974	1137.552	786.294	295.2	1081.494	1.052
	S4	574.308	138.546	712.854	557.91	143.256	701.166	1.017
	S12	665.450	230.728	896.178	622.854	230.1	852.954	1.051
3	S10	1027.667	369.395	1397.062	971.04	360.8	1331.84	1.049
	S11	1113.916	405.231	1519.147	1048.392	393.6	1441.992	1.054
	S4	768.884	185.524	954.408	743.88	191.008	934.888	1.021
	S12	889.597	307.972	1197.569	830.472	306.8	1137.272	1.053
2	S10	1291.092	463.330	1754.422	1213.8	451	1664.8	1.054
	S11	1395.271	506.864	1902.134	1310.49	492	1802.49	1.055
	S4	965.322	233.060	1198.382	929.85	238.76	1168.61	1.025
	S12	1112.346	384.586	1496.932	1038.09	383.5	1421.59	1.053
1	S10	1562.206	559.241	2121.447	1456.56	541.2	1997.76	1.062
	S11	1682.379	609.659	2292.038	1572.588	590.4	2162.988	1.060
	S4	1161.423	280.282	1441.705	1115.82	286.512	1402.332	1.028
	S12	1337.440	460.812	1798.252	1245.708	460.2	1705.908	1.054

Çizelge 3.19: 6 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları.

KAT	γ	KOLON	N_G (kN)	N_{YQ} (kN)	N_{G+YQ} (kN)	N_{G0} (kN)	N_{YQ0} (kN)	N_{G0+YQ0} (kN)	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
6	0.4	S10	260.018	47.109	307.127	242.76	45.1	287.86	1.067
	0.4	S11	281.375	51.347	332.722	262.098	49.200	311.298	1.069
	0.4	S4	190.219	22.747	212.966	185.97	23.876	209.846	1.015
	0.4	S12	219.366	37.277	256.643	207.618	38.350	245.968	1.043
5	0.6	S10	512.203	117.772	629.974	485.52	112.750	598.27	1.053
	0.6	S11	556.620	128.367	684.987	524.196	123.000	647.196	1.058
	0.6	S4	382.374	56.868	439.242	371.94	59.690	431.63	1.018
	0.6	S12	443.194	93.193	536.387	415.236	95.875	511.111	1.049
4	0.8	S10	767.123	211.989	979.112	728.28	202.950	931.23	1.051
	0.8	S11	833.579	231.061	1064.640	786.294	221.400	1007.694	1.057
	0.8	S4	574.308	102.363	676.671	557.91	107.442	665.352	1.017
	0.8	S12	665.450	167.747	833.196	622.854	172.575	795.429	1.047
3	1	S10	1027.667	329.760	1357.427	971.04	315.700	1286.74	1.055
	1	S11	1113.916	359.428	1473.344	1048.392	344.400	1392.792	1.058
	1	S4	768.884	159.231	928.115	743.88	167.132	911.012	1.019
	1	S12	889.597	260.939	1150.536	830.472	268.450	1098.922	1.047
2	1	S10	1291.092	447.532	1738.624	1213.8	428.450	1642.25	1.059
	1	S11	1395.271	487.795	1883.066	1310.49	467.400	1777.89	1.059
	1	S4	965.322	216.100	1181.421	929.85	226.822	1156.672	1.021
	1	S12	1112.346	354.132	1466.478	1038.09	364.325	1402.415	1.046
1	1	S10	1562.206	565.303	2127.509	1456.56	541.200	1997.76	1.065
	1	S11	1682.379	616.163	2298.541	1572.588	590.400	2162.988	1.063
	1	S4	1161.423	272.968	1434.391	1115.82	286.512	1402.332	1.023
	1	S12	1337.440	447.324	1784.765	1245.708	460.200	1705.908	1.046

Model 3

Çizelge 3.20: 6 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_{G+Q}/N_{G0+Q0}$
6	S10	266.414	120.483	386.897	242.76	112.75	355.51	1.088
	S3	199.012	58.624	257.637	200.11	63	263.11	0.979
	S11	288.493	131.032	419.525	262.098	123	385.098	1.089
	S4	187.762	56.131	243.892	185.97	59.69	245.66	0.993
	S12	218.305	92.906	311.210	207.618	95.875	303.493	1.025
5	S10	523.618	235.947	759.565	485.52	225.5	711.02	1.068
	S3	398.214	118.497	516.710	400.22	126	526.22	0.982
	S11	570.337	258.749	829.086	524.196	246	770.196	1.076
	S4	380.415	114.480	494.895	371.94	119.38	491.32	1.007
	S12	441.597	190.996	632.593	415.236	191.75	606.986	1.042
4	S10	783.225	352.712	1135.937	728.28	338.25	1066.53	1.065
	S3	597.519	178.101	775.620	600.33	189	789.33	0.983
	S11	853.323	387.143	1240.466	786.294	369	1155.294	1.074
	S4	572.232	172.459	744.691	557.91	179.07	736.98	1.010
	S12	663.257	287.806	951.063	622.854	287.625	910.479	1.045
3	S10	1048.467	470.868	1519.336	971.04	451	1422.04	1.068
	S3	796.802	237.500	1034.302	800.44	252	1052.44	0.983
	S11	1138.919	515.661	1654.580	1048.392	492	1540.392	1.074
	S4	765.748	230.854	996.603	743.88	238.76	982.64	1.014
	S12	886.885	384.222	1271.108	830.472	383.5	1213.972	1.047
2	S10	1316.658	590.416	1907.074	1213.8	563.75	1777.55	1.073
	S3	997.267	297.044	1294.311	1000.55	315	1315.55	0.984
	S11	1424.433	644.326	2068.759	1310.49	615	1925.49	1.074
	S4	959.835	289.585	1249.420	929.85	298.45	1228.3	1.017
	S12	1109.165	479.867	1589.032	1038.09	479.375	1517.465	1.047
1	S10	1592.785	712.515	2305.300	1456.56	676.5	2133.06	1.081
	S3	1200.005	356.532	1556.537	1200.66	378	1578.66	0.986
	S11	1714.268	774.002	2488.270	1572.588	738	2310.588	1.077
	S4	1152.000	347.478	1499.478	1115.82	358.14	1473.96	1.017
	S12	1333.766	575.014	1908.780	1245.708	575.25	1820.958	1.048

Çizelge 3.21: 6 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$ (kN)	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
6	S10	266.414	96.387	362.800	242.76	90.2	332.96	1.090
	S3	199.012	46.899	245.912	200.11	50.4	250.51	0.982
	S11	288.493	104.825	393.318	262.098	98.4	360.498	1.091
	S4	187.762	44.904	232.666	185.97	47.752	233.722	0.995
	S12	218.305	74.325	292.629	207.618	76.7	284.318	1.029
5	S10	523.618	188.758	712.376	485.52	180.4	665.92	1.070
	S3	398.214	94.797	493.011	400.22	100.8	501.02	0.984
	S11	570.337	206.999	777.336	524.196	196.8	720.996	1.078
	S4	380.415	91.584	471.999	371.94	95.504	467.444	1.010
	S12	441.597	152.796	594.394	415.236	153.4	568.636	1.045
4	S10	783.225	282.169	1065.394	728.28	270.6	998.88	1.067
	S3	597.519	142.481	740.000	600.33	151.2	751.53	0.985
	S11	853.323	309.714	1163.037	786.294	295.2	1081.494	1.075
	S4	572.232	137.968	710.199	557.91	143.256	701.166	1.013
	S12	663.257	230.245	893.502	622.854	230.1	852.954	1.048
3	S10	1048.467	376.695	1425.162	971.04	360.8	1331.84	1.070
	S3	796.802	190.000	986.802	800.44	201.6	1002.04	0.985
	S11	1138.919	412.529	1551.448	1048.392	393.6	1441.992	1.076
	S4	765.748	184.684	950.432	743.88	191.008	934.888	1.017
	S12	886.885	307.378	1194.263	830.472	306.8	1137.272	1.050
2	S10	1316.658	472.333	1788.991	1213.8	451	1664.8	1.075
	S3	997.267	237.635	1234.903	1000.55	252	1252.55	0.986
	S11	1424.433	515.461	1939.894	1310.49	492	1802.49	1.076
	S4	959.835	231.668	1191.503	929.85	238.76	1168.61	1.020
	S12	1109.165	383.894	1493.058	1038.09	383.5	1421.59	1.050
1	S10	1592.785	570.012	2162.797	1456.56	541.2	1997.76	1.083
	S3	1200.005	285.225	1485.230	1200.66	302.4	1503.06	0.988
	S11	1714.268	619.202	2333.470	1572.588	590.4	2162.988	1.079
	S4	1152.000	277.982	1429.983	1115.82	286.512	1402.332	1.020
	S12	1333.766	460.011	1793.777	1245.708	460.2	1705.908	1.052

Çizelge 3.22: 6 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	N_G (kN)	N_{YQ} (kN)	$N_G + YQ$ (kN)	N_{G0} (kN)	N_{YQ0} (kN)	$N_{G0} + YQ0$ (kN)	$k_{p\gamma} = N_G + YQ / N_{G0} + YQ0$
6	0.4	S10	266.414	48.193	314.607	242.76	45.1	287.86	1.093
	0.4	S3	199.012	23.450	222.462	200.11	25.2	225.31	0.987
	0.4	S11	288.493	52.413	340.906	262.098	49.2	311.298	1.095
	0.4	S4	187.762	22.452	210.214	185.97	23.876	209.846	1.002
	0.4	S12	218.305	37.162	255.467	207.618	38.35	245.968	1.039
5	0.6	S10	523.618	120.483	644.102	485.52	112.75	598.27	1.077
	0.6	S3	398.214	58.624	456.838	400.22	63	463.22	0.986
	0.6	S11	570.337	131.032	701.368	524.196	123	647.196	1.084
	0.6	S4	380.415	56.131	436.546	371.94	59.69	431.63	1.011
	0.6	S12	441.597	92.906	534.503	415.236	95.875	511.111	1.046
4	0.8	S10	783.225	216.870	1000.095	728.28	202.95	931.23	1.074
	0.8	S3	597.519	105.524	703.042	600.33	113.4	713.73	0.985
	0.8	S11	853.323	235.857	1089.180	786.294	221.4	1007.694	1.081
	0.8	S4	572.232	101.035	673.267	557.91	107.442	665.352	1.012
	0.8	S12	663.257	167.231	830.488	622.854	172.575	795.429	1.044
3	1	S10	1048.467	337.353	1385.820	971.04	315.7	1286.74	1.077
	1	S3	796.802	164.148	960.949	800.44	176.4	976.84	0.984
	1	S11	1138.919	366.888	1505.808	1048.392	344.4	1392.792	1.081
	1	S4	765.748	157.166	922.914	743.88	167.132	911.012	1.013
	1	S12	886.885	260.137	1147.022	830.472	268.45	1098.922	1.044
2	1	S10	1316.658	457.836	1774.494	1213.8	428.45	1642.25	1.081
	1	S3	997.267	222.772	1220.039	1000.55	239.4	1239.95	0.984
	1	S11	1424.433	497.920	1922.353	1310.49	467.4	1777.89	1.081
	1	S4	959.835	213.296	1173.132	929.85	226.822	1156.672	1.014
	1	S12	1109.165	353.042	1462.207	1038.09	364.325	1402.415	1.043
1	1	S10	1592.785	578.319	2171.104	1456.56	541.2	1997.76	1.087
	1	S3	1200.005	281.396	1481.401	1200.66	302.4	1503.06	0.986
	1	S11	1714.268	628.952	2343.220	1572.588	590.4	2162.988	1.083
	1	S4	1152.000	269.427	1421.427	1115.82	286.512	1402.332	1.014
	1	S12	1333.766	445.948	1779.715	1245.708	460.2	1705.908	1.043

Çizelge 3.23: 6 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	$N_G + Q$ (kN)	N_{G0} (kN)	N_{Q0} (kN)	$N_{G0} + Q_0$ (kN)	$k_p = N_G + Q / N_{G0} + Q_0$
6	S1	96.802	20.492	117.294	101.95	26.25	128.2	0.915
	S9	152.356	47.200	199.556	154.96	51.25	206.21	0.968
	S2	194.287	57.249	251.536	186.63	57.75	244.38	1.029
	S10	278.296	124.683	402.979	242.76	112.75	355.51	1.134
	S3	192.719	56.401	249.119	200.11	63	263.11	0.947
	S11	231.483	103.419	334.901	262.098	92.25	354.348	0.945
5	S1	200.584	43.830	244.415	203.9	52.5	256.4	0.953
	S9	307.016	96.215	403.230	309.92	102.5	412.42	0.978
	S2	387.757	114.869	502.627	373.26	115.5	488.76	1.028
	S10	545.513	243.201	788.715	485.52	225.5	711.02	1.109
	S3	387.553	114.605	502.158	400.22	126	526.22	0.954
	S11	452.449	200.921	653.370	524.196	184.5	708.696	0.922
4	S1	303.040	66.621	369.661	305.85	78.75	384.6	0.961
	S9	461.029	144.724	605.753	464.88	153.75	618.63	0.979
	S2	581.214	172.284	753.498	559.89	173.25	733.14	1.028
	S10	814.828	363.110	1177.938	728.28	338.25	1066.53	1.104
	S3	582.537	172.606	755.143	600.33	189	789.33	0.957
	S11	677.334	300.432	977.765	786.294	276.75	1063.044	0.920
3	S1	405.003	89.195	494.198	407.8	105	512.8	0.964
	S9	614.880	193.049	807.929	619.84	205	824.84	0.979
	S2	776.520	230.046	1006.567	746.52	231	977.52	1.030
	S10	1085.965	482.879	1568.844	971.04	451	1422.04	1.103
	S3	777.616	230.448	1008.064	800.44	252	1052.44	0.958
	S11	908.136	401.410	1309.546	1048.392	369	1417.392	0.924
2	S1	506.531	111.524	618.055	509.75	131.25	641	0.964
	S9	768.901	241.267	1010.168	774.8	256.25	1031.05	0.980
	S2	972.557	288.118	1260.675	933.15	288.75	1221.9	1.032
	S10	1356.145	602.571	1958.716	1213.8	563.75	1777.55	1.102
	S3	973.990	288.478	1262.468	1000.55	315	1315.55	0.960
	S11	1142.249	504.011	1646.260	1310.49	461.25	1771.74	0.929
1	S1	605.866	132.914	738.780	611.7	157.5	769.2	0.960
	S9	922.639	288.942	1211.581	929.76	307.5	1237.26	0.979
	S2	1168.257	345.774	1514.030	1119.78	346.5	1466.28	1.033
	S10	1632.098	724.296	2356.394	1456.56	676.5	2133.06	1.105
	S3	1172.630	346.475	1519.106	1200.66	378	1578.66	0.962
	S11	1385.596	609.845	1995.440	1572.588	553.5	2126.088	0.939

Çizelge 3.24: 6 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_{pQ} (kN)	$N_{G + pQ}$ (kN)	N_{G0} (kN)	N_{pQ0} (kN)	$N_{G0 + pQ0}$ (kN)	$k_{p\beta} = N_{G + pQ} / N_{G0 + pQ0}$
6	S1	96.802	16.393	113.196	101.95	21	122.95	0.921
	S9	152.356	37.760	190.116	154.96	41	195.96	0.970
	S2	194.287	45.799	240.086	186.63	46.2	232.83	1.031
	S10	278.296	99.746	378.042	242.76	90.2	332.96	1.135
	S3	192.719	45.121	237.839	200.11	50.4	250.51	0.949
	S11	231.483	82.735	314.217	262.098	73.8	335.898	0.935
5	S1	200.584	35.064	235.649	203.9	42	245.9	0.958
	S9	307.016	76.972	383.987	309.92	82	391.92	0.980
	S2	387.757	91.895	479.653	373.26	92.4	465.66	1.030
	S10	545.513	194.561	740.074	485.52	180.4	665.92	1.111
	S3	387.553	91.684	479.237	400.22	100.8	501.02	0.957
	S11	452.449	160.736	613.185	524.196	147.6	671.796	0.913
4	S1	303.040	53.297	356.337	305.85	63	368.85	0.966
	S9	461.029	115.779	576.808	464.88	123	587.88	0.981
	S2	581.214	137.827	719.041	559.89	138.6	698.49	1.029
	S10	814.828	290.488	1105.316	728.28	270.6	998.88	1.107
	S3	582.537	138.085	720.622	600.33	151.2	751.53	0.959
	S11	677.334	240.345	917.679	786.294	221.4	1007.694	0.911
3	S1	405.003	71.356	476.359	407.8	84	491.8	0.969
	S9	614.880	154.439	769.319	619.84	164	783.84	0.981
	S2	776.520	184.037	960.557	746.52	184.8	931.32	1.031
	S10	1085.965	386.303	1472.268	971.04	360.8	1331.84	1.105
	S3	777.616	184.358	961.974	800.44	201.6	1002.04	0.960
	S11	908.136	321.128	1229.264	1048.392	295.2	1343.592	0.915
2	S1	506.531	89.219	595.750	509.75	105	614.75	0.969
	S9	768.901	193.013	961.915	774.8	205	979.8	0.982
	S2	972.557	230.495	1203.052	933.15	231	1164.15	1.033
	S10	1356.145	482.057	1838.201	1213.8	451	1664.8	1.104
	S3	973.990	230.782	1204.772	1000.55	252	1252.55	0.962
	S11	1142.249	403.209	1545.458	1310.49	369	1679.49	0.920
1	S1	605.866	106.331	712.197	611.7	126	737.7	0.965
	S9	922.639	231.153	1153.793	929.76	246	1175.76	0.981
	S2	1168.257	276.619	1444.875	1119.78	277.2	1396.98	1.034
	S10	1632.098	579.437	2211.535	1456.56	541.2	1997.76	1.107
	S3	1172.630	277.180	1449.811	1200.66	302.4	1503.06	0.965
	S11	1385.596	487.876	1873.471	1572.588	442.8	2015.388	0.930

Çizelge 3.25: 6 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	N_G (kN)	N_{YQ} (kN)	N_{G+YQ} (kN)	N_{G0} (kN)	N_{YQ0} (kN)	N_{G0+YQ0} (kN)	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
6	0.4	S1	96.802	8.197	104.999	101.95	10.5	112.45	0.934
	0.4	S9	152.356	18.880	171.236	154.96	20.5	175.46	0.976
	0.4	S2	194.287	22.900	217.187	186.63	23.1	209.73	1.036
	0.4	S10	278.296	49.873	328.169	242.76	45.1	287.86	1.140
	0.4	S3	192.719	22.560	215.279	200.11	25.2	225.31	0.955
	0.4	S11	231.483	41.367	272.850	262.098	36.9	298.998	0.913
5	0.6	S1	200.584	20.492	221.076	203.9	26.25	230.15	0.961
	0.6	S9	307.016	47.200	354.216	309.92	51.25	361.17	0.981
	0.6	S2	387.757	57.249	445.006	373.26	57.75	431.01	1.032
	0.6	S10	545.513	124.683	670.196	485.52	112.75	598.27	1.120
	0.6	S3	387.553	56.401	443.954	400.22	63	463.22	0.958
	0.6	S11	452.449	103.419	555.868	524.196	92.25	616.446	0.902
4	0.8	S1	303.040	36.885	339.925	305.85	47.25	353.1	0.963
	0.8	S9	461.029	84.960	545.989	464.88	92.25	557.13	0.980
	0.8	S2	581.214	103.049	684.262	559.89	103.95	663.84	1.031
	0.8	S10	814.828	224.429	1039.258	728.28	202.95	931.23	1.116
	0.8	S3	582.537	101.522	684.059	600.33	113.4	713.73	0.958
	0.8	S11	677.334	186.154	863.487	786.294	166.05	952.344	0.907
3	1	S1	405.003	57.376	462.379	407.8	73.5	481.3	0.961
	1	S9	614.880	132.160	747.040	619.84	143.5	763.34	0.979
	1	S2	776.520	160.298	936.818	746.52	161.7	908.22	1.031
	1	S10	1085.965	349.112	1435.077	971.04	315.7	1286.74	1.115
	1	S3	777.616	157.923	935.539	800.44	176.4	976.84	0.958
	1	S11	908.136	289.572	1197.709	1048.392	258.3	1306.692	0.917
2	1	S1	506.531	77.868	584.399	509.75	99.75	609.5	0.959
	1	S9	768.901	179.360	948.261	774.8	194.75	969.55	0.978
	1	S2	972.557	217.547	1190.104	933.15	219.45	1152.6	1.033
	1	S10	1356.145	473.795	1829.940	1213.8	428.45	1642.25	1.114

1	1	S3	973.990	214.323	1188.313	1000.55	239.4	1239.95	0.958
	1	S11	1142.249	392.991	1535.240	1310.49	350.55	1661.04	0.924
	1	S1	605.866	98.360	704.226	611.7	126	737.7	0.955
	1	S9	922.639	226.560	1149.199	929.76	246	1175.76	0.977
	1	S2	1168.257	274.796	1443.053	1119.78	277.2	1396.98	1.033
	1	S10	1632.098	598.478	2230.576	1456.56	541.2	1997.76	1.117
	1	S3	1172.630	270.724	1443.355	1200.66	302.4	1503.06	0.960
	1	S11	1385.596	496.410	1882.006	1572.588	442.8	2015.388	0.934

Çizelge 3.26: 6 katlı içi k_p oranları.

KAT	k_p							
	S1	S9	S2	S10	S3	S11	S4	S12
6.KAT	0,92	0,97	1,02	1,11	0,97	1,08	0,99	1,03
5.KAT	0,96	0,98	1,02	1,09	0,98	1,07	1,00	1,04
4.KAT	0,97	0,98	1,02	1,09	0,99	1,07	1,01	1,04
3.KAT	0,97	0,98	1,03	1,09	0,98	1,07	1,01	1,01
2.KAT	0,97	0,98	1,03	1,09	0,98	1,07	1,01	1,01
1.KAT	0,96	0,98	1,03	1,09	0,98	1,07	1,02	1,05

Çizelge 3.27: 9 katlı için k_p oranları.

KAT	k_p							
	S1	S9	S2	S10	S3	S11	S4	S12
9.KAT	0.93	0.97	1.02	1.10	0.97	1.08	0.99	1.04
8.KAT	0.97	0.98	1.02	1.10	0.98	1.07	1.00	1.06
7.KAT	0.97	0.98	1.02	1.08	0.98	1.07	1.00	1.06
6.KAT	0.98	0.98	1.02	1.08	0.98	1.07	1.01	1.06
5.KAT	0.98	0.98	1.03	1.08	0.98	1.07	1.01	1.07
4.KAT	0.97	0.98	1.03	1.08	0.98	1.07	1.01	1.07
3.KAT	0.97	0.99	1.04	1.08	0.98	1.08	1.02	1.07
2.KAT	0.97	0.99	1.04	1.08	0.98	1.08	1.02	1.07
1.KAT	0.96	0.99	1.04	1.08	0.99	1.08	1.02	1.07

Çizelge 3.28: 12 katlı için k_p oranları.

KAT	k_p							
	S1	S9	S2	S10	S3	S11	S4	S12
12.KAT	0.99	0.97	1.01	1.10	0.97	1.08	0.98	1.05
11.KAT	0.98	0.98	1.01	1.08	0.98	1.07	1.00	1.07
10.KAT	0.99	0.98	1.01	1.08	0.98	1.07	1.00	1.08
9.KAT	0.99	0.98	1.02	1.08	0.98	1.07	1.00	1.08
8.KAT	0.99	0.98	1.02	1.08	0.98	1.07	1.00	1.08
7.KAT	0.99	0.98	1.02	1.08	0.98	1.07	1.01	1.09
6.KAT	0.98	0.99	1.02	1.08	0.98	1.08	1.01	1.09
5.KAT	0.98	0.99	1.03	1.08	0.98	1.08	1.01	1.09
4.KAT	0.98	0.99	1.03	1.08	0.99	1.08	1.02	1.09
3.KAT	0.98	1.00	1.03	1.08	0.99	1.08	1.02	1.09
2.KAT	0.98	1.00	1.03	1.08	1.02	1.08	1.02	1.09
1.KAT	0.98	1.00	1.04	1.08	1.02	1.08	1.03	1.09

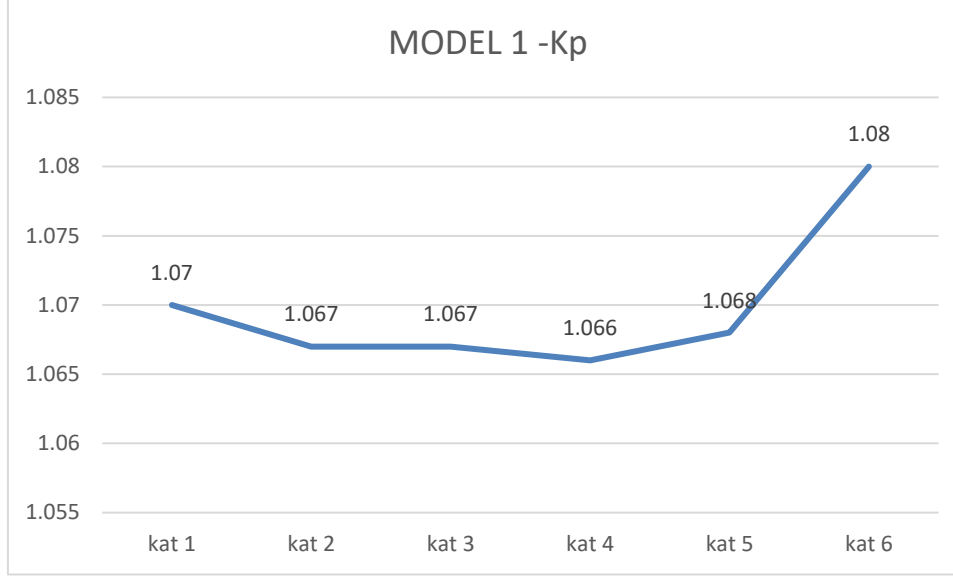
6 katlı binada yukarıda her bir Model için hesaplanan k_p değerleri tüm Modeller için toplu olarak Çizelge 3.29 da gösterilmiştir.

Çizelge 3.29: Tüm Modellerde 6 Katlı Hastane Binasına için k_p eksenel kuvvet oranları.

$k_p = N_G + Q/N_{G0} + Q_0$					
KAT	KOLON	Model 1	Model 2	Model 3	Model 4
6	S1	0.919	**	**	0.915
	S9	0.972	**	**	0.968
	S2	1.020	**	1.088	1.029
	S10	1.109	1.063	0.979	1.134
	S3	0.973	**	1.089	0.947
	S11	1.080	1.064	0.993	0.945
	S4	0.991	1.006	1.025	**
5	S12	1.026	1.030	**	**
	S1	0.957	**	**	0.953
	S9	0.981	**	**	0.978
	S2	1.021	**	1.068	1.028
	S10	1.089	1.045	0.982	1.109
	S3	0.983	**	1.076	0.954
	S11	1.068	1.052	1.007	0.922
4	S4	1.004	1.013	1.042	**
	S12	1.042	**	**	**
	S1	0.965	**	**	0.961
	S9	0.982	**	**	0.979
	S2	1.022	**	1.065	1.028
	S10	1.086	1.043	0.983	1.104
	S3	0.985	**	1.074	0.957
3	S11	1.066	1.050	1.010	0.920
	S4	1.007	1.014	**	**
	S12	1.044	1.048	**	**
	S1	0.967	**	**	0.964
	S9	0.982	**	**	0.979
	S2	1.024	**	1.068	1.030
	S10	1.086	1.047	0.983	1.103
2	S3	0.984	**	1.074	0.958
	S11	1.067	1.052	1.014	0.924
	S4	1.011	**	**	**
	S12	1.046	**	**	**
	S1	0.967	**	**	0.964
	S9	0.982	**	**	0.980
	S2	1.027	**	1.073	1.032
1	S10	1.086	1.052	0.984	1.102
	S3	0.983	**	1.074	0.960
	S11	1.067	1.054	1.017	0.929
	S4	1.014	**	**	**
	S12	1.046	**	**	**
	S1	0.963	**	**	0.960
	S9	0.981	**	**	0.979
	S2	1.028	**	1.081	1.033
	S10	1.089	1.060	0.986	1.105
	S3	0.983	**	1.077	0.962
	S11	1.070	1.058	1.017	0.939
	S4	1.015	1.026	1.048	**
	S12	1.047	1.051	**	**

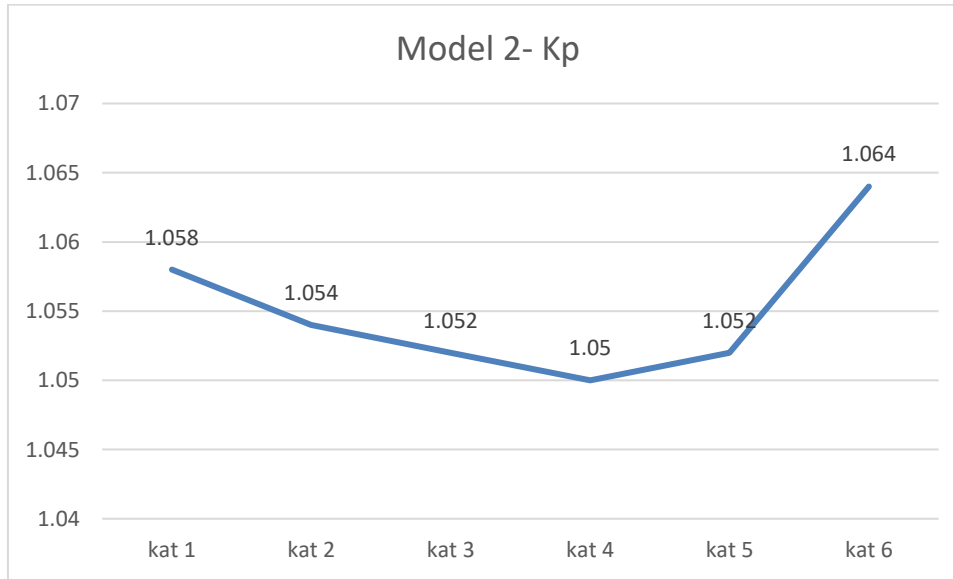
6 katlı binada dört Modelde de bulunan S11 kolonundaki k_p oranlarının katlara ve Modellere göre değişimleri Şekil 3.5 ila Şekil 3.8’de grafik olarak gösterilmiştir.

Model 1:



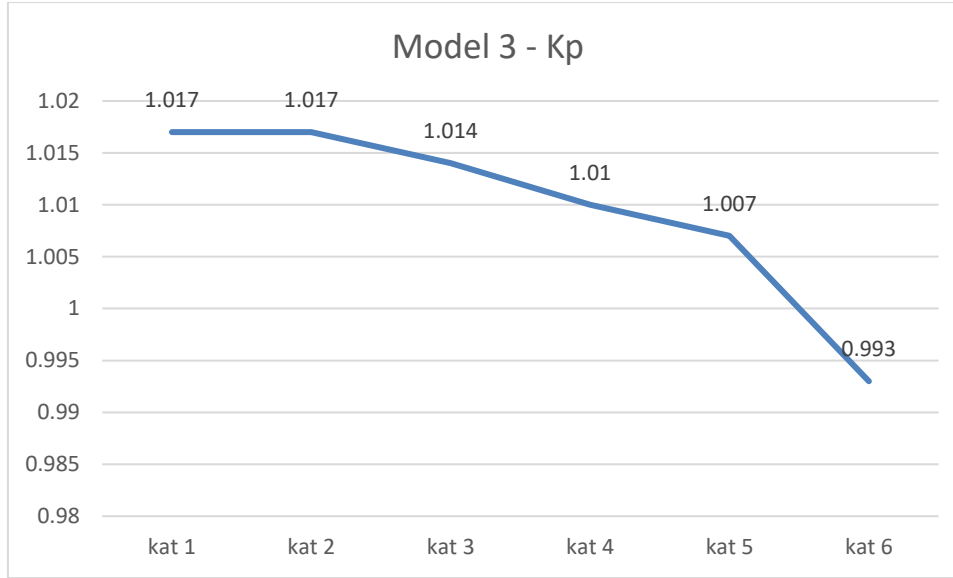
Şekil 3.5: S11 Kolonuna Ait k_p Oranının Değişim Grafiği.

Model 2:



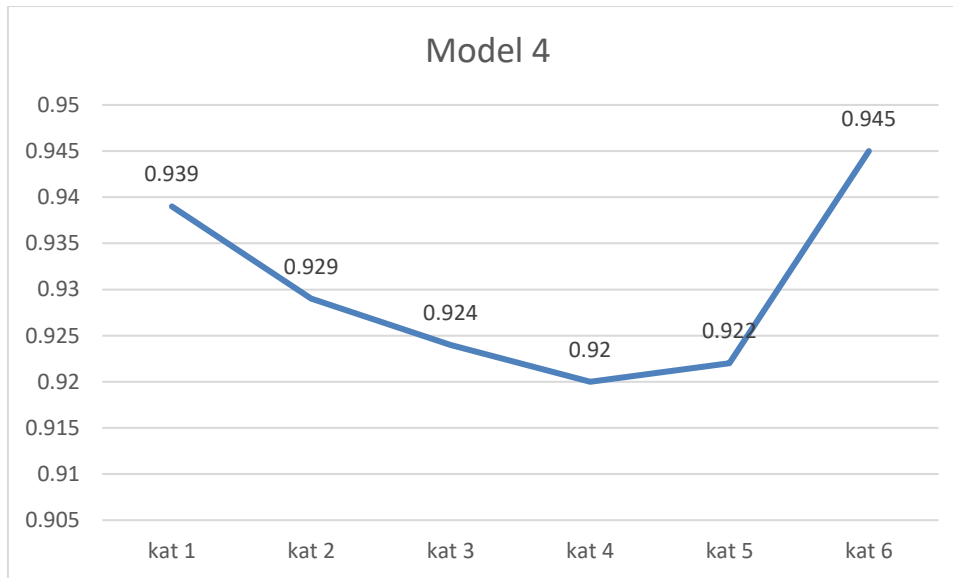
Şekil 3.6: S11 Kolonuna Ait k_p Oranının Değişim Grafiği.

Model 3:



Şekil 3.7: S11 Kolonuna Ait k_p Oranının Değişim Grafiği.

Model 4 :



Şekil 3.8: S11 Kolonuna Ait k_p Oranının Değişim Grafiği.

Çizelge 3.30: Tüm Modellerde 9 Katlı Hastane Binasına için k_p eksenel kuvvet oranları.

$k_p = N_G + Q/N_{G0} + Q_0$					
KAT	KOLON	Model 1	Model 2	Model 3	Model 4
9	S1	0.926	**	**	0.920
	S9	0.974	**	**	0.971
	S2	1.020	**	1.056	1.031
	S10	1.103	1.036	0.956	1.125
	S3	0.968	**	1.096	0.924
	S11	1.084	1.066	0.993	0.936
	S4	0.988	0.995	1.041	**
8	S12	1.040	1.053	**	**
	S1	0.965	**	**	0.960
	S9	0.982	**	**	0.980
	S2	1.021	**	1.032	1.028
	S10	1.083	1.015	0.957	1.100
	S3	0.977	**	1.082	0.929
	S11	1.072	1.052	1.007	0.909
7	S4	1.001	1.000	1.059	**
	S12	1.058	1.068	**	**
	S1	0.973	**	**	0.968
	S9	0.983	**	**	0.981
	S2	1.021	**	1.027	1.027
	S10	1.079	1.012	0.957	1.094
	S3	0.978	**	1.080	0.931
6	S11	1.070	1.050	1.010	0.905
	S4	1.004	**	**	**
	S12	1.061	**	**	**
	S1	0.976	**	**	0.971
	S9	0.983	**	**	0.982
	S2	1.024	**	1.030	1.029
	S10	1.079	1.015	0.956	1.093
5	S3	0.977	**	1.080	0.932
	S11	1.071	1.052	1.014	0.908
	S4	1.008	1.005	**	**
	S12	1.064	1.074	**	**
	S1	0.975	**	**	0.971
	S9	0.983	**	**	0.982
	S2	1.026	**	1.033	1.031
4	S10	1.079	1.020	0.957	1.091
	S3	0.976	**	1.080	0.933
	S11	1.072	1.054	1.017	0.912
	S4	1.011	1.009	**	**
	S12	1.065	1.075	**	**
	S1	0.973	**	**	0.969
	S9	0.983	**	**	0.982
3	S2	1.027	**	1.039	1.031
	S10	1.081	1.026	0.959	1.092
	S3	0.976	**	1.082	0.936
	S11	1.074	1.057	1.018	0.919
	S4	1.012	1.012	1.069	**
	S12	1.067	1.077	**	**
	S1	0.971	**	**	0.967
	S9	0.985	**	**	0.984

	S2	1.031	**	1.045	1.035
	S10	1.081	1.033	0.964	1.090
	S3	0.978	**	1.084	0.941
	S11	1.077	1.063	1.021	0.927
	S4	1.016	1.019	**	**
	S12	1.066	1.077	**	**
2	S1	0.967	**	**	0.964
	S9	0.989	**	**	0.988
	S2	1.035	**	1.053	1.038
	S10	1.082	1.041	0.971	1.090
	S3	0.981	**	1.085	0.947
	S11	1.077	1.067	1.025	0.932
	S4	1.020	**	**	**
	S12	1.067	**	**	**
1	S1	0.963	**	**	0.960
	S9	0.992	**	**	0.991
	S2	1.038	**	1.062	1.041
	S10	1.083	1.050	0.978	1.091
	S3	0.985	**	1.086	0.954
	S11	1.078	1.072	1.028	0.939
	S4	1.023	1.031	1.068	**
	S12	1.066	1.077	**	**

Çizelge 3.31: Tüm Modellerde 12 Katlı Hastane Binasına için k_p eksenel kuvvet oranları.

$k_p = N_G + Q/N_{G0} + Q_0$					
KAT	KOLON	Model 1	Model 2	Model 3	Model 4
12	S1	0.935	**	**	0.929
	S9	0.974	**	**	0.971
	S2	1.014	**	1.034	1.024
	S10	1.101	1.013	0.941	1.120
	S3	0.969	**	1.097	0.911
	S11	1.084	1.059	0.990	0.935
	S4	0.983	0.976	1.054	**
11	S12	1.053	1.057	**	**
	S1	0.976	**	**	0.969
	S9	0.982	**	**	0.980
	S2	1.014	**	1.006	1.019
	S10	1.080	0.988	0.942	1.093
	S3	0.977	**	1.083	0.914
	S11	1.074	1.045	1.003	0.907
10	S4	0.995	0.980	1.075	**
	S12	1.073	1.076	**	**
	S1	0.985	**	**	0.977
	S9	0.983	**	**	0.981
	S2	1.014	**	1.000	1.018
	S10	1.076	0.984	0.941	1.088
	S3	0.979	**	1.080	0.915
9	S11	1.071	1.043	1.006	0.903
	S4	0.998	0.981	1.079	**
	S12	1.076	1.079	**	**
	S1	0.988	**	**	0.980
	S9	0.983	**	**	0.981
	S2	1.016	**	1.002	1.019
	S10	1.076	0.987	0.941	1.086
9	S3	0.978	**	1.081	0.916
	S11	1.072	1.043	1.009	0.905
	S4	1.002	0.985	1.083	**
	S12	1.080	1.083	**	**
	S1	0.988	**	**	0.981
	S9	0.983	**	**	0.981
	S2	1.018	**	1.004	1.020
9	S10	1.076	0.990	0.941	1.083
	S3	0.977	**	1.081	0.916
	S11	1.073	1.045	1.012	0.908
	S4	1.004	0.989	1.085	**
	S12	1.082	1.085	**	**
	S1	0.986	**	**	0.979
	S9	0.982	**	**	0.981
7	S2	1.019	**	1.010	1.020
	S10	1.078	0.996	0.943	1.084
	S3	0.977	**	1.082	0.919
	S11	1.075	1.048	1.013	0.914
	S4	1.005	0.991	1.088	**
	S12	1.085	1.088	**	**
	S1	0.983	**	**	0.977
6	S9	0.985	**	**	0.984

	S2	1.023	**	1.015	1.023
	S10	1.078	1.002	0.948	1.082
	S3	0.979	**	1.085	0.924
	S11	1.077	1.053	1.016	0.921
	S4	1.009	0.997	1.088	**
	S12	1.085	1.088	**	**
5	S1	0.981	**	**	0.975
	S9	0.988	**	**	0.987
	S2	1.026	**	1.023	1.026
	S10	1.079	1.009	0.954	1.081
	S3	0.982	**	1.085	0.930
	S11	1.078	1.056	1.019	0.926
	S4	1.012	**	**	**
	S12	1.086	**	**	**
4	S1	0.977	**	**	0.972
	S9	0.991	**	**	0.990
	S2	1.029	**	1.030	1.029
	S10	1.079	1.016	0.961	1.081
	S3	0.986	**	1.085	0.937
	S11	1.079	1.060	1.022	0.931
	S4	1.016	**	**	**
	S12	1.086	**	**	**
3	S1	0.979	**	**	0.974
	S9	0.995	**	**	0.994
	S2	1.031	**	1.038	1.030
	S10	1.081	1.025	0.969	1.082
	S3	0.990	**	1.086	0.944
	S11	1.080	1.064	1.025	0.936
	S4	1.019	1.014	1.090	**
	S12	1.087	**	**	**
2	S1	0.982	**	**	0.977
	S9	0.999	**	**	0.998
	S2	1.034	**	1.046	1.033
	S10	1.081	1.033	0.976	1.082
	S3	0.995	**	1.086	0.952
	S11	1.080	1.068	1.029	0.940
	S4	1.024	**	**	**
	S12	1.086	**	**	**
1	S1	0.982	**	**	0.978
	S9	1.001	**	**	1.000
	S2	1.037	**	1.055	1.036
	S10	1.084	1.042	0.984	1.085
	S3	0.999	**	1.087	0.960
	S11	1.081	1.071	1.033	0.945
	S4	1.027	1.028	1.089	**
	S12	1.086	1.090	**	**

3.5.2. Deprem Yüklerinin Etkisinde Oluşan Eksenel Kuvvetler

Hastane binasının 6 katlı, 9 katlı ve 12 katlı versiyonlarında, yapıya etki eden deprem kuvvetleri ETABS programında ayrı ayrı X ve Y doğrultularında tanımlanmış ve bu kuvvetlerin etkisi altında kolonlardaki eksenel kuvvetler belirlenmiştir. TBDY 2018 standartlarına göre, taşıyıcı sistemin eşdeğer deprem yükü yöntemiyle hesaplanması durumunda, yatay doğrultulardaki deprem etkileri Denklem (3.3) ve Denklem (3.4)'da belirtildiği gibi birleştirilir. Her bir kolon için, deprem etkilerinden kaynaklanan eksenel kuvvetlerin en büyük değeri ($G_0 + Q_0$) eksenel yükünün oranı olarak k_E katsayısıyla elde edilmiştir. Bu katsayılar Ek B'de sunulmuştur.

$$E_d^{(H)} = \pm E_d^{(X)} \pm 0,3 E_d^{(Y)} \quad (3.3)$$

$$E_d^{(H)} = \pm 0,3 E_d^{(X)} \pm E_d^{(Y)} \quad (3.4)$$

Yapının deprem etkisinde taban kesme kuvveti, İzmir, İstanbul ve Ankara gibi önceki yönetmeliklere göre 1., 2. ve 3. derece deprem bölgelerindeki illerde, her bir il için ZA, ZB, ZC, ZD, ZE zemin sınıfı ve 4 Model için ayrı ayrı incelenmiştir. Yapı periyotları $1,4 \times T_{pA}$ olarak kabul edilerek deprem etkisinde taban kesme kuvveti TBDY 2018'e göre hesaplanmıştır. Elde edilen kesme kuvveti, X ve Y eksenlerinde ayrı ayrı düşünülerek, 6 katlı, 9 katlı ve 12 katlı yapının her bir katı ETABS programında tanımlanmıştır. Yapının sabit ve hareketli yükler altında analizi yapılarak kolonlarda oluşan eksenel basınç kuvvetleri tespit edilmiştir. Bulunan eksenel basınç kuvvetleri N_{Ex} , N_{Ey} ve bunların kombinasyonundan oluşan $N_{Ex} + 0,3N_{Ey}$ ve $N_{Ey} + 0,3N_{Ex}$ değerlerinin en büyüğü alınarak $N_{G0} + Q_0$, $N_{G0} + \beta_{Q0}$, $N_{G0} + \gamma_{Q0}$ basınç kuvvetlerine bölünmüş ve böylece k_E oranları elde edilmiştir. Çizelge 3.32 ve Çizelge 3.33'te Model 1 için İstanbul'daki 6 ve 9 katlı ZA zemindeki değerleri verilmiştir. Diğerler durumlara ait değerler EkB de verilmiştir.

Model 1

Çizelge 3.32: 6 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	7.335	6.185	9.191	8.385	128.2	122.95	112.45	0.072	0.075	0.082
	S9	9.669	1.802	10.209	4.702	206.21	195.96	175.46	0.050	0.052	0.058
	S2	1.038	8.326	3.535	8.637	244.38	232.83	209.73	0.035	0.037	0.041
	S10	2.835	3.101	3.766	3.952	355.51	332.96	287.86	0.011	0.012	0.014
	S3	0.122	8.354	2.629	8.391	263.11	250.51	225.31	0.032	0.033	0.037
	S11	0.121	4.218	1.386	4.254	385.098	360.498	311.298	0.011	0.012	0.014
	S4	0.863	8.397	3.382	8.656	245.66	233.722	209.846	0.035	0.037	0.041
	S12	2.372	3.314	3.366	4.026	303.493	284.318	245.968	0.013	0.014	0.016
5	S1	26.088	20.562	32.257	28.389	256.4	245.9	230.15	0.126	0.131	0.140
	S9	34.002	9.101	36.732	19.302	412.42	391.92	361.17	0.089	0.094	0.102
	S2	5.196	27.143	13.339	28.701	488.76	465.66	431.01	0.059	0.062	0.067
	S10	11.131	14.409	15.454	17.748	711.02	665.92	598.27	0.025	0.027	0.030
	S3	0.124	27.241	8.297	27.278	526.22	501.02	463.22	0.052	0.054	0.059
	S11	0.085	19.113	5.819	19.139	770.196	720.996	647.196	0.025	0.027	0.030
	S4	4.337	27.130	12.476	28.431	491.32	467.444	431.63	0.058	0.061	0.066
	S12	9.504	15.792	14.241	18.643	606.986	568.636	511.111	0.031	0.033	0.036
4	S1	54.564	41.768	67.094	58.138	384.6	368.85	353.1	0.174	0.182	0.190
	S9	71.345	20.188	77.401	41.591	618.63	587.88	557.13	0.125	0.132	0.139
	S2	12.641	54.723	29.057	58.515	733.14	698.49	663.84	0.080	0.084	0.088
	S10	25.654	31.314	35.048	39.011	1066.53	998.88	931.23	0.037	0.039	0.042
	S3	0.093	54.988	16.589	55.016	789.33	751.53	713.73	0.070	0.073	0.077
	S11	0.261	42.252	12.937	42.330	1155.294	1081.494	1007.694	0.037	0.039	0.042
	S4	9.618	54.598	25.998	57.484	736.98	701.166	665.352	0.078	0.082	0.086
	S12	20.687	34.577	31.060	40.783	910.479	852.954	795.429	0.045	0.048	0.051
3	S1	88.291	65.813	108.035	92.300	512.8	491.8	481.3	0.211	0.220	0.224
	S9	117.661	33.430	127.690	68.728	824.84	783.84	763.34	0.155	0.163	0.167
	S2	21.696	89.486	48.542	95.995	977.52	931.32	908.22	0.098	0.103	0.106
	S10	40.677	57.974	58.070	70.177	1422.04	1331.84	1286.74	0.049	0.053	0.055
	S3	0.195	88.204	26.656	88.262	1052.44	1002.04	976.84	0.084	0.088	0.090
	S11	0.349	77.929	23.727	78.034	1540.392	1441.992	1392.792	0.051	0.054	0.056
	S4	17.341	89.031	44.050	94.233	982.64	934.888	911.012	0.096	0.101	0.103
	S12	35.422	63.889	54.588	74.516	1213.972	1137.272	1098.922	0.061	0.066	0.068
2	S1	124.989	90.746	152.212	128.242	641	614.75	609.5	0.237	0.248	0.250
	S9	169.645	47.499	183.894	98.392	1031.05	979.8	969.55	0.178	0.188	0.190
	S2	31.995	128.661	70.593	138.259	1221.9	1164.15	1152.6	0.113	0.119	0.120
	S10	55.517	91.277	82.900	107.932	1777.55	1664.8	1642.25	0.061	0.065	0.066
	S3	0.192	124.255	37.469	124.312	1315.55	1252.55	1239.95	0.094	0.099	0.100
	S11	0.342	122.698	37.151	122.800	1925.49	1802.49	1777.89	0.064	0.068	0.069
	S4	27.376	127.990	65.773	136.202	1228.3	1168.61	1156.672	0.111	0.117	0.118
	S12	52.690	100.566	82.860	116.373	1517.465	1421.59	1402.415	0.077	0.082	0.083
1	S1	157.785	112.826	191.633	160.161	769.2	737.7	737.7	0.249	0.260	0.260
	S9	219.567	59.433	237.397	125.303	1237.26	1175.76	1175.76	0.192	0.202	0.202
	S2	39.791	165.407	89.413	177.344	1466.28	1396.98	1396.98	0.121	0.127	0.127
	S10	67.975	127.038	106.087	147.431	2133.06	1997.76	1997.76	0.069	0.074	0.074
	S3	0.331	158.270	47.812	158.369	1578.66	1503.06	1503.06	0.100	0.105	0.105

S11	0.252	169.185	51.008	169.260	2310.588	2162.988	2162.988	0.073	0.078	0.078
S4	34.068	164.439	83.400	174.659	1473.96	1402.332	1402.332	0.118	0.125	0.125
S12	69.814	139.744	111.738	160.688	1820.958	1705.908	1705.908	0.088	0.094	0.094

Çizelge 3.33: 9 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	7.374	7.495	9.623	9.707	128.2	117.7	104.575	0.076	0.082	0.093
	S9	9.893	1.268	10.273	4.235	206.21	185.71	160.085	0.050	0.055	0.064
	S2	0.924	10.813	4.168	11.090	244.38	221.28	192.405	0.045	0.050	0.058
	S10	0.722	1.297	1.111	1.513	355.51	310.41	254.035	0.004	0.005	0.006
	S3	0.450	10.644	3.643	10.779	263.11	237.91	206.41	0.041	0.045	0.052
	S11	0.470	2.276	1.153	2.417	385.098	335.898	274.398	0.006	0.007	0.009
	S4	0.240	10.792	3.478	10.865	245.66	221.784	191.939	0.044	0.049	0.057
	S12	1.613	1.269	1.994	1.753	303.493	265.143	217.2055	0.007	0.008	0.009
8	S1	27.414	24.488	34.761	32.712	256.4	235.4	211.775	0.136	0.148	0.164
	S9	36.096	8.748	38.720	19.576	412.42	371.42	325.295	0.094	0.104	0.119
	S2	1.033	33.939	11.214	34.249	488.76	442.56	390.585	0.070	0.077	0.088
	S10	6.876	11.711	10.390	13.774	711.02	620.82	519.345	0.019	0.022	0.027
	S3	0.685	33.619	10.770	33.824	526.22	475.82	419.12	0.064	0.071	0.081
	S11	0.669	16.394	5.587	16.594	770.196	671.796	561.096	0.022	0.025	0.030
	S4	3.389	33.675	13.491	34.692	491.32	443.568	389.847	0.071	0.078	0.089
	S12	8.540	12.700	12.350	15.262	606.986	530.286	443.9985	0.025	0.029	0.034
7	S1	58.678	49.362	73.486	66.965	384.6	353.1	318.975	0.191	0.208	0.230
	S9	77.299	20.639	83.491	43.829	618.63	557.13	490.505	0.135	0.150	0.170
	S2	6.811	67.163	26.960	69.206	733.14	663.84	588.765	0.094	0.104	0.118
	S10	20.259	28.562	28.827	34.639	1066.53	931.23	784.655	0.032	0.037	0.044
	S3	0.684	66.809	20.727	67.014	789.33	713.73	631.83	0.085	0.094	0.106
	S11	0.528	39.967	12.518	40.125	1155.294	1007.694	847.794	0.035	0.040	0.047
	S4	8.638	66.609	28.620	69.200	736.98	665.352	587.755	0.094	0.104	0.118
	S12	20.124	31.398	29.543	37.436	910.479	795.429	670.7915	0.041	0.047	0.056
6	S1	96.750	78.091	120.177	107.116	512.8	470.8	418.3	0.234	0.255	0.287
	S9	129.925	35.361	140.533	74.338	824.84	742.84	640.34	0.170	0.189	0.219
	S2	14.617	109.698	47.527	114.083	977.52	885.12	769.62	0.117	0.129	0.148
	S10	34.354	57.367	51.564	67.673	1422.04	1241.64	1016.14	0.048	0.055	0.067
	S3	0.816	107.186	32.972	107.431	1052.44	951.64	825.64	0.102	0.113	0.130
	S11	0.650	78.983	24.344	79.178	1540.392	1343.592	1097.592	0.051	0.059	0.072
	S4	16.916	108.564	49.486	113.639	982.64	887.136	767.756	0.116	0.128	0.148
	S12	36.125	62.981	55.019	73.818	1213.972	1060.572	868.822	0.061	0.070	0.085
5	S1	140.325	109.382	173.139	151.479	641	588.5	525.5	0.270	0.294	0.329
	S9	191.872	51.943	207.455	109.505	1031.05	928.55	805.55	0.201	0.223	0.258
	S2	24.496	159.798	72.436	167.147	1221.9	1106.4	967.8	0.137	0.151	0.173
	S10	48.994	95.361	77.602	110.059	1777.55	1552.05	1281.45	0.062	0.071	0.086
	S3	1.090	152.957	46.977	153.284	1315.55	1189.55	1038.35	0.117	0.129	0.148
	S11	0.836	130.809	40.078	131.059	1925.49	1679.49	1384.29	0.068	0.078	0.095
	S4	28.584	158.036	75.995	166.611	1228.3	1108.92	965.664	0.136	0.150	0.173
	S12	55.760	104.603	87.140	121.331	1517.465	1325.715	1095.615	0.080	0.092	0.111
4	S1	186.483	142.696	229.292	198.641	769.2	706.2	648.45	0.298	0.325	0.354
	S9	261.501	70.474	282.643	148.924	1237.26	1114.26	1001.51	0.228	0.254	0.282
	S2	33.043	214.881	97.508	224.794	1466.28	1327.68	1200.63	0.153	0.169	0.187
	S10	63.575	146.996	107.674	166.069	2133.06	1862.46	1614.41	0.078	0.089	0.103
	S3	1.142	203.974	62.334	204.317	1578.66	1427.46	1288.86	0.129	0.143	0.159
	S11	1.137	195.066	59.656	195.407	2310.588	2015.388	1744.788	0.085	0.097	0.112
	S4	37.574	212.364	101.283	223.636	1473.96	1330.704	1199.386	0.152	0.168	0.186

	S12	79.397	160.956	127.684	184.775	1820.958	1590.858	1379.933	0.101	0.116	0.134
3	S1	234.884	175.825	287.631	246.290	897.4	823.9	776.65	0.321	0.349	0.370
	S9	333.870	90.860	361.128	191.021	1443.47	1299.97	1207.72	0.250	0.278	0.299
	S2	39.780	273.747	121.904	285.681	1710.66	1548.96	1445.01	0.167	0.184	0.198
	S10	74.696	202.680	135.500	225.089	2488.57	2172.87	1969.92	0.090	0.104	0.114
	S3	1.598	261.398	80.017	261.878	1841.77	1665.37	1551.97	0.142	0.157	0.169
	S11	1.227	270.867	82.487	271.235	2695.686	2351.286	2129.886	0.101	0.115	0.127
	S4	50.332	270.040	131.344	285.139	1719.62	1552.488	1445.046	0.166	0.184	0.197
	S12	98.366	221.450	164.801	250.960	2124.451	1856.001	1683.426	0.118	0.135	0.149
2	S1	284.379	209.663	347.278	294.976	1025.6	941.6	904.85	0.339	0.369	0.384
	S9	409.486	120.666	445.686	243.512	1649.68	1485.68	1413.93	0.270	0.300	0.315
	S2	45.474	332.905	145.345	346.547	1955.04	1770.24	1689.39	0.177	0.196	0.205
	S10	88.454	260.589	166.631	287.125	2844.08	2483.28	2325.43	0.101	0.116	0.123
	S3	2.185	320.441	98.317	321.096	2104.88	1903.28	1815.08	0.153	0.169	0.177
	S11	1.143	346.655	105.139	346.998	3080.784	2687.184	2514.984	0.113	0.129	0.138
	S4	65.766	328.460	164.304	348.190	1965.28	1774.272	1690.706	0.177	0.196	0.206
	S12	117.484	284.481	202.828	319.726	2427.944	2121.144	1986.919	0.132	0.151	0.161
1	S1	326.683	238.066	398.102	336.071	1153.8	1059.3	1033.05	0.345	0.376	0.385
	S9	476.421	150.995	521.719	293.921	1855.89	1671.39	1620.14	0.281	0.312	0.322
	S2	48.635	383.210	163.598	397.801	2199.42	1991.52	1933.77	0.181	0.200	0.206
	S10	101.530	314.423	195.856	344.881	3199.59	2793.69	2680.94	0.108	0.123	0.129
	S3	2.828	370.887	114.094	371.736	2367.99	2141.19	2078.19	0.157	0.174	0.179
	S11	1.237	410.402	124.358	410.773	3465.882	3023.082	2900.082	0.119	0.136	0.142
	S4	79.139	377.971	192.531	401.713	2210.94	1996.056	1936.366	0.182	0.201	0.207
	S12	137.101	342.503	239.852	383.633	2731.437	2386.287	2290.412	0.140	0.161	0.167

Çizelge 3.34: 6 Katlı Hastane Binasının Ankara İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	KEZA				KEZB				KEZC				KEZD				KEZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
6	S1	0.033	**	**	0.033	0.033	**	**	0.033	0.062	**	**	0.063	0.097	**	**	0.098	0.165	**	**	0.161
	S9	0.023	**	**	0.027	0.023	**	**	0.027	0.043	**	**	0.050	0.067	**	**	0.079	0.114	**	**	0.129
	S2	0.016	**	**	0.008	0.016	**	**	0.008	0.030	**	**	0.016	0.048	**	**	0.025	0.081	**	**	0.038
	S10	0.005	0.005	0.006	0.011	0.005	0.005	0.006	0.011	0.010	0.010	0.011	0.021	0.015	0.016	0.018	0.032	0.026	0.026	0.027	0.053
	S3	0.015	**	0.017	0.013	0.015	**	0.017	0.013	0.028	**	0.033	0.024	0.043	**	0.051	0.037	0.073	**	0.079	0.056
	S11	0.005	0.006	0.005	0.057	0.005	0.006	0.005	0.057	0.010	0.011	0.009	0.106	0.015	0.017	0.013	0.166	0.025	0.027	0.020	0.274
	S4	0.016	0.019	0.008	**	0.016	0.019	0.008	**	0.030	0.036	0.016	**	0.048	0.057	0.023	**	0.081	0.092	0.036	**
	S12	0.006	0.004	0.004	**	0.006	0.004	0.004	**	0.011	0.008	0.008	**	0.018	0.013	0.012	**	0.030	0.021	0.019	**
5	S1	0.058	**	**	0.048	0.058	**	**	0.048	0.109	**	**	0.089	0.170	**	**	0.140	0.289	**	**	0.229
	S9	0.041	**	**	0.037	0.041	**	**	0.037	0.077	**	**	0.070	0.121	**	**	0.110	0.204	**	**	0.180
	S2	0.027	**	**	0.012	0.027	**	**	0.012	0.051	**	**	0.023	0.079	**	**	0.035	0.135	**	**	0.055
	S10	0.011	0.003	0.007	0.013	0.011	0.003	0.007	0.013	0.022	0.006	0.013	0.025	0.034	0.009	0.020	0.040	0.057	0.015	0.031	0.065
	S3	0.024	**	0.018	0.016	0.024	**	0.018	0.016	0.045	**	0.033	0.029	0.070	**	0.051	0.045	0.119	**	0.079	0.069
	S11	0.011	0.008	0.006	0.069	0.011	0.008	0.006	0.069	0.021	0.016	0.012	0.129	0.034	0.025	0.018	0.202	0.057	0.041	0.027	0.333
	S4	0.027	0.018	0.011	**	0.027	0.018	0.011	**	0.050	0.034	0.021	**	0.078	0.054	0.031	**	0.133	0.087	0.048	**
	S12	0.014	0.008	0.006	**	0.014	0.008	0.006	**	0.026	0.014	0.012	**	0.042	0.023	0.018	**	0.071	0.037	0.027	**

4	S1	0.080	**	**	0.053	0.080	**	**	0.053	0.150	**	**	0.100	0.236	**	**	0.156	0.401	**	**	0.256
	S9	0.058	**	**	0.041	0.058	**	**	0.041	0.108	**	**	0.078	0.169	**	**	0.122	0.287	**	**	0.200
	S2	0.037	**	**	0.014	0.037	**	**	0.014	0.069	**	**	0.026	0.108	**	**	0.040	0.183	**	**	0.061
	S10	0.017	0.003	0.007	0.015	0.017	0.003	0.007	0.015	0.032	0.005	0.013	0.028	0.050	0.008	0.021	0.043	0.084	0.013	0.032	0.071
	S3	0.032	**	0.018	0.017	0.032	**	0.018	0.017	0.060	**	0.033	0.031	0.094	**	0.051	0.048	0.160	**	0.079	0.073
	S11	0.017	0.009	0.007	0.074	0.017	0.009	0.007	0.074	0.032	0.018	0.013	0.139	0.050	0.028	0.019	0.218	0.084	0.045	0.029	0.359
	S4	0.036	0.019	0.012	**	0.036	0.019	0.012	**	0.067	0.035	0.023	**	0.106	0.055	0.034	**	0.179	0.090	0.052	**
	S12	0.021	0.009	0.007	**	0.021	0.009	0.007	**	0.039	0.016	0.014	**	0.061	0.026	0.020	**	0.103	0.042	0.031	**
3	S1	0.097	**	**	0.056	0.097	**	**	0.056	0.182	**	**	0.105	0.285	**	**	0.164	0.484	**	**	0.269
	S9	0.071	**	**	0.044	0.071	**	**	0.044	0.134	**	**	0.082	0.210	**	**	0.129	0.355	**	**	0.213
	S2	0.045	**	**	0.014	0.045	**	**	0.014	0.085	**	**	0.027	0.133	**	**	0.042	0.225	**	**	0.065
	S10	0.023	0.002	0.007	0.015	0.023	0.002	0.007	0.015	0.043	0.003	0.013	0.028	0.067	0.005	0.020	0.044	0.113	0.008	0.032	0.072
	S3	0.039	**	0.017	0.017	0.039	**	0.017	0.017	0.072	**	0.033	0.032	0.114	**	0.050	0.049	0.193	**	0.078	0.075
	S11	0.023	0.010	0.008	0.077	0.023	0.010	0.008	0.077	0.044	0.019	0.014	0.145	0.069	0.030	0.021	0.227	0.116	0.049	0.032	0.374
	S4	0.044	0.019	0.013	**	0.044	0.019	0.013	**	0.083	0.036	0.024	**	0.130	0.056	0.036	**	0.220	0.091	0.055	**
	S12	0.028	0.010	0.008	**	0.028	0.010	0.008	**	0.053	0.019	0.015	**	0.083	0.029	0.023	**	0.141	0.047	0.035	**
2	S1	0.109	**	**	0.056	0.109	**	**	0.056	0.205	**	**	0.105	0.321	**	**	0.165	0.545	**	**	0.270
	S9	0.082	**	**	0.045	0.082	**	**	0.045	0.154	**	**	0.084	0.241	**	**	0.131	0.409	**	**	0.216
	S2	0.052	**	**	0.015	0.052	**	**	0.015	0.098	**	**	0.028	0.153	**	**	0.043	0.260	**	**	0.066
	S10	0.028	0.001	0.007	0.015	0.028	0.001	0.007	0.015	0.052	0.001	0.012	0.027	0.082	0.002	0.019	0.043	0.139	0.003	0.030	0.070

1	S3	0.043	**	0.017	0.017	0.043	**	0.017	0.017	0.081	**	0.031	0.031	0.128	**	0.048	0.049	0.217	**	0.074	0.074
	S11	0.029	0.011	0.008	0.077	0.029	0.011	0.008	0.077	0.055	0.020	0.015	0.145	0.086	0.032	0.023	0.227	0.146	0.051	0.034	0.374
	S4	0.051	0.019	0.013	**	0.051	0.019	0.013	**	0.096	0.035	0.025	**	0.150	0.055	0.037	**	0.255	0.090	0.056	**
	S12	0.035	0.011	0.009	**	0.035	0.011	0.009	**	0.066	0.020	0.017	**	0.104	0.031	0.025	**	0.176	0.051	0.038	**
	S1	0.115	**	**	0.053	0.115	**	**	0.053	0.215	**	**	0.100	0.337	**	**	0.157	0.572	**	**	0.257
	S9	0.088	**	**	0.043	0.088	**	**	0.043	0.165	**	**	0.081	0.260	**	**	0.127	0.441	**	**	0.209
	S2	0.056	**	**	0.014	0.056	**	**	0.014	0.104	**	**	0.027	0.164	**	**	0.042	0.278	**	**	0.064
	S10	0.032	0.000	0.006	0.014	0.032	0.000	0.006	0.014	0.060	0.001	0.012	0.026	0.094	0.001	0.019	0.040	0.159	0.002	0.029	0.065
	S3	0.046	**	0.016	0.016	0.046	**	0.016	0.016	0.087	**	0.029	0.030	0.136	**	0.044	0.046	0.230	**	0.068	0.070
	S11	0.034	0.011	0.008	0.073	0.034	0.011	0.008	0.073	0.063	0.020	0.015	0.137	0.099	0.031	0.023	0.215	0.168	0.051	0.034	0.354
	S4	0.055	0.018	0.013	**	0.055	0.018	0.013	**	0.102	0.033	0.024	**	0.160	0.052	0.036	**	0.272	0.085	0.054	**
	S12	0.041	0.011	0.009	**	0.041	0.011	0.009	**	0.076	0.020	0.017	**	0.119	0.031	0.025	**	0.203	0.051	0.038	**

Çizelge 3.35: 6 Katlı Hastane Binasının İstanbul İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + q_0$																					
KAT	KOLON	keZA				keZB				keZC				keZD				keZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
6	S1	0.072	**	**	0.071	0.081	**	**	0.071	0.131	**	**	0.132	0.181	**	**	0.184	0.261	**	**	0.242
	S9	0.050	**	**	0.056	0.056	**	**	0.056	0.090	**	**	0.106	0.125	**	**	0.147	0.181	**	**	0.195
	S2	0.035	**	**	0.018	0.040	**	**	0.018	0.064	**	**	0.034	0.089	**	**	0.047	0.129	**	**	0.057
	S10	0.011	0.011	0.013	0.023	0.013	0.011	0.013	0.023	0.020	0.021	0.024	0.043	0.028	0.030	0.033	0.060	0.041	0.039	0.041	0.080
	S3	0.032	**	0.037	0.027	0.036	**	0.037	0.027	0.058	**	0.069	0.050	0.081	**	0.096	0.069	0.116	**	0.118	0.084
	S11	0.011	0.012	0.010	0.120	0.012	0.012	0.010	0.120	0.020	0.023	0.019	0.224	0.028	0.031	0.025	0.311	0.040	0.041	0.030	0.413
	S4	0.035	0.041	0.018	**	0.040	0.041	0.018	**	0.064	0.077	0.033	**	0.089	0.106	0.045	**	0.128	0.139	0.053	**
	S12	0.013	0.009	0.009	**	0.015	0.009	0.009	**	0.024	0.017	0.017	**	0.034	0.024	0.023	**	0.048	0.032	0.029	**
5	S1	0.126	**	**	0.101	0.142	**	**	0.101	0.229	**	**	0.189	0.318	**	**	0.262	0.459	**	**	0.345
	S9	0.089	**	**	0.079	0.100	**	**	0.079	0.162	**	**	0.148	0.225	**	**	0.205	0.325	**	**	0.272
	S2	0.059	**	**	0.026	0.066	**	**	0.026	0.107	**	**	0.048	0.148	**	**	0.067	0.214	**	**	0.082
	S10	0.025	0.007	0.014	0.028	0.028	0.007	0.014	0.028	0.046	0.013	0.027	0.053	0.063	0.018	0.038	0.074	0.091	0.023	0.047	0.097
	S3	0.052	**	0.037	0.033	0.058	**	0.037	0.033	0.095	**	0.070	0.062	0.131	**	0.097	0.085	0.189	**	0.119	0.103
	S11	0.025	0.018	0.014	0.145	0.028	0.018	0.014	0.145	0.045	0.034	0.025	0.273	0.063	0.047	0.034	0.378	0.091	0.061	0.040	0.502
	S4	0.058	0.039	0.024	**	0.065	0.039	0.024	**	0.105	0.072	0.045	**	0.146	0.100	0.060	**	0.211	0.131	0.072	**
	S12	0.031	0.016	0.013	**	0.035	0.016	0.013	**	0.056	0.030	0.025	**	0.078	0.042	0.034	**	0.112	0.055	0.040	**

4	S1	0.174	**	**	0.112	0.196	**	**	0.112	0.318	**	**	0.211	0.441	**	**	0.292	0.636	**	**	0.386
	S9	0.125	**	**	0.088	0.141	**	**	0.088	0.228	**	**	0.164	0.316	**	**	0.228	0.456	**	**	0.302
	S2	0.080	**	**	0.029	0.090	**	**	0.029	0.146	**	**	0.054	0.202	**	**	0.075	0.291	**	**	0.091
	S10	0.037	0.006	0.015	0.031	0.041	0.006	0.015	0.031	0.067	0.010	0.028	0.059	0.092	0.014	0.039	0.081	0.133	0.019	0.049	0.107
	S3	0.070	**	0.037	0.035	0.078	**	0.037	0.035	0.127	**	0.070	0.065	0.176	**	0.097	0.091	0.254	**	0.119	0.109
	S11	0.037	0.020	0.015	0.157	0.041	0.020	0.015	0.157	0.067	0.037	0.028	0.294	0.093	0.051	0.037	0.407	0.134	0.068	0.044	0.541
	S4	0.078	0.040	0.026	**	0.088	0.040	0.026	**	0.142	0.074	0.049	**	0.197	0.103	0.066	**	0.284	0.135	0.078	**
	S12	0.045	0.019	0.015	**	0.050	0.019	0.015	**	0.082	0.035	0.029	**	0.113	0.048	0.039	**	0.163	0.064	0.046	**
3	S1	0.211	**	**	0.118	0.237	**	**	0.118	0.384	**	**	0.221	0.533	**	**	0.307	0.768	**	**	0.405
	S9	0.155	**	**	0.093	0.174	**	**	0.093	0.282	**	**	0.174	0.391	**	**	0.242	0.564	**	**	0.321
	S2	0.098	**	**	0.031	0.110	**	**	0.031	0.179	**	**	0.057	0.248	**	**	0.080	0.358	**	**	0.097
	S10	0.049	0.003	0.015	0.032	0.056	0.003	0.015	0.032	0.090	0.006	0.027	0.059	0.125	0.009	0.038	0.082	0.180	0.012	0.047	0.108
	S3	0.084	**	0.037	0.036	0.094	**	0.037	0.036	0.153	**	0.069	0.067	0.212	**	0.095	0.093	0.306	**	0.117	0.112
	S11	0.051	0.022	0.016	0.163	0.057	0.022	0.016	0.163	0.092	0.040	0.030	0.306	0.128	0.056	0.041	0.424	0.185	0.074	0.048	0.564
	S4	0.096	0.040	0.027	**	0.108	0.040	0.027	**	0.175	0.075	0.051	**	0.242	0.104	0.069	**	0.350	0.137	0.082	**
	S12	0.061	0.021	0.017	**	0.069	0.021	0.017	**	0.112	0.039	0.032	**	0.155	0.054	0.044	**	0.224	0.071	0.052	**
2	S1	0.237	**	**	0.119	0.267	**	**	0.119	0.433	**	**	0.222	0.600	**	**	0.308	0.866	**	**	0.407
	S9	0.178	**	**	0.094	0.201	**	**	0.094	0.325	**	**	0.177	0.451	**	**	0.246	0.650	**	**	0.326
	S2	0.113	**	**	0.031	0.127	**	**	0.031	0.206	**	**	0.059	0.286	**	**	0.081	0.413	**	**	0.099
	S10	0.061	0.001	0.014	0.031	0.068	0.001	0.014	0.031	0.111	0.002	0.026	0.058	0.153	0.003	0.036	0.080	0.221	0.004	0.045	0.105

	S3	0.094	**	0.035	0.035	0.106	**	0.035	0.035	0.172	**	0.066	0.066	0.239	**	0.090	0.092	0.345	**	0.111	0.111
	S11	0.064	0.023	0.017	0.163	0.072	0.023	0.017	0.163	0.116	0.042	0.032	0.306	0.161	0.059	0.044	0.424	0.233	0.077	0.051	0.564
	S4	0.111	0.040	0.028	**	0.125	0.040	0.028	**	0.202	0.074	0.052	**	0.280	0.103	0.071	**	0.404	0.135	0.084	**
	S12	0.077	0.022	0.019	**	0.086	0.022	0.019	**	0.140	0.042	0.035	**	0.194	0.058	0.047	**	0.280	0.077	0.056	**
1	S1	0.249	**	**	0.113	0.280	**	**	0.113	0.454	**	**	0.212	0.630	**	**	0.294	0.908	**	**	0.388
	S9	0.192	**	**	0.091	0.216	**	**	0.091	0.350	**	**	0.171	0.485	**	**	0.237	0.700	**	**	0.314
	S2	0.121	**	**	0.031	0.136	**	**	0.031	0.221	**	**	0.057	0.306	**	**	0.079	0.441	**	**	0.097
	S10	0.069	0.001	0.013	0.029	0.078	0.001	0.013	0.029	0.126	0.001	0.025	0.054	0.175	0.002	0.035	0.075	0.252	0.003	0.043	0.098
	S3	0.100	**	0.033	0.034	0.113	**	0.033	0.034	0.183	**	0.062	0.063	0.254	**	0.084	0.088	0.366	**	0.102	0.106
	S11	0.073	0.022	0.017	0.154	0.082	0.022	0.017	0.154	0.134	0.042	0.032	0.289	0.185	0.058	0.044	0.401	0.267	0.077	0.051	0.534
	S4	0.118	0.038	0.027	**	0.133	0.038	0.027	**	0.216	0.070	0.051	**	0.300	0.098	0.068	**	0.432	0.128	0.081	**
	S12	0.088	0.023	0.019	**	0.099	0.023	0.019	**	0.161	0.042	0.036	**	0.223	0.059	0.048	**	0.322	0.077	0.057	**

Çizelge 3.36: 6 Katlı Hastane Binasının İzmir İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	KEZA				KEZB				KEZC				KEZD				KEZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
6	S1	0.082	**	**	0.070	0.092	**	**	0.070	0.130	**	**	0.131	0.180	**	**	0.183	0.260	**	**	0.247
	S9	0.056	**	**	0.056	0.063	**	**	0.056	0.090	**	**	0.105	0.124	**	**	0.146	0.180	**	**	0.199
	S2	0.040	**	**	0.018	0.045	**	**	0.018	0.064	**	**	0.033	0.089	**	**	0.046	0.128	**	**	0.058
	S10	0.013	0.011	0.013	0.023	0.014	0.011	0.013	0.023	0.020	0.021	0.024	0.043	0.028	0.030	0.033	0.060	0.040	0.040	0.042	0.081
	S3	0.036	**	0.037	0.026	0.041	**	0.037	0.026	0.058	**	0.069	0.050	0.080	**	0.096	0.069	0.116	**	0.120	0.085
	S11	0.013	0.012	0.010	0.119	0.014	0.012	0.010	0.119	0.020	0.022	0.018	0.223	0.028	0.031	0.026	0.309	0.040	0.042	0.030	0.420
	S4	0.040	0.041	0.018	**	0.045	0.041	0.018	**	0.064	0.076	0.033	**	0.089	0.106	0.046	**	0.128	0.142	0.055	**
	S12	0.015	0.009	0.009	**	0.017	0.009	0.009	**	0.024	0.017	0.017	**	0.033	0.024	0.023	**	0.048	0.032	0.029	**
5	S1	0.143	**	**	0.100	0.161	**	**	0.100	0.228	**	**	0.187	0.316	**	**	0.260	0.457	**	**	0.352
	S9	0.101	**	**	0.078	0.114	**	**	0.078	0.161	**	**	0.146	0.224	**	**	0.203	0.323	**	**	0.277
	S2	0.067	**	**	0.026	0.075	**	**	0.026	0.106	**	**	0.048	0.148	**	**	0.067	0.213	**	**	0.084
	S10	0.028	0.007	0.014	0.028	0.032	0.007	0.014	0.028	0.045	0.013	0.027	0.053	0.063	0.018	0.037	0.074	0.091	0.024	0.048	0.099
	S3	0.059	**	0.037	0.033	0.066	**	0.037	0.033	0.094	**	0.070	0.061	0.130	**	0.097	0.085	0.188	**	0.122	0.105
	S11	0.028	0.018	0.013	0.144	0.032	0.018	0.013	0.144	0.045	0.033	0.025	0.270	0.062	0.046	0.035	0.376	0.090	0.062	0.041	0.511
	S4	0.066	0.038	0.024	**	0.074	0.038	0.024	**	0.105	0.072	0.044	**	0.145	0.100	0.062	**	0.210	0.134	0.073	**

	S12	0.035	0.016	0.013	**	0.039	0.016	0.013	**	0.056	0.030	0.025	**	0.077	0.042	0.035	**	0.111	0.056	0.041	**
4	S1	0.198	**	**	0.112	0.223	**	**	0.112	0.316	**	**	0.209	0.438	**	**	0.291	0.633	**	**	0.393
	S9	0.142	**	**	0.087	0.160	**	**	0.087	0.226	**	**	0.163	0.314	**	**	0.226	0.454	**	**	0.308
	S2	0.091	**	**	0.029	0.102	**	**	0.029	0.144	**	**	0.054	0.201	**	**	0.074	0.290	**	**	0.093
	S10	0.042	0.006	0.015	0.031	0.047	0.006	0.015	0.031	0.066	0.010	0.028	0.058	0.092	0.014	0.039	0.081	0.133	0.019	0.050	0.109
	S3	0.079	**	0.037	0.035	0.089	**	0.037	0.035	0.126	**	0.070	0.065	0.175	**	0.097	0.090	0.253	**	0.121	0.112
	S11	0.042	0.020	0.015	0.155	0.047	0.020	0.015	0.155	0.066	0.037	0.028	0.291	0.092	0.051	0.038	0.405	0.133	0.069	0.045	0.551
	S4	0.089	0.039	0.026	**	0.100	0.039	0.026	**	0.141	0.074	0.048	**	0.196	0.102	0.067	**	0.283	0.137	0.080	**
	S12	0.051	0.018	0.015	**	0.057	0.018	0.015	**	0.081	0.035	0.028	**	0.113	0.048	0.040	**	0.163	0.065	0.047	**
3	S1	0.240	**	**	0.117	0.270	**	**	0.117	0.381	**	**	0.220	0.530	**	**	0.305	0.765	**	**	0.413
	S9	0.176	**	**	0.092	0.198	**	**	0.092	0.280	**	**	0.173	0.389	**	**	0.240	0.562	**	**	0.327
	S2	0.112	**	**	0.030	0.126	**	**	0.030	0.178	**	**	0.057	0.247	**	**	0.079	0.356	**	**	0.099
	S10	0.056	0.003	0.015	0.031	0.063	0.003	0.015	0.031	0.089	0.006	0.027	0.059	0.124	0.009	0.038	0.082	0.179	0.012	0.048	0.110
	S3	0.095	**	0.036	0.035	0.107	**	0.036	0.035	0.152	**	0.068	0.067	0.211	**	0.095	0.092	0.304	**	0.119	0.114
	S11	0.058	0.021	0.016	0.162	0.065	0.021	0.016	0.162	0.092	0.040	0.030	0.304	0.127	0.056	0.042	0.422	0.184	0.075	0.049	0.574
	S4	0.109	0.040	0.027	**	0.123	0.040	0.027	**	0.173	0.075	0.051	**	0.241	0.104	0.071	**	0.348	0.140	0.084	**
	S12	0.070	0.021	0.017	**	0.079	0.021	0.017	**	0.111	0.039	0.032	**	0.154	0.054	0.045	**	0.223	0.073	0.053	**
2	S1	0.270	**	**	0.118	0.304	**	**	0.118	0.430	**	**	0.221	0.597	**	**	0.306	0.862	**	**	0.414
	S9	0.203	**	**	0.094	0.228	**	**	0.094	0.323	**	**	0.176	0.448	**	**	0.244	0.647	**	**	0.332
	S2	0.129	**	**	0.031	0.145	**	**	0.031	0.205	**	**	0.058	0.284	**	**	0.081	0.411	**	**	0.101

	S10	0.069	0.001	0.014	0.031	0.078	0.001	0.014	0.031	0.110	0.002	0.026	0.057	0.153	0.003	0.036	0.080	0.220	0.004	0.046	0.107
	S3	0.107	**	0.035	0.035	0.121	**	0.035	0.035	0.171	**	0.065	0.066	0.238	**	0.091	0.092	0.343	**	0.113	0.113
	S11	0.073	0.022	0.017	0.162	0.082	0.022	0.017	0.162	0.115	0.042	0.032	0.303	0.160	0.059	0.045	0.422	0.232	0.079	0.052	0.574
	S4	0.126	0.039	0.028	**	0.142	0.039	0.028	**	0.201	0.074	0.052	**	0.279	0.102	0.072	**	0.403	0.138	0.085	**
	S12	0.087	0.022	0.019	**	0.098	0.022	0.019	**	0.139	0.042	0.035	**	0.193	0.058	0.048	**	0.278	0.078	0.057	**
1	S1	0.283	**	**	0.112	0.319	**	**	0.112	0.451	**	**	0.210	0.626	**	**	0.292	0.904	**	**	0.395
	S9	0.218	**	**	0.090	0.245	**	**	0.090	0.347	**	**	0.170	0.482	**	**	0.236	0.697	**	**	0.320
	S2	0.138	**	**	0.030	0.155	**	**	0.030	0.219	**	**	0.057	0.304	**	**	0.079	0.439	**	**	0.099
	S10	0.079	0.001	0.013	0.029	0.088	0.001	0.013	0.029	0.125	0.001	0.025	0.054	0.174	0.002	0.034	0.075	0.251	0.003	0.044	0.100
	S3	0.114	**	0.033	0.034	0.128	**	0.033	0.034	0.181	**	0.062	0.063	0.252	**	0.086	0.087	0.364	**	0.104	0.108
	S11	0.083	0.022	0.017	0.153	0.094	0.022	0.017	0.153	0.133	0.042	0.032	0.287	0.184	0.058	0.045	0.399	0.266	0.078	0.052	0.544
	S4	0.135	0.037	0.027	**	0.152	0.037	0.027	**	0.214	0.070	0.050	**	0.298	0.097	0.070	**	0.430	0.131	0.083	**
	S12	0.100	0.022	0.019	**	0.113	0.022	0.019	**	0.160	0.042	0.035	**	0.222	0.058	0.049	**	0.320	0.079	0.059	**

Çizelge 3.37: 9 Katlı Hastane Binasının Ankara İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	keZA				keZB				keZC				keZD				keZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
9	S1	0.028	**	**	0.042	0.032	**	**	0.042	0.048	**	**	0.078	0.076	**	**	0.122	0.128	**	**	0.207
	S9	0.019	**	**	0.031	0.021	**	**	0.031	0.032	**	**	0.059	0.050	**	**	0.093	0.084	**	**	0.157
	S2	0.017	**	**	0.011	0.019	**	**	0.011	0.029	**	**	0.020	0.045	**	**	0.032	0.077	**	**	0.054
	S10	0.002	0.009	0.008	0.008	0.002	0.009	0.008	0.008	0.003	0.016	0.016	0.015	0.004	0.026	0.024	0.024	0.007	0.043	0.041	0.040
	S3	0.015	**	0.025	0.021	0.017	**	0.025	0.021	0.026	**	0.048	0.039	0.041	**	0.075	0.062	0.069	**	0.127	0.105
	S11	0.002	0.008	0.005	0.062	0.003	0.008	0.005	0.062	0.004	0.015	0.010	0.116	0.006	0.023	0.016	0.183	0.011	0.039	0.027	0.310
	S4	0.017	0.029	0.010	**	0.019	0.029	0.010	**	0.028	0.054	0.020	**	0.044	0.085	0.031	**	0.075	0.145	0.052	**
	S12	0.002	0.005	0.005	**	0.003	0.005	0.005	**	0.004	0.010	0.010	**	0.007	0.015	0.016	**	0.011	0.025	0.027	**
8	S1	0.051	**	**	0.060	0.057	**	**	0.060	0.086	**	**	0.112	0.135	**	**	0.176	0.230	**	**	0.299
	S9	0.035	**	**	0.045	0.040	**	**	0.045	0.060	**	**	0.085	0.094	**	**	0.133	0.159	**	**	0.225
	S2	0.026	**	**	0.016	0.030	**	**	0.016	0.045	**	**	0.030	0.070	**	**	0.047	0.119	**	**	0.080
	S10	0.007	0.005	0.010	0.011	0.008	0.005	0.010	0.011	0.012	0.010	0.018	0.021	0.019	0.015	0.028	0.032	0.033	0.026	0.048	0.055
	S3	0.024	**	0.026	0.025	0.027	**	0.026	0.025	0.041	**	0.050	0.047	0.064	**	0.078	0.074	0.109	**	0.132	0.126
	S11	0.008	0.012	0.007	0.078	0.009	0.012	0.007	0.078	0.014	0.022	0.014	0.145	0.022	0.034	0.022	0.228	0.036	0.058	0.037	0.387
	S4	0.027	0.028	0.014	**	0.030	0.028	0.014	**	0.045	0.052	0.026	**	0.071	0.082	0.041	**	0.120	0.140	0.070	**

	S12	0.009	0.010	0.008	**	0.011	0.010	0.008	**	0.016	0.019	0.015	**	0.025	0.030	0.023	**	0.043	0.051	0.039	**
7	S1	0.072	**	**	0.068	0.081	**	**	0.068	0.122	**	**	0.127	0.191	**	**	0.199	0.324	**	**	0.338
	S9	0.051	**	**	0.051	0.057	**	**	0.051	0.086	**	**	0.096	0.135	**	**	0.150	0.229	**	**	0.255
	S2	0.036	**	**	0.018	0.040	**	**	0.018	0.060	**	**	0.034	0.094	**	**	0.053	0.160	**	**	0.090
	S10	0.012	0.004	0.010	0.013	0.014	0.004	0.010	0.013	0.021	0.008	0.019	0.024	0.032	0.013	0.030	0.038	0.055	0.021	0.051	0.064
	S3	0.032	**	0.027	0.027	0.036	**	0.027	0.027	0.054	**	0.051	0.050	0.085	**	0.079	0.079	0.144	**	0.135	0.134
	S11	0.013	0.013	0.008	0.086	0.015	0.013	0.008	0.086	0.022	0.025	0.015	0.161	0.035	0.039	0.024	0.252	0.059	0.066	0.041	0.428
	S4	0.035	0.030	0.015	**	0.040	0.030	0.015	**	0.060	0.056	0.029	**	0.094	0.088	0.045	**	0.159	0.148	0.076	**
	S12	0.015	0.012	0.009	**	0.017	0.012	0.009	**	0.026	0.023	0.016	**	0.041	0.036	0.026	**	0.070	0.060	0.043	**
6	S1	0.088	**	**	0.073	0.099	**	**	0.073	0.149	**	**	0.137	0.234	**	**	0.214	0.397	**	**	0.364
	S9	0.064	**	**	0.056	0.072	**	**	0.056	0.108	**	**	0.105	0.170	**	**	0.165	0.289	**	**	0.279
	S2	0.044	**	**	0.020	0.049	**	**	0.020	0.074	**	**	0.037	0.117	**	**	0.058	0.198	**	**	0.098
	S10	0.018	0.003	0.010	0.014	0.020	0.003	0.010	0.014	0.030	0.005	0.019	0.026	0.048	0.008	0.029	0.040	0.081	0.014	0.050	0.069
	S3	0.038	**	0.027	0.028	0.043	**	0.027	0.028	0.065	**	0.051	0.052	0.102	**	0.080	0.082	0.173	**	0.135	0.139
	S11	0.019	0.015	0.009	0.093	0.022	0.015	0.009	0.093	0.033	0.028	0.017	0.174	0.051	0.045	0.027	0.274	0.087	0.076	0.046	0.464
	S4	0.044	0.031	0.016	**	0.049	0.031	0.016	**	0.074	0.058	0.031	**	0.115	0.092	0.048	**	0.196	0.155	0.082	**
	S12	0.023	0.014	0.010	**	0.026	0.014	0.010	**	0.039	0.027	0.018	**	0.061	0.042	0.028	**	0.103	0.072	0.048	**
5	S1	0.102	**	**	0.077	0.114	**	**	0.077	0.172	**	**	0.144	0.270	**	**	0.225	0.458	**	**	0.383
	S9	0.076	**	**	0.060	0.085	**	**	0.060	0.128	**	**	0.112	0.201	**	**	0.176	0.341	**	**	0.299
	S2	0.051	**	**	0.021	0.058	**	**	0.021	0.087	**	**	0.039	0.137	**	**	0.062	0.232	**	**	0.105

	S10	0.023	0.001	0.010	0.014	0.026	0.001	0.010	0.014	0.039	0.003	0.019	0.027	0.062	0.004	0.029	0.042	0.105	0.007	0.050	0.071
	S3	0.044	**	0.027	0.028	0.049	**	0.027	0.028	0.074	**	0.051	0.053	0.116	**	0.080	0.084	0.197	**	0.135	0.142
	S11	0.026	0.017	0.010	0.099	0.029	0.017	0.010	0.099	0.043	0.032	0.019	0.186	0.068	0.050	0.030	0.291	0.115	0.085	0.051	0.494
	S4	0.051	0.032	0.017	**	0.057	0.032	0.017	**	0.086	0.060	0.033	**	0.135	0.095	0.051	**	0.230	0.161	0.087	**
	S12	0.030	0.016	0.011	**	0.034	0.016	0.011	**	0.051	0.031	0.020	**	0.080	0.048	0.032	**	0.135	0.082	0.054	**
4	S1	0.112	**	**	0.079	0.126	**	**	0.079	0.190	**	**	0.147	0.298	**	**	0.231	0.505	**	**	0.392
	S9	0.086	**	**	0.063	0.097	**	**	0.063	0.145	**	**	0.118	0.228	**	**	0.185	0.387	**	**	0.314
	S2	0.058	**	**	0.022	0.065	**	**	0.022	0.098	**	**	0.041	0.153	**	**	0.064	0.260	**	**	0.109
	S10	0.029	0.002	0.010	0.014	0.033	0.002	0.010	0.014	0.050	0.003	0.019	0.027	0.078	0.005	0.029	0.043	0.132	0.009	0.050	0.072
	S3	0.049	**	0.027	0.029	0.055	**	0.027	0.029	0.082	**	0.050	0.054	0.129	**	0.079	0.084	0.219	**	0.133	0.143
	S11	0.032	0.018	0.011	0.103	0.036	0.018	0.011	0.103	0.054	0.035	0.021	0.194	0.084	0.054	0.032	0.304	0.143	0.092	0.055	0.516
	S4	0.057	0.033	0.018	**	0.064	0.033	0.018	**	0.097	0.061	0.033	**	0.152	0.096	0.052	**	0.257	0.164	0.089	**
	S12	0.038	0.018	0.012	**	0.043	0.018	0.012	**	0.065	0.034	0.023	**	0.101	0.054	0.035	**	0.172	0.092	0.060	**
3	S1	0.121	**	**	0.080	0.136	**	**	0.080	0.204	**	**	0.149	0.320	**	**	0.234	0.543	**	**	0.398
	S9	0.094	**	**	0.065	0.106	**	**	0.065	0.159	**	**	0.122	0.250	**	**	0.191	0.424	**	**	0.324
	S2	0.063	**	**	0.022	0.071	**	**	0.022	0.106	**	**	0.041	0.167	**	**	0.065	0.283	**	**	0.110
	S10	0.034	0.003	0.010	0.014	0.038	0.003	0.010	0.014	0.058	0.005	0.018	0.027	0.090	0.009	0.028	0.042	0.153	0.015	0.048	0.071
	S3	0.053	**	0.026	0.029	0.060	**	0.026	0.029	0.090	**	0.049	0.054	0.142	**	0.076	0.085	0.241	**	0.129	0.144
	S11	0.038	0.020	0.012	0.107	0.043	0.020	0.012	0.107	0.064	0.037	0.022	0.200	0.100	0.058	0.034	0.314	0.170	0.099	0.058	0.533
	S4	0.062	0.033	0.018	**	0.070	0.033	0.018	**	0.106	0.061	0.034	**	0.166	0.096	0.053	**	0.281	0.163	0.090	**

	S12	0.044	0.020	0.013	**	0.050	0.020	0.013	**	0.075	0.037	0.024	**	0.118	0.058	0.038	**	0.200	0.098	0.064	**
2	S1	0.127	**	**	0.079	0.143	**	**	0.079	0.215	**	**	0.149	0.338	**	**	0.233	0.574	**	**	0.396
	S9	0.102	**	**	0.066	0.114	**	**	0.066	0.172	**	**	0.123	0.270	**	**	0.193	0.458	**	**	0.327
	S2	0.067	**	**	0.022	0.075	**	**	0.022	0.113	**	**	0.041	0.177	**	**	0.064	0.300	**	**	0.109
	S10	0.038	0.004	0.009	0.014	0.043	0.004	0.009	0.014	0.064	0.008	0.017	0.027	0.101	0.012	0.027	0.042	0.171	0.020	0.046	0.071
	S3	0.057	**	0.025	0.028	0.065	**	0.025	0.028	0.097	**	0.046	0.053	0.152	**	0.072	0.083	0.258	**	0.123	0.142
	S11	0.042	0.020	0.012	0.107	0.048	0.020	0.012	0.107	0.072	0.038	0.022	0.200	0.112	0.060	0.035	0.314	0.191	0.101	0.059	0.534
	S4	0.067	0.032	0.018	**	0.075	0.032	0.018	**	0.113	0.060	0.034	**	0.177	0.093	0.053	**	0.300	0.158	0.089	**
	S12	0.050	0.020	0.013	**	0.056	0.020	0.013	**	0.084	0.037	0.024	**	0.131	0.059	0.038	**	0.223	0.099	0.065	**
1	S1	0.130	**	**	0.076	0.146	**	**	0.076	0.220	**	**	0.143	0.345	**	**	0.225	0.584	**	**	0.382
	S9	0.106	**	**	0.064	0.119	**	**	0.064	0.179	**	**	0.120	0.281	**	**	0.189	0.476	**	**	0.320
	S2	0.068	**	**	0.021	0.077	**	**	0.021	0.115	**	**	0.040	0.181	**	**	0.062	0.306	**	**	0.106
	S10	0.041	0.005	0.009	0.014	0.046	0.005	0.009	0.014	0.069	0.009	0.016	0.026	0.108	0.014	0.025	0.042	0.183	0.023	0.043	0.071
	S3	0.059	**	0.023	0.027	0.066	**	0.023	0.027	0.100	**	0.043	0.051	0.157	**	0.068	0.080	0.266	**	0.115	0.136
	S11	0.045	0.020	0.011	0.102	0.050	0.020	0.011	0.102	0.075	0.037	0.022	0.192	0.118	0.059	0.034	0.302	0.201	0.099	0.057	0.512
	S4	0.068	0.030	0.017	**	0.077	0.030	0.017	**	0.116	0.057	0.032	**	0.181	0.089	0.051	**	0.308	0.151	0.086	**
	S12	0.053	0.020	0.013	**	0.059	0.020	0.013	**	0.089	0.037	0.024	**	0.140	0.058	0.038	**	0.238	0.098	0.064	**

Çizelge 3.38: 9 Katlı Hastane Binasının İzmir İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	keZA				keZB				keZC				keZD				keZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
9	S1	0.086	**	**	0.087	0.097	**	**	0.096	0.129	**	**	0.163	0.140	**	**	0.227	0.203	**	**	0.328
	S9	0.057	**	**	0.066	0.064	**	**	0.073	0.085	**	**	0.124	0.092	**	**	0.172	0.133	**	**	0.248
	S2	0.052	**	**	0.023	0.058	**	**	0.025	0.077	**	**	0.043	0.084	**	**	0.060	0.122	**	**	0.086
	S10	0.005	0.018	0.017	0.017	0.005	0.020	0.019	0.019	0.007	0.034	0.033	0.032	0.008	0.048	0.045	0.044	0.011	0.069	0.065	0.064
	S3	0.047	**	0.053	0.044	0.052	**	0.059	0.049	0.070	**	0.100	0.083	0.076	**	0.139	0.115	0.110	**	0.200	0.166
	S11	0.007	0.017	0.011	0.130	0.008	0.018	0.012	0.143	0.011	0.031	0.021	0.244	0.012	0.043	0.029	0.339	0.017	0.062	0.042	0.490
	S4	0.050	0.061	0.022	**	0.057	0.067	0.024	**	0.075	0.114	0.041	**	0.082	0.158	0.057	**	0.118	0.229	0.083	**
	S12	0.007	0.011	0.011	**	0.008	0.012	0.013	**	0.011	0.020	0.022	**	0.012	0.028	0.030	**	0.018	0.040	0.043	**
8	S1	0.154	**	**	0.126	0.173	**	**	0.138	0.231	**	**	0.236	0.251	**	**	0.327	0.363	**	**	0.473
	S9	0.107	**	**	0.095	0.120	**	**	0.104	0.160	**	**	0.178	0.174	**	**	0.247	0.251	**	**	0.356
	S2	0.080	**	**	0.034	0.090	**	**	0.037	0.120	**	**	0.063	0.130	**	**	0.088	0.188	**	**	0.127
	S10	0.022	0.011	0.020	0.023	0.025	0.012	0.022	0.025	0.033	0.020	0.038	0.043	0.036	0.028	0.052	0.060	0.052	0.041	0.075	0.087
	S3	0.073	**	0.055	0.053	0.082	**	0.061	0.058	0.110	**	0.104	0.099	0.119	**	0.144	0.138	0.172	**	0.209	0.199
	S11	0.025	0.024	0.016	0.163	0.028	0.027	0.017	0.179	0.037	0.046	0.029	0.305	0.040	0.063	0.041	0.424	0.058	0.092	0.059	0.612
	S4	0.080	0.059	0.029	**	0.090	0.065	0.032	**	0.120	0.110	0.055	**	0.131	0.153	0.077	**	0.189	0.221	0.111	**
	S12	0.029	0.021	0.016	**	0.032	0.024	0.018	**	0.043	0.040	0.031	**	0.047	0.056	0.043	**	0.067	0.081	0.062	**

7	S1	0.217	**	**	0.142	0.244	**	**	0.156	0.326	**	**	0.266	0.354	**	**	0.370	0.512	**	**	0.534
	S9	0.153	**	**	0.107	0.173	**	**	0.118	0.230	**	**	0.201	0.250	**	**	0.279	0.361	**	**	0.403
	S2	0.107	**	**	0.038	0.121	**	**	0.042	0.161	**	**	0.071	0.175	**	**	0.099	0.253	**	**	0.142
	S10	0.037	0.009	0.021	0.027	0.042	0.010	0.023	0.030	0.055	0.017	0.040	0.051	0.060	0.023	0.055	0.070	0.087	0.034	0.080	0.102
	S3	0.097	**	0.057	0.056	0.109	**	0.062	0.062	0.145	**	0.106	0.105	0.157	**	0.147	0.146	0.227	**	0.213	0.211
	S11	0.039	0.028	0.017	0.180	0.044	0.030	0.019	0.198	0.059	0.052	0.032	0.337	0.064	0.072	0.045	0.468	0.093	0.104	0.065	0.677
	S4	0.107	0.062	0.032	**	0.120	0.069	0.035	**	0.160	0.117	0.060	**	0.174	0.163	0.084	**	0.251	0.235	0.121	**
	S12	0.047	0.025	0.018	**	0.053	0.028	0.020	**	0.070	0.048	0.034	**	0.076	0.066	0.047	**	0.110	0.095	0.068	**
6	S1	0.267	**	**	0.153	0.300	**	**	0.168	0.400	**	**	0.287	0.435	**	**	0.398	0.628	**	**	0.575
	S9	0.194	**	**	0.117	0.218	**	**	0.129	0.291	**	**	0.220	0.316	**	**	0.306	0.456	**	**	0.442
	S2	0.133	**	**	0.041	0.149	**	**	0.045	0.199	**	**	0.077	0.216	**	**	0.107	0.313	**	**	0.155
	S10	0.054	0.006	0.021	0.029	0.061	0.006	0.023	0.032	0.081	0.011	0.039	0.054	0.088	0.015	0.055	0.075	0.127	0.022	0.079	0.108
	S3	0.116	**	0.057	0.058	0.131	**	0.063	0.064	0.174	**	0.107	0.109	0.189	**	0.148	0.152	0.273	**	0.214	0.219
	S11	0.058	0.032	0.019	0.195	0.066	0.035	0.021	0.215	0.088	0.060	0.036	0.366	0.095	0.083	0.050	0.508	0.138	0.120	0.073	0.734
	S4	0.132	0.065	0.034	**	0.148	0.072	0.038	**	0.197	0.123	0.065	**	0.214	0.170	0.090	**	0.310	0.246	0.129	**
	S12	0.069	0.030	0.020	**	0.078	0.033	0.022	**	0.104	0.056	0.038	**	0.113	0.078	0.052	**	0.163	0.113	0.075	**
5	S1	0.307	**	**	0.161	0.346	**	**	0.177	0.461	**	**	0.301	0.501	**	**	0.419	0.723	**	**	0.605
	S9	0.229	**	**	0.126	0.257	**	**	0.138	0.343	**	**	0.236	0.373	**	**	0.327	0.539	**	**	0.473
	S2	0.156	**	**	0.044	0.175	**	**	0.048	0.233	**	**	0.082	0.254	**	**	0.115	0.366	**	**	0.165
	S10	0.070	0.003	0.021	0.030	0.079	0.003	0.023	0.033	0.106	0.005	0.039	0.056	0.115	0.007	0.054	0.078	0.166	0.011	0.078	0.112

	S3	0.133	**	0.057	0.060	0.149	**	0.062	0.066	0.199	**	0.106	0.112	0.216	**	0.148	0.155	0.312	**	0.213	0.224
	S11	0.077	0.036	0.021	0.208	0.087	0.039	0.024	0.229	0.116	0.067	0.040	0.389	0.126	0.093	0.056	0.541	0.182	0.134	0.080	0.781
	S4	0.154	0.068	0.036	**	0.174	0.074	0.040	**	0.231	0.127	0.068	**	0.252	0.176	0.095	**	0.363	0.254	0.137	**
	S12	0.091	0.034	0.023	**	0.102	0.038	0.025	**	0.136	0.065	0.042	**	0.148	0.090	0.059	**	0.214	0.129	0.085	**
4	S1	0.339	**	**	0.165	0.381	**	**	0.181	0.508	**	**	0.309	0.553	**	**	0.429	0.798	**	**	0.620
	S9	0.260	**	**	0.132	0.292	**	**	0.145	0.390	**	**	0.247	0.424	**	**	0.344	0.612	**	**	0.496
	S2	0.174	**	**	0.046	0.196	**	**	0.050	0.262	**	**	0.085	0.284	**	**	0.119	0.411	**	**	0.171
	S10	0.089	0.004	0.021	0.030	0.100	0.004	0.023	0.033	0.133	0.007	0.039	0.057	0.144	0.010	0.054	0.079	0.209	0.014	0.079	0.114
	S3	0.147	**	0.056	0.060	0.166	**	0.062	0.066	0.221	**	0.105	0.113	0.240	**	0.146	0.157	0.347	**	0.211	0.226
	S11	0.096	0.039	0.023	0.217	0.108	0.043	0.025	0.239	0.144	0.073	0.043	0.407	0.157	0.101	0.060	0.565	0.227	0.146	0.087	0.816
	S4	0.173	0.069	0.037	**	0.194	0.076	0.041	**	0.259	0.129	0.070	**	0.281	0.179	0.097	**	0.406	0.259	0.141	**
	S12	0.115	0.039	0.025	**	0.130	0.042	0.028	**	0.173	0.072	0.047	**	0.188	0.100	0.066	**	0.272	0.145	0.095	**
3	S1	0.364	**	**	0.167	0.410	**	**	0.184	0.547	**	**	0.313	0.594	**	**	0.435	0.858	**	**	0.628
	S9	0.285	**	**	0.136	0.320	**	**	0.150	0.427	**	**	0.255	0.464	**	**	0.354	0.670	**	**	0.512
	S2	0.190	**	**	0.046	0.214	**	**	0.051	0.285	**	**	0.087	0.310	**	**	0.121	0.447	**	**	0.174
	S10	0.103	0.006	0.020	0.030	0.116	0.007	0.022	0.033	0.154	0.011	0.038	0.056	0.168	0.016	0.052	0.077	0.242	0.023	0.076	0.112
	S3	0.162	**	0.054	0.060	0.182	**	0.060	0.066	0.243	**	0.102	0.113	0.264	**	0.141	0.157	0.381	**	0.204	0.227
	S11	0.114	0.042	0.024	0.224	0.129	0.046	0.027	0.246	0.172	0.078	0.046	0.420	0.187	0.108	0.063	0.583	0.269	0.156	0.092	0.842
	S4	0.189	0.068	0.038	**	0.212	0.075	0.042	**	0.283	0.128	0.071	**	0.307	0.178	0.098	**	0.444	0.257	0.142	**
	S12	0.134	0.041	0.027	**	0.151	0.045	0.029	**	0.202	0.077	0.050	**	0.219	0.107	0.070	**	0.316	0.154	0.101	**

2	S1	0.385	**	**	0.166	0.433	**	**	0.183	0.578	**	**	0.312	0.628	**	**	0.433	0.907	**	**	0.626
	S9	0.307	**	**	0.137	0.346	**	**	0.151	0.461	**	**	0.258	0.501	**	**	0.358	0.724	**	**	0.517
	S2	0.202	**	**	0.046	0.227	**	**	0.051	0.302	**	**	0.086	0.329	**	**	0.120	0.475	**	**	0.173
	S10	0.115	0.008	0.019	0.030	0.129	0.009	0.021	0.033	0.172	0.016	0.036	0.056	0.187	0.022	0.050	0.078	0.270	0.032	0.072	0.113
	S3	0.173	**	0.052	0.060	0.195	**	0.057	0.066	0.260	**	0.097	0.112	0.283	**	0.134	0.155	0.409	**	0.194	0.224
	S11	0.128	0.043	0.025	0.224	0.144	0.047	0.027	0.247	0.192	0.080	0.046	0.420	0.209	0.111	0.064	0.584	0.302	0.160	0.093	0.843
	S4	0.201	0.067	0.038	**	0.227	0.073	0.041	**	0.302	0.125	0.070	**	0.329	0.173	0.098	**	0.475	0.251	0.141	**
	S12	0.150	0.042	0.027	**	0.168	0.046	0.030	**	0.225	0.078	0.051	**	0.244	0.109	0.071	**	0.353	0.157	0.102	**
1	S1	0.392	**	**	0.160	0.441	**	**	0.177	0.589	**	**	0.301	0.640	**	**	0.418	0.924	**	**	0.604
	S9	0.320	**	**	0.134	0.360	**	**	0.148	0.480	**	**	0.252	0.521	**	**	0.350	0.753	**	**	0.506
	S2	0.206	**	**	0.044	0.231	**	**	0.049	0.309	**	**	0.083	0.335	**	**	0.115	0.484	**	**	0.167
	S10	0.123	0.010	0.018	0.030	0.138	0.011	0.020	0.033	0.184	0.018	0.034	0.055	0.200	0.026	0.047	0.077	0.289	0.037	0.068	0.111
	S3	0.179	**	0.048	0.057	0.201	**	0.053	0.063	0.268	**	0.091	0.107	0.291	**	0.126	0.149	0.420	**	0.182	0.215
	S11	0.135	0.042	0.024	0.215	0.152	0.046	0.027	0.237	0.202	0.078	0.045	0.403	0.220	0.109	0.063	0.560	0.317	0.157	0.091	0.809
	S4	0.207	0.063	0.036	**	0.232	0.070	0.040	**	0.310	0.119	0.068	**	0.337	0.165	0.094	**	0.487	0.238	0.136	**
	S12	0.160	0.041	0.027	**	0.180	0.046	0.030	**	0.240	0.078	0.051	**	0.260	0.108	0.070	**	0.376	0.156	0.102	**

Çizelge 3.39: 12 Katlı Hastane Binasının Ankara İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	keZA				keZB				keZC				keZD				keZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
12	S1	0.034	**	**	0.044	0.038	**	**	0.044	0.055	**	**	0.083	0.072	**	**	0.131	0.123	**	**	0.221
	S9	0.018	**	**	0.031	0.021	**	**	0.031	0.030	**	**	0.058	0.039	**	**	0.091	0.067	**	**	0.155
	S2	0.023	**	**	0.016	0.025	**	**	0.016	0.037	**	**	0.029	0.048	**	**	0.046	0.082	**	**	0.078
	S10	0.002	0.011	0.011	0.004	0.003	0.011	0.011	0.004	0.004	0.021	0.020	0.007	0.005	0.032	0.031	0.011	0.009	0.055	0.053	0.018
	S3	0.020	**	0.034	0.032	0.022	**	0.034	0.032	0.032	**	0.064	0.060	0.043	**	0.100	0.093	0.072	**	0.169	0.158
	S11	0.001	0.009	0.006	0.055	0.001	0.009	0.006	0.055	0.001	0.017	0.012	0.104	0.002	0.026	0.019	0.163	0.003	0.045	0.032	0.276
	S4	0.021	0.036	0.015	**	0.024	0.036	0.015	**	0.035	0.067	0.027	**	0.046	0.105	0.043	**	0.077	0.179	0.073	**
	S12	0.002	0.004	0.006	**	0.002	0.004	0.006	**	0.003	0.008	0.012	**	0.004	0.012	0.019	**	0.007	0.021	0.032	**
11	S1	0.056	**	**	0.065	0.063	**	**	0.065	0.091	**	**	0.121	0.119	**	**	0.190	0.203	**	**	0.323
	S9	0.036	**	**	0.046	0.041	**	**	0.046	0.059	**	**	0.087	0.078	**	**	0.136	0.132	**	**	0.230
	S2	0.033	**	**	0.022	0.037	**	**	0.022	0.054	**	**	0.041	0.070	**	**	0.065	0.119	**	**	0.110
	S10	0.004	0.006	0.012	0.008	0.005	0.006	0.012	0.008	0.007	0.012	0.023	0.014	0.009	0.019	0.036	0.023	0.016	0.032	0.061	0.038
	S3	0.030	**	0.036	0.038	0.034	**	0.036	0.038	0.049	**	0.067	0.071	0.064	**	0.105	0.111	0.109	**	0.178	0.188
	S11	0.006	0.012	0.009	0.071	0.007	0.012	0.009	0.071	0.010	0.023	0.018	0.133	0.013	0.036	0.027	0.209	0.022	0.062	0.047	0.354
	S4	0.032	0.036	0.020	**	0.036	0.036	0.020	**	0.052	0.067	0.037	**	0.068	0.106	0.057	**	0.116	0.179	0.097	**
	S12	0.006	0.011	0.010	**	0.007	0.011	0.010	**	0.010	0.020	0.018	**	0.014	0.031	0.029	**	0.023	0.053	0.048	**

10	S1	0.077	**	**	0.073	0.087	**	**	0.073	0.126	**	**	0.137	0.166	**	**	0.216	0.281	**	**	0.366
	S9	0.053	**	**	0.053	0.060	**	**	0.053	0.086	**	**	0.099	0.113	**	**	0.155	0.192	**	**	0.263
	S2	0.041	**	**	0.025	0.046	**	**	0.025	0.067	**	**	0.046	0.088	**	**	0.073	0.150	**	**	0.123
	S10	0.010	0.005	0.013	0.009	0.011	0.005	0.013	0.009	0.016	0.010	0.025	0.018	0.021	0.016	0.039	0.028	0.035	0.027	0.066	0.047
	S3	0.039	**	0.037	0.040	0.043	**	0.037	0.040	0.063	**	0.069	0.075	0.082	**	0.108	0.117	0.140	**	0.183	0.199
	S11	0.011	0.014	0.010	0.080	0.013	0.014	0.010	0.080	0.018	0.027	0.019	0.149	0.024	0.042	0.030	0.234	0.041	0.071	0.052	0.397
	S4	0.041	0.038	0.021	**	0.047	0.038	0.021	**	0.067	0.072	0.040	**	0.089	0.113	0.063	**	0.150	0.192	0.106	**
	S12	0.013	0.013	0.011	**	0.015	0.013	0.011	**	0.021	0.024	0.020	**	0.028	0.038	0.032	**	0.047	0.065	0.054	**
9	S1	0.095	**	**	0.079	0.107	**	**	0.079	0.154	**	**	0.149	0.203	**	**	0.234	0.345	**	**	0.396
	S9	0.067	**	**	0.058	0.076	**	**	0.058	0.109	**	**	0.109	0.144	**	**	0.172	0.244	**	**	0.291
	S2	0.050	**	**	0.027	0.056	**	**	0.027	0.082	**	**	0.050	0.107	**	**	0.079	0.182	**	**	0.134
	S10	0.016	0.003	0.013	0.011	0.018	0.003	0.013	0.011	0.026	0.006	0.024	0.021	0.034	0.010	0.038	0.033	0.057	0.017	0.065	0.057
	S3	0.046	**	0.037	0.042	0.051	**	0.037	0.042	0.074	**	0.070	0.078	0.098	**	0.110	0.122	0.166	**	0.186	0.207
	S11	0.018	0.017	0.012	0.088	0.020	0.017	0.012	0.088	0.029	0.032	0.022	0.165	0.039	0.050	0.035	0.258	0.066	0.085	0.059	0.438
	S4	0.050	0.041	0.023	**	0.057	0.041	0.023	**	0.082	0.076	0.043	**	0.108	0.119	0.068	**	0.183	0.202	0.115	**
	S12	0.021	0.016	0.012	**	0.024	0.016	0.012	**	0.034	0.030	0.023	**	0.045	0.047	0.036		0.076	0.080	0.061	**
8	S1	0.110	**	**	0.084	0.124	**	**	0.084	0.178	**	**	0.158	0.235	**	**	0.248	0.399	**	**	0.421
	S9	0.080	**	**	0.064	0.090	**	**	0.064	0.130	**	**	0.119	0.171	**	**	0.187	0.291	**	**	0.317
	S2	0.059	**	**	0.029	0.066	**	**	0.029	0.095	**	**	0.054	0.125	**	**	0.085	0.213	**	**	0.144
	S10	0.022	0.002	0.013	0.013	0.024	0.002	0.013	0.013	0.035	0.004	0.025	0.025	0.046	0.006	0.038	0.039	0.078	0.011	0.065	0.066

	S3	0.052	**	0.038	0.043	0.058	**	0.038	0.043	0.084	**	0.070	0.080	0.111	**	0.111	0.126	0.188	**	0.187	0.214
	S11	0.025	0.020	0.013	0.096	0.028	0.020	0.013	0.096	0.041	0.037	0.025	0.179	0.053	0.058	0.039	0.281	0.091	0.098	0.066	0.477
	S4	0.059	0.043	0.025	**	0.066	0.043	0.025	**	0.096	0.080	0.046	**	0.126	0.125	0.072	**	0.214	0.212	0.122	**
	S12	0.029	0.019	0.014	**	0.032	0.019	0.014	**	0.047	0.036	0.026	**	0.062	0.056	0.040	**	0.105	0.095	0.068	**
7	S1	0.122	**	**	0.088	0.137	**	**	0.088	0.198	**	**	0.165	0.261	**	**	0.259	0.442	**	**	0.440
	S9	0.092	**	**	0.068	0.103	**	**	0.068	0.149	**	**	0.128	0.196	**	**	0.201	0.333	**	**	0.341
	S2	0.066	**	**	0.030	0.074	**	**	0.030	0.107	**	**	0.057	0.141	**	**	0.090	0.239	**	**	0.152
	S10	0.028	0.003	0.013	0.015	0.032	0.003	0.013	0.015	0.046	0.006	0.025	0.028	0.061	0.009	0.039	0.044	0.103	0.016	0.066	0.075
	S3	0.057	**	0.038	0.044	0.065	**	0.038	0.044	0.093	**	0.071	0.082	0.123	**	0.111	0.129	0.208	**	0.189	0.219
	S11	0.032	0.022	0.015	0.103	0.036	0.022	0.015	0.103	0.052	0.042	0.027	0.193	0.068	0.066	0.043	0.302	0.116	0.111	0.073	0.513
	S4	0.066	0.044	0.026	**	0.074	0.044	0.026	**	0.107	0.083	0.048	**	0.141	0.130	0.075	**	0.239	0.221	0.127	**
	S12	0.038	0.022	0.016	**	0.043	0.022	0.016	**	0.062	0.042	0.030	**	0.081	0.066	0.046	**	0.138	0.112	0.079	**
6	S1	0.132	**	**	0.092	0.149	**	**	0.092	0.215	**	**	0.172	0.283	**	**	0.271	0.480	**	**	0.459
	S9	0.102	**	**	0.073	0.114	**	**	0.073	0.165	**	**	0.136	0.217	**	**	0.214	0.368	**	**	0.363
	S2	0.072	**	**	0.032	0.081	**	**	0.032	0.117	**	**	0.060	0.154	**	**	0.093	0.262	**	**	0.159
	S10	0.034	0.005	0.013	0.016	0.038	0.005	0.013	0.016	0.055	0.010	0.024	0.031	0.073	0.015	0.038	0.048	0.123	0.025	0.065	0.082
	S3	0.063	**	0.038	0.045	0.071	**	0.038	0.045	0.103	**	0.071	0.085	0.136	**	0.111	0.133	0.230	**	0.188	0.226
	S11	0.039	0.025	0.016	0.111	0.044	0.025	0.016	0.111	0.063	0.047	0.030	0.207	0.084	0.074	0.047	0.325	0.142	0.126	0.080	0.552
	S4	0.072	0.045	0.026	**	0.082	0.045	0.026	**	0.118	0.085	0.050	**	0.155	0.133	0.078	**	0.263	0.226	0.132	**
	S12	0.045	0.025	0.017	**	0.051	0.025	0.017	**	0.074	0.047	0.032	**	0.097	0.073	0.051	**	0.164	0.125	0.086	**

5	S1	0.142	**	**	0.096	0.159	**	**	0.096	0.230	**	**	0.179	0.303	**	**	0.281	0.514	**	**	0.477
	S9	0.112	**	**	0.077	0.125	**	**	0.077	0.181	**	**	0.145	0.239	**	**	0.227	0.405	**	**	0.386
	S2	0.078	**	**	0.033	0.087	**	**	0.033	0.126	**	**	0.061	0.166	**	**	0.096	0.282	**	**	0.163
	S10	0.039	0.007	0.013	0.018	0.044	0.007	0.013	0.018	0.064	0.014	0.024	0.033	0.084	0.022	0.037	0.052	0.142	0.037	0.063	0.088
	S3	0.069	**	0.038	0.046	0.077	**	0.038	0.046	0.112	**	0.071	0.087	0.147	**	0.112	0.136	0.250	**	0.190	0.230
	S11	0.045	0.028	0.017	0.117	0.050	0.028	0.017	0.117	0.073	0.052	0.032	0.219	0.096	0.081	0.050	0.344	0.163	0.138	0.085	0.583
	S4	0.078	0.046	0.027	**	0.088	0.046	0.027	**	0.127	0.086	0.051	**	0.168	0.135	0.080	**	0.285	0.230	0.136	**
	S12	0.052	0.027	0.018	**	0.059	0.027	0.018	**	0.085	0.051	0.035	**	0.111	0.080	0.054	**	0.189	0.135	0.092	**
4	S1	0.150	**	**	0.098	0.169	**	**	0.098	0.244	**	**	0.184	0.322	**	**	0.289	0.546	**	**	0.490
	S9	0.121	**	**	0.081	0.136	**	**	0.081	0.197	**	**	0.152	0.259	**	**	0.238	0.439	**	**	0.404
	S2	0.082	**	**	0.033	0.093	**	**	0.033	0.134	**	**	0.062	0.176	**	**	0.098	0.299	**	**	0.166
	S10	0.044	0.009	0.012	0.019	0.050	0.009	0.012	0.019	0.072	0.017	0.023	0.035	0.095	0.027	0.036	0.055	0.161	0.046	0.061	0.094
	S3	0.074	**	0.038	0.047	0.083	**	0.038	0.047	0.120	**	0.071	0.087	0.158	**	0.112	0.137	0.267	**	0.190	0.233
	S11	0.050	0.029	0.018	0.121	0.056	0.029	0.018	0.121	0.081	0.055	0.033	0.227	0.106	0.086	0.052	0.356	0.180	0.145	0.087	0.604
	S4	0.084	0.046	0.028	**	0.094	0.046	0.028	**	0.136	0.086	0.052	**	0.179	0.136	0.081	**	0.304	0.230	0.138	**
	S12	0.059	0.029	0.019	**	0.066	0.029	0.019	**	0.095	0.054	0.037	**	0.125	0.085	0.057	**	0.213	0.144	0.097	**
3	S1	0.160	**	**	0.100	0.180	**	**	0.100	0.260	**	**	0.188	0.343	**	**	0.296	0.581	**	**	0.501
	S9	0.130	**	**	0.083	0.146	**	**	0.083	0.211	**	**	0.156	0.277	**	**	0.245	0.470	**	**	0.416
	S2	0.086	**	**	0.033	0.097	**	**	0.033	0.140	**	**	0.062	0.185	**	**	0.098	0.314	**	**	0.166
	S10	0.049	0.010	0.012	0.019	0.055	0.010	0.012	0.019	0.080	0.020	0.022	0.036	0.105	0.031	0.035	0.057	0.178	0.052	0.060	0.097

	S3	0.078	**	0.038	0.046	0.088	**	0.038	0.046	0.127	**	0.070	0.087	0.167	**	0.110	0.137	0.283	**	0.187	0.232
	S11	0.054	0.030	0.018	0.123	0.061	0.030	0.018	0.123	0.088	0.056	0.033	0.231	0.115	0.088	0.052	0.363	0.196	0.150	0.088	0.616
	S4	0.088	0.045	0.028	**	0.099	0.045	0.028	**	0.143	0.085	0.052	**	0.188	0.134	0.081	**	0.319	0.227	0.138	**
	S12	0.064	0.030	0.020	**	0.073	0.030	0.020	**	0.105	0.056	0.038	**	0.138	0.088	0.059	**	0.234	0.149	0.100	**
2	S1	0.169	**	**	0.101	0.190	**	**	0.101	0.275	**	**	0.190	0.362	**	**	0.298	0.614	**	**	0.506
	S9	0.137	**	**	0.084	0.154	**	**	0.084	0.222	**	**	0.158	0.293	**	**	0.247	0.496	**	**	0.420
	S2	0.089	**	**	0.033	0.101	**	**	0.033	0.145	**	**	0.062	0.191	**	**	0.097	0.324	**	**	0.164
	S10	0.053	0.011	0.012	0.020	0.059	0.011	0.012	0.020	0.086	0.021	0.022	0.037	0.113	0.033	0.034	0.058	0.192	0.056	0.057	0.098
	S3	0.081	**	0.036	0.045	0.091	**	0.036	0.045	0.131	**	0.068	0.085	0.173	**	0.107	0.134	0.293	**	0.182	0.227
	S11	0.057	0.030	0.018	0.123	0.064	0.030	0.018	0.123	0.093	0.056	0.033	0.231	0.122	0.089	0.052	0.362	0.207	0.150	0.088	0.614
	S4	0.091	0.044	0.027	**	0.102	0.044	0.027	**	0.148	0.083	0.051	**	0.195	0.130	0.080	**	0.330	0.220	0.136	**
	S12	0.069	0.030	0.020	**	0.078	0.030	0.020	**	0.113	0.057	0.038	**	0.148	0.089	0.059	**	0.251	0.150	0.101	**
1	S1	0.172	**	**	0.099	0.194	**	**	0.099	0.280	**	**	0.186	0.369	**	**	0.293	0.625	**	**	0.496
	S9	0.139	**	**	0.082	0.156	**	**	0.082	0.226	**	**	0.154	0.298	**	**	0.242	0.505	**	**	0.411
	S2	0.090	**	**	0.032	0.101	**	**	0.032	0.146	**	**	0.060	0.192	**	**	0.094	0.326	**	**	0.159
	S10	0.054	0.011	0.011	0.019	0.061	0.011	0.011	0.019	0.088	0.021	0.021	0.036	0.116	0.034	0.032	0.057	0.198	0.057	0.055	0.097
	S3	0.081	**	0.035	0.044	0.092	**	0.035	0.044	0.132	**	0.065	0.082	0.174	**	0.102	0.129	0.295	**	0.174	0.218
	S11	0.058	0.029	0.017	0.119	0.065	0.029	0.017	0.119	0.094	0.055	0.032	0.224	0.124	0.086	0.050	0.351	0.211	0.146	0.085	0.595
	S4	0.092	0.042	0.026	**	0.103	0.042	0.026	**	0.149	0.079	0.049	**	0.196	0.124	0.077	**	0.332	0.211	0.131	**
	S12	0.071	0.029	0.020	**	0.080	0.029	0.020	**	0.116	0.055	0.037	**	0.152	0.087	0.058	**	0.258	0.147	0.098	**

Çizelge 3.40: 12 Katlı Hastane Binasının İstanbul İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	KEZA				KEZB				KEZC				KEZD				KEZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
12	S1	0.090	**	**	0.099	0.101	**	**	0.112	0.135	**	**	0.176	0.135	**	**	0.244	0.195	**	**	0.352
	S9	0.049	**	**	0.070	0.055	**	**	0.078	0.073	**	**	0.123	0.073	**	**	0.171	0.106	**	**	0.246
	S2	0.060	**	**	0.035	0.068	**	**	0.039	0.090	**	**	0.062	0.090	**	**	0.086	0.130	**	**	0.124
	S10	0.006	0.025	0.024	0.008	0.007	0.028	0.027	0.009	0.010	0.044	0.042	0.014	0.010	0.060	0.059	0.020	0.014	0.087	0.084	0.029
	S3	0.053	**	0.076	0.071	0.060	**	0.085	0.080	0.080	**	0.134	0.126	0.080	**	0.186	0.175	0.115	**	0.269	0.252
	S11	0.002	0.020	0.015	0.124	0.003	0.023	0.016	0.139	0.004	0.035	0.026	0.219	0.004	0.049	0.036	0.304	0.005	0.071	0.051	0.438
	S4	0.057	0.080	0.033	**	0.064	0.090	0.037	**	0.085	0.142	0.058	**	0.085	0.197	0.080	**	0.123	0.284	0.116	**
	S12	0.005	0.009	0.014	**	0.006	0.011	0.016	**	0.008	0.017	0.025	**	0.008	0.023	0.035	**	0.011	0.033	0.051	**
11	S1	0.148	**	**	0.145	0.167	**	**	0.163	0.223	**	**	0.256	0.223	**	**	0.355	0.322	**	**	0.512
	S9	0.097	**	**	0.103	0.109	**	**	0.116	0.145	**	**	0.183	0.145	**	**	0.254	0.209	**	**	0.366
	S2	0.088	**	**	0.049	0.098	**	**	0.056	0.131	**	**	0.087	0.132	**	**	0.121	0.190	**	**	0.175
	S10	0.012	0.014	0.028	0.017	0.013	0.016	0.031	0.019	0.017	0.025	0.049	0.030	0.017	0.035	0.068	0.042	0.025	0.051	0.097	0.061
	S3	0.080	**	0.080	0.084	0.090	**	0.090	0.095	0.120	**	0.141	0.149	0.120	**	0.196	0.207	0.173	**	0.283	0.298
	S11	0.016	0.028	0.021	0.159	0.018	0.031	0.024	0.179	0.024	0.049	0.037	0.281	0.024	0.068	0.051	0.390	0.034	0.098	0.074	0.563
	S4	0.085	0.080	0.044	**	0.095	0.091	0.049	**	0.127	0.142	0.077	**	0.127	0.197	0.107	**	0.183	0.285	0.155	**
	S12	0.017	0.024	0.022	**	0.019	0.027	0.024	**	0.026	0.042	0.038	**	0.026	0.058	0.053	**	0.037	0.084	0.077	**

10	S1	0.206	**	**	0.164	0.231	**	**	0.185	0.309	**	**	0.290	0.309	**	**	0.403	0.446	**	**	0.581
	S9	0.141	**	**	0.118	0.158	**	**	0.133	0.211	**	**	0.209	0.212	**	**	0.289	0.305	**	**	0.417
	S2	0.110	**	**	0.055	0.123	**	**	0.062	0.164	**	**	0.098	0.165	**	**	0.136	0.238	**	**	0.196
	S10	0.026	0.012	0.029	0.021	0.029	0.013	0.033	0.024	0.038	0.021	0.052	0.038	0.038	0.029	0.072	0.052	0.055	0.042	0.104	0.075
	S3	0.102	**	0.082	0.089	0.115	**	0.092	0.100	0.154	**	0.145	0.158	0.154	**	0.201	0.219	0.222	**	0.291	0.316
	S11	0.030	0.032	0.023	0.178	0.034	0.036	0.026	0.201	0.045	0.056	0.041	0.316	0.045	0.078	0.057	0.438	0.065	0.113	0.082	0.631
	S4	0.110	0.086	0.048	**	0.124	0.097	0.054	**	0.165	0.152	0.085	**	0.165	0.211	0.117	**	0.239	0.304	0.169	**
	S12	0.034	0.029	0.024	**	0.039	0.033	0.027	**	0.052	0.052	0.043	**	0.052	0.072	0.060	**	0.074	0.103	0.086	**
9	S1	0.252	**	**	0.178	0.284	**	**	0.200	0.379	**	**	0.315	0.379	**	**	0.436	0.547	**	**	0.629
	S9	0.179	**	**	0.131	0.201	**	**	0.147	0.268	**	**	0.231	0.269	**	**	0.321	0.388	**	**	0.463
	S2	0.133	**	**	0.060	0.150	**	**	0.068	0.200	**	**	0.107	0.200	**	**	0.148	0.289	**	**	0.213
	S10	0.042	0.007	0.029	0.025	0.047	0.008	0.033	0.029	0.063	0.013	0.051	0.045	0.063	0.018	0.071	0.062	0.091	0.026	0.103	0.090
	S3	0.121	**	0.083	0.093	0.137	**	0.094	0.105	0.182	**	0.148	0.165	0.182	**	0.205	0.228	0.263	**	0.295	0.329
	S11	0.048	0.038	0.026	0.197	0.054	0.043	0.030	0.221	0.072	0.067	0.047	0.348	0.072	0.093	0.065	0.483	0.104	0.134	0.094	0.696
	S4	0.134	0.091	0.051	**	0.151	0.102	0.058	**	0.201	0.161	0.091	**	0.202	0.223	0.126	**	0.291	0.321	0.182	**
	S12	0.056	0.036	0.027	**	0.063	0.040	0.031	**	0.083	0.064	0.048	**	0.084	0.088	0.067	**	0.121	0.127	0.096	**
8	S1	0.292	**	**	0.189	0.328	**	**	0.213	0.438	**	**	0.335	0.439	**	**	0.464	0.633	**	**	0.669
	S9	0.213	**	**	0.142	0.240	**	**	0.160	0.319	**	**	0.252	0.320	**	**	0.349	0.462	**	**	0.504
	S2	0.156	**	**	0.065	0.175	**	**	0.073	0.234	**	**	0.115	0.234	**	**	0.159	0.338	**	**	0.229
	S10	0.057	0.005	0.029	0.029	0.065	0.006	0.033	0.033	0.086	0.009	0.052	0.052	0.086	0.012	0.072	0.072	0.125	0.017	0.104	0.104

	S3	0.138	**	0.084	0.096	0.155	**	0.095	0.108	0.206	**	0.149	0.170	0.207	**	0.206	0.236	0.298	**	0.298	0.340
	S11	0.066	0.044	0.030	0.214	0.075	0.050	0.034	0.241	0.099	0.078	0.053	0.379	0.100	0.108	0.073	0.525	0.144	0.156	0.105	0.758
	S4	0.157	0.095	0.055	**	0.176	0.107	0.062	**	0.235	0.169	0.097	**	0.235	0.234	0.135	**	0.340	0.337	0.194	**
	S12	0.077	0.043	0.031	**	0.086	0.048	0.035	**	0.115	0.075	0.054	**	0.115	0.105	0.075	**	0.166	0.151	0.109	**
7	S1	0.324	**	**	0.197	0.364	**	**	0.222	0.486	**	**	0.349	0.487	**	**	0.484	0.702	**	**	0.698
	S9	0.244	**	**	0.153	0.274	**	**	0.172	0.366	**	**	0.270	0.367	**	**	0.375	0.529	**	**	0.541
	S2	0.175	**	**	0.068	0.197	**	**	0.077	0.263	**	**	0.121	0.263	**	**	0.167	0.380	**	**	0.241
	S10	0.076	0.007	0.030	0.034	0.085	0.008	0.033	0.038	0.113	0.013	0.053	0.060	0.114	0.018	0.073	0.083	0.164	0.025	0.105	0.120
	S3	0.153	**	0.085	0.098	0.172	**	0.095	0.111	0.229	**	0.150	0.174	0.230	**	0.208	0.241	0.331	**	0.300	0.348
	S11	0.085	0.050	0.033	0.230	0.096	0.056	0.037	0.259	0.127	0.088	0.058	0.407	0.128	0.123	0.081	0.564	0.184	0.177	0.116	0.814
	S4	0.175	0.099	0.057	**	0.197	0.111	0.064	**	0.263	0.175	0.101	**	0.263	0.243	0.140	**	0.380	0.350	0.202	**
	S12	0.101	0.050	0.035	**	0.114	0.056	0.040	**	0.152	0.089	0.062	**	0.152	0.123	0.087	**	0.219	0.177	0.125	**
6	S1	0.351	**	**	0.206	0.395	**	**	0.232	0.527	**	**	0.364	0.528	**	**	0.505	0.762	**	**	0.729
	S9	0.270	**	**	0.163	0.304	**	**	0.183	0.405	**	**	0.288	0.406	**	**	0.399	0.585	**	**	0.576
	S2	0.192	**	**	0.071	0.216	**	**	0.080	0.288	**	**	0.126	0.289	**	**	0.175	0.416	**	**	0.252
	S10	0.090	0.011	0.029	0.037	0.101	0.013	0.033	0.042	0.135	0.020	0.051	0.065	0.136	0.028	0.071	0.091	0.195	0.040	0.103	0.131
	S3	0.169	**	0.084	0.101	0.190	**	0.095	0.114	0.253	**	0.149	0.179	0.253	**	0.207	0.248	0.365	**	0.299	0.358
	S11	0.104	0.057	0.036	0.248	0.117	0.064	0.040	0.278	0.156	0.100	0.064	0.438	0.156	0.139	0.088	0.607	0.225	0.200	0.127	0.876
	S4	0.193	0.102	0.059	**	0.217	0.114	0.067	**	0.289	0.180	0.105	**	0.290	0.249	0.145	**	0.418	0.359	0.210	**
	S12	0.120	0.056	0.039	**	0.136	0.063	0.043	**	0.181	0.099	0.068	**	0.181	0.137	0.095	**	0.261	0.198	0.137	**

5	S1	0.377	**	**	0.214	0.424	**	**	0.241	0.565	**	**	0.379	0.566	**	**	0.525	0.816	**	**	0.757
	S9	0.297	**	**	0.173	0.334	**	**	0.195	0.445	**	**	0.306	0.446	**	**	0.425	0.643	**	**	0.613
	S2	0.207	**	**	0.073	0.232	**	**	0.083	0.310	**	**	0.130	0.311	**	**	0.180	0.448	**	**	0.260
	S10	0.104	0.016	0.028	0.040	0.117	0.018	0.032	0.044	0.156	0.029	0.050	0.070	0.156	0.040	0.069	0.097	0.226	0.058	0.099	0.140
	S3	0.183	**	0.085	0.103	0.206	**	0.096	0.116	0.274	**	0.151	0.183	0.275	**	0.209	0.254	0.396	**	0.302	0.366
	S11	0.119	0.062	0.038	0.262	0.134	0.070	0.043	0.294	0.179	0.109	0.067	0.463	0.179	0.152	0.093	0.642	0.258	0.219	0.135	0.926
	S4	0.208	0.103	0.061	**	0.234	0.116	0.069	**	0.313	0.182	0.108	**	0.313	0.253	0.150	**	0.452	0.365	0.216	**
	S12	0.138	0.061	0.041	**	0.156	0.068	0.046	**	0.207	0.107	0.073	**	0.208	0.149	0.101	**	0.300	0.214	0.146	**
4	S1	0.400	**	**	0.220	0.450	**	**	0.247	0.600	**	**	0.389	0.601	**	**	0.539	0.867	**	**	0.778
	S9	0.322	**	**	0.181	0.362	**	**	0.204	0.482	**	**	0.321	0.483	**	**	0.445	0.697	**	**	0.642
	S2	0.219	**	**	0.074	0.247	**	**	0.084	0.329	**	**	0.132	0.329	**	**	0.183	0.475	**	**	0.264
	S10	0.118	0.020	0.028	0.042	0.133	0.023	0.031	0.047	0.177	0.036	0.049	0.074	0.177	0.050	0.068	0.103	0.255	0.073	0.097	0.149
	S3	0.196	**	0.085	0.104	0.220	**	0.096	0.117	0.294	**	0.151	0.185	0.295	**	0.209	0.256	0.425	**	0.301	0.369
	S11	0.132	0.065	0.039	0.271	0.148	0.073	0.044	0.305	0.198	0.115	0.069	0.480	0.198	0.160	0.096	0.665	0.286	0.231	0.139	0.960
	S4	0.222	0.103	0.062	**	0.250	0.116	0.070	**	0.333	0.183	0.110	**	0.334	0.253	0.152	**	0.482	0.365	0.219	**
	S12	0.156	0.065	0.044	**	0.175	0.073	0.049	**	0.234	0.114	0.077	**	0.234	0.158	0.107	**	0.338	0.228	0.154	**
3	S1	0.426	**	**	0.225	0.479	**	**	0.253	0.639	**	**	0.398	0.640	**	**	0.552	0.923	**	**	0.796
	S9	0.345	**	**	0.187	0.388	**	**	0.210	0.517	**	**	0.330	0.518	**	**	0.458	0.747	**	**	0.660
	S2	0.230	**	**	0.075	0.258	**	**	0.084	0.345	**	**	0.132	0.345	**	**	0.183	0.498	**	**	0.264
	S10	0.130	0.023	0.027	0.044	0.147	0.026	0.030	0.049	0.195	0.041	0.047	0.077	0.196	0.057	0.066	0.107	0.283	0.083	0.095	0.154

	S3	0.207	**	0.084	0.104	0.233	**	0.095	0.117	0.311	**	0.149	0.184	0.311	**	0.206	0.255	0.449	**	0.297	0.368
	S11	0.143	0.067	0.040	0.276	0.161	0.076	0.045	0.311	0.215	0.119	0.070	0.489	0.215	0.165	0.097	0.678	0.311	0.238	0.141	0.979
	S4	0.234	0.102	0.062	**	0.263	0.114	0.070	**	0.350	0.180	0.110	**	0.351	0.250	0.152	**	0.506	0.360	0.219	**
	S12	0.171	0.067	0.045	**	0.193	0.075	0.050	**	0.257	0.118	0.079	**	0.258	0.164	0.110	**	0.372	0.236	0.159	**
2	S1	0.450	**	**	0.227	0.506	**	**	0.255	0.675	**	**	0.402	0.676	**	**	0.557	0.975	**	**	0.804
	S9	0.364	**	**	0.188	0.409	**	**	0.212	0.545	**	**	0.333	0.547	**	**	0.462	0.788	**	**	0.666
	S2	0.238	**	**	0.074	0.267	**	**	0.083	0.356	**	**	0.131	0.357	**	**	0.181	0.515	**	**	0.261
	S10	0.141	0.025	0.026	0.044	0.158	0.028	0.029	0.050	0.211	0.045	0.046	0.078	0.211	0.062	0.063	0.108	0.305	0.089	0.091	0.156
	S3	0.215	**	0.082	0.102	0.242	**	0.092	0.114	0.322	**	0.145	0.180	0.323	**	0.200	0.250	0.466	**	0.289	0.360
	S11	0.152	0.067	0.039	0.276	0.171	0.076	0.044	0.310	0.228	0.119	0.070	0.488	0.228	0.166	0.097	0.677	0.329	0.239	0.140	0.976
	S4	0.242	0.099	0.061	**	0.272	0.111	0.069	**	0.363	0.175	0.108	**	0.364	0.243	0.149	**	0.525	0.350	0.216	**
	S12	0.184	0.067	0.045	**	0.207	0.076	0.051	**	0.276	0.119	0.080	**	0.277	0.166	0.111	**	0.399	0.239	0.160	**
1	S1	0.458	**	**	0.223	0.515	**	**	0.250	0.687	**	**	0.394	0.689	**	**	0.546	0.993	**	**	0.788
	S9	0.370	**	**	0.184	0.416	**	**	0.207	0.555	**	**	0.326	0.556	**	**	0.452	0.801	**	**	0.653
	S2	0.239	**	**	0.071	0.269	**	**	0.080	0.358	**	**	0.126	0.359	**	**	0.175	0.518	**	**	0.253
	S10	0.145	0.026	0.025	0.043	0.163	0.029	0.028	0.049	0.217	0.045	0.043	0.077	0.218	0.063	0.060	0.107	0.314	0.091	0.087	0.154
	S3	0.216	**	0.078	0.098	0.243	**	0.088	0.110	0.325	**	0.138	0.173	0.325	**	0.191	0.240	0.469	**	0.276	0.346
	S11	0.154	0.066	0.038	0.267	0.173	0.074	0.043	0.300	0.231	0.116	0.067	0.473	0.232	0.161	0.094	0.655	0.334	0.232	0.135	0.945
	S4	0.244	0.094	0.059	**	0.274	0.106	0.066	**	0.365	0.167	0.104	**	0.366	0.232	0.144	**	0.528	0.334	0.208	**
	S12	0.189	0.066	0.044	**	0.213	0.074	0.050	**	0.283	0.117	0.078	**	0.284	0.162	0.108	**	0.410	0.233	0.156	**

Çizelge 3.41: 12 Katlı Hastane Binasının İzmir İlinde Bulunduğu Duruma Ait k_E Değerleri.

$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	KEZA				KEZB				KEZC				KEZD				KEZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
12	S1	0.102	**	**	0.113	0.115	**	**	0.127	0.153	**	**	0.174	0.138	**	**	0.242	0.194	**	**	0.350
	S9	0.056	**	**	0.079	0.062	**	**	0.089	0.083	**	**	0.122	0.075	**	**	0.170	0.105	**	**	0.245
	S2	0.068	**	**	0.040	0.077	**	**	0.045	0.102	**	**	0.062	0.092	**	**	0.085	0.130	**	**	0.046
	S10	0.007	0.028	0.027	0.009	0.008	0.031	0.031	0.010	0.011	0.043	0.042	0.014	0.010	0.060	0.058	0.020	0.014	0.087	0.084	0.022
	S3	0.060	**	0.086	0.081	0.068	**	0.097	0.091	0.090	**	0.133	0.125	0.081	**	0.185	0.173	0.114	**	0.267	0.096
	S11	0.003	0.023	0.017	0.141	0.003	0.026	0.019	0.158	0.004	0.035	0.025	0.218	0.004	0.049	0.035	0.302	0.005	0.071	0.051	0.437
	S4	0.064	0.091	0.037	**	0.072	0.103	0.042	**	0.097	0.141	0.057	**	0.087	0.196	0.080	**	0.122	0.283	0.115	**
	S12	0.006	0.011	0.016	**	0.007	0.012	0.018	**	0.009	0.016	0.025	**	0.008	0.023	0.035	**	0.011	0.033	0.051	**
11	S1	0.169	**	**	0.165	0.190	**	**	0.185	0.253	**	**	0.254	0.227	**	**	0.353	0.320	**	**	0.510
	S9	0.110	**	**	0.118	0.124	**	**	0.132	0.165	**	**	0.182	0.148	**	**	0.252	0.208	**	**	0.364
	S2	0.100	**	**	0.056	0.112	**	**	0.063	0.149	**	**	0.087	0.134	**	**	0.120	0.189	**	**	0.053
	S10	0.013	0.016	0.031	0.019	0.015	0.018	0.035	0.022	0.020	0.025	0.048	0.030	0.018	0.035	0.067	0.042	0.025	0.051	0.097	0.046
	S3	0.091	**	0.091	0.096	0.102	**	0.102	0.108	0.136	**	0.140	0.148	0.122	**	0.195	0.206	0.172	**	0.282	0.100
	S11	0.018	0.031	0.024	0.181	0.020	0.035	0.027	0.203	0.027	0.048	0.037	0.279	0.024	0.067	0.051	0.388	0.034	0.097	0.074	0.560
	S4	0.096	0.091	0.050	**	0.108	0.103	0.056	**	0.144	0.141	0.077	**	0.129	0.196	0.107	**	0.183	0.284	0.154	**
	S12	0.020	0.027	0.025	**	0.022	0.030	0.028	**	0.029	0.042	0.038	**	0.026	0.058	0.053	**	0.037	0.084	0.077	**

10	S1	0.234	**	**	0.187	0.263	**	**	0.210	0.351	**	**	0.288	0.314	**	**	0.400	0.444	**	**	0.578
	S9	0.160	**	**	0.134	0.180	**	**	0.151	0.240	**	**	0.207	0.215	**	**	0.288	0.304	**	**	0.415
	S2	0.125	**	**	0.063	0.140	**	**	0.071	0.187	**	**	0.097	0.168	**	**	0.135	0.237	**	**	0.065
	S10	0.029	0.014	0.033	0.024	0.033	0.015	0.038	0.027	0.044	0.021	0.052	0.037	0.039	0.029	0.072	0.052	0.055	0.042	0.104	0.062
	S3	0.116	**	0.093	0.101	0.131	**	0.105	0.114	0.175	**	0.144	0.157	0.157	**	0.200	0.218	0.221	**	0.289	0.103
	S11	0.034	0.036	0.026	0.203	0.038	0.041	0.030	0.228	0.051	0.056	0.041	0.313	0.046	0.078	0.057	0.435	0.065	0.112	0.082	0.628
	S4	0.125	0.098	0.054	**	0.141	0.110	0.061	**	0.188	0.151	0.084	**	0.168	0.210	0.117	**	0.238	0.303	0.168	**
	S12	0.039	0.033	0.028	**	0.044	0.037	0.031	**	0.059	0.051	0.043	**	0.053	0.071	0.059	**	0.074	0.103	0.086	**
9	S1	0.287	**	**	0.202	0.323	**	**	0.227	0.431	**	**	0.312	0.386	**	**	0.434	0.545	**	**	0.626
	S9	0.204	**	**	0.149	0.229	**	**	0.167	0.305	**	**	0.230	0.274	**	**	0.319	0.386	**	**	0.461
	S2	0.152	**	**	0.069	0.171	**	**	0.077	0.227	**	**	0.106	0.204	**	**	0.147	0.288	**	**	0.075
	S10	0.048	0.008	0.033	0.029	0.054	0.009	0.037	0.033	0.071	0.013	0.051	0.045	0.064	0.018	0.071	0.062	0.090	0.026	0.102	0.070
	S3	0.138	**	0.095	0.106	0.155	**	0.107	0.119	0.207	**	0.146	0.163	0.186	**	0.203	0.227	0.262	**	0.294	0.107
	S11	0.055	0.043	0.030	0.224	0.061	0.049	0.034	0.252	0.082	0.067	0.046	0.345	0.073	0.093	0.065	0.480	0.104	0.134	0.093	0.693
	S4	0.152	0.103	0.058	**	0.172	0.116	0.066	**	0.229	0.159	0.090	**	0.205	0.222	0.125	**	0.289	0.320	0.181	**
	S12	0.063	0.041	0.031	**	0.071	0.046	0.035	**	0.095	0.063	0.048	**	0.085	0.088	0.066	**	0.120	0.127	0.096	**
8	S1	0.332	**	**	0.215	0.374	**	**	0.242	0.498	**	**	0.332	0.446	**	**	0.461	0.630	**	**	0.666
	S9	0.242	**	**	0.162	0.272	**	**	0.182	0.363	**	**	0.250	0.326	**	**	0.347	0.460	**	**	0.501
	S2	0.177	**	**	0.074	0.199	**	**	0.083	0.266	**	**	0.114	0.238	**	**	0.158	0.336	**	**	0.084
	S10	0.065	0.006	0.033	0.033	0.074	0.006	0.037	0.038	0.098	0.009	0.051	0.052	0.088	0.012	0.071	0.072	0.124	0.017	0.103	0.076

	S3	0.156	**	0.096	0.109	0.176	**	0.108	0.123	0.235	**	0.148	0.169	0.210	**	0.205	0.234	0.297	**	0.296	0.113
	S11	0.075	0.050	0.034	0.243	0.085	0.056	0.038	0.274	0.113	0.077	0.052	0.376	0.101	0.108	0.073	0.522	0.143	0.155	0.105	0.754
	S4	0.178	0.108	0.062	**	0.200	0.122	0.070	**	0.267	0.167	0.096	**	0.239	0.233	0.134	**	0.338	0.336	0.194	**
	S12	0.087	0.048	0.035	**	0.098	0.055	0.039	**	0.131	0.075	0.054	**	0.117	0.104	0.075	**	0.166	0.150	0.108	**
7	S1	0.368	**	**	0.224	0.414	**	**	0.252	0.553	**	**	0.347	0.495	**	**	0.481	0.699	**	**	0.695
	S9	0.277	**	**	0.174	0.312	**	**	0.195	0.416	**	**	0.268	0.373	**	**	0.373	0.527	**	**	0.538
	S2	0.199	**	**	0.078	0.224	**	**	0.087	0.299	**	**	0.120	0.268	**	**	0.166	0.378	**	**	0.089
	S10	0.086	0.008	0.034	0.038	0.097	0.009	0.038	0.043	0.129	0.013	0.052	0.059	0.115	0.018	0.073	0.083	0.163	0.025	0.105	0.081
	S3	0.174	**	0.096	0.112	0.195	**	0.108	0.126	0.260	**	0.149	0.173	0.233	**	0.207	0.240	0.330	**	0.299	0.117
	S11	0.097	0.057	0.037	0.262	0.109	0.064	0.042	0.294	0.145	0.088	0.058	0.404	0.130	0.122	0.080	0.561	0.183	0.176	0.116	0.811
	S4	0.199	0.113	0.065	**	0.224	0.127	0.073	**	0.299	0.174	0.100	**	0.268	0.242	0.139	**	0.378	0.349	0.201	**
	S12	0.115	0.057	0.040	**	0.129	0.064	0.045	**	0.173	0.088	0.062	**	0.155	0.122	0.086	**	0.218	0.177	0.124	**
6	S1	0.399	**	**	0.234	0.449	**	**	0.263	0.599	**	**	0.362	0.537	**	**	0.502	0.758	**	**	0.726
	S9	0.307	**	**	0.185	0.345	**	**	0.208	0.460	**	**	0.286	0.413	**	**	0.397	0.582	**	**	0.574
	S2	0.218	**	**	0.081	0.246	**	**	0.091	0.327	**	**	0.125	0.293	**	**	0.174	0.414	**	**	0.091
	S10	0.103	0.013	0.033	0.042	0.115	0.015	0.037	0.047	0.154	0.020	0.051	0.065	0.138	0.028	0.071	0.090	0.195	0.040	0.102	0.081
	S3	0.192	**	0.096	0.115	0.216	**	0.108	0.129	0.287	**	0.148	0.178	0.258	**	0.206	0.247	0.364	**	0.297	0.125
	S11	0.118	0.064	0.041	0.281	0.133	0.072	0.046	0.317	0.177	0.099	0.063	0.435	0.159	0.138	0.088	0.604	0.224	0.199	0.127	0.872
	S4	0.219	0.115	0.067	**	0.246	0.130	0.076	**	0.329	0.178	0.104	**	0.295	0.248	0.145	**	0.416	0.358	0.209	**
	S12	0.137	0.064	0.044	**	0.154	0.071	0.049	**	0.205	0.098	0.068	**	0.184	0.136	0.094	**	0.260	0.197	0.136	**

5	S1	0.428	**	**	0.243	0.482	**	**	0.274	0.642	**	**	0.376	0.576	**	**	0.522	0.813	**	**	0.754
	S9	0.337	**	**	0.197	0.379	**	**	0.221	0.506	**	**	0.304	0.453	**	**	0.422	0.640	**	**	0.610
	S2	0.235	**	**	0.083	0.264	**	**	0.094	0.352	**	**	0.129	0.316	**	**	0.179	0.446	**	**	0.092
	S10	0.118	0.019	0.032	0.045	0.133	0.021	0.036	0.051	0.177	0.029	0.049	0.069	0.159	0.040	0.069	0.096	0.225	0.058	0.099	0.083
	S3	0.208	**	0.097	0.118	0.234	**	0.109	0.132	0.312	**	0.150	0.182	0.280	**	0.208	0.252	0.395	**	0.300	0.134
	S11	0.136	0.070	0.043	0.298	0.153	0.079	0.049	0.335	0.203	0.109	0.067	0.460	0.182	0.151	0.093	0.639	0.257	0.218	0.134	0.922
	S4	0.237	0.117	0.069	**	0.267	0.132	0.078	**	0.356	0.181	0.107	**	0.319	0.251	0.149	**	0.450	0.363	0.215	**
	S12	0.157	0.069	0.047	**	0.177	0.077	0.053	**	0.236	0.106	0.073	**	0.211	0.148	0.101	**	0.298	0.213	0.146	**
4	S1	0.455	**	**	0.250	0.512	**	**	0.281	0.682	**	**	0.386	0.611	**	**	0.536	0.863	**	**	0.775
	S9	0.366	**	**	0.206	0.411	**	**	0.232	0.549	**	**	0.318	0.492	**	**	0.442	0.694	**	**	0.639
	S2	0.249	**	**	0.085	0.280	**	**	0.095	0.374	**	**	0.131	0.335	**	**	0.182	0.473	**	**	0.091
	S10	0.134	0.023	0.031	0.048	0.151	0.026	0.035	0.054	0.201	0.036	0.048	0.074	0.180	0.050	0.067	0.102	0.254	0.072	0.097	0.087
	S3	0.223	**	0.097	0.119	0.251	**	0.109	0.134	0.334	**	0.150	0.183	0.300	**	0.208	0.255	0.423	**	0.300	0.142
	S11	0.150	0.074	0.045	0.308	0.169	0.083	0.050	0.347	0.225	0.115	0.069	0.476	0.202	0.159	0.096	0.661	0.285	0.230	0.138	0.955
	S4	0.253	0.117	0.070	**	0.284	0.132	0.079	**	0.379	0.181	0.109	**	0.340	0.252	0.151	**	0.480	0.363	0.218	**
	S12	0.177	0.073	0.050	**	0.199	0.083	0.056	**	0.266	0.113	0.077	**	0.238	0.157	0.106	**	0.336	0.227	0.154	**
3	S1	0.484	**	**	0.256	0.545	**	**	0.288	0.726	**	**	0.395	0.651	**	**	0.549	0.919	**	**	0.793
	S9	0.392	**	**	0.212	0.441	**	**	0.239	0.588	**	**	0.328	0.527	**	**	0.455	0.744	**	**	0.657
	S2	0.261	**	**	0.085	0.294	**	**	0.095	0.392	**	**	0.131	0.351	**	**	0.182	0.496	**	**	0.093
	S10	0.148	0.027	0.030	0.049	0.167	0.030	0.034	0.056	0.222	0.041	0.047	0.076	0.199	0.057	0.065	0.106	0.281	0.082	0.094	0.090

	S3	0.235	**	0.096	0.118	0.265	**	0.107	0.133	0.353	**	0.148	0.183	0.317	**	0.205	0.254	0.447	**	0.296	0.146
	S11	0.163	0.076	0.045	0.314	0.183	0.086	0.051	0.354	0.244	0.118	0.070	0.486	0.219	0.164	0.097	0.675	0.309	0.237	0.140	0.974
	S4	0.266	0.116	0.070	**	0.299	0.130	0.079	**	0.398	0.179	0.109	**	0.357	0.248	0.151	**	0.504	0.358	0.218	**
	S12	0.195	0.076	0.051	**	0.219	0.085	0.057	**	0.292	0.117	0.079	**	0.262	0.163	0.109	**	0.370	0.235	0.158	**
2	S1	0.512	**	**	0.258	0.575	**	**	0.290	0.767	**	**	0.399	0.688	**	**	0.554	0.971	**	**	0.800
	S9	0.413	**	**	0.214	0.465	**	**	0.241	0.620	**	**	0.331	0.556	**	**	0.459	0.785	**	**	0.664
	S2	0.270	**	**	0.084	0.304	**	**	0.094	0.405	**	**	0.130	0.363	**	**	0.180	0.513	**	**	0.095
	S10	0.160	0.029	0.029	0.050	0.180	0.032	0.033	0.057	0.240	0.044	0.045	0.078	0.215	0.062	0.063	0.108	0.303	0.089	0.091	0.093
	S3	0.244	**	0.093	0.116	0.275	**	0.104	0.130	0.367	**	0.143	0.179	0.329	**	0.199	0.248	0.464	**	0.288	0.148
	S11	0.173	0.077	0.045	0.314	0.194	0.086	0.050	0.353	0.259	0.118	0.069	0.484	0.232	0.165	0.096	0.673	0.327	0.238	0.139	0.972
	S4	0.275	0.112	0.069	**	0.310	0.127	0.078	**	0.413	0.174	0.107	**	0.370	0.241	0.149	**	0.522	0.349	0.215	**
	S12	0.209	0.077	0.051	**	0.236	0.086	0.058	**	0.314	0.119	0.079	**	0.282	0.165	0.110	**	0.397	0.238	0.160	**
1	S1	0.521	**	**	0.253	0.586	**	**	0.285	0.781	**	**	0.391	0.700	**	**	0.543	0.989	**	**	0.785
	S9	0.420	**	**	0.210	0.473	**	**	0.236	0.631	**	**	0.324	0.565	**	**	0.450	0.798	**	**	0.650
	S2	0.272	**	**	0.081	0.306	**	**	0.091	0.408	**	**	0.126	0.365	**	**	0.174	0.516	**	**	0.094
	S10	0.165	0.029	0.028	0.049	0.185	0.033	0.031	0.056	0.247	0.045	0.043	0.076	0.221	0.062	0.060	0.106	0.312	0.090	0.087	0.092
	S3	0.246	**	0.089	0.111	0.277	**	0.100	0.125	0.369	**	0.137	0.172	0.331	**	0.190	0.239	0.467	**	0.275	0.145
	S11	0.175	0.075	0.043	0.304	0.197	0.084	0.049	0.342	0.263	0.115	0.067	0.469	0.236	0.160	0.093	0.652	0.333	0.231	0.134	0.941
	S4	0.277	0.107	0.067	**	0.312	0.121	0.075	**	0.415	0.166	0.103	**	0.372	0.231	0.144	**	0.526	0.333	0.207	**
	S12	0.215	0.075	0.050	**	0.242	0.084	0.057	**	0.322	0.116	0.078	**	0.289	0.161	0.108	**	0.408	0.232	0.156	**

Çizelge 3.42: 9 Katlı Hastane Binasının İstanbul İlinde Bulunduğu Duruma Ait k_E Değerleri.

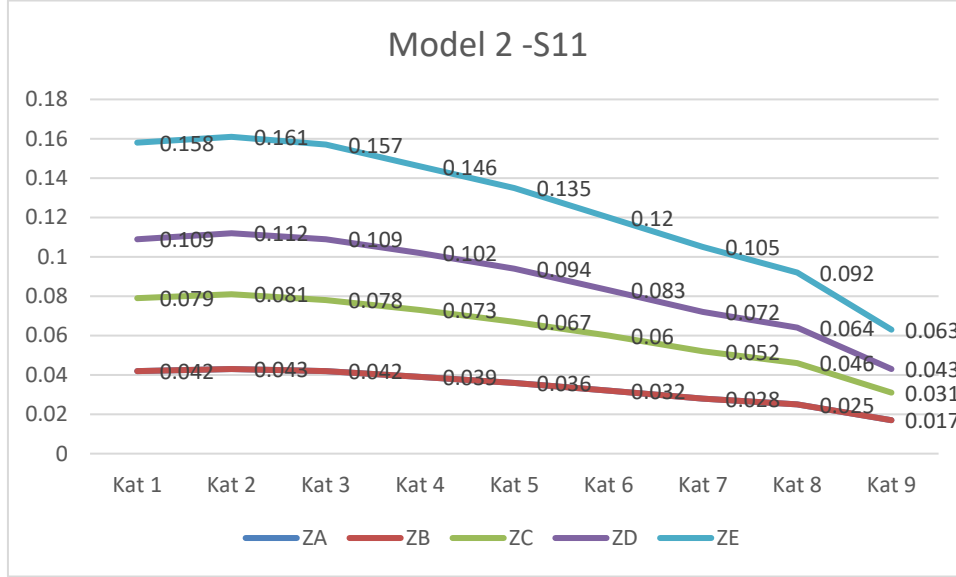
$k_E = N_E / N_{G0} + Q_0$																					
KAT	KOLON	keZA				keZB				keZC				keZD				keZE			
		Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4	Model 1	Model 2	Model 3	Model 4
9	S1	0.076	**	**	0.088	0.085	**	**	0.088	0.114	**	**	0.165	0.141	**	**	0.228	0.204	**	**	0.329
	S9	0.050	**	**	0.066	0.056	**	**	0.066	0.075	**	**	0.125	0.093	**	**	0.173	0.134	**	**	0.249
	S2	0.045	**	**	0.023	0.051	**	**	0.023	0.068	**	**	0.043	0.085	**	**	0.060	0.122	**	**	0.086
	S10	0.004	0.018	0.017	0.017	0.005	0.018	0.017	0.017	0.006	0.034	0.033	0.032	0.008	0.048	0.045	0.045	0.011	0.069	0.066	0.064
	S3	0.041	**	0.054	0.044	0.046	**	0.054	0.044	0.061	**	0.101	0.083	0.076	**	0.139	0.116	0.110	**	0.201	0.167
	S11	0.006	0.017	0.011	0.131	0.007	0.017	0.011	0.131	0.009	0.031	0.021	0.246	0.012	0.043	0.029	0.341	0.017	0.063	0.042	0.492
	S4	0.044	0.061	0.022	**	0.050	0.061	0.022	**	0.066	0.115	0.042	**	0.082	0.159	0.058	**	0.119	0.230	0.083	**
	S12	0.007	0.011	0.012	**	0.007	0.011	0.012	**	0.010	0.020	0.022	**	0.012	0.028	0.030	**	0.018	0.040	0.043	**
8	S1	0.136	**	**	0.127	0.153	**	**	0.127	0.203	**	**	0.237	0.253	**	**	0.329	0.365	**	**	0.475
	S9	0.094	**	**	0.095	0.106	**	**	0.095	0.141	**	**	0.179	0.175	**	**	0.248	0.253	**	**	0.358
	S2	0.070	**	**	0.034	0.079	**	**	0.034	0.105	**	**	0.064	0.131	**	**	0.088	0.189	**	**	0.127
	S10	0.019	0.011	0.020	0.023	0.022	0.011	0.020	0.023	0.029	0.021	0.038	0.044	0.036	0.028	0.052	0.061	0.052	0.041	0.076	0.087
	S3	0.064	**	0.056	0.053	0.072	**	0.056	0.053	0.096	**	0.105	0.100	0.120	**	0.145	0.138	0.173	**	0.209	0.200
	S11	0.022	0.025	0.016	0.164	0.024	0.025	0.016	0.164	0.032	0.046	0.029	0.307	0.040	0.064	0.041	0.426	0.058	0.092	0.059	0.615
	S4	0.071	0.059	0.030	**	0.079	0.059	0.030	**	0.106	0.111	0.056	**	0.132	0.154	0.077	**	0.190	0.222	0.111	**
	S12	0.025	0.022	0.017	**	0.028	0.022	0.017	**	0.038	0.040	0.031	**	0.047	0.056	0.043	**	0.068	0.081	0.062	**

7	S1	0.191	**	**	0.143	0.215	**	**	0.143	0.287	**	**	0.268	0.356	**	**	0.372	0.514	**	**	0.536
	S9	0.135	**	**	0.108	0.152	**	**	0.108	0.202	**	**	0.202	0.252	**	**	0.280	0.363	**	**	0.404
	S2	0.094	**	**	0.038	0.106	**	**	0.038	0.142	**	**	0.071	0.176	**	**	0.099	0.254	**	**	0.143
	S10	0.032	0.009	0.021	0.027	0.037	0.009	0.021	0.027	0.049	0.017	0.040	0.051	0.061	0.024	0.056	0.071	0.087	0.034	0.080	0.102
	S3	0.085	**	0.057	0.056	0.096	**	0.057	0.056	0.127	**	0.107	0.106	0.158	**	0.148	0.147	0.228	**	0.214	0.212
	S11	0.035	0.028	0.017	0.181	0.039	0.028	0.017	0.181	0.052	0.052	0.032	0.340	0.065	0.072	0.045	0.471	0.093	0.105	0.065	0.679
	S4	0.094	0.063	0.032	**	0.106	0.063	0.032	**	0.141	0.118	0.061	**	0.175	0.163	0.084	**	0.253	0.236	0.121	**
	S12	0.041	0.026	0.018	**	0.046	0.026	0.018	**	0.062	0.048	0.034	**	0.077	0.066	0.048	**	0.111	0.096	0.069	**
6	S1	0.234	**	**	0.154	0.264	**	**	0.154	0.352	**	**	0.289	0.437	**	**	0.400	0.630	**	**	0.578
	S9	0.170	**	**	0.118	0.192	**	**	0.118	0.256	**	**	0.222	0.318	**	**	0.307	0.458	**	**	0.443
	S2	0.117	**	**	0.042	0.131	**	**	0.042	0.175	**	**	0.078	0.218	**	**	0.108	0.314	**	**	0.156
	S10	0.048	0.006	0.021	0.029	0.054	0.006	0.021	0.029	0.071	0.011	0.040	0.054	0.089	0.015	0.055	0.076	0.128	0.022	0.079	0.109
	S3	0.102	**	0.057	0.059	0.115	**	0.057	0.059	0.153	**	0.108	0.110	0.190	**	0.149	0.153	0.275	**	0.215	0.220
	S11	0.051	0.032	0.019	0.196	0.058	0.032	0.019	0.196	0.077	0.060	0.036	0.368	0.096	0.083	0.051	0.511	0.138	0.120	0.073	0.737
	S4	0.116	0.066	0.035	**	0.130	0.066	0.035	**	0.173	0.123	0.065	**	0.216	0.171	0.090	**	0.311	0.247	0.130	**
	S12	0.061	0.030	0.020	**	0.068	0.030	0.020	**	0.091	0.057	0.038	**	0.113	0.079	0.052	**	0.164	0.114	0.076	**
5	S1	0.270	**	**	0.162	0.304	**	**	0.162	0.405	**	**	0.304	0.504	**	**	0.421	0.727	**	**	0.607
	S9	0.201	**	**	0.127	0.226	**	**	0.127	0.302	**	**	0.238	0.375	**	**	0.329	0.541	**	**	0.475
	S2	0.137	**	**	0.044	0.154	**	**	0.044	0.205	**	**	0.083	0.255	**	**	0.115	0.368	**	**	0.166
	S10	0.062	0.003	0.021	0.030	0.070	0.003	0.021	0.030	0.093	0.005	0.039	0.056	0.115	0.008	0.055	0.078	0.167	0.011	0.079	0.113
	S3	0.117	**	0.057	0.060	0.131	**	0.057	0.060	0.175	**	0.107	0.113	0.217	**	0.149	0.156	0.313	**	0.214	0.225

	S11	0.068	0.036	0.022	0.209	0.077	0.036	0.022	0.209	0.102	0.067	0.040	0.392	0.127	0.094	0.056	0.544	0.183	0.135	0.081	0.784
	S4	0.136	0.068	0.037	**	0.153	0.068	0.037	**	0.203	0.128	0.069	**	0.253	0.177	0.095	**	0.365	0.256	0.138	**
	S12	0.080	0.035	0.023	**	0.090	0.035	0.023	**	0.120	0.065	0.043	**	0.149	0.090	0.059	**	0.215	0.130	0.086	**
4	S1	0.298	**	**	0.166	0.335	**	**	0.166	0.447	**	**	0.311	0.556	**	**	0.432	0.802	**	**	0.623
	S9	0.228	**	**	0.133	0.257	**	**	0.133	0.343	**	**	0.249	0.426	**	**	0.346	0.615	**	**	0.499
	S2	0.153	**	**	0.046	0.172	**	**	0.046	0.230	**	**	0.086	0.286	**	**	0.119	0.412	**	**	0.172
	S10	0.078	0.004	0.021	0.031	0.088	0.004	0.021	0.031	0.117	0.007	0.039	0.057	0.145	0.010	0.055	0.080	0.209	0.014	0.079	0.115
	S3	0.129	**	0.056	0.061	0.146	**	0.056	0.061	0.194	**	0.106	0.114	0.241	**	0.147	0.158	0.348	**	0.212	0.227
	S11	0.085	0.039	0.023	0.219	0.095	0.039	0.023	0.219	0.127	0.073	0.043	0.410	0.158	0.102	0.060	0.568	0.228	0.146	0.087	0.820
	S4	0.152	0.069	0.038	**	0.171	0.069	0.038	**	0.228	0.130	0.071	**	0.283	0.180	0.098	**	0.408	0.260	0.141	**
	S12	0.101	0.039	0.025	**	0.114	0.039	0.025	**	0.152	0.073	0.048	**	0.189	0.101	0.066	**	0.273	0.146	0.095	**
3	S1	0.321	**	**	0.168	0.361	**	**	0.168	0.481	**	**	0.316	0.598	**	**	0.438	0.862	**	**	0.631
	S9	0.250	**	**	0.137	0.281	**	**	0.137	0.375	**	**	0.257	0.467	**	**	0.356	0.673	**	**	0.514
	S2	0.167	**	**	0.047	0.188	**	**	0.047	0.251	**	**	0.087	0.311	**	**	0.121	0.449	**	**	0.175
	S10	0.090	0.006	0.020	0.030	0.102	0.006	0.020	0.030	0.136	0.012	0.038	0.056	0.169	0.016	0.053	0.078	0.243	0.023	0.076	0.112
	S3	0.142	**	0.055	0.061	0.160	**	0.055	0.061	0.213	**	0.103	0.114	0.265	**	0.142	0.158	0.383	**	0.205	0.228
	S11	0.101	0.042	0.025	0.226	0.113	0.042	0.025	0.226	0.151	0.078	0.046	0.423	0.188	0.109	0.064	0.587	0.271	0.157	0.092	0.846
	S4	0.166	0.069	0.038	**	0.187	0.069	0.038	**	0.249	0.129	0.071	**	0.309	0.179	0.099	**	0.446	0.258	0.143	**
	S12	0.118	0.041	0.027	**	0.133	0.041	0.027	**	0.177	0.078	0.051	**	0.220	0.108	0.070	**	0.318	0.155	0.101	**
2	S1	0.339	**	**	0.168	0.381	**	**	0.168	0.508	**	**	0.314	0.632	**	**	0.436	0.911	**	**	0.628
	S9	0.270	**	**	0.138	0.304	**	**	0.138	0.405	**	**	0.260	0.504	**	**	0.360	0.727	**	**	0.519

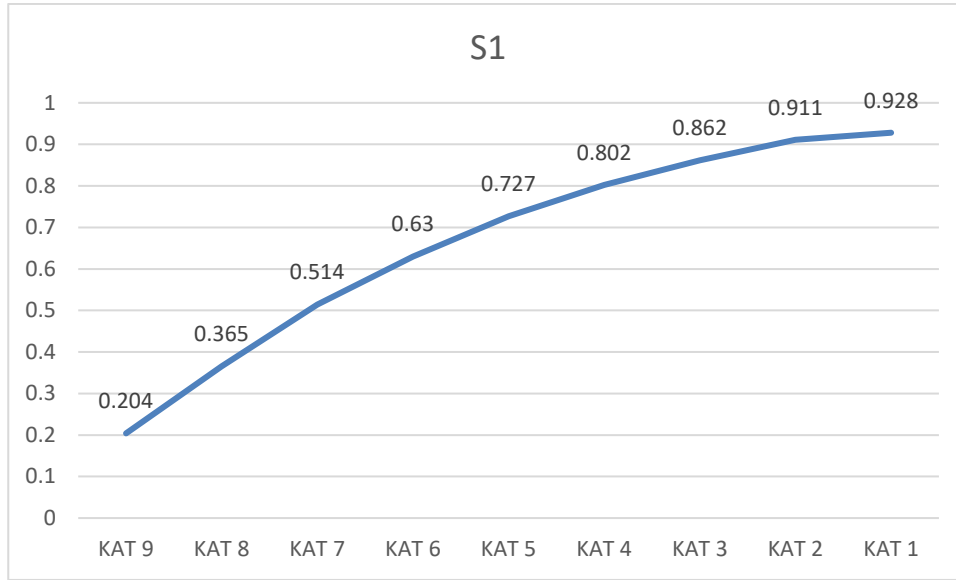
	S2	0.177	**	**	0.046	0.199	**	**	0.046	0.266	**	**	0.087	0.331	**	**	0.120	0.477	**	**	0.174
	S10	0.101	0.008	0.019	0.030	0.114	0.008	0.019	0.030	0.151	0.016	0.036	0.057	0.188	0.022	0.050	0.079	0.272	0.032	0.072	0.113
	S3	0.153	**	0.052	0.060	0.172	**	0.052	0.060	0.229	**	0.098	0.112	0.285	**	0.135	0.156	0.410	**	0.195	0.225
	S11	0.113	0.043	0.025	0.226	0.127	0.043	0.025	0.226	0.169	0.081	0.047	0.424	0.210	0.112	0.065	0.587	0.303	0.161	0.093	0.847
	S4	0.177	0.067	0.038	**	0.199	0.067	0.038	**	0.266	0.126	0.071	**	0.330	0.174	0.098	**	0.477	0.252	0.142	**
	S12	0.132	0.042	0.027	**	0.148	0.042	0.027	**	0.198	0.079	0.051	**	0.246	0.110	0.071	**	0.354	0.158	0.103	**
1	S1	0.345	**	**	0.162	0.388	**	**	0.162	0.518	**	**	0.303	0.644	**	**	0.420	0.928	**	**	0.606
	S9	0.281	**	**	0.135	0.316	**	**	0.135	0.422	**	**	0.254	0.524	**	**	0.352	0.756	**	**	0.508
	S2	0.181	**	**	0.045	0.203	**	**	0.045	0.271	**	**	0.084	0.337	**	**	0.116	0.487	**	**	0.167
	S10	0.108	0.010	0.018	0.030	0.121	0.010	0.018	0.030	0.162	0.019	0.034	0.056	0.201	0.026	0.047	0.078	0.290	0.037	0.068	0.112
	S3	0.157	**	0.049	0.058	0.177	**	0.049	0.058	0.235	**	0.091	0.108	0.293	**	0.127	0.150	0.422	**	0.183	0.216
	S11	0.119	0.042	0.024	0.217	0.133	0.042	0.024	0.217	0.178	0.079	0.046	0.406	0.221	0.109	0.063	0.563	0.319	0.158	0.091	0.812
	S4	0.182	0.064	0.037	**	0.204	0.064	0.037	**	0.273	0.120	0.068	**	0.339	0.166	0.095	**	0.489	0.239	0.137	**
	S12	0.140	0.042	0.027	**	0.158	0.042	0.027	**	0.211	0.078	0.051	**	0.262	0.108	0.071	**	0.378	0.156	0.102	**

İstanbul da 9 katlı binanın Model 2, S11 kolonuna ait k_E oranının zemin sınıflarına göre değişimi grafik olarak Şekil 3.9'da verilmiştir. Görüldüğü gibi ZA ve ZB sınıfına ait değerler yaklaşık olarak aynı olmaktadır.

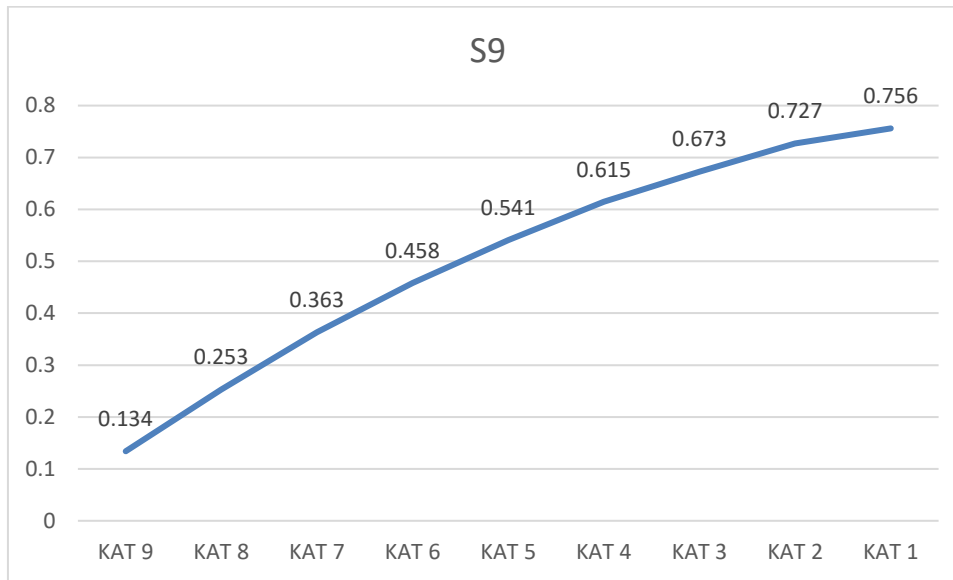


Şekil 3.9: Model 2 için S11 kolonuna ait k_E Oranını Zemin Sınıfına Göre Değişim Grafiği.

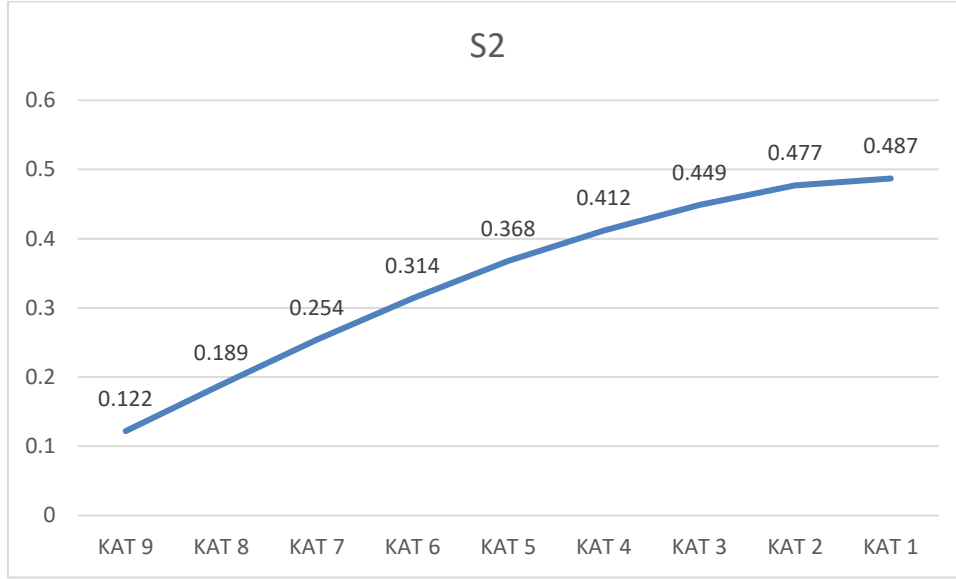
Kolonlarında Model 1 ait 9 katlı binanın sırayla S1, S9, S2, S10, S3, S4, S11 ve S12 kolonlarında ZE zemini ile ilgili k_E oranlarının değişimi Şekil 3.10 ila Şekil 3.17 da grafik olarak gösterilmiştir.



Şekil 3.10: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S1 kolonuna ait k_E Oranın Grafiği.



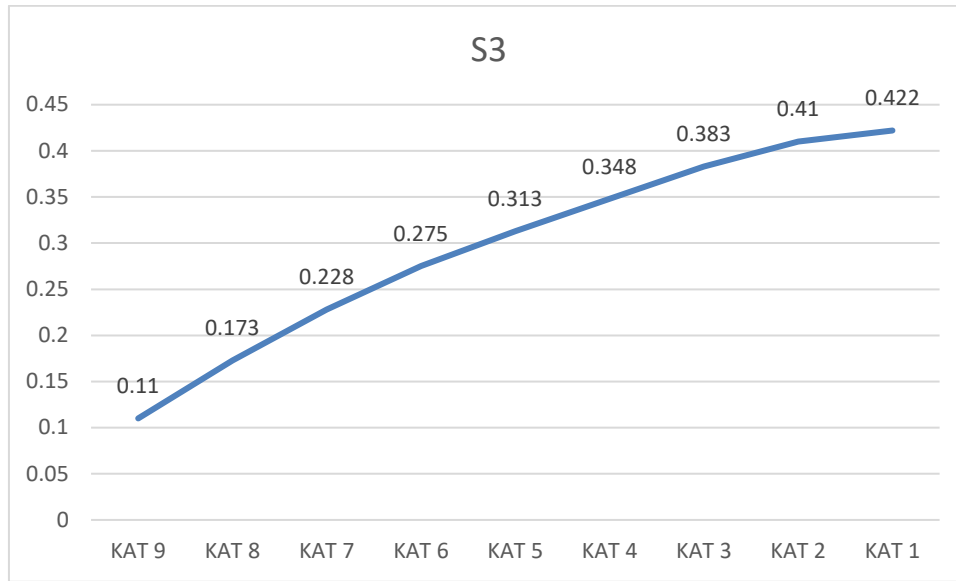
Şekil 3.11: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S9 kolonuna ait k_E Oranın Grafiği.



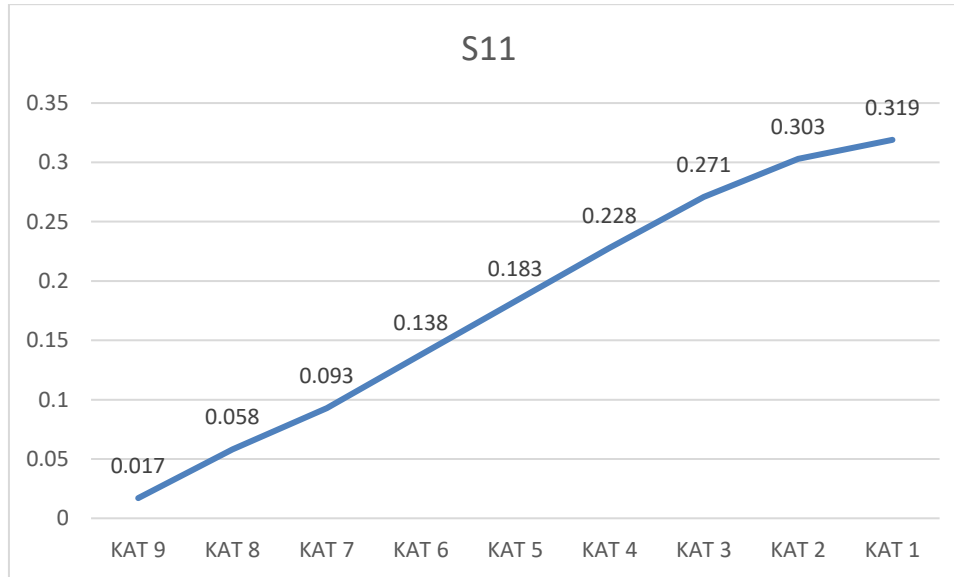
Şekil 3.12: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S2 kolonuna ait k_E Oranın Grafiği.



Şekil 3.13: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S10 kolonuna ait k_E Oranın Grafiği.



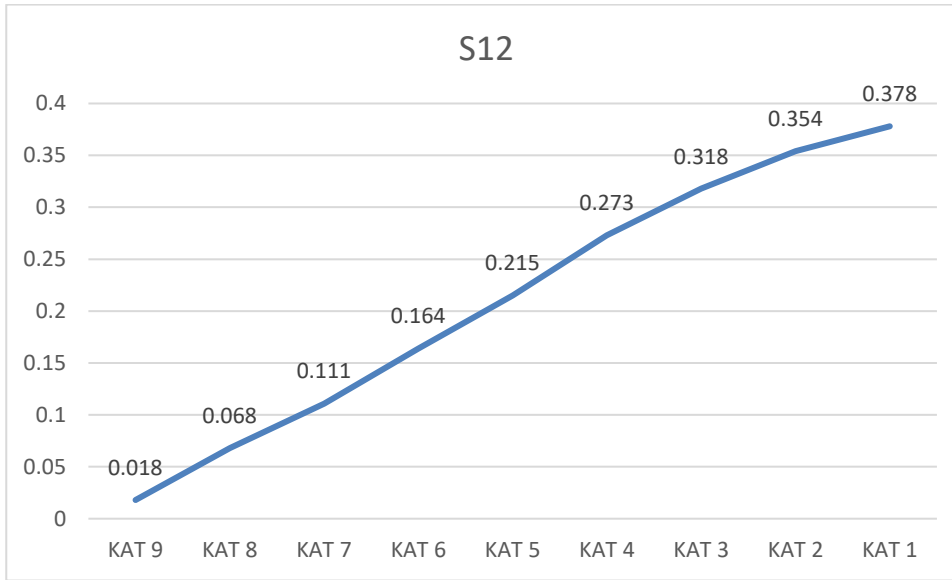
Şekil 3.14: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S3 kolonuna ait K_E Oranın Grafiği.



Şekil 3.15: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S11 kolonuna ait k_E Oranın Grafiği.



Şekil 3.16: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S4 kolonuna ait k_E Oranın Grafiği.



Şekil 3.17: 9 katlı İstanbul Model 1 ZE Zemin Sınıfı için S12 kolonuna ait k_E Oranın Grafiği.

3.5.3. k_p , k_E , k_{vt} , β , N_{G0} ve N_{Q0} değerlerine bağlı olarak Kolon enkesiti için gerekli N_{dm} eksenel kuvvetinin hesabı

Yapıların kolon brüt en kesit alanını hesaplamak için kullanılan N_{dm} , TBDY 2018'e göre $G + Q + E$ tanımlanmaktadır. Bu tez kapsamında sunulan oranlar kullanılarak yapıların $G_0 + Q_0$ yüküyle çarpılmasıyla, kolonlarda meydana gelen deprem etkisinden kaynaklanan eksenel basınç kuvveti yaklaşık olarak hesaplandığında, kolon en kesit alanlarının gerçek değerlerle tasarımın uyumlu olduğu görülmüştür. Bu sayede, kolonlar için belirtilen k_p ve k_E oranları kullanılarak N_{dm} değeri aşağıdaki eşitliklerle hesaplanabilir.

$$N_G + \beta N_Q = k_p \times N_{(G_0 + \beta Q_0)} \quad (3.5)$$

$$N_E = k_E \times N_{(G_0 + \beta Q_0)} \quad (3.6)$$

$$N_{dm} = N_G + \beta N_Q + N_E \quad (3.7)$$

Veya

$$N_{dm} = (k_{p\beta} + k_{EZC}) (G_0 + \beta Q_0) \quad (3.8)$$

ZA sınıfı k_{ZA} değerleri, G_0 ve Q_0 değerleri, $k_{p\beta}$ değerleri, k_{vt} değerlerine bağlı olarak ZC sınıfı bir zeminde kolanlarının gerekli alanlarını bulmak için kullanılacak eksenel kuvvetle

$$N_{EZA} = k_{ZA} \times N_{(G_0 + \beta Q_0)} \quad (3.9)$$

$$N_{EZC} = N_{EZA} \times k_{vt} \quad (3.10)$$

$$N_{dm} = N_{(G + \beta Q)} + N_{ZC} \quad (3.11)$$

Veya

$$N_{dm} = (k_{p\beta} + k_{EZA} \times k_{vt}) (G_0 + \beta Q_0) \quad (3.12)$$

Eşitliklerinden hesaplanır.

3.5.4. Örnekler

Örnek1

Çizelgelerde verilen k değerleri ve G_0 ve Q_0 değerleri kullanılarak ZC sınıfı bir zeminde S1 kolonun 6.kat ve zemin katındaki boyutlarının hesabı:

6.Kat

6. Katta Çizelge 3.14'ten $N_{G0} = 101,95$, $N_{Q0} = 26,25$ alınır. 6.katlı bina için bina azaltma katsayısı $\beta = 0,8$ dir. Çizelge 3.15'ten $k_{p\beta} = 0,925$ ve Çizelge 3.35'ten $k_{EZC} = 0,131$ alınır.

Buna göre:

$$\beta N_{Q0} = 0,8 \times 26,25 = 21,00, \text{ ve } N_{(G0 + \beta Q0)} = 101,95 + 21,000 = 122,95 \text{ kN bulunur.}$$

Depren etkisinden meydana gelen aksenal kuvvet

$$N_{EZC} = 0,131 \times 122,95 = 16,106 \text{ kN,}$$

TBDY 2018'e göre boyutlandırma da göz önüne alınacak aksenal kuvvet

$$N_{(G + \beta Q)} = 0,925 \times 122,95 = 113,729 \text{ kNm}$$

$$N_{dm} = N_G + \beta N_Q + N_E = 113,729 + 16,106 = 129,835 \text{ kN}$$

Veya

$$N_{dm} = (k_{p\beta} + k_{EZC}) (G_0 + \beta Q_0) = (0,925 + 0,131) (101,95 + 0,8 \times 26,25) = 129,835 \text{ kN}$$

$$A_C = 129,835 / (0,4 \times 3) = 108,20 \text{ cm}^2$$

Bulunur.

1. Kat

1.katta Çizelge 3.14'ten $N_{G0} = 611,7 \text{ kN}$, $N_{Q0} = 157,5 \text{ kN}$ alınır. 6.katlı bina için bina azaltma katsayısı $\beta = 0,8$ 'dir. Çizelge 3.15'ten $k_{p\beta} = 0,968$ ve Çizelge 3.35'ten $k_{ZC} = 0,454$ alınır.

Buna göre:

$$\beta N_{Q0} = 0,8 \times 157,5 = 126,000 \text{ kN, ve } N_{(G0 + \beta Q0)} = 611,700 + 126,000 = 737,700 \text{ kN bulunur.}$$

Deprem etkisinden meydana gelen aksenal kuvvet

$$N_{EZC} = 0,454 \times 737,700 = 334,916 \text{ kN,}$$

TBDY 2018'e göre boyutlandırma da göz önüne alınacak aksenal kuvvet

$$N_{(G + \beta Q)} = 0,968 \times 737,700 = 714,094 \text{ kN}$$

$$N_{dm} = N_G + \beta N_Q + N_E = 714,09 + 334,916 = 1049,01 \text{ kN}$$

Veya

$$N_{dm} = (k_{p\beta} + k_{EZC}) (G_0 + \beta Q_0) = (0,968 + 0,454) (611,700 + 0,8 \times 157,500) = 1049,010 \text{ kN}$$

$$A_C = 1049,10 / (0,4 \times 3) = 874 \text{ cm}^2$$

Bulunur.

Model 1 de $k_{p\beta}$, ZC sınıfı zeminlerdeki k_{EZC} , β azaltma sayısı ve G_0 ve Q_0 değerleri gözönüne alınarak S1 ve S10 kolonları enkesitleri Çizelge 3.26'da verilmiştir.

Çizelge 3.43: Model 1 için Deprem etkisi de göz önüne alınarak S1 ve S10 kolonları enkesitleri.

Kolon	KAT	N_{G0} (kN)	N_{Q0} (kN)	β	βN_{Q0} (kN)	$N_{(G0 + \beta Q0)}$ (kN)	$k_{p\beta}$	$N_{(G + \beta Q)}$ (kN)	k_{ZC}	$N_E = k_{ZC} \cdot N_{(G0 + \beta Q0)}$ (kN)	$N_{dm} = N_G + \beta N_Q + N_E$ (kN)	$A_C = N_{dm} / (0,4 f_{ck})$ (cm ²)
S1	6.KAT	101,95	26,25	0,8	21,000	122,95	0,925	113,729	0,131	16,106	129,835	108,20
	5.KAT	203,9	52,5	0,8	42,000	245,900	0,962	236,556	0,229	56,3111	292,867	244,06
	4.KAT	305,85	78,75	0,8	63	368,85	0,97	357,7845	0,318	113,775471	471,560	392,97
	3.KAT	407,8	105	0,8	84,000	491,8	0,972	478,030	0,386	189,8348	667,8644	556,55
	2.KAT	509,75	131,25	0,8	105,000	614,75	0,972	597,537	0,433	266,18675	863,72375	719,77
	1.KAT	611,7	157,5	0,8	126,000	737,7	0,968	714,094	0,454	334,916	1049,01	874,00
S10	6.KAT	242,76	112,75	0,8	90,160	332,96	1,111	369,586	0,02	6,659	374,24	313,54
	5.KAT	485,52	225,5	0,8	180,400	665,920	1,091	726,519	0,046	30,63232	757,15104	630,96
	4.KAT	728,28	338,25	0,8	270,600	998,88	1,088	1086,781	0,067	66,92496	1153,7064	961,42
	3.KAT	971,04	451	0,8	360,800	1331,84	1,088	1449,042	0,09	119,8656	1568,90752	1307,42
	2.KAT	1213,8	563,75	0,8	451,000	1664,8	1,088	1811,302	0,111	184,7928	1996,0952	1663,41
	1.KAT	1456,56	676,5	0,8	541,200	1997,76	1,092	2181,554	0,126	221,751	2403,305	2002,75

Örnek 2

Çizelgelerde verilen ZA sınıfı k_{ZA} değerleri, G_0 ve Q_0 değerleri, $k_{p\beta}$ değerleri k_{Vt} değerleri kullanılarak ZC sınıfı bir zeminde S1 ve S10 kolanlarının gerekli alanlarının hesabı:

S1Kolonu

6.Kat

Çizelge 3.15 den $N_{G0} = 101,95 \text{ kN}$, $N_{Q0} = 26,25 \text{ kN}$, $k_{p\beta} = 0,919$ ve Çizelge 3.35'ten $k_{EZA} = 0,072$, Çizelge 3.1'den $k_{VtZC}/k_{VtZA} = 1,824$ alınır.

6 katlı bina için hareketli yük azaltma sayısı $\beta = 0,8$ 'dir.

Bu değerlere göre

$$N_{(G_0 + \beta Q_0)} = 101,95 + 0,8 \times 26,25 = 122,950 \text{ kN}$$

$$k_{p\beta} \times N_{(G + \beta Q)} = 0,919 \times 122,950 = 112,99 \text{ kN}$$

$$N_{ZA} = k_{ZA} \times N_{(G_0 + \beta Q_0)} = 122,950 \times 0,072 = 8,852 \text{ kN}, N_{ZC} = N_{EZA} \times k_{vt} = 8,852 \times 1,824 = 16,147 \text{ kN}$$

$$N_{dm} = k_{p\beta} \times N_{(G + \beta Q)} + N_{ZC} = 112,990 + 16,147 = 129,138 \text{ kN}$$

Veya

$$N_{dm} = (k_{p\beta} + k_{EZA} \times k_{vt}) (N_{G_0} + \beta N_{Q_0})$$

$$N_{dm} = (0,919 + 0,072 \times 1,824) (101,95 + 0,8 \times 26,500) = 129,138 \text{ kN}$$

$$A_C = 129,138 / (0,4 \times 3) = 107,61 \text{ cm}^2$$

Bulunur.

Model 1 için Çizelgelerde verilen ZA sınıfı k_{EZA} değerleri, G_0 ve Q_0 değerleri, $k_{p\beta}$ değerleri k_{vt} değerleri kullanılarak ZC sınıfı bir zeminde S1 ve S10 kolanlarının gerekli alanları Çizelge 3.27'de verilmiştir.

Çizelge 3.44: K_{ZA} değerleri, N_{G0} ve N_{Q0} değerleri, $k_{p\beta}$ değerler k_{vt} değerleri kullanılarak ZC sınıfı bir zeminde S1 ve S10 kolanlarının gerekli alanları.

Kolon No	KAT	N_{G0} (kN)	N_{Q0} (kN)	$N_{(G0 + \beta Q0)}$ (kN)	$k_{p\beta}$	$N_{G + \beta Q} = k_{p\beta} N_{G0 + \beta Q0}$ (kN)	K_{ZA}	$N_{EZA} = k_{ZA} \times N_{(G0 + \beta Q0)}$ (kN)	k_{vt}	$N_{EZC} = N_{EZA} \times k_{vt}$ (kN)	$N_{dm} = N_G + \beta N_Q + N_E$ (kN)	$A_C = N_{dm} / 0,4 f_{ck}$ (cm ²)
S1	6.KAT	101,95	26,25	122,95	0,919	112,99105	0,072	8,852	1,824	16,147	129,138	107,61
	5.KAT	203,9	52,5	245,9	0,957	235,3263	0,126	30,983	1,824	56,514	291,840	243,20
	4.KAT	305,85	78,75	368,85	0,965	355,94025	0,174	64,180	1,824	117,064	473,004	394,17
	3.KAT	407,8	105	491,8	0,967	475,5706	0,211	103,770	1,824	189,276	664,847	554,04
	2.KAT	509,75	131,25	614,75	0,967	594,46325	0,237	145,696	1,824	265,749	860,212	716,84
	1.KAT	611,7	157,5	737,7	0,963	710,4051	0,249	183,687	1,824	335,046	1.045,451	871,21
S10	6.KAT	242,76	112,75	332,96	1,109	369,25264	0,011	3,663	1,824	6,681	375,933	313,28
	5.KAT	485,52	225,5	665,92	1,089	725,18688	0,025	16,648	1,824	30,366	755,553	629,63
	4.KAT	728,28	338,25	998,88	1,086	1084,78368	0,037	36,959	1,824	67,412	1.152,196	960,16
	3.KAT	971,04	451	1331,84	1,086	1446,37824	0,049	65,260	1,824	119,035	1.565,413	1.304,51
	2.KAT	1213,8	563,75	1664,8	1,086	1807,9728	0,061	101,553	1,824	185,232	1.993,205	1.661,00
	1.KAT	1456,56	676,5	1997,76	1,089	2175,56064	0,069	137,845	1,824	251,430	2.426,991	2.022,49

SONUÇ VE DEĞERLENDİRME

Bu çalışmada incelenen Hastane binasının analizleri ETABS programı kullanılarak gerçekleştirilmiştir. Kolonlardaki $N_G + Q$ ve bununla ilişkili $N_G + \beta Q$, $N_G + \gamma Q$ eksenel basınç kuvvetleri ETABS programından alınmıştır. Kiriş uç momentleri hesaba katılmadan hesaplanan $N_{G0} + Q_0$, $N_{G0} + \beta Q_0$ ve $N_{G0} + \gamma Q_0$ değerleri yukarıda 2.2.2.3 bölümünde elle hesaplanmıştır. $k_p = N_G + Q / N_{G0} + Q_0$, $k_p = N_G + \beta Q / N_{G0} + \beta Q_0$ ve $k_p = N_G + \gamma Q / N_{G0} + \gamma Q_0$ eşitliklerinden hesaplanmış ve 6 katlı bina için Model 1, Model2, Model3 ve Model 4 için değerler çizelge 3.14 ile 3.22'de, 9 ve 12 katlı binalar için ise Ek A bölümünde Çizelge A.1 ile A.24'te sunulmuştur.

Model 1 ve Model 4 için köşe kolonu olan S1'de k_p değerleri altıncı katta 0,92, 5. Katta 0,96, 4. Katta 0,97, 3.katta 0,97, 2. Katta 0,97 ve 1. Katta 0,96'dır. Açıklıkların yakın olduğu dış kenardaki S2 kolonunda tüm katlarda yaklaşık k_p 1,02, Açıklıkların farklı olduğu dış kenardaki S9 kolonunda k_p değeri tüm katlarda yaklaşık olarak 0,98. İçte ikinci sırada bulunan S10 kolonunda tüm katlarda yaklaşık 1,1 olmaktadır. Alt katlarda kolon boyutlarının büyümesinden dolayı bu sayılar da bire doğru yaklaşmaktadır. Model 1 için 6, 9, 12 kat için k_p değerleri Çizelge 3.26, Çizelge 3.27 ve Çizelge 3.28'de verilmiştir.

Kiriş rijitlikleri 0,35 ve kolonların rijitlikleri 0,7 alındığında sanki kirişler kolonlara kısmen ankastre bağlanmıyormuş gibi davranmaktadır, alt katlara doğru gidildikçe kolon rijitlikleri daha da büyüdüğünden bu durum daha da doğrulanmaktadır ve bu düşünce daha da belirginleşmektedir. Perdeli sistemlerde perdelerin yeri değiştikçe oranlar da değişmektedir, dış kolonlarında k_p oranının yaklaşık olarak 1 olduğu, iç kolonlarda ise bu oranın hep 1'den biraz üstüdür. Alt katlara doğru kiriş rijitliğinin sabit kalmasına rağmen, kolon rijitliğinin artmasıyla her kolonda üst katlardan en alta kata doğru k_p oranının arttığı gözlenmiştir.

k_p oranlarındaki değişim, 6 katlı Hastane binası S11 kolonu için 4 ayrı Model için Şekil 3.5, 3.6, 3.7, 3.8'de grafik olarak gösterilmiştir. k_p oranları tüm Modeller için 6 katlı, 9 katlı ve 12 katlı için sırayla Çizelge 3.29, Çizelge 3.30 ve Çizelge 3.31'de verilmiştir.

Yapının deprem etkisinde taban kesme kuvveti, İzmir, İstanbul ve Ankara gibi önceki yönetmeliklere göre 1., 2. ve 3. derece deprem bölgelerindeki illerde, her bir il için ZA, ZB, ZC, ZD, ZE zemin sınıfı ve 4 Model için ayrı ayrı incelenmiştir. Yapı periyotları $1,4 \times T_{pA}$ olarak kabul edilerek deprem etkisinde taban kesme kuvveti TBDY 2018'e göre hesaplanmıştır. Elde edilen kesme kuvveti, X ve Y eksenlerinde ayrı ayrı düşünülerek, 6 katlı, 9 katlı ve 12 katlı yapının her

bir katı ETABS programında tanımlanmıştır. Model 2 S11 kolonuna ait k_E Oranını Zemin Sınıfına Göre Değişim Grafiği Şekil 3.9'da grafik olarak gösterilmiştir.

İstanbul'da Model 1'e ait 9 katlı binanın sırayla S1, S9, S2, S10, S3, S4, S11 ve S12 kolonlarında ZE zemini ile ilgili k_E oranlarının değişimi Şekil 3.10 ila Şekil 3.17'de grafik olarak gösterilmiştir.

Yapının bu yükler altında analizi yapılarak kolonlarda oluşan eksenel basınç kuvvetleri tespit edilmiştir. Bulunan eksenel basınç kuvvetleri N_{Ex} , N_{Ey} ve bunların kombinasyonundan oluşan $N_{Ex} + 0,3N_{Ey}$ ve $N_{Ey} + 0,3N_{Ex}$ değerlerinin en büyüğü alınarak $N_{G0} + Q_0$, $N_{G0} + \beta_{Q0}$, $N_{G0} + Y_{Q0}$ basınç kuvvetlerine bölünmüş ve böylece k_E oranları elde edilmiştir. Oranlar detaylı olarak incelendiğinde, bu oranların yapının altında iç kolonlarda dış kolonlara göre daha küçük değerler sergilediği ve alt katlara doğru artış gösterdiği görülmüştür. Oranların yapının farklı zemin sınıfında bulunması durumuna göre incelendiğinde, her üç ilde k_E oranının en küçük değerini Hastane binasının ZA zemin sınıfında, en büyük değerini ise ZE zemin sınıfında aldığı görülmüştür. Bulunan oranlar ise Çizelge 3.34 ila Çizelge 3.42'de verilmiştir.

Yapıların kolon brüt en kesit alanını hesaplamak için kullanılan N_{dm} , TBDY 2018'e göre $G+Q+E$ tanımlanmaktadır. Bu tez kapsamında sunulan oranlar kullanılarak yapıların $G_0 + Q_0$ yüküyle çarpılmasıyla, kolonlarda meydana gelen deprem etkisinden kaynaklanan eksenel basınç kuvveti yaklaşık olarak hesaplandığında, kolon en kesit alanlarının gerçek değerlerle tasarımın uyumlu olduğu görülmüştür. N_{dm} değeri kolonlar için belirtilen k_P ve k_E oranları, G_0 ve Q_0 değeri kullanılarak (1.10) eşitliğinden elde edilir. ZA sınıfına k_{ZA} değerleri, G_0 ve Q_0 değerleri, k_{pb} değerleri, k_{vt} değerlerine bağlı olarak ZC sınıfı bir zeminde kolonlarda N_{dm} (1.14) eşitliğinden hesaplanabilir.

İstanbul'da 6katlı binanın 1 katındaki kolonların k_P değerleri:

S1 kolonu Model1'de 0,97, Model4'te 0,96, S9 kolonu Model1'de 0,98, Model4'te 0,98, S2 kolonu Model1'de 1,03, Model3'te 1,03, S10 kolonu Model1'de 1,09, Model2'de 1,06, Model3'te 0,99 ve Model4'te 1,11'dir.

İstanbul'da 12 katlı binanın 1 katındaki kolonların k_P değerleri:

S1 kolonu Model1'de 0,97, Model4'te 0,98, S9 kolonu Model1'de 1,00, Model4'te 1,00, S2 kolonu Model1'de 1,04, Model4'te 1,04, S10 kolonu Model1'de 1,08, Model2'de 1,07, Model3'te 1,03 ve Model4'te 1,09 dur.

Görüldüğü gibi k_P değerleri perdeli ve perdesiz sistemlerde çok az değişmektedir.

İstanbul'da ZE sınıfında bulunan 6 katlı binanın 1 katındaki kolonların k_E değerleri:

S1 kolonu Model1'de 0,261, Model4'te 0,242, S9 kolonu Model1'de 0,181, Model4'te 0,195tir. S2 kolonu Model1'de 0,129, Model4'te 0,057, S10 kolonu Model1'de 0,041, Model2'de 0,039, Model3'te 0,041 ve Model4'te 0,08dir.

İstanbul'da ZE sınıfında bulunan 12 katlı binanın 1 katındaki kolonların k_E değerleri:

S1 kolonu Model1'de 0,195, Model4'te 0,352, S9 kolonu Model1'de 0,106, Model4'te 0,24, S2 kolonu Model1'de 0,130, Model4'te 0,124, S10 kolonu Model1'de 0,014, Model2'de 0,087, Model3'te 0,084 ve Model4'te 0,029dır.

Perdeli sistemlerde kolonların k_E oranları perdesiz sistemlerdekinden beklenildiği gibi daha küçüktür. Buda deprem kuvvetlerinin önemli bir kısmını perdelerin taşıdığını göstermektedir.

Bu çalışmada, üç farklı yapı tipi (6 katlı, 9 katlı, 12 katlı) için dört model (Model 1, Model 2, Model 3, Model 4) üzerinde hesaplamalar gerçekleştirilmiştir. Her bir model için katsayılar çıkarıldıktan sonra, Model 1'in katsayıları ile diğer modellerin (Model 2, Model 3, Model 4) katsayıları arasındaki farkları belirlemek amacıyla tablolar oluşturulmuştur.

Örnek olarak, 6. Kat için S1 kolonu için k_P değeri Model 1'de 0,915 ve Model 4'te 0,919'dur. Model 4'teki k_P değerinin Model 1'den farkı 0,004'tür.

S10 kolonu için:

Model 2 ve Model 1 arasındaki fark: $1,109 - 1,063 = 0,046$

Model 3 ve Model 1 arasındaki fark: $1,109 - 0,979 = 0,13$

Model 4'teki K_P değerinin Model 1'e farkı: $1,109 - 1,134 = -0,025$

Tüm kolonlar, 6, 9, 12 katlı ve Model 2, Model 3, Model 4'teki değerlerin Model 1'e göre farklarını detaylı bir şekilde gösteren sonuçlar aşağıdaki Çizelge S.1, Çizelge S.2 ve Çizelge S.3'te sunulmuştur. Bu Çizelgelerde Model 1 sütununda, Model 1'in değerleri; Model 2, 3, 4 sütunlarında bu modellerin katsayılarının Model 1'e göre arasındaki fark ne kadar olduğu verilmiştir.

Çizelge S.1: 6 Katlı Yapı İçin k_p Katsayı Farkları.

$k_p=N_{G+Q}/N_{G0+Q0}$					
KAT	KOLON	Model 1	Model 2	Model 3	Model 4
6	S1	0.919	**	**	0.004
	S9	0.972	**	**	0.004
	S2	1.02	**	-0.068	-0.009
	S10	1.109	0.046	0.13	-0.025
	S3	0.973	**	-0.116	0.026
	S11	1.08	0.016	0.087	0.135
	S4	0.991	-0.015	-0.034	**
5	S12	1.026	-0.004	**	**
	S1	0.957	**	**	0.004
	S9	0.981	**	**	0.003
	S2	1.021	**	-0.047	-0.007
	S10	1.089	0.044	0.107	-0.02
	S3	0.983	**	-0.093	0.029
	S11	1.068	0.016	0.061	0.146
4	S4	1.004	-0.009	-0.038	**
	S12	1.042	**	**	**
	S1	0.965	**	**	0.004
	S9	0.982	**	**	0.003
	S2	1.022	**	-0.043	-0.006
	S10	1.086	0.043	0.103	-0.018
	S3	0.985	**	-0.089	0.028
3	S11	1.066	0.016	0.056	0.146
	S4	1.007	-0.007	**	**
	S12	1.044	-0.004	**	**
	S1	0.967	**	**	0.003
	S9	0.982	**	**	0.003
	S2	1.024	**	-0.044	-0.006
	S10	1.086	0.039	0.103	-0.017
2	S3	0.984	**	-0.09	0.026
	S11	1.067	0.015	0.053	0.143
	S4	1.011	**	**	**
	S12	1.046	**	**	**
	S1	0.967	**	**	0.003
	S9	0.982	**	**	0.002
	S2	1.027	**	-0.046	-0.005
1	S10	1.086	0.034	0.102	-0.016
	S3	0.983	**	-0.091	0.023
	S11	1.067	0.013	0.05	0.138
	S4	1.014	**	**	**
	S12	1.046	**	**	**
	S1	0.963	**	**	0.003
	S9	0.981	**	**	0.002
	S2	1.028	**	-0.053	-0.005
	S10	1.089	0.029	0.103	-0.016
	S3	0.983	**	-0.094	0.021
	S11	1.07	0.012	0.053	0.131
	S4	1.015	-0.011	-0.033	**
	S12	1.047	-0.004	**	**

Çizelge S.2: 9 Katlı Yapı İçin k_p Katsayı Farkları.

$k_p = N_{G+0}/N_{G0+00}$					
KAT	KOLON	Model 1	Model 2	Model 3	Model 4
9	S1	0.926	**	**	0.006
	S9	0.974	**	**	0.003
	S2	1.02	**	-0.036	-0.011
	S10	1.103	0.067	0.147	-0.022
	S3	0.968	**	-0.128	0.044
	S11	1.084	0.018	0.091	0.148
	S4	0.988	-0.007	-0.053	**
	S12	1.04	-0.013	**	**
8	S1	0.965	**	**	0.005
	S9	0.982	**	**	0.002
	S2	1.021	**	-0.011	-0.007
	S10	1.083	0.068	0.126	-0.017
	S3	0.977	**	-0.105	0.048
	S11	1.072	0.02	0.065	0.163
	S4	1.001	0.001	-0.058	**
	S12	1.058	-0.01	**	**
7	S1	0.973	**	**	0.005
	S9	0.983	**	**	0.002
	S2	1.021	**	-0.006	-0.006
	S10	1.079	0.067	0.122	-0.015
	S3	0.978	**	-0.102	0.047
	S11	1.07	0.02	0.06	0.165
	S4	1.004	**	**	**
	S12	1.061	**	**	**
6	S1	0.976	**	**	0.005
	S9	0.983	**	**	0.001
	S2	1.024	**	-0.006	-0.005
	S10	1.079	0.064	0.123	-0.014
	S3	0.977	**	-0.103	0.045
	S11	1.071	0.019	0.057	0.163
	S4	1.008	0.003	**	**
	S12	1.064	-0.01	**	**
5	S1	0.975	**	**	0.004
	S9	0.983	**	**	0.001
	S2	1.026	**	-0.007	-0.005
	S10	1.079	0.059	0.122	-0.012
	S3	0.976	**	-0.104	0.043
	S11	1.072	0.018	0.055	0.16
	S4	1.011	0.002	**	**
	S12	1.065	-0.01	**	**
4	S1	0.973	**	**	0.004
	S9	0.983	**	**	0.001
	S2	1.027	**	-0.012	-0.004
	S10	1.081	0.055	0.122	-0.011
	S3	0.976	**	-0.106	0.04
	S11	1.074	0.017	0.056	0.155
	S4	1.012	0	-0.057	**
	S12	1.067	-0.01	**	**

3	S1	0.971	**	**	0.004
	S9	0.985	**	**	0.001
	S2	1.031	**	-0.014	-0.004
	S10	1.081	0.048	0.117	-0.009
	S3	0.978	**	-0.106	0.037
	S11	1.077	0.014	0.056	0.15
	S4	1.016	-0.003	**	**
2	S12	1.066	-0.011	**	**
	S1	0.967	**	**	0.003
	S9	0.989	**	**	0.001
	S2	1.035	**	-0.018	-0.003
	S10	1.082	0.041	0.111	-0.008
	S3	0.981	**	-0.104	0.034
	S11	1.077	0.01	0.052	0.145
1	S4	1.02	**	**	**
	S12	1.067	**	**	**
	S1	0.963	**	**	0.003
	S9	0.992	**	**	0.001
	S2	1.038	**	-0.024	-0.003
	S10	1.083	0.033	0.105	-0.008
	S3	0.985	**	-0.101	0.031
	S11	1.078	0.006	0.05	0.139
	S4	1.023	-0.008	-0.045	**
	S12	1.066	-0.011	**	**

Çizelge S.3: 12 Katlı Yapı İçin k_p Katsayı Farkları.

$k_p = N_{G+Q} / N_{G0+Q0}$					
KAT	KOLON	Model 1	Model 2	Model 3	Model 4
12	S1	0.935	**	**	0.006
	S9	0.974	**	**	0.003
	S2	1.014	**	-0.02	-0.01
	S10	1.101	0.088	0.16	-0.019
	S3	0.969	**	-0.128	0.058
	S11	1.084	0.025	0.094	0.149
	S4	0.983	0.007	-0.071	**
	S12	1.053	-0.004	**	**
11	S1	0.976	**	**	0.007
	S9	0.982	**	**	0.002
	S2	1.014	**	0.008	-0.005
	S10	1.08	0.092	0.138	-0.013
	S3	0.977	**	-0.106	0.063
	S11	1.074	0.029	0.071	0.167
	S4	0.995	0.015	-0.08	**
	S12	1.073	-0.003	**	**
10	S1	0.985	**	**	0.008
	S9	0.983	**	**	0.002
	S2	1.014	**	0.014	-0.004
	S10	1.076	0.092	0.135	-0.012
	S3	0.979	**	-0.101	0.064
	S11	1.071	0.028	0.065	0.168
	S4	0.998	0.017	-0.081	**
	S12	1.076	-0.003	**	**
9	S1	0.988	**	**	0.008
	S9	0.983	**	**	0.002
	S2	1.016	**	0.014	-0.003
	S10	1.076	0.089	0.135	-0.01
	S3	0.978	**	-0.103	0.062
	S11	1.072	0.029	0.063	0.167
	S4	1.002	0.017	-0.081	**
	S12	1.08	-0.003	**	**
9	S1	0.988	**	**	0.007
	S9	0.983	**	**	0.002
	S2	1.018	**	0.014	-0.002
	S10	1.076	0.086	0.135	-0.007
	S3	0.977	**	-0.104	0.061
	S11	1.073	0.028	0.061	0.165
	S4	1.004	0.015	-0.081	**
	S12	1.082	-0.003	**	**
7	S1	0.986	**	**	0.007
	S9	0.982	**	**	0.001
	S2	1.019	**	0.009	-0.001
	S10	1.078	0.082	0.135	-0.006
	S3	0.977	**	-0.105	0.058
	S11	1.075	0.027	0.062	0.161
	S4	1.005	0.014	-0.083	**

	S12	1.085	-0.003	**	**
6	S1	0.983	**	**	0.006
	S9	0.985	**	**	0.001
	S2	1.023	**	0.008	0
	S10	1.078	0.076	0.13	-0.004
	S3	0.979	**	-0.106	0.055
	S11	1.077	0.024	0.061	0.156
	S4	1.009	0.012	-0.079	**
	S12	1.085	-0.003	**	**
5	S1	0.981	**	**	0.006
	S9	0.988	**	**	0.001
	S2	1.026	**	0.003	0
	S10	1.079	0.07	0.125	-0.002
	S3	0.982	**	-0.103	0.052
	S11	1.078	0.022	0.059	0.152
	S4	1.012	**	**	**
	S12	1.086	**	**	**
4	S1	0.977	**	**	0.005
	S9	0.991	**	**	0.001
	S2	1.029	**	-0.001	0
	S10	1.079	0.063	0.118	-0.002
	S3	0.986	**	-0.099	0.049
	S11	1.079	0.019	0.057	0.148
	S4	1.016	**	**	**
	S12	1.086	**	**	**
3	S1	0.979	**	**	0.005
	S9	0.995	**	**	0.001
	S2	1.031	**	-0.007	0.001
	S10	1.081	0.056	0.112	-0.001
	S3	0.99	**	-0.096	0.046
	S11	1.08	0.016	0.055	0.144
	S4	1.019	0.005	-0.071	**
	S12	1.087	**	**	**
2	S1	0.982	**	**	0.005
	S9	0.999	**	**	0.001
	S2	1.034	**	-0.012	0.001
	S10	1.081	0.048	0.105	-0.001
	S3	0.995	**	-0.091	0.043
	S11	1.08	0.012	0.051	0.14
	S4	1.024	**	**	**
	S12	1.086	**	**	**
1	S1	0.982	**	**	0.004
	S9	1.001	**	**	0.001
	S2	1.037	**	-0.018	0.001
	S10	1.084	0.042	0.1	-0.001
	S3	0.999	**	-0.088	0.039
	S11	1.081	0.01	0.048	0.136
	S4	1.027	-0.001	-0.062	**
	S12	1.086	-0.004	**	**

Bu çalışmada, beş farklı zemin sınıfı (ZA, ZB, ZC, ZD, ZE) ve dört farklı model (Model1, Model2, Model3, Model4) üzerinde hesaplamalar gerçekleştirilmiştir. Hesaplamalar, üç farklı hastane binası (6 katlı, 9 katlı, 12 katlı) ve üç farklı il (İstanbul, Ankara, İzmir) için yapılmıştır. Her bir kombinasyon için maksimum K_E oranlar hesaplanmış ve sonuçlar bir tabloda sunulmuştur.

Aşağıda, elde edilen sonuçların genel bir özeti yer almaktadır:

Zemin Sınıfları: ZA, ZB, ZC, ZD, ZE

Modeller: Model1, Model2, Model3, Model4

Hastane Binası Kat Sayıları: 6 Katlı, 9 Katlı, 12 Katlı

İller: İstanbul, Ankara, İzmir

Her kombinasyon için maksimum K_E oranları gösteren Çizelge S.4'te verilmiştir:

Çizelge S.4: Zemin Sınıfı ve Kat Sayısına Göre Maksimum K_E Oranlar Tablosu (İstanbul, Ankara, İzmir)

	$k_E = N_E / N_{G0} + Q_0$										
Zemin Sınıfı	Model	6 katlı				9 katlı			12 katlı		
		Ankara		İstanbul	İzmir	Ankara	İstanbul	İzmir	Ankara	İstanbul	İzmir
keZA	Model 1	S1	0.115	0.249	0.283	0.13	0.345	0.392	0.172	0.458	0.521
	Model 2	S4	0.019	0.041	0.041	0.033	0.069	0.069	0.046	0.103	0.117
	Model 3	S3	0.018	0.037	0.037	0.027	0.057	0.057	0.038	0.085	0.097
	Model 4	S11	0.077	0.163	0.162	0.107	0.226	0.224	0.123	0.276	0.314
keZB	Model 1	S1	0.115	0.28	0.319	0.146	0.388	0.441	0.194	0.515	0.586
	Model 2	S4	0.019	0.041	0.041	0.033	0.069	0.076	0.046	0.116	0.132
	Model 3	S3	0.018	0.037	0.037	0.027	0.057	0.063	0.038	0.096	0.109
	Model 4	S11	0.077	0.163	0.162	0.107	0.226	0.247	0.123	0.311	0.354
keZC	Model 1	S1	0.215	0.454	0.451	0.22	0.518	0.589	0.28	0.687	0.781
	Model 2	S4	0.036	0.077	0.076	0.061	0.13	0.129	0.086	0.183	0.181
	Model 3	S3	0.033	0.07	0.07	0.051	0.108	0.107	0.071	0.151	0.15
	Model 4	S11	0.145	0.306	0.304	0.2	0.424	0.42	0.231	0.489	0.486
keZD	Model 1	S1	0.337	0.63	0.626	0.345	0.644	0.64	0.369	0.689	0.7
	Model 2	S4	0.057	0.106	0.106	0.096	0.18	0.179	0.136	0.253	0.252
	Model 3	S3	0.051	0.097	0.097	0.08	0.149	0.148	0.112	0.209	0.208
	Model 4	S11	0.227	0.424	0.422	0.314	0.587	0.584	0.363	0.678	0.675
keZE	Model 1	S1	0.572	0.908	0.904	0.584	0.928	0.924	0.625	0.993	0.989
	Model 2	S4	0.092	0.139	0.142	0.164	0.26	0.259	0.23	0.365	0.363
	Model 3	S3	0.079	0.119	0.122	0.135	0.215	0.214	0.19	0.302	0.3
	Model 4	S11	0.374	0.564	0.574	0.534	0.847	0.843	0.616	0.979	0.974

Bu tablo, her bir zemin sınıfı ve model kombinasyonu için, 6 katlı, 9 katlı ve 12 katlı hastane binaları için İstanbul, Ankara ve İzmir'de yapılan hesaplamaların maksimum oranlarını göstermektedir. Bu sonuçlar, hastane binalarının zemin sınıfı ve kat sayısına göre nasıl performans gösterdiğini detaylı bir şekilde analiz etmek için kullanılmıştır.

Örnek 1 de İstanbul'daki ZC sınıfında inşa edilecek 6 katlı binada bir köşe kolon S1 ve bir içteki kolonun S10 k_{ZC} , $k_{p\beta}$, G_0 ve Q_0 değerlerine bağlı olarak kolon boyutlarının nasıl hesaplanabileceği gösterilmiştir.

Örnek 2'de kolonların sadece ZA sınıfındaki k_{EZA} taban kesme kuvvetleri oranı k_{vt} , G_0 ve Q_0 değerlerine bağlı olarak kolon boyutlarının nasıl hesaplanabileceği gösterilmiştir.

Sonuç olarak burada verilen k_p ve k_E moment etkisi göz önüne alınmadan N_{G0} ve N_{Q0} değerlerine bağlı olarak N_E eksenel kuvveti hesaplanır.

$$A_c = (N_{G0} + N_{\beta Q0} + N_E) > 0,4 f_{ck}$$

Eşitliğinden kolonların enkesit alanları hesaplanabilir.

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EKLER

EK A: Düşey Yüklerin Etkisinde Oluşan Eksenel Kuvvetler
EK B: Deprem Yüklerin Etkisinde Oluşan Eksenel Kuvvetler

EK A: Düşey Yüklerin Etkisinde Oluşan Eksenel Kuvvetler

MODEL 1:"

Çizelge A.1: 9 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	$N_G + Q$ (kN)	N_{G0} (kN)	N_{Q0} (kN)	$N_{G0} + Q_0$ (kN)	$k_p = N_G + Q / N_{G0} + Q_0$
9	S1	97.426	21.267	118.693	101.95	26.25	128.2	0.926
	S9	152.890	47.922	200.811	154.96	51.25	206.21	0.974
	S2	192.536	56.709	249.244	186.63	57.75	244.38	1.020
	S10	271.875	120.197	392.072	242.76	112.75	355.51	1.103
	S3	196.117	58.504	254.621	200.11	63	263.11	0.968
	S11	287.127	130.157	417.284	262.098	123	385.098	1.084
	S4	186.812	55.956	242.768	185.97	59.69	245.66	0.988
	S12	221.308	94.411	315.719	207.618	95.875	303.493	1.040
8	S1	201.798	45.619	247.417	203.9	52.5	256.4	0.965
	S9	307.490	97.552	405.043	309.92	102.5	412.42	0.982
	S2	385.007	114.108	499.114	373.26	115.5	488.76	1.021
	S10	534.984	234.758	769.742	485.52	225.5	711.02	1.083
	S3	394.808	119.103	513.911	400.22	126	526.22	0.977
	S11	568.902	257.119	826.021	524.196	246	770.196	1.072
	S4	377.897	114.132	492.029	371.94	119.380	491.32	1.001
	S12	448.112	194.184	642.295	415.236	191.750	606.986	1.058
7	S1	304.860	69.384	374.244	305.85	78.75	384.6	0.973
	S9	461.631	146.750	608.381	464.88	153.75	618.63	0.983
	S2	577.418	171.211	748.629	559.89	173.25	733.14	1.021
	S10	799.850	350.537	1150.387	728.28	338.25	1066.53	1.079
	S3	592.850	179.142	771.992	600.33	189	789.33	0.978
	S11	851.752	384.732	1236.483	786.294	369	1155.294	1.070
	S4	568.271	171.902	740.173	557.91	179.07	736.98	1.004
	S12	673.307	292.697	966.005	622.854	287.625	910.479	1.061
6	S1	407.336	92.908	500.244	407.8	105	512.8	0.976
	S9	615.376	195.720	811.096	619.84	205	824.84	0.983
	S2	771.855	228.767	1000.622	746.52	231	977.52	1.024
	S10	1067.450	466.455	1533.904	971.04	451	1422.04	1.079
	S3	789.727	238.635	1028.362	800.44	252	1052.44	0.977
	S11	1137.422	512.411	1649.833	1048.392	492	1540.392	1.071
	S4	760.421	230.147	990.569	743.88	238.76	982.64	1.008
	S12	900.825	391.013	1291.838	830.472	383.5	1213.972	1.064
5	S1	509.121	116.102	625.223	509.75	131.25	641	0.975
	S9	769.140	244.552	1013.692	774.8	256.25	1031.05	0.983
	S2	967.063	286.656	1253.719	933.15	288.75	1221.9	1.026
	S10	1334.768	582.504	1917.272	1213.8	563.75	1777.55	1.079
	S3	986.408	297.818	1284.226	1000.55	315	1315.55	0.976
	S11	1423.391	640.303	2063.694	1310.49	615	1925.49	1.072
	S4	953.133	288.736	1241.869	929.85	298.45	1228.3	1.011
	S12	1127.361	488.764	1616.125	1038.09	479.375	1517.465	1.065
4	S1	609.984	138.828	748.812	611.7	157.5	769.2	0.973
	S9	923.006	293.176	1216.182	929.76	307.5	1237.26	0.983
	S2	1161.768	344.177	1505.945	1119.78	346.5	1466.28	1.027
	S10	1605.997	699.496	2305.493	1456.56	676.5	2133.06	1.081
	S3	1184.541	356.894	1541.435	1200.66	378	1578.66	0.976
	S11	1712.482	768.463	2480.945	1572.588	738	2310.588	1.074
	S4	1144.962	346.934	1491.896	1115.82	358.14	1473.96	1.012
	S12	1356.603	586.273	1942.876	1245.708	575.25	1820.958	1.067
3	S1	709.857	161.084	870.941	713.65	183.75	897.4	0.971
	S9	1079.638	342.338	1421.976	1084.72	358.75	1443.47	0.985

	S2	1361.410	402.535	1763.945	1306.41	404.25	1710.66	1.031
	S10	1874.276	815.633	2689.908	1699.32	789.25	2488.57	1.081
	S3	1385.123	416.362	1801.484	1400.77	441	1841.77	0.978
	S11	2005.807	896.231	2902.039	1834.686	861	2695.686	1.077
	S4	1341.445	405.883	1747.328	1301.79	417.83	1719.62	1.016
	S12	1583.190	682.495	2265.685	1453.326	671.125	2124.451	1.066
2	S1	809.176	182.992	992.167	815.6	210	1025.6	0.967
	S9	1239.396	392.013	1631.409	1239.68	410	1649.68	0.989
	S2	1561.505	461.074	2022.579	1493.04	462	1955.04	1.035
	S10	2144.675	931.719	3076.395	1942.08	902	2844.08	1.082
	S3	1589.255	476.586	2065.840	1600.88	504	2104.88	0.981
	S11	2296.067	1022.890	3318.957	2096.784	984	3080.784	1.077
	S4	1538.978	465.198	2004.176	1487.76	477.52	1965.28	1.020
	S12	1811.606	777.900	2589.506	1660.944	767	2427.944	1.067
1	S1	906.683	204.005	1110.688	917.55	236.25	1153.8	0.963
	S9	1399.541	441.440	1840.981	1394.64	461.25	1855.89	0.992
	S2	1763.833	519.665	2283.497	1679.67	519.75	2199.42	1.038
	S10	2416.304	1049.251	3465.554	2184.84	1014.75	3199.59	1.083
	S3	1795.922	536.814	2332.736	1800.99	567	2367.99	0.985
	S11	2587.752	1149.845	3737.597	2358.882	1107	3465.882	1.078
	S4	1737.929	524.253	2262.182	1673.73	537.21	2210.94	1.023
	S12	2038.639	872.606	2911.245	1868.562	862.875	2731.437	1.066

Çizelge A.2: 9 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_{pQ} (kN)	$N_G + pQ$	N_{G0} (kN)	N_{pQ0} (kN)	$N_{G0} + p_{Q0}$ (kN)	$k_{p\beta} = N_G + pQ / N_{G0} + p_{Q0}$
9	S1	97.426	12.760	110.186	101.95	15.75	117.7	0.936
	S9	152.890	28.753	181.643	154.96	30.75	185.71	0.978
	S2	192.536	34.025	226.561	186.63	34.65	221.28	1.024
	S10	271.875	72.118	343.993	242.76	67.65	310.41	1.108
	S3	196.117	35.102	231.219	200.11	37.8	237.91	0.972
	S11	287.127	78.094	365.221	262.098	73.8	335.898	1.087
	S4	186.812	33.574	220.386	185.97	35.814	221.784	0.994
	S12	221.308	56.646	277.955	207.618	57.525	265.143	1.048
8	S1	201.798	27.371	229.169	203.9	31.5	235.4	0.974
	S9	307.490	58.531	366.022	309.92	61.5	371.42	0.985
	S2	385.007	68.465	453.471	373.26	69.3	442.56	1.025
	S10	534.984	140.855	675.838	485.52	135.3	620.82	1.089
	S3	394.808	71.462	466.270	400.22	75.6	475.82	0.980
	S11	568.902	154.271	723.173	524.196	147.6	671.796	1.076
	S4	377.897	68.479	446.376	371.94	71.628	443.568	1.006
	S12	448.112	116.510	564.622	415.236	115.05	530.286	1.065
7	S1	304.860	41.630	346.490	305.85	47.25	353.1	0.981
	S9	461.631	88.050	549.681	464.88	92.25	557.13	0.987
	S2	577.418	102.726	680.144	559.89	103.95	663.84	1.025
	S10	799.850	210.322	1010.172	728.28	202.95	931.23	1.085
	S3	592.850	107.485	700.335	600.33	113.4	713.73	0.981
	S11	851.752	230.839	1082.591	786.294	221.4	1007.694	1.074
	S4	568.271	103.141	671.412	557.91	107.442	665.352	1.009
	S12	673.307	175.618	848.926	622.854	172.575	795.429	1.067
6	S1	407.336	55.745	463.081	407.8	63	470.8	0.984
	S9	615.376	117.432	732.808	619.84	123	742.84	0.986
	S2	771.855	137.260	909.115	746.52	138.6	885.12	1.027
	S10	1067.450	279.873	1347.323	971.04	270.6	1241.64	1.085
	S3	789.727	143.181	932.908	800.44	151.2	951.64	0.980
	S11	1137.422	307.447	1444.869	1048.392	295.2	1343.592	1.075
	S4	760.421	138.088	898.510	743.88	143.256	887.136	1.013
	S12	900.825	234.608	1135.433	830.472	230.1	1060.572	1.071
5	S1	509.121	69.661	578.782	509.75	78.75	588.5	0.983
	S9	769.140	146.731	915.871	774.8	153.75	928.55	0.986
	S2	967.063	171.994	1139.056	933.15	173.25	1106.4	1.030
	S10	1334.768	349.502	1684.270	1213.8	338.25	1552.05	1.085
	S3	986.408	178.691	1165.099	1000.55	189	1189.55	0.979
	S11	1423.391	384.182	1807.573	1310.49	369	1679.49	1.076
	S4	953.133	173.241	1126.375	929.85	179.07	1108.92	1.016
	S12	1127.361	293.259	1420.619	1038.09	287.625	1325.715	1.072
4	S1	609.984	83.297	693.281	611.7	94.5	706.2	0.982
	S9	923.006	175.906	1098.912	929.76	184.5	1114.26	0.986
	S2	1161.768	206.506	1368.274	1119.78	207.9	1327.68	1.031
	S10	1605.997	419.698	2025.695	1456.56	405.9	1862.46	1.088
	S3	1184.541	214.136	1398.677	1200.66	226.8	1427.46	0.980
	S11	1712.482	461.078	2173.559	1572.588	442.8	2015.388	1.078
	S4	1144.962	208.160	1353.122	1115.82	214.884	1330.704	1.017
	S12	1356.603	351.764	1708.366	1245.708	345.15	1590.858	1.074
3	S1	709.857	96.650	806.507	713.65	110.25	823.9	0.979
	S9	1079.638	205.403	1285.041	1084.72	215.25	1299.97	0.989
	S2	1361.410	241.521	1602.931	1306.41	242.55	1548.96	1.035
	S10	1874.276	489.380	2363.655	1699.32	473.55	2172.87	1.088

	S3	1385.123	249.817	1634.940	1400.77	264.6	1665.37	0.982
	S11	2005.807	537.739	2543.546	1834.686	516.6	2351.286	1.082
	S4	1341.445	243.530	1584.974	1301.79	250.698	1552.488	1.021
	S12	1583.190	409.497	1992.687	1453.326	402.675	1856.001	1.074
2	S1	809.176	109.795	918.970	815.6	126	941.6	0.976
	S9	1239.396	235.208	1474.604	1239.68	246	1485.68	0.993
	S2	1561.505	276.644	1838.149	1493.04	277.2	1770.24	1.038
	S10	2144.675	559.032	2703.707	1942.08	541.2	2483.28	1.089
	S3	1589.255	285.951	1875.206	1600.88	302.4	1903.28	0.985
	S11	2296.067	613.734	2909.801	2096.784	590.4	2687.184	1.083
	S4	1538.978	279.119	1818.097	1487.76	286.512	1774.272	1.025
	S12	1811.606	466.740	2278.346	1660.944	460.2	2121.144	1.074
1	S1	906.683	122.403	1029.086	917.55	141.75	1059.3	0.971
	S9	1399.541	264.864	1664.405	1394.64	276.75	1671.39	0.996
	S2	1763.833	311.799	2075.632	1679.67	311.85	1991.52	1.042
	S10	2416.304	629.550	3045.854	2184.84	608.85	2793.69	1.090
	S3	1795.922	322.089	2118.010	1800.99	340.2	2141.19	0.989
	S11	2587.752	689.907	3277.659	2358.882	664.2	3023.082	1.084
	S4	1737.929	314.552	2052.480	1673.73	322.326	1996.056	1.028
	S12	2038.639	523.564	2562.203	1868.562	517.725	2386.287	1.074

Çizelge A.3: 9 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	Y	KOLON	N_G (kN)	N_{YQ} (kN)	N_{G+YQ} (kN)	N_{G0} (kN)	N_{YQ0} (kN)	N_{G0+YQ0} (kN)	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
9	0.1	S1	97.426	2.127	99.553	101.95	2.625	104.575	0.952
	0.1	S9	152.890	4.792	157.682	154.96	5.125	160.085	0.622
	0.1	S2	192.536	5.671	198.206	186.63	5.775	192.405	0.517
	0.1	S10	271.875	12.020	283.895	242.76	11.275	254.035	0.392
	0.1	S3	196.117	5.850	201.968	200.11	6.3	206.41	0.482
	0.1	S11	287.127	13.016	300.143	262.098	12.3	274.398	0.363
	0.1	S4	186.812	5.596	192.408	185.97	5.969	191.939	0.519
	0.1	S12	221.308	9.441	230.749	207.618	9.5875	217.2055	0.458
8	0.2	S1	201.798	6.380	208.178	203.9	7.875	211.775	0.470
	0.2	S9	307.490	14.376	321.867	309.92	15.375	325.295	0.306
	0.2	S2	385.007	17.013	402.019	373.26	17.325	390.585	0.255
	0.2	S10	534.984	36.059	571.043	485.52	33.825	519.345	0.192
	0.2	S3	394.808	17.551	412.359	400.22	18.9	419.12	0.238
	0.2	S11	568.902	39.047	607.949	524.196	36.9	561.096	0.177
	0.2	S4	377.897	16.787	394.683	371.94	17.907	389.847	0.255
	0.2	S12	448.112	28.323	476.435	415.236	28.7625	443.9985	0.224
7	0.2	S1	304.860	10.633	315.493	305.85	13.125	318.975	0.312
	0.2	S9	461.631	23.961	485.592	464.88	25.625	490.505	0.203
	0.2	S2	577.418	28.354	605.772	559.89	28.875	588.765	0.169
	0.2	S10	799.850	60.099	859.948	728.28	56.375	784.655	0.127
	0.2	S3	592.850	29.252	622.101	600.33	31.5	631.83	0.158
	0.2	S11	851.752	65.079	916.830	786.294	61.5	847.794	0.117
	0.2	S4	568.271	27.978	596.249	557.91	29.845	587.755	0.169
	0.2	S12	673.307	47.205	720.513	622.854	47.9375	670.7915	0.148
6	0.4	S1	407.336	19.140	426.476	407.8	10.5	418.3	0.238
	0.4	S9	615.376	43.129	658.506	619.84	20.500	640.34	0.155
	0.4	S2	771.855	51.038	822.893	746.52	23.1	769.62	0.129
	0.4	S10	1067.450	108.177	1175.627	971.04	45.1	1016.14	0.098
	0.4	S3	789.727	52.653	842.380	800.44	25.2	825.64	0.121
	0.4	S11	1137.422	117.141	1254.563	1048.392	49.2	1097.592	0.091
	0.4	S4	760.421	50.360	810.782	743.88	23.876	767.756	0.130
	0.4	S12	900.825	84.970	985.795	830.472	38.35	868.822	0.115
5	0.6	S1	509.121	31.900	541.021	509.75	15.75	525.5	0.189
	0.6	S9	769.140	71.882	841.023	774.8	30.750	805.55	0.124
	0.6	S2	967.063	85.063	1052.126	933.15	34.65	967.8	0.103

	0.6	S10	1334.768	180.296	1515.064	1213.8	67.65	1281.45	0.078
	0.6	S3	986.408	87.755	1074.164	1000.55	37.8	1038.35	0.096
	0.6	S11	1423.391	195.236	1618.627	1310.49	73.8	1384.29	0.072
	0.6	S4	953.133	83.934	1037.067	929.85	35.814	965.664	0.103
	0.6	S12	1127.361	141.616	1268.977	1038.09	57.525	1095.615	0.091
4	0.8	S1	609.984	48.914	658.898	611.7	36.75	648.45	0.154
	0.8	S9	923.006	110.219	1033.226	929.76	71.750	1001.51	0.099
	0.8	S2	1161.768	130.430	1292.199	1119.78	80.85	1200.63	0.083
	0.8	S10	1605.997	276.453	1882.450	1456.56	157.85	1614.41	0.062
	0.8	S3	1184.541	134.558	1319.099	1200.66	88.2	1288.86	0.077
	0.8	S11	1712.482	299.361	2011.843	1572.588	172.2	1744.788	0.057
	0.8	S4	1144.962	128.699	1273.660	1115.82	83.566	1199.386	0.083
	0.8	S12	1356.603	217.145	1573.747	1245.708	134.225	1379.933	0.072
3	1	S1	709.857	70.180	780.037	713.65	63	776.65	0.128
	1	S9	1079.638	158.141	1237.779	1084.72	123.000	1207.72	0.082
	1	S2	1361.410	187.139	1548.549	1306.41	138.6	1445.01	0.069
	1	S10	1874.276	396.650	2270.926	1699.32	270.6	1969.92	0.051
	1	S3	1385.123	193.062	1578.184	1400.77	151.2	1551.97	0.064
	1	S11	2005.807	429.518	2435.326	1834.686	295.2	2129.886	0.047
	1	S4	1341.445	184.654	1526.099	1301.79	143.256	1445.046	0.069
	1	S12	1583.190	311.556	1894.746	1453.326	230.1	1683.426	0.059
2	1	S1	809.176	91.447	900.623	815.6	89.25	904.85	0.110
	1	S9	1239.396	206.062	1445.459	1239.68	174.250	1413.93	0.070
	1	S2	1561.505	243.848	1805.353	1493.04	196.35	1689.39	0.059
	1	S10	2144.675	516.848	2661.523	1942.08	383.35	2325.43	0.043
	1	S3	1589.255	251.565	1840.820	1600.88	214.2	1815.08	0.055
	1	S11	2296.067	559.676	2855.742	2096.784	418.2	2514.984	0.040
	1	S4	1538.978	240.610	1779.589	1487.76	202.946	1690.706	0.059
	1	S12	1811.606	405.966	2217.573	1660.944	325.975	1986.919	0.050
1	1	S1	906.683	21.267	927.949	917.55	115.5	1033.05	0.096
	1	S9	1399.541	47.922	1447.463	1394.64	225.500	1620.14	0.061
	1	S2	1763.833	56.709	1820.542	1679.67	254.1	1933.77	0.051
	1	S10	2416.304	120.197	2536.501	2184.84	496.1	2680.94	0.037
	1	S3	1795.922	58.504	1854.425	1800.99	277.2	2078.19	0.048
	1	S11	2587.752	130.157	2717.910	2358.882	541.2	2900.082	0.034
	1	S4	1737.929	55.956	1793.885	1673.73	262.636	1936.366	0.051
	1	S12	2038.639	94.411	2133.050	1868.562	421.85	2290.412	0.043

Çizelge A.4: 12 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_{G+Q}/N_{G0+Q0}$
12	S1	98.001	21.918	119.919	101.95	26.25	128.2	0.935
	S9	152.585	48.175	200.760	154.96	51.25	206.21	0.974
	S2	191.231	56.504	247.735	186.63	57.75	244.38	1.014
	S10	272.226	119.120	391.346	242.76	112.75	355.51	1.101
	S3	195.919	58.938	254.857	200.11	63	263.11	0.969
	S11	287.712	129.907	417.619	262.098	123	385.098	1.084
	S4	185.548	55.816	241.363	185.97	59.69	245.66	0.983
	S12	224.041	95.643	319.684	207.618	95.875	303.493	1.053
11	S1	203.064	47.217	250.281	203.9	52.5	256.4	0.976
	S9	306.746	98.146	404.892	309.92	102.5	412.42	0.982
	S2	382.022	113.642	495.663	373.26	115.5	488.76	1.014
	S10	535.799	232.209	768.008	485.52	225.5	711.02	1.080
	S3	394.154	120.061	514.216	400.22	126	526.22	0.977
	S11	570.366	256.468	826.833	524.196	246	770.196	1.074
	S4	375.020	113.970	488.990	371.94	119.380	491.32	0.995
	S12	454.371	196.929	651.300	415.236	191.750	606.986	1.073
10	S1	306.824	71.911	378.735	305.85	78.75	384.6	0.985
	S9	460.443	147.681	608.124	464.88	153.75	618.63	0.983
	S2	572.764	170.471	743.235	559.89	173.25	733.14	1.014
	S10	801.125	346.544	1147.670	728.28	338.25	1066.53	1.076
	S3	591.782	180.622	772.404	600.33	189	789.33	0.979
	S11	854.042	383.686	1237.727	786.294	369	1155.294	1.071
	S4	563.813	171.692	735.505	557.91	179.07	736.98	0.998
	S12	683.074	296.974	980.048	622.854	287.625	910.479	1.076
9	S1	410.022	96.384	506.407	407.8	105	512.8	0.988
	S9	613.705	197.020	810.725	619.84	205	824.84	0.983
	S2	765.418	227.766	993.183	746.52	231	977.52	1.016
	S10	1069.200	460.911	1530.110	971.04	451	1422.04	1.076
	S3	788.220	240.657	1028.877	800.44	252	1052.44	0.978
	S11	1140.549	510.905	1651.455	1048.392	492	1540.392	1.072
	S4	754.246	229.899	984.145	743.88	238.76	982.64	1.002
	S12	914.483	397.016	1311.499	830.472	383.5	1213.972	1.080
8	S1	512.562	120.548	633.109	509.75	131.25	641	0.988
	S9	766.948	246.248	1013.196	774.8	256.25	1031.05	0.983
	S2	958.734	285.393	1244.126	933.15	288.75	1221.9	1.018
	S10	1337.013	575.320	1912.333	1213.8	563.75	1777.55	1.076
	S3	984.452	300.402	1284.854	1000.55	315	1315.55	0.977
	S11	1427.353	638.286	2065.639	1310.49	615	1925.49	1.073
	S4	945.124	288.449	1233.573	929.85	298.45	1228.3	1.004
	S12	1145.247	496.666	1641.914	1038.09	479.375	1517.465	1.082
7	S1	614.219	144.261	758.480	611.7	157.5	769.2	0.986
	S9	920.245	295.294	1215.539	929.76	307.5	1237.26	0.982
	S2	1151.444	342.624	1494.067	1119.78	346.5	1466.28	1.019
	S10	1608.730	690.593	2299.323	1456.56	676.5	2133.06	1.078
	S3	1182.128	360.073	1542.201	1200.66	378	1578.66	0.977
	S11	1717.259	765.870	2483.129	1572.588	738	2310.588	1.075
	S4	1135.068	346.585	1481.653	1115.82	358.14	1473.96	1.005
	S12	1379.028	596.283	1975.312	1245.708	575.25	1820.958	1.085
6	S1	714.962	167.565	882.527	713.65	183.75	897.4	0.983
	S9	1076.249	344.941	1421.190	1084.72	358.75	1443.47	0.985
	S2	1348.935	400.689	1749.623	1306.41	404.25	1710.66	1.023
	S10	1877.494	804.837	2682.330	1699.32	789.25	2488.57	1.078
	S3	1382.184	420.198	1802.382	1400.77	441	1841.77	0.979

	S11	2011.436	892.957	2904.393	1834.686	861	2695.686	1.077
	S4	1329.528	405.485	1735.013	1301.79	417.83	1719.62	1.009
	S12	1610.595	694.822	2305.417	1453.326	671.125	2124.451	1.085
5	S1	815.111	190.549	1005.660	815.6	210	1025.6	0.981
	S9	1235.217	395.105	1630.323	1239.68	410	1649.68	0.988
	S2	1546.683	458.879	2005.562	1493.04	462	1955.04	1.026
	S10	2148.640	918.967	3067.607	1942.08	902	2844.08	1.079
	S3	1585.609	481.046	2066.655	1600.88	504	2104.88	0.982
	S11	2302.742	1018.952	3321.694	2096.784	984	3080.784	1.078
	S4	1524.760	464.682	1989.442	1487.76	477.52	1965.28	1.012
	S12	1844.426	792.777	2637.203	1660.944	767	2427.944	1.086
4	S1	914.684	213.106	1127.790	917.55	236.25	1153.8	0.977
	S9	1394.831	445.258	1840.088	1394.64	461.25	1855.89	0.991
	S2	1746.448	517.139	2263.587	1679.67	519.75	2199.42	1.029
	S10	2419.509	1033.625	3453.134	2184.84	1014.75	3199.59	1.079
	S3	1792.215	542.305	2334.520	1800.99	567	2367.99	0.986
	S11	2594.138	1144.470	3738.608	2358.882	1107	3465.882	1.079
	S4	1722.118	523.946	2246.064	1673.73	537.21	2210.94	1.016
	S12	2076.880	890.091	2966.972	1868.562	862.875	2731.437	1.086
3	S1	1019.113	236.329	1255.441	1019.5	262.5	1282	0.979
	S9	1557.427	495.369	2052.796	1549.6	512.5	2062.1	0.995
	S2	1944.673	574.711	2519.384	1866.3	577.5	2443.8	1.031
	S10	2693.237	1148.534	3841.771	2427.6	1127.5	3555.1	1.081
	S3	2001.404	603.821	2605.224	2001.1	630	2631.1	0.990
	S11	2888.256	1269.664	4157.920	2620.98	1230	3850.98	1.080
	S4	1919.898	583.193	2503.091	1859.7	596.9	2456.6	1.019
	S12	2311.826	986.757	3298.584	2076.18	958.75	3034.93	1.087
2	S1	1124.753	259.800	1384.553	1121.45	288.75	1410.2	0.982
	S9	1720.145	545.390	2265.534	1704.56	563.75	2268.31	0.999
	S2	2147.308	632.587	2779.896	2052.93	635.25	2688.18	1.034
	S10	2965.241	1263.333	4228.573	2670.36	1240.25	3910.61	1.081
	S3	2213.260	665.477	2878.737	2201.21	693	2894.21	0.995
	S11	3180.647	1394.450	4575.098	2883.078	1353	4236.078	1.080
	S4	2122.863	642.996	2765.859	2045.67	656.59	2702.26	1.024
	S12	2544.404	1082.334	3626.738	2283.798	1054.625	3338.423	1.086
1	S1	1228.849	282.396	1511.245	1223.4	315	1538.4	0.982
	S9	1882.773	594.988	2477.761	1859.52	615	2474.52	1.001
	S2	2351.030	690.757	3041.787	2239.56	693	2932.56	1.037
	S10	3242.847	1379.755	4622.602	2913.12	1353	4266.12	1.084
	S3	2427.246	726.994	3154.240	2401.32	756	3157.32	0.999
	S11	3474.628	1519.565	4994.193	3145.176	1476	4621.176	1.081
	S4	2326.186	702.717	3028.903	2231.64	716.28	2947.92	1.027
	S12	2779.300	1177.025	3956.325	2491.416	1150.5	3641.916	1.086

Çizelge A.5: 12 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
12	S1	98.001	13.151	111.152	101.95	15.75	117.7	0.944
	S9	152.585	28.905	181.490	154.96	30.75	185.71	0.977
	S2	191.231	33.902	225.133	186.63	34.65	221.28	1.017
	S10	272.226	71.472	343.698	242.76	67.65	310.41	1.107
	S3	195.919	35.363	231.281	200.11	37.8	237.91	0.972
	S11	287.712	77.944	365.656	262.098	73.8	335.898	1.089
	S4	185.548	33.489	219.037	185.97	35.814	221.784	0.988
	S12	224.041	57.386	281.427	207.618	57.525	265.143	1.061
11	S1	203.064	28.330	231.394	203.9	31.5	235.4	0.983
	S9	306.746	58.888	365.633	309.92	61.5	371.42	0.984
	S2	382.022	68.185	450.207	373.26	69.3	442.56	1.017
	S10	535.799	139.326	675.124	485.52	135.3	620.82	1.087
	S3	394.154	72.037	466.191	400.22	75.6	475.82	0.980
	S11	570.366	153.881	724.246	524.196	147.6	671.796	1.078
	S4	375.020	68.382	443.402	371.94	71.628	443.568	1.000
	S12	454.371	118.157	572.528	415.236	115.05	530.286	1.080
10	S1	306.824	43.147	349.970	305.85	47.25	353.1	0.991
	S9	460.443	88.609	549.051	464.88	92.25	557.13	0.985
	S2	572.764	102.283	675.047	559.89	103.95	663.84	1.017
	S10	801.125	207.926	1009.052	728.28	202.95	931.23	1.084
	S3	591.782	108.373	700.155	600.33	113.4	713.73	0.981
	S11	854.042	230.211	1084.253	786.294	221.4	1007.694	1.076
	S4	563.813	103.015	666.828	557.91	107.442	665.352	1.002
	S12	683.074	178.184	861.258	622.854	172.575	795.429	1.083
9	S1	410.022	57.830	467.853	407.8	63	470.8	0.994
	S9	613.705	118.212	731.917	619.84	123	742.84	0.985
	S2	765.418	136.659	902.077	746.52	138.6	885.12	1.019
	S10	1069.200	276.546	1345.746	971.04	270.6	1241.64	1.084
	S3	788.220	144.394	932.614	800.44	151.2	951.64	0.980
	S11	1140.549	306.543	1447.092	1048.392	295.2	1343.592	1.077
	S4	754.246	137.939	892.185	743.88	143.256	887.136	1.006
	S12	914.483	238.209	1152.692	830.472	230.1	1060.572	1.087
8	S1	512.562	72.329	584.890	509.75	78.75	588.5	0.994
	S9	766.948	147.749	914.697	774.8	153.75	928.55	0.985
	S2	958.734	171.236	1129.969	933.15	173.25	1106.4	1.021
	S10	1337.013	345.192	1682.205	1213.8	338.25	1552.05	1.084
	S3	984.452	180.241	1164.693	1000.55	189	1189.55	0.979
	S11	1427.353	382.971	1810.325	1310.49	369	1679.49	1.078
	S4	945.124	173.070	1118.194	929.85	179.07	1108.92	1.008
	S12	1145.247	298.000	1443.247	1038.09	287.625	1325.715	1.089
7	S1	614.219	86.557	700.775	611.7	94.5	706.2	0.992
	S9	920.245	177.176	1097.421	929.76	184.5	1114.26	0.985
	S2	1151.444	205.574	1357.018	1119.78	207.9	1327.68	1.022
	S10	1608.730	414.356	2023.086	1456.56	405.9	1862.46	1.086
	S3	1182.128	216.044	1398.172	1200.66	226.8	1427.46	0.979
	S11	1717.259	459.522	2176.781	1572.588	442.8	2015.388	1.080
	S4	1135.068	207.951	1343.019	1115.82	214.884	1330.704	1.009
	S12	1379.028	357.770	1736.798	1245.708	345.15	1590.858	1.092
6	S1	714.962	100.539	815.501	713.65	110.25	823.9	0.990
	S9	1076.249	206.965	1283.214	1084.72	215.25	1299.97	0.987
	S2	1348.935	240.413	1589.348	1306.41	242.55	1548.96	1.026
	S10	1877.494	482.902	2360.396	1699.32	473.55	2172.87	1.086
	S3	1382.184	252.119	1634.302	1400.77	264.6	1665.37	0.981

	S11	2011.436	535.774	2547.210	1834.686	516.6	2351.286	1.083
	S4	1329.528	243.291	1572.819	1301.79	250.698	1552.488	1.013
	S12	1610.595	416.893	2027.489	1453.326	402.675	1856.001	1.092
5	S1	815.111	114.329	929.440	815.6	126	941.6	0.987
	S9	1235.217	237.063	1472.281	1239.68	246	1485.68	0.991
	S2	1546.683	275.327	1822.010	1493.04	277.2	1770.24	1.029
	S10	2148.640	551.380	2700.020	1942.08	541.2	2483.28	1.087
	S3	1585.609	288.628	1874.237	1600.88	302.4	1903.28	0.985
	S11	2302.742	611.371	2914.114	2096.784	590.4	2687.184	1.084
	S4	1524.760	278.809	1803.569	1487.76	286.512	1774.272	1.017
	S12	1844.426	475.666	2320.092	1660.944	460.2	2121.144	1.094
4	S1	914.684	127.864	1042.548	917.55	141.75	1059.3	0.984
	S9	1394.831	267.155	1661.985	1394.64	276.75	1671.39	0.994
	S2	1746.448	310.283	2056.731	1679.67	311.85	1991.52	1.033
	S10	2419.509	620.175	3039.684	2184.84	608.85	2793.69	1.088
	S3	1792.215	325.383	2117.598	1800.99	340.2	2141.19	0.989
	S11	2594.138	686.682	3280.820	2358.882	664.2	3023.082	1.085
	S4	1722.118	314.367	2036.486	1673.73	322.326	1996.056	1.020
	S12	2076.880	534.055	2610.935	1868.562	517.725	2386.287	1.094
3	S1	1019.113	141.797	1160.910	1019.5	157.5	1177	0.986
	S9	1557.427	297.221	1854.648	1549.6	307.5	1857.1	0.999
	S2	1944.673	344.827	2289.500	1866.3	346.5	2212.8	1.035
	S10	2693.237	689.120	3382.357	2427.6	676.5	3104.1	1.090
	S3	2001.404	362.292	2363.696	2001.1	378	2379.1	0.994
	S11	2888.256	761.798	3650.054	2620.98	738	3358.98	1.087
	S4	1919.898	349.916	2269.814	1859.7	358.14	2217.84	1.023
	S12	2311.826	592.054	2903.881	2076.18	575.25	2651.43	1.095
2	S1	1124.753	155.880	1280.633	1121.45	173.25	1294.7	0.989
	S9	1720.145	327.234	2047.378	1704.56	338.25	2042.81	1.002
	S2	2147.308	379.552	2526.861	2052.93	381.15	2434.08	1.038
	S10	2965.241	758.000	3723.240	2670.36	744.15	3414.51	1.090
	S3	2213.260	399.286	2612.546	2201.21	415.8	2617.01	0.998
	S11	3180.647	836.670	4017.317	2883.078	811.8	3694.878	1.087
	S4	2122.863	385.798	2508.661	2045.67	393.954	2439.624	1.028
	S12	2544.404	649.400	3193.805	2283.798	632.775	2916.573	1.095
1	S1	1228.849	169.437	1398.287	1223.4	189	1412.4	0.990
	S9	1882.773	356.993	2239.765	1859.52	369	2228.52	1.005
	S2	2351.030	414.454	2765.484	2239.56	415.8	2655.36	1.041
	S10	3242.847	827.853	4070.700	2913.12	811.8	3724.92	1.093
	S3	2427.246	436.196	2863.442	2401.32	453.6	2854.92	1.003
	S11	3474.628	911.739	4386.367	3145.176	885.6	4030.776	1.088
	S4	2326.186	421.630	2747.816	2231.64	429.768	2661.408	1.032
	S12	2779.300	706.215	3485.515	2491.416	690.3	3181.716	1.095

Çizelge A.6: 12 Katlı Hatane Binasına Ait Düşey Yüklerden Oluşan Eksenel Kuvvetler ve Oranları (Y).

KAT	Y	KOLON	N _G (kN)	N _{YQ} (kN)	N _{G+YQ} (kN)	N _{G0} (kN)	N _{YQ0} (kN)	N _{G0+YQ0} (kN)	$k_{PY}=N_{G+YQ}/N_{G0+YQ0}$
12	0.6	S1	98.001	13.151	111.152	101.95	15.75	117.700	0.944
	0.6	S9	152.585	28.905	181.490	154.96	30.75	185.710	0.977
	0.6	S2	191.231	33.902	225.133	186.63	34.65	221.280	1.017
	0.6	S10	272.226	71.472	343.698	242.76	67.65	310.410	1.107
	0.6	S3	195.919	35.363	231.281	200.11	37.8	237.910	0.972
	0.6	S11	287.712	77.944	365.656	262.098	73.8	335.898	1.089
	0.6	S4	185.548	33.489	219.037	185.97	35.814	221.784	0.988
	0.6	S12	224.041	57.386	281.427	207.618	57.525	265.143	1.061
11	0.6	S1	203.064	26.302	229.366	203.9	31.5	235.400	0.974
	0.6	S9	306.746	57.810	364.555	309.92	61.5	371.420	0.982
	0.6	S2	382.022	67.804	449.826	373.26	69.3	442.560	1.016
	0.6	S10	535.799	142.944	678.743	485.52	135.3	620.820	1.093
	0.6	S3	394.154	70.726	464.880	400.22	75.6	475.820	0.977
	0.6	S11	570.366	155.888	726.254	524.196	147.6	671.796	1.081
	0.6	S4	375.020	66.979	441.998	371.94	71.628	443.568	0.996
	0.6	S12	454.371	114.772	569.143	415.236	115.05	530.286	1.073
10	0.6	S1	306.824	39.453	346.277	305.85	47.25	353.100	0.981
	0.6	S9	460.443	86.715	547.157	464.88	92.25	557.130	0.982
	0.6	S2	572.764	101.707	674.471	559.89	103.95	663.840	1.016
	0.6	S10	801.125	214.417	1015.542	728.28	202.95	931.230	1.091
	0.6	S3	591.782	106.089	697.871	600.33	113.4	713.730	0.978
	0.6	S11	854.042	233.832	1087.874	786.294	221.4	1007.694	1.080
	0.6	S4	563.813	100.468	664.281	557.91	107.442	665.352	0.998
	0.6	S12	683.074	172.158	855.232	622.854	172.575	795.429	1.075
9	0.1	S1	410.022	41.645	451.667	407.8	49.875	457.675	0.987
	0.1	S9	613.705	91.532	705.238	619.84	97.375	717.215	0.983
	0.1	S2	765.418	107.357	872.775	746.52	109.725	856.245	1.019
	0.1	S10	1069.200	226.329	1295.528	971.04	214.225	1185.265	1.093
	0.1	S3	788.220	111.983	900.203	800.44	119.7	920.140	0.978
	0.1	S11	1140.549	246.823	1387.372	1048.392	233.7	1282.092	1.082
	0.1	S4	754.246	106.049	860.295	743.88	113.411	857.291	1.004
	0.1	S12	914.483	181.722	1096.205	830.472	182.1625	1012.635	1.083
8	0.2	S1	512.562	46.029	558.590	509.75	55.125	564.875	0.989
	0.2	S9	766.948	101.167	868.116	774.8	107.625	882.425	0.984
	0.2	S2	958.734	118.658	1077.391	933.15	121.275	1054.425	1.022

	0.2	S10	1337.013	250.153	1587.166	1213.8	236.775	1450.575	1.094
	0.2	S3	984.452	123.770	1108.223	1000.55	132.3	1132.850	0.978
	0.2	S11	1427.353	272.804	1700.157	1310.49	258.3	1568.790	1.084
	0.2	S4	945.124	117.213	1062.336	929.85	125.349	1055.199	1.007
	0.2	S12	1145.247	200.851	1346.098	1038.09	201.3375	1239.428	1.086
7	0.2	S1	614.219	46.029	660.247	611.7	60.375	672.075	0.982
	0.2	S9	920.245	101.167	1021.412	929.76	117.875	1047.635	0.975
	0.2	S2	1151.444	118.658	1270.101	1119.78	132.825	1252.605	1.014
	0.2	S10	1608.730	250.153	1858.883	1456.56	259.325	1715.885	1.083
	0.2	S3	1182.128	123.770	1305.898	1200.66	144.9	1345.560	0.971
	0.2	S11	1717.259	272.804	1990.063	1572.588	282.9	1855.488	1.073
	0.2	S4	1135.068	117.213	1252.280	1115.82	137.287	1253.107	0.999
	0.2	S12	1379.028	200.851	1579.879	1245.708	220.5125	1466.221	1.078
6	0.4	S1	714.962	59.180	774.141	713.65	70.875	784.525	0.987
	0.4	S9	1076.249	130.072	1206.322	1084.72	138.375	1223.095	0.986
	0.4	S2	1348.935	152.560	1501.495	1306.41	155.925	1462.335	1.027
	0.4	S10	1877.494	321.625	2199.118	1699.32	304.425	2003.745	1.098
	0.4	S3	1382.184	159.133	1541.317	1400.77	170.1	1570.870	0.981
	0.4	S11	2011.436	350.748	2362.184	1834.686	332.1	2166.786	1.090
	0.4	S4	1329.528	150.702	1480.230	1301.79	161.163	1462.953	1.012
	0.4	S12	1610.595	258.237	1868.832	1453.326	258.8625	1712.189	1.091
5	0.6	S1	815.111	72.331	887.441	815.6	86.625	902.225	0.984
	0.6	S9	1235.217	158.977	1394.195	1239.68	169.125	1408.805	0.990
	0.6	S2	1546.683	186.462	1733.145	1493.04	190.575	1683.615	1.029
	0.6	S10	2148.640	393.097	2541.737	1942.08	372.075	2314.155	1.098
	0.6	S3	1585.609	194.496	1780.105	1600.88	207.9	1808.780	0.984
	0.6	S11	2302.742	428.692	2731.434	2096.784	405.9	2502.684	1.091
	0.6	S4	1524.760	184.191	1708.951	1487.76	196.977	1684.737	1.014
	0.6	S12	1844.426	315.623	2160.048	1660.944	316.3875	1977.332	1.092
4	0.8	S1	914.684	89.865	1004.549	917.55	107.625	1025.175	0.980
	0.8	S9	1394.831	197.517	1592.348	1394.64	210.125	1604.765	0.992
	0.8	S2	1746.448	231.665		1679.67	236.775	1916.445	1.032
	0.8	S10	2419.509	488.393	2907.902	2184.84	462.275	2647.115	1.099
	0.8	S3	1792.215	241.647	2033.861	1800.99	258.3	2059.290	0.988
	0.8	S11	2594.138	532.617	3126.756	2358.882	504.3	2863.182	1.092
	0.8	S4	1722.118	228.844	1950.962	1673.73	244.729	1918.459	1.017
	0.8	S12	2076.880	392.137	2469.017	1868.562	393.0875	2261.650	1.092
3	1	S1	1019.113	111.784	1130.896	1019.5	133.875	1153.375	0.981

	1	S9	1557.427	245.692	1803.119	1549.6	261.375	1810.975	0.996
	1	S2	1944.673	288.169	2232.842	1866.3	294.525	2160.825	1.033
	1	S10	2693.237	607.514	3300.751	2427.6	575.025	3002.625	1.099
	1	S3	2001.404	300.585	2301.988	2001.1	321.3	2322.400	0.991
	1	S11	2888.256	662.524	3550.780	2620.98	627.3	3248.280	1.093
	1	S4	1919.898	284.659	2204.557	1859.7	304.419	2164.119	1.019
	1	S12	2311.826	487.780	2799.607	2076.18	488.9625	2565.143	1.091
2	1	S1	1124.753	133.702	1258.456	1121.45	160.125	1281.575	0.982
	1	S9	1720.145	293.867	2014.011	1704.56	312.625	2017.185	0.998
	1	S2	2147.308	344.673	2491.981	2052.93	352.275	2405.205	1.036
	1	S10	2965.241	726.634	3691.874	2670.36	687.775	3358.135	1.099
	1	S3	2213.260	359.523	2572.783	2201.21	384.300	2585.510	0.995
	1	S11	3180.647	792.431	3973.078	2883.078	750.300	3633.378	1.093
	1	S4	2122.863	340.475	2463.337	2045.67	364.109	2409.779	1.022
	1	S12	2544.404	583.424	3127.828	2283.798	584.838	2868.636	1.090
1	1	S1	1228.849	155.621	1384.470	1223.4	186.375	1409.775	0.982
	1	S9	1882.773	342.042	2224.814	1859.52	363.875	2223.395	1.001
	1	S2	2351.030	401.176	2752.207	2239.56	410.025	2649.585	1.039
	1	S10	3242.847	845.754	4088.602	2913.12	800.525	3713.645	1.101
	1	S3	2427.246	418.461	2845.707	2401.32	447.3	2848.620	0.999
	1	S11	3474.628	922.338	4396.966	3145.176	873.3	4018.476	1.094
	1	S4	2326.186	396.290	2722.476	2231.64	423.799	2655.439	1.025
	1	S12	2779.300	679.067	3458.366	2491.416	680.7125	3172.129	1.090

Model 2

Çizelge A.7: 9 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_G+Q/N_{G0}+Q_0$
9	S10	253.135	114.000	367.135	242.76	112.75	355.51	1.033
	S11	281.161	127.933	409.094	262.098	123	385.098	1.062
	S4	187.105	56.101	243.206	185.97	59.69	245.66	0.990
	S12	222.284	94.713	316.997	207.618	95.875	303.493	1.044
8	S10	496.649	222.447	719.096	485.52	225.5	711.02	1.011
	S11	555.570	252.438	808.008	524.196	246	770.196	1.049
	S4	375.477	113.607	489.084	371.94	119.38	491.32	0.995
	S12	449.713	194.755	644.468	415.236	191.75	606.986	1.062
7	S10	742.983	332.390	1075.373	728.28	338.25	1066.53	1.008
	S11	831.776	377.851	1209.627	786.294	369	1155.294	1.047
	S4	563.631	170.855	734.485	557.91	179.07	736.98	0.997
	S12	675.590	293.566	969.156	622.854	287.625	910.479	1.064
6	S10	994.566	443.502	1438.068	971.04	451	1422.04	1.011
	S11	1111.172	503.479	1614.651	1048.392	492	1540.392	1.048
	S4	754.316	228.803	983.119	743.88	238.76	982.64	1.000
	S12	903.792	392.200	1295.993	830.472	383.5	1213.972	1.068
5	S10	1248.901	555.909	1804.810	1213.8	563.75	1777.55	1.015
	S11	1391.640	629.581	2021.221	1310.49	615	1925.49	1.050
	S4	946.618	287.402	1234.019	929.85	298.45	1228.3	1.005
	S12	1131.006	490.279	1621.285	1038.09	479.375	1517.465	1.068
4	S10	1509.396	669.881	2179.277	1456.56	676.5	2133.06	1.022
	S11	1676.579	756.430	2433.009	1572.588	738	2310.588	1.053
	S4	1139.351	346.014	1485.365	1115.82	358.14	1473.96	1.008
	S12	1360.988	588.173	1949.161	1245.708	575.25	1820.958	1.070
3	S10	1772.876	785.368	2558.244	1699.32	789.25	2488.57	1.028
	S11	1968.650	884.150	2852.800	1834.686	861	2695.686	1.058
	S4	1337.903	405.727	1743.630	1301.79	417.83	1719.62	1.014
	S12	1588.323	684.806	2273.129	1453.326	671.125	2124.451	1.070
2	S10	2043.616	902.847	2946.463	1942.08	902	2844.08	1.036
	S11	2260.184	1011.754	3271.938	2096.784	984	3080.784	1.062
	S4	1538.702	466.154	2004.857	1487.76	477.52	1965.28	1.020
	S12	1817.470	780.616	2598.086	1660.944	767	2427.944	1.070
1	S10	2318.771	1022.781	3341.552	2184.84	1014.75	3199.59	1.044
	S11	2555.338	1140.462	3695.800	2358.882	1107	3465.882	1.066
	S4	1741.991	526.601	2268.592	1673.73	537.21	2210.94	1.026
	S12	2045.297	875.734	2921.030	1868.562	862.875	2731.437	1.069

Çizelge A.8: 9 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
9	S10	253.135	68.400	321.535	242.76	67.65	310.41	1.036
	S11	281.161	76.760	357.921	262.098	73.8	335.898	1.066
	S4	187.105	33.661	220.766	185.97	35.814	221.784	0.995
	S12	222.284	56.828	279.111	207.618	57.525	265.143	1.053
8	S10	496.649	133.468	630.117	485.52	135.3	620.82	1.015
	S11	555.570	151.463	707.032	524.196	147.6	671.796	1.052
	S4	375.477	68.164	443.641	371.94	71.628	443.568	1.000
	S12	449.713	116.853	566.566	415.236	115.05	530.286	1.068
7	S10	742.983	199.434	942.417	728.28	202.95	931.23	1.012
	S11	831.776	226.711	1058.486	786.294	221.4	1007.694	1.050
	S4	563.631	102.513	666.143	557.91	107.442	665.352	1.001
	S12	675.590	176.140	851.729	622.854	172.575	795.429	1.071
6	S10	994.566	266.101	1260.667	971.04	270.6	1241.64	1.015
	S11	1111.172	302.087	1413.259	1048.392	295.2	1343.592	1.052
	S4	754.316	137.282	891.598	743.88	143.256	887.136	1.005
	S12	903.792	235.320	1139.112	830.472	230.1	1060.572	1.074
5	S10	1248.901	333.545	1582.447	1213.8	338.25	1552.05	1.020
	S11	1391.640	377.748	1769.389	1310.49	369	1679.49	1.054
	S4	946.618	172.441	1119.058	929.85	179.07	1108.92	1.009
	S12	1131.006	294.167	1425.173	1038.09	287.625	1325.715	1.075
4	S10	1509.396	401.929	1911.324	1456.56	405.9	1862.46	1.026
	S11	1676.579	453.858	2130.437	1572.588	442.8	2015.388	1.057
	S4	1139.351	207.609	1346.959	1115.82	214.884	1330.704	1.012
	S12	1360.988	352.904	1713.891	1245.708	345.15	1590.858	1.077
3	S10	1772.876	471.221	2244.097	1699.32	473.55	2172.87	1.033
	S11	1968.650	530.490	2499.140	1834.686	516.6	2351.286	1.063
	S4	1337.903	243.436	1581.339	1301.79	250.698	1552.488	1.019
	S12	1588.323	410.884	1999.207	1453.326	402.675	1856.001	1.077
2	S10	2043.616	541.708	2585.324	1942.08	541.2	2483.28	1.041
	S11	2260.184	607.052	2867.237	2096.784	590.4	2687.184	1.067
	S4	1538.702	279.693	1818.395	1487.76	286.512	1774.272	1.025
	S12	1817.470	468.370	2285.840	1660.944	460.2	2121.144	1.078
1	S10	2318.771	613.669	2932.440	2184.84	608.85	2793.69	1.050
	S11	2555.338	684.277	3239.615	2358.882	664.2	3023.082	1.072
	S4	1741.991	315.960	2057.951	1673.73	322.326	1996.056	1.031
	S12	2045.297	525.440	2570.737	1868.562	517.725	2386.287	1.077

Çizelge A.9: Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	Y	KOLON	$N_G(kN)$	$N_{YQ}(kN)$	$N_{G+YQ}(kN)$	$N_{G0}(kN)$	$N_{YQ0}(kN)$	$N_{G0+YQ0}(kN)$	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
9	0.1	S10	253.135	11.400	264.535	242.76	11.275	254.035	1.041
	0.1	S11	281.161	12.793	293.954	262.098	12.300	274.398	0.964
	0.1	S4	187.105	5.610	192.715	185.97	5.969	191.939	1.378
	0.1	S12	222.284	9.471	231.755	207.618	9.588	217.2055	1.218
8	0.2	S10	496.649	34.200	530.848	485.52	33.825	519.345	0.509
	0.2	S11	555.570	38.380	593.949	524.196	36.900	561.096	0.471
	0.2	S4	375.477	16.830	392.307	371.94	17.907	389.847	0.679
	0.2	S12	449.713	28.414	478.126	415.236	28.763	443.9985	0.596
7	0.2	S10	742.983	57.000	799.983	728.28	56.375	784.655	0.337
	0.2	S11	831.776	63.967	895.742	786.294	61.500	847.794	0.312
	0.2	S4	563.631	28.050	591.681	557.91	29.845	587.755	0.450
	0.2	S12	675.590	47.356	722.946	622.854	47.938	670.7915	0.394
6	0.4	S10	994.566	102.600	1097.166	971.04	101.475	1072.515	0.247
	0.4	S11	1111.172	115.140	1226.312	1048.392	110.700	1159.092	0.228
	0.4	S4	754.316	50.491	804.806	743.88	53.721	797.601	0.332
	0.4	S12	903.792	85.241	989.034	830.472	86.288	916.7595	0.289
5	0.6	S10	1248.901	171.000	1419.901	1213.8	169.125	1382.925	0.191
	0.6	S11	1391.640	191.900	1583.540	1310.49	184.500	1494.99	0.177
	0.6	S4	946.618	84.151	1030.769	929.85	89.535	1019.385	0.260
	0.6	S12	1131.006	142.069	1273.075	1038.09	143.813	1181.9025	0.224
4	0.8	S10	1509.396	262.200	1771.595	1456.56	259.325	1715.885	0.154
	0.8	S11	1676.579	294.246	1970.825	1572.588	282.900	1855.488	0.143
	0.8	S4	1139.351	129.032	1268.383	1115.82	137.287	1253.107	0.211
	0.8	S12	1360.988	217.839	1578.827	1245.708	220.513	1466.2205	0.180
3	1	S10	1772.876	376.200	2149.076	1699.32	372.075	2071.395	0.128
	1	S11	1968.650	422.179	2390.829	1834.686	405.900	2240.586	0.118
	1	S4	1337.903	185.133	1523.036	1301.79	196.977	1498.767	0.177
	1	S12	1588.323	312.552	1900.875	1453.326	316.388	1769.7135	0.149
2	1	S10	2043.616	490.200	2533.816	1942.08	484.825	2426.905	0.109
	1	S11	2260.184	550.112	2810.297	2096.784	528.900	2625.684	0.101
	1	S4	1538.702	241.234	1779.936	1487.76	256.667	1744.427	0.152
	1	S12	1817.470	407.265	2224.735	1660.944	412.263	2073.2065	0.128
1	1	S10	2318.771	604.199	2922.970	2184.84	597.575	2782.415	0.095
	1	S11	2555.338	678.045	3233.383	2358.882	651.900	3010.782	0.088
	1	S4	1741.991	297.335	2039.326	1673.73	316.357	1990.087	0.133
	1	S12	2045.297	501.977	2547.274	1868.562	508.138	2376.6995	0.111

Çizelge A.10: 12 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_{G+Q}/N_{G0+Q0}$
12	S10	248.754	111.209	359.963	242.76	112.75	355.51	1.013
	S11	280.647	127.301	407.948	262.098	123	385.098	1.059
	S4	184.383	55.463	239.845	185.97	59.69	245.66	0.976
	S12	224.974	95.931	320.905	207.618	95.875	303.493	1.057
11	S10	486.684	216.070	702.754	485.52	225.5	711.02	0.988
	S11	554.069	250.774	804.843	524.196	246	770.196	1.045
	S4	369.387	112.338	481.725	371.94	119.38	491.32	0.980
	S12	455.768	197.429	653.197	415.236	191.75	606.986	1.076
10	S10	727.496	322.468	1049.963	728.28	338.25	1066.53	0.984
	S11	829.338	375.200	1204.538	786.294	369	1155.294	1.043
	S4	554.190	168.928	723.118	557.91	179.07	736.98	0.981
	S12	685.008	297.719	982.727	622.854	287.625	910.479	1.079
9	S10	973.325	429.887	1403.212	971.04	451	1422.04	0.987
	S11	1107.639	499.721	1607.360	1048.392	492	1540.392	1.043
	S4	741.375	226.225	967.600	743.88	238.76	982.64	0.985
	S12	916.951	398.024	1314.975	830.472	383.5	1213.972	1.083
8	S10	1221.709	538.480	1760.189	1213.8	563.75	1777.55	0.990
	S11	1386.903	624.638	2011.541	1310.49	615	1925.49	1.045
	S4	930.037	284.172	1214.208	929.85	298.45	1228.3	0.989
	S12	1148.241	497.946	1646.186	1038.09	479.375	1517.465	1.085
7	S10	1476.029	648.496	2124.525	1456.56	676.5	2133.06	0.996
	S11	1670.523	750.219	2420.742	1572.588	738	2310.588	1.048
	S4	1119.061	342.117	1461.179	1115.82	358.14	1473.96	0.991
	S12	1382.633	597.900	1980.532	1245.708	575.25	1820.958	1.088
6	S10	1733.065	759.863	2492.929	1699.32	789.25	2488.57	1.002
	S11	1961.139	876.564	2837.703	1834.686	861	2695.686	1.053
	S4	1313.658	401.143	1714.802	1301.79	417.83	1719.62	0.997
	S12	1614.808	696.801	2311.609	1453.326	671.125	2124.451	1.088
5	S10	1997.294	873.171	2870.465	1942.08	902	2844.08	1.009
	S11	2251.305	1002.821	3254.127	2096.784	984	3080.784	1.056
	S4	1510.139	460.793	1970.932	1487.76	477.52	1965.28	1.003
	S12	1849.265	795.128	2644.393	1660.944	767	2427.944	1.089
4	S10	2264.320	988.000	3252.319	2184.84	1014.75	3199.59	1.016
	S11	2543.887	1129.537	3673.424	2358.882	1107	3465.882	1.060
	S4	1709.835	520.838	2230.674	1673.73	537.21	2210.94	1.009
	S12	2082.476	892.870	2975.346	1868.562	862.875	2731.437	1.089
3	S10	2538.426	1104.664	3643.090	2427.6	1127.5	3555.1	1.025
	S11	2841.058	1256.649	4097.707	2620.98	1230	3850.98	1.064
	S4	1910.889	581.152	2492.040	1859.7	596.9	2456.6	1.014
	S12	2318.210	989.982	3308.192	2076.18	958.75	3034.93	1.090
2	S10	2815.032	1222.804	4037.836	2670.36	1240.25	3910.61	1.033
	S11	3138.252	1383.976	4522.228	2883.078	1353	4236.078	1.068
	S4	2117.970	642.286	2760.256	2045.67	656.59	2702.26	1.021
	S12	2551.549	1085.990	3637.539	2283.798	1054.625	3338.423	1.090
1	S10	3100.135	1343.516	4443.652	2913.12	1353	4266.12	1.042
	S11	3438.737	1512.248	4950.985	3145.176	1476	4621.176	1.071
	S4	2326.158	703.553	3029.711	2231.64	716.28	2947.92	1.028
	S12	2787.245	1181.095	3968.340	2491.416	1150.5	3641.916	1.090

Çizelge A.11: 12 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_G+\beta Q/N_{G0}+\beta Q0$
12	S10	248.754	66.725	315.480	242.76	67.65	310.41	1.016
	S11	280.647	76.380	357.027	262.098	73.8	335.898	1.063
	S4	184.383	33.278	217.660	185.97	35.814	221.784	0.981
	S12	224.974	57.559	282.533	207.618	57.525	265.143	1.066
11	S10	486.684	129.642	616.326	485.52	135.3	620.82	0.993
	S11	554.069	150.464	704.533	524.196	147.6	671.796	1.049
	S4	369.387	67.403	436.789	371.94	71.628	443.568	0.985
	S12	455.768	118.457	574.225	415.236	115.05	530.286	1.083
10	S10	727.496	193.481	920.976	728.28	202.95	931.23	0.989
	S11	829.338	225.120	1054.458	786.294	221.4	1007.694	1.046
	S4	554.190	101.357	655.547	557.91	107.442	665.352	0.985
	S12	685.008	178.631	863.639	622.854	172.575	795.429	1.086
9	S10	973.325	257.932	1231.257	971.04	270.6	1241.64	0.992
	S11	1107.639	299.833	1407.472	1048.392	295.2	1343.592	1.048
	S4	741.375	135.735	877.110	743.88	143.256	887.136	0.989
	S12	916.951	238.814	1155.765	830.472	230.1	1060.572	1.090
8	S10	1221.709	323.088	1544.797	1213.8	338.25	1552.05	0.995
	S11	1386.903	374.783	1761.686	1310.49	369	1679.49	1.049
	S4	930.037	170.503	1100.540	929.85	179.07	1108.92	0.992
	S12	1148.241	298.767	1447.008	1038.09	287.625	1325.715	1.091
7	S10	1476.029	389.097	1865.127	1456.56	405.9	1862.46	1.001
	S11	1670.523	450.131	2120.654	1572.588	442.8	2015.388	1.052
	S4	1119.061	205.270	1324.332	1115.82	214.884	1330.704	0.995
	S12	1382.633	358.740	1741.372	1245.708	345.15	1590.858	1.095
6	S10	1733.065	455.918	2188.983	1699.32	473.55	2172.87	1.007
	S11	1961.139	525.939	2487.077	1834.686	516.6	2351.286	1.058
	S4	1313.658	240.686	1554.344	1301.79	250.698	1552.488	1.001
	S12	1614.808	418.080	2032.889	1453.326	402.675	1856.001	1.095
5	S10	1997.294	523.903	2521.197	1942.08	541.2	2483.28	1.015
	S11	2251.305	601.693	2852.998	2096.784	590.4	2687.184	1.062
	S4	1510.139	276.476	1786.615	1487.76	286.512	1774.272	1.007
	S12	1849.265	477.077	2326.342	1660.944	460.2	2121.144	1.097
4	S10	2264.320	592.800	2857.119	2184.84	608.85	2793.69	1.023
	S11	2543.887	677.722	3221.609	2358.882	664.2	3023.082	1.066
	S4	1709.835	312.503	2022.338	1673.73	322.326	1996.056	1.013
	S12	2082.476	535.722	2618.198	1868.562	517.725	2386.287	1.097
3	S10	2538.426	662.798	3201.224	2427.6	676.5	3104.1	1.031
	S11	2841.058	753.989	3595.047	2620.98	738	3358.98	1.070
	S4	1910.889	348.691	2259.580	1859.7	358.14	2217.84	1.019
	S12	2318.210	593.989	2912.199	2076.18	575.25	2651.43	1.098
2	S10	2815.032	733.682	3548.715	2670.36	744.15	3414.51	1.039
	S11	3138.252	830.386	3968.637	2883.078	811.8	3694.878	1.074
	S4	2117.970	385.371	2503.341	2045.67	393.954	2439.624	1.026
	S12	2551.549	651.594	3203.143	2283.798	632.775	2916.573	1.098
1	S10	3100.135	806.110	3906.245	2913.12	811.8	3724.92	1.049
	S11	3438.737	907.349	4346.086	3145.176	885.6	4030.776	1.078
	S4	2326.158	422.132	2748.290	2231.64	429.768	2661.408	1.033
	S12	2787.245	708.657	3495.902	2491.416	690.3	3181.716	1.099

Çizelge A.12: 12 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	$N_G(kN)$	$N_{YQ}(kN)$	$N_{G+YQ}(kN)$	$N_{G0}(kN)$	$N_{YQ0}(kN)$	$N_{G0+YQ0}(kN)$	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
12	0.6	S10	248.754	66.725	315.480	242.76	67.650	310.41	1.016
	0.6	S11	280.647	76.380	357.027	262.098	73.800	335.898	1.063
	0.6	S4	184.383	33.278	217.660	185.97	35.814	221.784	0.981
	0.6	S12	224.974	57.559	282.533	207.618	57.525	265.143	1.066
11	0.6	S10	486.684	133.451	620.135	485.52	135.300	620.82	0.999
	0.6	S11	554.069	152.761	706.830	524.196	147.600	671.796	1.052
	0.6	S4	369.387	66.555	435.942	371.94	71.628	443.568	0.983
	0.6	S12	455.768	115.117	570.885	415.236	115.050	530.286	1.077
10	0.6	S10	727.496	200.176	927.672	728.28	202.950	931.23	0.996
	0.6	S11	829.338	229.141	1058.480	786.294	221.400	1007.694	1.050
	0.6	S4	554.190	99.833	654.023	557.91	107.442	665.352	0.983
	0.6	S12	685.008	172.676	857.684	622.854	172.575	795.429	1.078
9	0.1	S10	973.325	211.297	1184.621	971.04	214.225	1185.265	0.999
	0.1	S11	1107.639	241.871	1349.510	1048.392	233.700	1282.092	1.053
	0.1	S4	741.375	105.379	846.753	743.88	113.411	857.291	0.988
	0.1	S12	916.951	182.269	1099.220	830.472	182.163	1012.6345	1.086
8	0.2	S10	1221.709	233.539	1455.248	1213.8	236.775	1450.575	1.003
	0.2	S11	1386.903	267.331	1654.235	1310.49	258.300	1568.79	1.054
	0.2	S4	930.037	116.471	1046.508	929.85	125.349	1055.199	0.992
	0.2	S12	1148.241	201.456	1349.696	1038.09	201.338	1239.4275	1.089
7	0.2	S10	1476.029	255.780	1731.810	1456.56	259.325	1715.885	1.009
	0.2	S11	1670.523	292.792	1963.315	1572.588	282.900	1855.488	1.058
	0.2	S4	1119.061	127.564	1246.625	1115.82	137.287	1253.107	0.995
	0.2	S12	1382.633	220.642	1603.274	1245.708	220.513	1466.2205	1.093
6	0.4	S10	1733.065	300.264	2033.329	1699.32	304.425	2003.745	1.015
	0.4	S11	1961.139	343.712	2304.851	1834.686	332.100	2166.786	1.064
	0.4	S4	1313.658	149.749	1463.407	1301.79	161.163	1462.953	1.000
	0.4	S12	1614.808	259.014	1873.822	1453.326	258.863	1712.1885	1.094
5	0.6	S10	1997.294	366.989	2364.283	1942.08	372.075	2314.155	1.022
	0.6	S11	2251.305	420.092	2671.398	2096.784	405.900	2502.684	1.067
	0.6	S4	1510.139	183.027	1693.166	1487.76	196.977	1684.737	1.005
	0.6	S12	1849.265	316.573	2165.838	1660.944	316.388	1977.3315	1.095
4	0.8	S10	2264.320	455.956	2720.276	2184.84	462.275	2647.115	1.028
	0.8	S11	2543.887	521.933	3065.820	2358.882	504.300	2863.182	1.071
	0.8	S4	1709.835	227.397	1937.232	1673.73	244.729	1918.459	1.010
	0.8	S12	2082.476	393.318	2475.794	1868.562	393.088	2261.6495	1.095
3	1	S10	2538.426	567.165	3105.592	2427.6	575.025	3002.625	1.034
	1	S11	2841.058	649.234	3490.292	2620.98	627.300	3248.28	1.075

	1	S4	1910.889	282.859	2193.748	1859.7	304.419	2164.119	1.014
	1	S12	2318.210	489.249	2807.459	2076.18	488.963	2565.1425	1.094
2	1	S10	2815.032	678.374	3493.406	2670.36	687.775	3358.135	1.040
	1	S11	3138.252	776.534	3914.786	2883.078	750.300	3633.378	1.077
	1	S4	2117.970	338.322	2456.292	2045.67	364.109	2409.779	1.019
	1	S12	2551.549	585.180	3136.729	2283.798	584.838	2868.6355	1.093
1	1	S10	3100.135	789.583	3889.718	2913.12	800.525	3713.645	1.047
	1	S11	3438.737	903.835	4342.572	3145.176	873.300	4018.476	1.081
	1	S4	2326.158	393.784	2719.943	2231.64	423.799	2655.439	1.024
	1	S12	2787.245	681.112	3468.356	2491.416	680.713	3172.1285	1.093

Model 3

Çizelge A.13: 9 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p = N_{G+Q}/N_{G0+Q0}$
9	S10	259.017	116.572	375.589	242.76	112.75	355.51	1.056
	S3	193.965	57.444	251.409	200.11	63	263.11	0.956
	S11	290.614	131.369	421.984	262.098	123	385.098	1.096
	S4	187.738	56.302	244.040	185.97	59.69	245.66	0.993
	S12	221.351	94.467	315.818	207.618	95.875	303.493	1.041
8	S10	506.811	226.997	733.808	485.52	225.5	711.02	1.032
	S3	387.328	116.074	503.402	400.22	126	526.22	0.957
	S11	574.510	259.138	833.648	524.196	246	770.196	1.082
	S4	379.984	114.944	494.928	371.94	119.38	491.32	1.007
	S12	448.583	194.486	643.069	415.236	191.75	606.986	1.059
7	S10	757.034	338.749	1095.784	728.28	338.25	1066.53	1.027
	S3	580.741	174.401	755.141	600.33	189	789.33	0.957
	S11	859.636	387.638	1247.275	786.294	369	1155.294	1.080
	S4	571.458	173.200	744.657	557.91	179.07	736.98	1.010
	S12	674.154	293.250	967.403	622.854	287.625	910.479	1.063
6	S10	1012.506	451.691	1464.197	971.04	451	1422.04	1.030
	S3	773.977	232.507	1006.485	800.44	252	1052.44	0.956
	S11	1147.349	516.183	1663.532	1048.392	492	1540.392	1.080
	S4	764.615	231.922	996.537	743.88	238.76	982.64	1.014
	S12	902.147	391.878	1294.024	830.472	383.5	1213.972	1.066
5	S10	1270.732	565.935	1836.667	1213.8	563.75	1777.55	1.033
	S3	968.153	290.690	1258.843	1000.55	315	1315.55	0.957
	S11	1435.206	644.930	2080.136	1310.49	615	1925.49	1.080
	S4	958.239	290.978	1249.217	929.85	298.45	1228.3	1.017
	S12	1129.204	489.975	1619.178	1038.09	479.375	1517.465	1.067
4	S10	1535.190	681.768	2216.958	1456.56	676.5	2133.06	1.039
	S3	1165.249	349.262	1514.511	1200.66	378	1578.66	0.959
	S11	1725.986	773.900	2499.886	1572.588	738	2310.588	1.082
	S4	1150.742	349.561	1500.303	1115.82	358.14	1473.96	1.018
	S12	1359.004	587.875	1946.879	1245.708	575.25	1820.958	1.069
3	S10	1802.501	799.051	2601.552	1699.32	789.25	2488.57	1.045
	S3	1366.777	408.922	1775.699	1400.77	441	1841.77	0.964
	S11	2020.788	902.412	2923.200	1834.686	861	2695.686	1.084
	S4	1347.629	408.816	1756.445	1301.79	417.83	1719.62	1.021
	S12	1586.094	684.457	2270.550	1453.326	671.125	2124.451	1.069
2	S10	2077.204	918.359	2995.563	1942.08	902	2844.08	1.053
	S3	1573.251	469.841	2043.092	1600.88	504	2104.88	0.971
	S11	2312.300	1029.708	3342.008	2096.784	984	3080.784	1.085
	S4	1545.409	468.374	2013.783	1487.76	477.52	1965.28	1.025
	S12	1814.890	780.155	2595.045	1660.944	767	2427.944	1.069
1	S10	2356.614	1040.192	3396.806	2184.84	1014.75	3199.59	1.062
	S3	1783.821	531.283	2315.104	1800.99	567	2367.99	0.978
	S11	2605.047	1157.194	3762.241	2358.882	1107	3465.882	1.086
	S4	1744.355	527.548	2271.903	1673.73	537.21	2210.94	1.028
	S12	2042.198	875.094	2917.292	1868.562	862.875	2731.437	1.068

Çizelge A.14: 9 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
9	S10	259.017	69.943	328.960	242.76	67.65	310.41	1.060
	S3	193.965	34.466	228.431	200.11	37.8	237.91	0.960
	S11	290.614	78.822	369.436	262.098	73.8	335.898	1.100
	S4	187.738	33.781	221.519	185.97	35.814	221.784	0.999
	S12	221.351	56.680	278.032	207.618	57.525	265.143	1.049
8	S10	506.811	136.198	643.009	485.52	135.3	620.82	1.036
	S3	387.328	69.645	456.972	400.22	75.6	475.82	0.960
	S11	574.510	155.483	729.992	524.196	147.6	671.796	1.087
	S4	379.984	68.966	448.950	371.94	71.628	443.568	1.012
	S12	448.583	116.692	565.274	415.236	115.05	530.286	1.066
7	S10	757.034	203.250	960.284	728.28	202.95	931.23	1.031
	S3	580.741	104.641	685.381	600.33	113.4	713.73	0.960
	S11	859.636	232.583	1092.219	786.294	221.4	1007.694	1.084
	S4	571.458	103.920	675.378	557.91	107.442	665.352	1.015
	S12	674.154	175.950	850.103	622.854	172.575	795.429	1.069
6	S10	1012.506	271.014	1283.520	971.04	270.6	1241.64	1.034
	S3	773.977	139.504	913.482	800.44	151.2	951.64	0.960
	S11	1147.349	309.710	1457.059	1048.392	295.2	1343.592	1.084
	S4	764.615	139.153	903.768	743.88	143.256	887.136	1.019
	S12	902.147	235.127	1137.273	830.472	230.1	1060.572	1.072
5	S10	1270.732	339.561	1610.293	1213.8	338.25	1552.05	1.038
	S3	968.153	174.414	1142.567	1000.55	189	1189.55	0.961
	S11	1435.206	386.958	1822.164	1310.49	369	1679.49	1.085
	S4	958.239	174.587	1132.826	929.85	179.07	1108.92	1.022
	S12	1129.204	293.985	1423.188	1038.09	287.625	1325.715	1.074
4	S10	1535.190	409.061	1944.251	1456.56	405.9	1862.46	1.044
	S3	1165.249	209.557	1374.806	1200.66	226.8	1427.46	0.963
	S11	1725.986	464.340	2190.326	1572.588	442.8	2015.388	1.087
	S4	1150.742	209.736	1360.479	1115.82	214.884	1330.704	1.022
	S12	1359.004	352.725	1711.729	1245.708	345.15	1590.858	1.076
3	S10	1802.501	479.430	2281.931	1699.32	473.55	2172.87	1.050
	S3	1366.777	245.353	1612.130	1400.77	264.6	1665.37	0.968
	S11	2020.788	541.447	2562.235	1834.686	516.6	2351.286	1.090
	S4	1347.629	245.289	1592.918	1301.79	250.698	1552.488	1.026
	S12	1586.094	410.674	1996.768	1453.326	402.675	1856.001	1.076
2	S10	2077.204	551.015	2628.219	1942.08	541.2	2483.28	1.058
	S3	1573.251	281.905	1855.156	1600.88	302.4	1903.28	0.975
	S11	2312.300	617.825	2930.125	2096.784	590.4	2687.184	1.090
	S4	1545.409	281.024	1826.433	1487.76	286.512	1774.272	1.029
	S12	1814.890	468.093	2282.983	1660.944	460.2	2121.144	1.076
1	S10	2356.614	624.115	2980.729	2184.84	608.85	2793.69	1.067
	S3	1783.821	318.770	2102.591	1800.99	340.2	2141.19	0.982
	S11	2605.047	694.316	3299.364	2358.882	664.2	3023.082	1.091
	S4	1744.355	316.529	2060.884	1673.73	322.326	1996.056	1.032
	S12	2042.198	525.057	2567.255	1868.562	517.725	2386.287	1.076

Çizelge A.15: 9 Katlı Hastane Binasına için $k_{p-\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	$N_G(kN)$	$N_{YQ}(kN)$	$N_{G+YQ}(kN)$	$N_{G0}(kN)$	$N_{YQ0}(kN)$	$N_{G0+YQ0}(kN)$	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
9	0.1	S10	259.017	11.657	270.674	242.76	11.275	254.035	1.065
	0.1	S3	193.965	5.744	199.709	200.11	6.3	206.41	0.968
	0.1	S11	290.614	13.137	303.751	262.098	12.3	274.398	1.107
	0.1	S4	187.738	5.630	193.368	185.97	5.969	191.939	1.007
	0.1	S12	221.351	9.447	230.798	207.618	9.5875	217.2055	1.063
8	0.2	S10	506.811	34.972	541.782	485.52	33.825	519.345	1.043
	0.2	S3	387.328	17.233	404.561	400.22	18.9	419.12	0.965
	0.2	S11	574.510	39.411	613.921	524.196	36.9	561.096	1.094
	0.2	S4	379.984	16.891	396.875	371.94	17.907	389.847	1.018
	0.2	S12	448.583	28.340	476.923	415.236	28.7625	443.9985	1.074
7	0.2	S10	757.034	268.115	1025.150	728.28	259.325	987.605	1.038
	0.2	S3	580.741	132.121	712.861	600.33	144.9	745.23	0.957
	0.2	S11	859.636	302.150	1161.786	786.294	282.9	1069.194	1.087
	0.2	S4	571.458	129.495	700.953	557.91	137.287	695.197	1.008
	0.2	S12	674.154	217.274	891.428	622.854	220.5125	843.3665	1.057
6	0.4	S10	1012.506	314.744	1327.250	971.04	304.425	1275.465	1.041
	0.4	S3	773.977	155.098	929.075	800.44	170.1	970.54	0.957
	0.4	S11	1147.349	354.697	1502.047	1048.392	332.1	1380.492	1.088
	0.4	S4	764.615	152.016	916.630	743.88	161.163	905.043	1.013
	0.4	S12	902.147	255.061	1157.208	830.472	258.8625	1089.3345	1.062
5	0.6	S10	1270.732	384.687	1655.419	1213.8	372.075	1585.875	1.044
	0.6	S3	968.153	189.565	1157.717	1000.55	207.9	1208.45	0.958
	0.6	S11	1435.206	433.519	1868.725	1310.49	405.9	1716.39	1.089
	0.6	S4	958.239	185.797	1144.036	929.85	196.977	1126.827	1.015
	0.6	S12	1129.204	311.741	1440.945	1038.09	316.3875	1354.4775	1.064
4	0.8	S10	1535.190	477.945	2013.135	1456.56	462.275	1918.835	1.049
	0.8	S3	1165.249	235.520	1400.768	1200.66	258.3	1458.96	0.960
	0.8	S11	1725.986	538.615	2264.601	1572.588	504.3	2076.888	1.090
	0.8	S4	1150.742	230.839	1381.581	1115.82	244.729	1360.549	1.015
	0.8	S12	1359.004	387.315	1746.319	1245.708	393.0875	1638.7955	1.066
3	1	S10	1802.501	594.517	2397.018	1699.32	575.025	2274.345	1.054
	1	S3	1366.777	292.963	1659.740	1400.77	321.3	1722.07	0.964
	1	S11	2020.788	669.984	2690.772	1834.686	627.3	2461.986	1.093
	1	S4	1347.629	287.141	1634.770	1301.79	304.419	1606.209	1.018
	1	S12	1586.094	481.782	2067.876	1453.326	488.9625	1942.2885	1.065

2	1	S10	2077.204	711.089	2788.293	1942.08	687.775	2629.855	1.060
	1	S3	1573.251	350.407	1923.658	1600.88	384.3	1985.18	0.969
	1	S11	2312.300	801.353	3113.653	2096.784	750.3	2847.084	1.094
	1	S4	1545.409	343.443	1888.851	1487.76	364.109	1851.869	1.020
	1	S12	1814.890	576.249	2391.139	1660.944	584.8375	2245.7815	1.065
1	1	S10	2356.614	827.660	3184.274	2184.84	800.525	2985.365	1.067
	1	S3	1783.821	407.851	2191.672	1800.99	447.3	2248.29	0.975
	1	S11	2605.047	932.723	3537.770	2358.882	873.3	3232.182	1.095
	1	S4	1744.355	399.745	2144.100	1673.73	423.799	2097.529	1.022
	1	S12	2042.198	670.716	2712.914	1868.562	680.7125	2549.2745	1.064

Çizelge A.16: 12 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_{G+Q}/N_{G0+Q0}$
12	S10	253.924	113.577	367.501	242.76	112.75	355.51	1.034
	S3	190.863	56.812	247.675	200.11	63	263.11	0.941
	S11	291.358	131.206	422.565	262.098	123	385.098	1.097
	S4	186.892	56.293	243.185	185.97	59.69	245.66	0.990
	S12	224.252	95.749	320.001	207.618	95.875	303.493	1.054
11	S10	495.130	220.084	715.214	485.52	225.5	711.02	1.006
	S3	380.620	114.827	495.447	400.22	126	526.22	0.942
	S11	575.826	258.493	834.319	524.196	246	770.196	1.083
	S4	377.764	114.987	492.752	371.94	119.38	491.32	1.003
	S12	455.217	197.358	652.575	415.236	191.75	606.986	1.075
10	S10	738.794	327.941	1066.735	728.28	338.25	1066.53	1.000
	S3	570.394	172.508	742.902	600.33	189	789.33	0.941
	S11	861.584	386.560	1248.144	786.294	369	1155.294	1.080
	S4	567.931	173.285	741.216	557.91	179.07	736.98	1.006
	S12	684.489	297.725	982.215	622.854	287.625	910.479	1.079
9	S10	987.436	436.836	1424.271	971.04	451	1422.04	1.002
	S3	759.896	229.968	989.864	800.44	252	1052.44	0.941
	S11	1149.861	514.583	1664.444	1048.392	492	1540.392	1.081
	S4	759.687	232.077	991.764	743.88	238.76	982.64	1.009
	S12	916.588	398.164	1314.752	830.472	383.5	1213.972	1.083
8	S10	1238.595	546.901	1785.497	1213.8	563.75	1777.55	1.004
	S3	950.228	287.493	1237.721	1000.55	315	1315.55	0.941
	S11	1438.266	642.757	2081.023	1310.49	615	1925.49	1.081
	S4	951.857	291.231	1243.087	929.85	298.45	1228.3	1.012
	S12	1148.097	498.255	1646.351	1038.09	479.375	1517.465	1.085
7	S10	1495.718	658.403	2154.120	1456.56	676.5	2133.06	1.010
	S3	1143.341	345.390	1488.732	1200.66	378	1578.66	0.943
	S11	1729.589	771.099	2500.688	1572.588	738	2310.588	1.082
	S4	1142.817	349.870	1492.687	1115.82	358.14	1473.96	1.013
	S12	1382.684	598.374	1981.058	1245.708	575.25	1820.958	1.088
6	S10	1755.433	771.210	2526.643	1699.32	789.25	2488.57	1.015
	S3	1340.741	404.433	1745.174	1400.77	441	1841.77	0.948
	S11	2024.981	898.880	2923.861	1834.686	861	2695.686	1.085
	S4	1338.005	409.197	1747.202	1301.79	417.83	1719.62	1.016
	S12	1614.963	697.363	2312.325	1453.326	671.125	2124.451	1.088
5	S10	2022.418	885.968	2908.387	1942.08	902	2844.08	1.023
	S3	1542.835	464.695	2007.529	1600.88	504	2104.88	0.954
	S11	2317.346	1025.488	3342.834	2096.784	984	3080.784	1.085
	S4	1533.816	468.771	2002.587	1487.76	477.52	1965.28	1.019
	S12	1849.430	795.729	2645.159	1660.944	767	2427.944	1.089
4	S10	2292.343	1002.264	3294.606	2184.84	1014.75	3199.59	1.030
	S3	1749.710	525.940	2275.650	1800.99	567	2367.99	0.961
	S11	2609.731	1151.587	3761.318	2358.882	1107	3465.882	1.085
	S4	1731.603	528.352	2259.955	1673.73	537.21	2210.94	1.022
	S12	2082.528	893.469	2975.996	1868.562	862.875	2731.437	1.090
3	S10	2569.514	1120.430	3689.944	2427.6	1127.5	3555.1	1.038
	S3	1960.396	587.882	2548.278	2001.1	630	2631.1	0.969
	S11	2904.741	1277.309	4182.050	2620.98	1230	3850.98	1.086
	S4	1929.706	587.874	2517.580	1859.7	596.9	2456.6	1.025
	S12	2318.011	990.512	3308.522	2076.18	958.75	3034.93	1.090
2	S10	2849.505	1240.171	4089.675	2670.36	1240.25	3910.61	1.046
	S3	2175.343	650.493	2825.836	2201.21	693	2894.21	0.976
	S11	3197.993	1402.586	4600.579	2883.078	1353	4236.078	1.086

	S4	2132.823	647.876	2780.699	2045.67	656.59	2702.26	1.029
	S12	2550.997	1086.403	3637.399	2283.798	1054.625	3338.423	1.090
1	S10	3138.406	1362.597	4501.003	2913.12	1353	4266.12	1.055
	S3	2393.505	713.335	3106.840	2401.32	756	3157.32	0.984
	S11	3492.841	1528.151	5020.993	3145.176	1476	4621.176	1.087
	S4	2336.196	707.731	3043.927	2231.64	716.28	2947.92	1.033
	S12	2786.145	1181.306	3967.451	2491.416	1150.5	3641.916	1.089

Çizelge A.17: 12 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	$N_{\beta Q}$ (kN)	$N_{G+\beta Q}$	N_{G0} (kN)	$N_{\beta Q0}$ (kN)	$N_{G0+\beta Q0}$ (kN)	$k_{p\beta}=N_{G+\beta Q}/N_{G0+\beta Q0}$
12	S10	253.924	68.146	322.070	242.76	67.65	310.41	1.038
	S3	190.863	34.087	224.950	200.11	37.8	237.91	0.946
	S11	291.358	78.724	370.082	262.098	73.8	335.898	1.102
	S4	186.892	33.776	220.668	185.97	35.814	221.784	0.995
	S12	224.252	57.450	281.701	207.618	57.525	265.143	1.062
11	S10	495.130	132.050	627.180	485.52	135.3	620.82	1.010
	S3	380.620	68.896	449.516	400.22	75.6	475.82	0.945
	S11	575.826	155.096	730.921	524.196	147.6	671.796	1.088
	S4	377.764	68.992	446.757	371.94	71.628	443.568	1.007
	S12	455.217	118.415	573.632	415.236	115.05	530.286	1.082
10	S10	738.794	196.765	935.558	728.28	202.95	931.23	1.005
	S3	570.394	103.505	673.899	600.33	113.4	713.73	0.944
	S11	861.584	231.936	1093.520	786.294	221.4	1007.694	1.085
	S4	567.931	103.971	671.902	557.91	107.442	665.352	1.010
	S12	684.489	178.635	863.125	622.854	172.575	795.429	1.085
9	S10	987.436	262.101	1249.537	971.04	270.6	1241.64	1.006
	S3	759.896	137.981	897.877	800.44	151.2	951.64	0.944
	S11	1149.861	308.750	1458.610	1048.392	295.2	1343.592	1.086
	S4	759.687	139.246	898.934	743.88	143.256	887.136	1.013
	S12	916.588	238.898	1155.486	830.472	230.1	1060.572	1.089
8	S10	1238.595	328.141	1566.736	1213.8	338.25	1552.05	1.009
	S3	950.228	172.496	1122.723	1000.55	189	1189.55	0.944
	S11	1438.266	385.654	1823.920	1310.49	369	1679.49	1.086
	S4	951.857	174.738	1126.595	929.85	179.07	1108.92	1.016
	S12	1148.097	298.953	1447.050	1038.09	287.625	1325.715	1.092
7	S10	1495.718	395.042	1890.759	1456.56	405.9	1862.46	1.015
	S3	1143.341	207.234	1350.575	1200.66	226.8	1427.46	0.946
	S11	1729.589	462.659	2192.248	1572.588	442.8	2015.388	1.088
	S4	1142.817	209.922	1352.739	1115.82	214.884	1330.704	1.017
	S12	1382.684	359.024	1741.708	1245.708	345.15	1590.858	1.095
6	S10	1755.433	462.726	2218.159	1699.32	473.55	2172.87	1.021
	S3	1340.741	242.660	1583.401	1400.77	264.6	1665.37	0.951
	S11	2024.981	539.328	2564.309	1834.686	516.6	2351.286	1.091
	S4	1338.005	245.518	1583.523	1301.79	250.698	1552.488	1.020
	S12	1614.963	418.418	2033.380	1453.326	402.675	1856.001	1.096
5	S10	2022.418	531.581	2553.999	1942.08	541.2	2483.28	1.028
	S3	1542.835	278.817	1821.651	1600.88	302.4	1903.28	0.957
	S11	2317.346	615.293	2932.639	2096.784	590.4	2687.184	1.091
	S4	1533.816	281.262	1815.078	1487.76	286.512	1774.272	1.023
	S12	1849.430	477.437	2326.867	1660.944	460.2	2121.144	1.097
4	S10	2292.343	601.358	2893.701	2184.84	608.85	2793.69	1.036
	S3	1749.710	315.564	2065.274	1800.99	340.2	2141.19	0.965
	S11	2609.731	690.952	3300.683	2358.882	664.2	3023.082	1.092
	S4	1731.603	317.011	2048.614	1673.73	322.326	1996.056	1.026
	S12	2082.528	536.081	2618.609	1868.562	517.725	2386.287	1.097
3	S10	2569.514	672.258	3241.772	2427.6	676.5	3104.1	1.044
	S3	1960.396	352.729	2313.126	2001.1	378	2379.1	0.972
	S11	2904.741	766.385	3671.127	2620.98	738	3358.98	1.093
	S4	1929.706	352.724	2282.430	1859.7	358.14	2217.84	1.029
	S12	2318.011	594.307	2912.318	2076.18	575.25	2651.43	1.098
2	S10	2849.505	744.102	3593.607	2670.36	744.15	3414.51	1.052
	S3	2175.343	390.296	2565.639	2201.21	415.8	2617.01	0.980
	S11	3197.993	841.552	4039.544	2883.078	811.8	3694.878	1.093

	S4	2132.823	388.726	2521.549	2045.67	393.954	2439.624	1.034
	S12	2550.997	651.842	3202.838	2283.798	632.775	2916.573	1.098
1	S10	3138.406	817.558	3955.964	2913.12	811.8	3724.92	1.062
	S3	2393.505	428.001	2821.506	2401.32	453.6	2854.92	0.988
	S11	3492.841	916.891	4409.732	3145.176	885.6	4030.776	1.094
	S4	2336.196	424.638	2760.835	2231.64	429.768	2661.408	1.037
	S12	2786.145	708.784	3494.928	2491.416	690.3	3181.716	1.098

Çizelge A.18: 12 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	$N_G(kN)$	$N_{YQ}(kN)$	$N_{G+YQ}(kN)$	$N_{G0}(kN)$	$N_{YQ0}(kN)$	$N_{G0+YQ0}(kN)$	$k_{pY} = N_{G+YQ} / N_{G0+YQ0}$
12	0.6	S10	253.924	68.146	322.070	242.76	67.65	310.41	1.038
	0.6	S3	190.863	34.087	224.950	200.11	37.8	237.91	0.946
	0.6	S11	291.358	78.724	370.082	262.098	73.8	335.898	1.102
	0.6	S4	186.892	33.776	220.668	185.97	35.814	221.784	0.995
	0.6	S12	224.252	57.450	281.701	207.618	57.525	265.143	1.062
11	0.6	S10	495.130	136.293	631.423	485.52	135.3	620.82	1.017
	0.6	S3	380.620	68.174	448.795	400.22	75.6	475.82	0.943
	0.6	S11	575.826	157.448	733.273	524.196	147.6	671.796	1.092
	0.6	S4	377.764	67.551	445.315	371.94	71.628	443.568	1.004
	0.6	S12	455.217	114.899	570.116	415.236	115.05	530.286	1.075
10	0.6	S10	738.794	204.439	943.233	728.28	202.95	931.23	1.013
	0.6	S3	570.394	102.262	672.656	600.33	113.4	713.73	0.942
	0.6	S11	861.584	236.172	1097.756	786.294	221.4	1007.694	1.089
	0.6	S4	567.931	101.327	669.258	557.91	107.442	665.352	1.006
	0.6	S12	684.489	172.349	856.838	622.854	172.575	795.429	1.077
9	0.1	S10	987.436	215.797	1203.233	971.04	214.225	1185.265	1.015
	0.1	S3	759.896	107.943	867.839	800.44	119.7	920.14	0.943
	0.1	S11	1149.861	249.292	1399.153	1048.392	233.7	1282.092	1.091
	0.1	S4	759.687	106.956	866.643	743.88	113.411	857.291	1.011
	0.1	S12	916.588	181.923	1098.511	830.472	182.1625	1012.6345	1.085
8	0.2	S10	1238.595	238.512	1477.107	1213.8	236.775	1450.575	1.018
	0.2	S3	950.228	119.305	1069.533	1000.55	132.3	1132.85	0.944
	0.2	S11	1438.266	275.533	1713.800	1310.49	258.3	1568.79	1.092
	0.2	S4	951.857	118.214	1070.071	929.85	125.349	1055.199	1.014
	0.2	S12	1148.097	201.073	1349.170	1038.09	201.3375	1239.4275	1.089
7	0.2	S10	1495.718	261.228	1756.945	1456.56	259.325	1715.885	1.024
	0.2	S3	1143.341	130.668	1274.009	1200.66	144.9	1345.56	0.947
	0.2	S11	1729.589	301.775	2031.364	1572.588	282.9	1855.488	1.095
	0.2	S4	1142.817	129.473	1272.290	1115.82	137.287	1253.107	1.015
	0.2	S12	1382.684	220.223	1602.907	1245.708	220.5125	1466.2205	1.093
6	0.4	S10	1755.433	306.658	2062.092	1699.32	304.425	2003.745	1.029
	0.4	S3	1340.741	153.392	1494.133	1400.77	170.1	1570.87	0.951
	0.4	S11	2024.981	354.257	2379.238	1834.686	332.1	2166.786	1.098
	0.4	S4	1338.005	151.990	1489.995	1301.79	161.163	1462.953	1.018
	0.4	S12	1614.963	258.523	1873.485	1453.326	258.8625	1712.1885	1.094

5	0.6	S10	2022.418	374.805	2397.223	1942.08	372.075	2314.155	1.036
	0.6	S3	1542.835	187.480	1730.314	1600.88	207.9	1808.78	0.957
	0.6	S11	2317.346	432.981	2750.327	2096.784	405.9	2502.684	1.099
	0.6	S4	1533.816	185.766	1719.581	1487.76	196.977	1684.737	1.021
	0.6	S12	1849.430	315.972	2165.402	1660.944	316.3875	1977.3315	1.095
4	0.8	S10	2292.343	465.667	2758.009	2184.84	462.275	2647.115	1.042
	0.8	S3	1749.710	232.929	1982.639	1800.99	258.3	2059.29	0.963
	0.8	S11	2609.731	537.946	3147.677	2358.882	504.3	2863.182	1.099
	0.8	S4	1731.603	230.800	1962.403	1673.73	244.729	1918.459	1.023
	0.8	S12	2082.528	392.572	2475.099	1868.562	393.0875	2261.6495	1.094
3	1	S10	2569.514	579.244	3148.758	2427.6	575.025	3002.625	1.049
	1	S3	1960.396	289.741	2250.138	2001.1	321.3	2322.4	0.969
	1	S11	2904.741	669.153	3573.894	2620.98	627.3	3248.28	1.100
	1	S4	1929.706	287.092	2216.798	1859.7	304.419	2164.119	1.024
	1	S12	2318.011	488.321	2806.332	2076.18	488.9625	2565.1425	1.094
2	1	S10	2849.505	692.821	3542.326	2670.36	687.775	3358.135	1.055
	1	S3	2175.343	346.553	2521.897	2201.21	384.3	2585.51	0.975
	1	S11	3197.993	800.359	3998.352	2883.078	750.3	3633.378	1.100
	1	S4	2132.823	343.385	2476.208	2045.67	364.109	2409.779	1.028
	1	S12	2550.997	584.070	3135.067	2283.798	584.8375	2868.6355	1.093
1	1	S10	3138.406	806.398	3944.804	2913.12	800.525	3713.645	1.062
	1	S3	2393.505	403.365	2796.870	2401.32	447.3	2848.62	0.982
	1	S11	3492.841	931.565	4424.407	3145.176	873.3	4018.476	1.101
	1	S4	2336.196	399.677	2735.874	2231.64	423.799	2655.439	1.030
	1	S12	2786.145	679.819	3465.964	2491.416	680.7125	3172.1285	1.093

Çizelge A.19: 9 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p = N_{G+Q}/N_{G0+Q0}$
9	S1	96.934	21.043	117.977	101.95	26.25	128.2	0.920
	S9	152.433	47.694	200.127	154.96	51.25	206.21	0.971
	S2	194.488	57.432	251.920	186.63	57.75	244.38	1.031
	S10	277.276	122.762	400.037	242.76	112.75	355.51	1.125
	S3	187.811	55.367	243.177	200.11	63	263.11	0.924
	S11	229.784	101.801	331.585	262.098	92.25	354.348	0.936
8	S1	200.891	45.199	246.090	203.9	52.5	256.4	0.960
	S9	306.955	97.258	404.214	309.92	102.5	412.42	0.980
	S2	387.520	115.059	502.578	373.26	115.5	488.76	1.028
	S10	543.141	238.695	781.835	485.52	225.5	711.02	1.100
	S3	376.714	112.316	489.030	400.22	126	526.22	0.929
	S11	447.609	196.597	644.206	524.196	184.5	708.696	0.909
7	S1	303.469	68.767	372.236	305.85	78.75	384.6	0.968
	S9	460.807	146.302	607.109	464.88	153.75	618.63	0.981
	S2	580.606	172.487	753.093	559.89	173.25	733.14	1.027
	S10	811.133	356.070	1167.203	728.28	338.25	1066.53	1.094
	S3	565.787	169.064	734.851	600.33	189	789.33	0.931
	S11	669.219	293.355	962.573	786.294	276.75	1063.044	0.905
6	S1	405.563	92.140	497.703	407.8	105	512.8	0.971
	S9	614.458	195.203	809.661	619.84	205	824.84	0.982
	S2	775.470	230.295	1005.764	746.52	231	977.52	1.029
	S10	1080.630	473.037	1553.668	971.04	451	1422.04	1.093
	S3	754.800	225.637	980.437	800.44	252	1052.44	0.932
	S11	896.187	391.195	1287.382	1048.392	369	1417.392	0.908
5	S1	507.051	115.223	622.273	509.75	131.25	641	0.971
	S9	768.210	244.001	1012.211	774.8	256.25	1031.05	0.982
	S2	970.987	288.412	1259.399	933.15	288.75	1221.9	1.031
	S10	1349.185	589.842	1939.027	1213.8	563.75	1777.55	1.091
	S3	944.827	282.316	1227.143	1000.55	315	1315.55	0.933
	S11	1126.033	490.383	1616.415	1310.49	461.25	1771.74	0.912
4	S1	607.682	137.881	745.563	611.7	157.5	769.2	0.969
	S9	922.048	292.604	1214.652	929.76	307.5	1237.26	0.982
	S2	1165.836	346.109	1511.945	1119.78	346.5	1466.28	1.031
	S10	1621.355	707.480	2328.835	1456.56	676.5	2133.06	1.092
	S3	1137.748	339.397	1477.145	1200.66	378	1578.66	0.936
	S11	1363.010	591.657	1954.668	1572.588	553.5	2126.088	0.919
3	S1	707.449	160.140	867.589	713.65	183.75	897.4	0.967
	S9	1078.759	341.829	1420.588	1084.72	358.75	1443.47	0.984
	S2	1365.370	404.554	1769.925	1306.41	404.25	1710.66	1.035
	S10	1889.596	823.757	2713.352	1699.32	789.25	2488.57	1.090
	S3	1334.913	397.456	1732.369	1400.77	441	1841.77	0.941
	S11	1605.865	693.235	2299.100	1834.686	645.75	2480.436	0.927
2	S1	806.739	182.093	988.832	815.6	210	1025.6	0.964
	S9	1238.590	391.598	1630.188	1239.68	410	1649.68	0.988
	S2	1565.390	463.191	2028.581	1493.04	462	1955.04	1.038
	S10	2160.027	939.993	3100.020	1942.08	902	2844.08	1.090
	S3	1537.056	456.750	1993.806	1600.88	504	2104.88	0.947
	S11	1847.946	794.842	2642.789	2096.784	738	2834.784	0.932
1	S1	904.306	203.170	1107.476	917.55	236.25	1153.8	0.960
	S9	1398.799	441.094	1839.893	1394.64	461.25	1855.89	0.991
	S2	1767.738	521.908	2289.645	1679.67	519.75	2199.42	1.041
	S10	2432.532	1058.084	3490.616	2184.84	1014.75	3199.59	1.091
	S3	1743.411	516.616	2260.027	1800.99	567	2367.99	0.954
	S11	2094.849	898.453	2993.302	2358.882	830.25	3189.132	0.939

Çizelge A.20: 9 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_{pQ} (kN)	N_{G+pQ}	N_{G0} (kN)	N_{pQ0} (kN)	N_{G0+pQ0} (kN)	$k_{p\beta}=N_{G+pQ}/N_{G0+pQ0}$
9	S1	96.934	12.626	109.560	101.95	15.75	117.7	0.931
	S9	152.433	28.617	181.049	154.96	30.75	185.71	0.975
	S2	194.488	34.459	228.947	186.63	34.65	221.28	1.035
	S10	277.276	73.657	350.933	242.76	67.65	310.41	1.131
	S3	187.811	33.220	221.031	200.11	37.8	237.91	0.929
	S11	229.784	61.080	290.864	262.098	55.35	317.448	0.916
8	S1	200.891	27.119	228.011	203.9	31.5	235.4	0.969
	S9	306.955	58.355	365.310	309.92	61.5	371.42	0.984
	S2	387.520	69.035	456.555	373.26	69.3	442.56	1.032
	S10	543.141	143.217	686.357	485.52	135.3	620.82	1.106
	S3	376.714	67.390	444.103	400.22	75.6	475.82	0.933
	S11	447.609	117.958	565.567	524.196	110.7	634.896	0.891
7	S1	303.469	41.260	344.730	305.85	47.25	353.1	0.976
	S9	460.807	87.781	548.588	464.88	92.25	557.13	0.985
	S2	580.606	103.492	684.098	559.89	103.95	663.84	1.031
	S10	811.133	213.642	1024.775	728.28	202.95	931.23	1.100
	S3	565.787	101.439	667.225	600.33	113.4	713.73	0.935
	S11	669.219	176.013	845.232	786.294	166.05	952.344	0.888
6	S1	405.563	55.284	460.847	407.8	63	470.8	0.979
	S9	614.458	117.122	731.580	619.84	123	742.84	0.985
	S2	775.470	138.177	913.647	746.52	138.6	885.12	1.032
	S10	1080.630	283.822	1364.453	971.04	270.6	1241.64	1.099
	S3	754.800	135.382	890.182	800.44	151.2	951.64	0.935
	S11	896.187	234.717	1130.904	1048.392	221.4	1269.792	0.891
5	S1	507.051	69.134	576.184	509.75	78.75	588.5	0.979
	S9	768.210	146.400	914.610	774.8	153.75	928.55	0.985
	S2	970.987	173.047	1144.034	933.15	173.25	1106.4	1.034
	S10	1349.185	353.905	1703.090	1213.8	338.25	1552.05	1.097
	S3	944.827	169.389	1114.216	1000.55	189	1189.55	0.937
	S11	1126.033	294.230	1420.262	1310.49	276.75	1587.24	0.895
4	S1	607.682	82.729	690.411	611.7	94.5	706.2	0.978
	S9	922.048	175.562	1097.610	929.76	184.5	1114.26	0.985
	S2	1165.836	207.666	1373.501	1119.78	207.9	1327.68	1.035
	S10	1621.355	424.488	2045.843	1456.56	405.9	1862.46	1.098
	S3	1137.748	203.638	1341.386	1200.66	226.8	1427.46	0.940
	S11	1363.010	354.994	1718.005	1572.588	332.1	1904.688	0.902
3	S1	707.449	96.084	803.533	713.65	110.25	823.9	0.975
	S9	1078.759	205.097	1283.856	1084.72	215.25	1299.97	0.988
	S2	1365.370	242.733	1608.103	1306.41	242.55	1548.96	1.038
	S10	1889.596	494.254	2383.850	1699.32	473.55	2172.87	1.097
	S3	1334.913	238.474	1573.387	1400.77	264.6	1665.37	0.945
	S11	1605.865	415.941	2021.806	1834.686	387.45	2222.136	0.910
2	S1	806.739	109.256	915.995	815.6	126	941.6	0.973
	S9	1238.590	234.959	1473.549	1239.68	246	1485.68	0.992
	S2	1565.390	277.915	1843.305	1493.04	277.2	1770.24	1.041
	S10	2160.027	563.996	2724.023	1942.08	541.2	2483.28	1.097
	S3	1537.056	274.050	1811.106	1600.88	302.4	1903.28	0.952
	S11	1847.946	476.905	2324.852	2096.784	442.8	2539.584	0.915
1	S1	904.306	121.902	1026.208	917.55	141.75	1059.3	0.969
	S9	1398.799	264.657	1663.455	1394.64	276.75	1671.39	0.995
	S2	1767.738	313.145	2080.882	1679.67	311.85	1991.52	1.045
	S10	2432.532	634.850	3067.383	2184.84	608.85	2793.69	1.098
	S3	1743.411	309.970	2053.381	1800.99	340.2	2141.19	0.959
	S11	2094.849	539.072	2633.920	2358.882	498.15	2857.032	0.922

Çizelge A.21: 9 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	$N_G(kN)$	$N_{YQ}(kN)$	$N_{G+YQ}(kN)$	$N_{G0}(kN)$	$N_{YQ0}(kN)$	$N_{G0+YQ0}(kN)$	$k_{p\gamma}=N_{G+YQ}/N_{G0+YQ0}$
9	0.1	S1	96.934	2.104	99.038	101.95	2.625	104.575	0.947
	0.1	S9	152.433	4.769	157.202	154.96	5.125	160.085	0.982
	0.1	S2	194.488	5.743	200.231	186.63	5.775	192.405	1.041
	0.1	S10	277.276	12.276	289.552	242.76	11.275	254.035	1.140
	0.1	S3	187.811	5.537	193.347	200.11	6.3	206.41	0.937
	0.1	S11	229.784	10.180	239.964	262.098	9.225	271.323	0.884
8	0.2	S1	200.891	2.525	203.416	203.9	3.15	207.05	0.982
	0.2	S9	306.955	5.723	312.679	309.92	6.15	316.07	0.989
	0.2	S2	387.520	6.892	394.412	373.26	6.93	380.19	1.037
	0.2	S10	543.141	14.731	557.872	485.52	13.53	499.05	1.118
	0.2	S3	376.714	6.644	383.357	400.22	7.56	407.78	0.940
	0.2	S11	447.609	12.216	459.825	524.196	11.07	535.266	0.859
7	0.2	S1	303.469	6.734	310.203	305.85	8.4	314.25	0.987
	0.2	S9	460.807	15.262	476.070	464.88	16.4	481.28	0.989
	0.2	S2	580.606	18.378	598.984	559.89	18.48	578.37	1.036
	0.2	S10	811.133	39.284	850.416	728.28	36.08	764.36	1.113
	0.2	S3	565.787	17.717	583.504	600.33	20.16	620.49	0.940
	0.2	S11	669.219	32.576	701.795	786.294	29.52	815.814	0.860
6	0.4	S1	405.563	15.151	420.714	407.8	18.9	426.7	0.986
	0.4	S9	614.458	34.340	648.798	619.84	36.9	656.74	0.988
	0.4	S2	775.470	41.351	816.821	746.52	41.58	788.1	1.036
	0.4	S10	1080.630	88.388	1169.019	971.04	81.18	1052.22	1.111
	0.4	S3	754.800	39.864	794.664	800.44	45.36	845.8	0.940
	0.4	S11	896.187	73.296	969.484	1048.392	66.42	1114.812	0.870
5	0.6	S1	507.051	27.777	534.827	509.75	34.65	544.4	0.982
	0.6	S9	768.210	62.957	831.167	774.8	67.65	842.45	0.987
	0.6	S2	970.987	75.810	1046.797	933.15	76.23	1009.38	1.037
	0.6	S10	1349.185	162.045	1511.230	1213.8	148.83	1362.63	1.109
	0.6	S3	944.827	73.084	1017.911	1000.55	83.16	1083.71	0.939
	0.6	S11	1126.033	134.377	1260.409	1310.49	121.77	1432.26	0.880
4	0.8	S1	607.682	44.611	652.293	611.7	55.65	667.35	0.977
	0.8	S9	922.048	101.112	1023.160	929.76	108.65	1038.41	0.985
	0.8	S2	1165.836	121.756	1287.591	1119.78	122.43	1242.21	1.037

	0.8	S10	1621.355	260.255	1881.610	1456.56	239.03	1695.59	1.110
	0.8	S3	1137.748	117.377	1255.125	1200.66	133.56	1334.22	0.941
	0.8	S11	1363.010	215.817	1578.828	1572.588	195.57	1768.158	0.893
3	1	S1	707.449	65.654	773.102	713.65	81.9	795.55	0.972
	1	S9	1078.759	148.807	1227.565	1084.72	159.9	1244.62	0.986
	1	S2	1365.370	179.188	1544.558	1306.41	180.18	1486.59	1.039
	1	S10	1889.596	383.017	2272.612	1699.32	351.78	2051.1	1.108
	1	S3	1334.913	172.743	1507.656	1400.77	196.56	1597.33	0.944
	1	S11	1605.865	317.618	1923.482	1834.686	287.82	2122.506	0.906
2	1	S1	806.739	86.697	893.436	815.6	108.15	923.75	0.967
	1	S9	1238.590	196.501	1435.091	1239.68	211.15	1450.83	0.989
	1	S2	1565.390	236.619	1802.009	1493.04	237.93	1730.97	1.041
	1	S10	2160.027	505.778	2665.805	1942.08	464.53	2406.61	1.108
	1	S3	1537.056	228.110	1765.166	1600.88	259.56	1860.44	0.949
	1	S11	1847.946	419.418	2267.365	2096.784	380.07	2476.854	0.915
1	1	S1	904.306	107.740	1012.046	917.55	134.4	1051.95	0.962
	1	S9	1398.799	244.195	1642.994	1394.64	262.4	1657.04	0.992
	1	S2	1767.738	294.051	2061.789	1679.67	295.68	1975.35	1.044
	1	S10	2432.532	628.540	3061.072	2184.84	577.28	2762.12	1.108
	1	S3	1743.411	283.476	2026.888	1800.99	322.56	2123.55	0.954
	1	S11	2094.849	521.219	2616.068	2358.882	472.32	2831.202	0.924

Çizelge A.22: 12 Katlı Hastane Binasına için k_p eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_Q (kN)	N_{G+Q} (kN)	N_{G0} (kN)	N_{Q0} (kN)	N_{G0+Q0} (kN)	$k_p=N_{G+Q}/N_{G0+Q0}$
12	S1	97.423	21.626	119.049	101.95	26.25	128.2	0.929
	S9	152.301	48.005	200.306	154.96	51.25	206.21	0.971
	S2	193.133	57.128	250.261	186.63	57.75	244.38	1.024
	S10	276.810	121.259	398.069	242.76	112.75	355.51	1.120
	S3	184.802	54.843	239.645	200.11	63	263.11	0.911
	S11	230.247	101.176	331.424	262.098	92.25	354.348	0.935
11	S1	201.901	46.584	248.485	203.9	52.5	256.4	0.969
	S9	306.423	97.871	404.294	309.92	102.5	412.42	0.980
	S2	384.009	114.221	498.230	373.26	115.5	488.76	1.019
	S10	542.102	235.175	777.277	485.52	225.5	711.02	1.093
	S3	369.942	111.116	481.058	400.22	126	526.22	0.914
	S11	447.943	194.670	642.613	524.196	184.5	708.696	0.907
10	S1	304.978	70.925	375.903	305.85	78.75	384.6	0.977
	S9	459.858	147.205	607.064	464.88	153.75	618.63	0.981
	S2	574.997	171.118	746.116	559.89	173.25	733.14	1.018
	S10	809.521	350.565	1160.086	728.28	338.25	1066.53	1.088
	S3	555.277	167.189	722.466	600.33	189	789.33	0.915
	S11	669.345	290.098	959.443	786.294	276.75	1063.044	0.903
9	S1	407.592	95.092	502.683	407.8	105	512.8	0.980
	S9	613.035	196.419	809.454	619.84	205	824.84	0.981
	S2	767.628	228.395	996.024	746.52	231	977.52	1.019
	S10	1078.300	465.355	1543.655	971.04	451	1422.04	1.086
	S3	740.454	223.078	963.533	800.44	252	1052.44	0.916
	S11	895.860	386.363	1282.222	1048.392	369	1417.392	0.905
8	S1	509.616	118.987	628.604	509.75	131.25	641	0.981
	S9	766.258	245.548	1011.807	774.8	256.25	1031.05	0.981
	S2	960.799	285.977	1246.777	933.15	288.75	1221.9	1.020
	S10	1346.029	579.827	1925.856	1213.8	563.75	1777.55	1.083
	S3	926.550	279.065	1205.614	1000.55	315	1315.55	0.916
	S11	1125.014	483.756	1608.770	1310.49	461.25	1771.74	0.908
7	S1	610.817	142.477	753.294	611.7	157.5	769.2	0.979
	S9	919.497	294.494	1213.992	929.76	307.5	1237.26	0.981
	S2	1153.127	343.092	1496.219	1119.78	346.5	1466.28	1.020
	S10	1617.179	694.969	2312.148	1456.56	676.5	2133.06	1.084
	S3	1115.411	335.445	1450.856	1200.66	378	1578.66	0.919
	S11	1361.064	583.004	1944.068	1572.588	553.5	2126.088	0.914
6	S1	711.208	165.620	876.828	713.65	183.75	897.4	0.977
	S9	1075.542	344.122	1419.664	1084.72	358.75	1443.47	0.984
	S2	1349.842	400.898	1750.740	1306.41	404.25	1710.66	1.023
	S10	1884.132	808.437	2692.568	1699.32	789.25	2488.57	1.082
	S3	1308.204	392.759	1700.963	1400.77	441	1841.77	0.924
	S11	1602.463	682.107	2284.569	1834.686	645.75	2480.436	0.921
5	S1	811.016	188.455	999.472	815.6	210	1025.6	0.975
	S9	1234.390	394.223	1628.614	1239.68	410	1649.68	0.987
	S2	1546.729	458.807	2005.535	1493.04	462	1955.04	1.026
	S10	2153.366	921.740	3075.106	1942.08	902	2844.08	1.081
	S3	1505.581	451.195	1956.775	1600.88	504	2104.88	0.930
	S11	1842.965	781.086	2624.050	2096.784	738	2834.784	0.926
4	S1	910.280	210.880	1121.160	917.55	236.25	1153.8	0.972
	S9	1393.739	444.256	1837.995	1394.64	461.25	1855.89	0.990
	S2	1745.683	516.826	2262.509	1679.67	519.75	2199.42	1.029
	S10	2422.870	1035.868	3458.739	2184.84	1014.75	3199.59	1.081
	S3	1707.696	510.583	2218.278	1800.99	567	2367.99	0.937

	S11	2086.596	881.146	2967.742	2358.882	830.25	3189.132	0.931
3	S1	1014.439	234.008	1248.447	1019.5	262.5	1282	0.974
	S9	1556.107	494.292	2050.399	1549.6	512.5	2062.1	0.994
	S2	1943.261	574.236	2517.497	1866.3	577.5	2443.8	1.030
	S10	2695.585	1150.417	3846.002	2427.6	1127.5	3555.1	1.082
	S3	1913.865	570.748	2484.613	2001.1	630	2631.1	0.944
	S11	2334.957	981.953	3316.910	2620.98	922.5	3543.48	0.936
2	S1	1119.913	257.447	1377.360	1121.45	288.75	1410.2	0.977
	S9	1718.671	544.293	2262.964	1704.56	563.75	2268.31	0.998
	S2	2145.457	632.044	2777.501	2052.93	635.25	2688.18	1.033
	S10	2967.037	1265.074	4232.111	2670.36	1240.25	3910.61	1.082
	S3	2124.471	631.667	2756.138	2201.21	693	2894.21	0.952
	S11	2582.686	1083.076	3665.762	2883.078	1014.75	3897.828	0.940
1	S1	1224.039	280.081	1504.120	1223.4	315	1538.4	0.978
	S9	1881.355	593.939	2475.293	1859.52	615	2474.52	1.000
	S2	2349.007	690.240	3039.247	2239.56	693	2932.56	1.036
	S10	3244.994	1381.775	4626.769	2913.12	1353	4266.12	1.085
	S3	2338.551	692.925	3031.476	2401.32	756	3157.32	0.960
	S11	2833.889	1185.602	4019.491	3145.176	1107	4252.176	0.945

Çizelge A.23: 12 Katlı Hastane Binasına için $k_{p\beta}$ eksenel kuvvet oranları

KAT	KOLON	N_G (kN)	N_{pQ} (kN)	N_{G+pQ}	N_{G0} (kN)	N_{pQ0} (kN)	N_{G0+pQ0} (kN)	$k_{p\beta}=N_{G+pQ}/N_{G0+pQ0}$
12	S1	97.423	12.975	110.398	101.95	15.75	117.7	0.938
	S9	152.301	28.803	181.104	154.96	30.75	185.71	0.975
	S2	193.133	34.277	227.410	186.63	34.65	221.28	1.028
	S10	276.810	72.756	349.566	242.76	67.65	310.41	1.126
	S3	184.802	32.906	217.708	200.11	37.8	237.91	0.915
	S11	230.247	60.706	290.953	262.098	55.35	317.448	0.917
11	S1	201.901	27.950	229.851	203.9	31.5	235.4	0.976
	S9	306.423	58.722	365.146	309.92	61.5	371.42	0.983
	S2	384.009	68.533	452.542	373.26	69.3	442.56	1.023
	S10	542.102	141.105	683.207	485.52	135.3	620.82	1.100
	S3	369.942	66.670	436.611	400.22	75.6	475.82	0.918
	S11	447.943	116.802	564.745	524.196	110.7	634.896	0.890
10	S1	304.978	42.555	347.533	305.85	47.25	353.1	0.984
	S9	459.858	88.323	548.182	464.88	92.25	557.13	0.984
	S2	574.997	102.671	677.668	559.89	103.95	663.84	1.021
	S10	809.521	210.339	1019.860	728.28	202.95	931.23	1.095
	S3	555.277	100.313	655.590	600.33	113.4	713.73	0.919
	S11	669.345	174.059	843.404	786.294	166.05	952.344	0.886
9	S1	407.592	57.055	464.647	407.8	63	470.8	0.987
	S9	613.035	117.851	730.887	619.84	123	742.84	0.984
	S2	767.628	137.037	904.666	746.52	138.6	885.12	1.022
	S10	1078.300	279.213	1357.513	971.04	270.6	1241.64	1.093
	S3	740.454	133.847	874.301	800.44	151.2	951.64	0.919
	S11	895.860	231.818	1127.677	1048.392	221.4	1269.792	0.888
8	S1	509.616	71.392	581.009	509.75	78.75	588.5	0.987
	S9	766.258	147.329	913.587	774.8	153.75	928.55	0.984
	S2	960.799	171.586	1132.386	933.15	173.25	1106.4	1.023
	S10	1346.029	347.896	1693.925	1213.8	338.25	1552.05	1.091
	S3	926.550	167.439	1093.988	1000.55	189	1189.55	0.920
	S11	1125.014	290.253	1415.267	1310.49	276.75	1587.24	0.892
7	S1	610.817	85.486	696.303	611.7	94.5	706.2	0.986
	S9	919.497	176.697	1096.194	929.76	184.5	1114.26	0.984
	S2	1153.127	205.855	1358.982	1119.78	207.9	1327.68	1.024
	S10	1617.179	416.981	2034.160	1456.56	405.9	1862.46	1.092
	S3	1115.411	201.267	1316.678	1200.66	226.8	1427.46	0.922
	S11	1361.064	349.803	1710.866	1572.588	332.1	1904.688	0.898
6	S1	711.208	99.372	810.580	713.65	110.25	823.9	0.984
	S9	1075.542	206.473	1282.015	1084.72	215.25	1299.97	0.986
	S2	1349.842	240.539	1590.381	1306.41	242.55	1548.96	1.027
	S10	1884.132	485.062	2369.194	1699.32	473.55	2172.87	1.090
	S3	1308.204	235.655	1543.859	1400.77	264.6	1665.37	0.927
	S11	1602.463	409.264	2011.727	1834.686	387.45	2222.136	0.905
5	S1	811.016	113.073	924.089	815.6	126	941.6	0.981
	S9	1234.390	236.534	1470.924	1239.68	246	1485.68	0.990
	S2	1546.729	275.284	1822.013	1493.04	277.2	1770.24	1.029
	S10	2153.366	553.044	2706.410	1942.08	541.2	2483.28	1.090
	S3	1505.581	270.717	1776.297	1600.88	302.4	1903.28	0.933
	S11	1842.965	468.651	2311.616	2096.784	442.8	2539.584	0.910
4	S1	910.280	126.528	1036.808	917.55	141.75	1059.3	0.979
	S9	1393.739	266.554	1660.293	1394.64	276.75	1671.39	0.993
	S2	1745.683	310.096	2055.779	1679.67	311.85	1991.52	1.032
	S10	2422.870	621.521	3044.391	2184.84	608.85	2793.69	1.090

	S3	1707.696	306.350	2014.045	1800.99	340.2	2141.19	0.941
	S11	2086.596	528.688	2615.284	2358.882	498.15	2857.032	0.915
3	S1	1014.439	140.405	1154.844	1019.5	157.5	1177	0.981
	S9	1556.107	296.575	1852.682	1549.6	307.5	1857.1	0.998
	S2	1943.261	344.542	2287.803	1866.3	346.5	2212.8	1.034
	S10	2695.585	690.250	3385.835	2427.6	676.5	3104.1	1.091
	S3	1913.865	342.449	2256.314	2001.1	378	2379.1	0.948
	S11	2334.957	589.172	2924.128	2620.98	553.5	3174.48	0.921
2	S1	1119.913	154.468	1274.381	1121.45	173.25	1294.7	0.984
	S9	1718.671	326.576	2045.246	1704.56	338.25	2042.81	1.001
	S2	2145.457	379.226	2524.684	2052.93	381.15	2434.08	1.037
	S10	2967.037	759.045	3726.081	2670.36	744.15	3414.51	1.091
	S3	2124.471	379.000	2503.471	2201.21	415.8	2617.01	0.957
	S11	2582.686	649.846	3232.532	2883.078	608.85	3491.928	0.926
1	S1	1224.039	168.048	1392.088	1223.4	189	1412.4	0.986
	S9	1881.355	356.363	2237.718	1859.52	369	2228.52	1.004
	S2	2349.007	414.144	2763.151	2239.56	415.8	2655.36	1.041
	S10	3244.994	829.065	4074.059	2913.12	811.8	3724.92	1.094
	S3	2338.551	415.755	2754.306	2401.32	453.6	2854.92	0.965
	S11	2833.889	711.361	3545.250	3145.176	664.2	3809.376	0.931

Çizelge A.24: 12 Katlı Hastane Binasına için $k_{p\gamma}$ eksenel kuvvet oranları

KAT	γ	KOLON	$N_G(kN)$	$N_{YQ}(kN)$	$N_{G+YQ}(kN)$	$N_{G0}(kN)$	$N_{YQ0}(kN)$	$N_{G0+YQ0}(kN)$	$k_{p\gamma} = N_{G+YQ} / N_{G0+YQ0}$
12	0.6	S1	97.423	12.975	110.398	101.95	15.75	117.7	0.938
	0.6	S9	152.301	28.803	181.104	154.96	30.75	185.71	0.975
	0.6	S2	193.133	34.277	227.410	186.63	34.65	221.28	1.028
	0.6	S10	276.810	72.756	349.566	242.76	67.65	310.41	1.126
	0.6	S3	184.802	32.906	217.708	200.11	37.8	237.91	0.915
	0.6	S11	230.247	60.706	290.953	262.098	55.35	317.448	0.917
11	0.6	S1	201.901	25.951	227.852	203.9	31.5	235.4	0.968
	0.6	S9	306.423	57.606	364.029	309.92	61.5	371.42	0.980
	0.6	S2	384.009	68.553	452.562	373.26	69.3	442.56	1.023
	0.6	S10	542.102	145.511	687.613	485.52	135.3	620.82	1.108
	0.6	S3	369.942	65.811	435.753	400.22	75.6	475.82	0.916
	0.6	S11	447.943	121.411	569.354	524.196	110.7	634.896	0.897
10	0.6	S1	304.978	38.926	343.904	305.85	47.25	353.1	0.974
	0.6	S9	459.858	86.409	546.267	464.88	92.25	557.13	0.981
	0.6	S2	574.997	102.830	677.827	559.89	103.95	663.84	1.021
	0.6	S10	809.521	218.267	1027.788	728.28	202.95	931.23	1.104
	0.6	S3	555.277	98.717	653.994	600.33	113.4	713.73	0.916
	0.6	S11	669.345	182.117	851.462	786.294	166.05	952.344	0.894
9	0.1	S1	407.592	41.089	448.680	407.8	49.875	457.675	0.980
	0.1	S9	613.035	91.209	704.244	619.84	97.375	717.215	0.982
	0.1	S2	767.628	108.543	876.171	746.52	109.725	856.245	1.023
	0.1	S10	1078.300	230.393	1308.693	971.04	214.225	1185.265	1.104
	0.1	S3	740.454	104.202	844.656	800.44	119.7	920.14	0.918
	0.1	S11	895.860	192.235	1088.094	1048.392	175.275	1223.667	0.889
8	0.2	S1	509.616	45.414	555.030	509.75	55.125	564.875	0.983
	0.2	S9	766.258	100.810	867.069	774.8	107.625	882.425	0.983
	0.2	S2	960.799	119.968	1080.768	933.15	121.275	1054.425	1.025
	0.2	S10	1346.029	254.645	1600.674	1213.8	236.775	1450.575	1.103
	0.2	S3	926.550	115.170	1041.720	1000.55	132.3	1132.85	0.920
	0.2	S11	1125.014	212.470	1337.484	1310.49	193.725	1504.215	0.889
7	0.2	S1	610.817	49.739	660.556	611.7	60.375	672.075	0.983
	0.2	S9	919.497	110.411	1029.908	929.76	117.875	1047.635	0.983
	0.2	S2	1153.127	131.394	1284.521	1119.78	132.825	1252.605	1.025
	0.2	S10	1617.179	278.896	1896.075	1456.56	259.325	1715.885	1.105
	0.2	S3	1115.411	126.139	1241.550	1200.66	144.9	1345.56	0.923
	0.2	S11	1361.064	232.705	1593.769	1572.588	212.175	1784.763	0.893

6	0.4	S1	711.208	58.389	769.597	713.65	70.875	784.525	0.981
	0.4	S9	1075.542	129.613	1205.155	1084.72	138.375	1223.095	0.985
	0.4	S2	1349.842	154.245	1504.087	1306.41	155.925	1462.335	1.029
	0.4	S10	1884.132	327.400	2211.532	1699.32	304.425	2003.745	1.104
	0.4	S3	1308.204	148.076	1456.280	1400.77	170.1	1570.87	0.927
	0.4	S11	1602.463	273.175	1875.638	1834.686	249.075	2083.761	0.900
5	0.6	S1	811.016	71.364	882.381	815.6	86.625	902.225	0.978
	0.6	S9	1234.390	158.416	1392.807	1239.68	169.125	1408.805	0.989
	0.6	S2	1546.729	188.521	1735.250	1493.04	190.575	1683.615	1.031
	0.6	S10	2153.366	400.156	2553.522	1942.08	372.075	2314.155	1.103
	0.6	S3	1505.581	180.982	1686.562	1600.88	207.9	1808.78	0.932
	0.6	S11	1842.965	333.881	2176.846	2096.784	304.425	2401.209	0.907
4	0.8	S1	910.280	88.665	998.944	917.55	107.625	1025.175	0.974
	0.8	S9	1393.739	196.820	1590.559	1394.64	210.125	1604.765	0.991
	0.8	S2	1745.683	234.224	1979.907	1679.67	236.775	1916.445	1.033
	0.8	S10	2422.870	497.163	2920.034	2184.84	462.275	2647.115	1.103
	0.8	S3	1707.696	224.856	1932.552	1800.99	258.3	2059.29	0.938
	0.8	S11	2086.596	414.822	2501.418	2358.882	378.225	2737.107	0.914
3	1	S1	1014.439	110.291	1124.730	1019.5	133.875	1153.375	0.975
	1	S9	1556.107	244.825	1800.932	1549.6	261.375	1810.975	0.994
	1	S2	1943.261	291.351	2234.612	1866.3	294.525	2160.825	1.034
	1	S10	2695.585	618.422	3314.007	2427.6	575.025	3002.625	1.104
	1	S3	1913.865	279.699	2193.564	2001.1	321.3	2322.4	0.945
	1	S11	2334.957	515.998	2850.955	2620.98	470.475	3091.455	0.922
2	1	S1	1119.913	131.916	1251.829	1121.45	160.125	1281.575	0.977
	1	S9	1718.671	292.830	2011.500	1704.56	312.625	2017.185	0.997
	1	S2	2145.457	348.479	2493.936	2052.93	352.275	2405.205	1.037
	1	S10	2967.037	739.682	3706.719	2670.36	687.775	3358.135	1.104
	1	S3	2124.471	334.542	2459.013	2201.21	384.3	2585.51	0.951
	1	S11	2582.686	617.174	3199.860	2883.078	562.725	3445.803	0.929
1	1	S1	1224.039	153.542	1377.581	1223.4	186.375	1409.775	0.977
	1	S9	1881.355	340.835	2222.189	1859.52	363.875	2223.395	0.999
	1	S2	2349.007	405.607	2754.614	2239.56	410.025	2649.585	1.040
	1	S10	3244.994	860.941	4105.935	2913.12	800.525	3713.645	1.106
	1	S3	2338.551	389.385	2727.936	2401.32	447.3	2848.62	0.958
	1	S11	2833.889	718.350	3552.239	3145.176	654.975	3800.151	0.935

EK B: Deprem Yüklerin Etkisinde Oluşan Eksenel Kuvvetler

Model 1

Çizelge B.1: 12 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	7.392	9.318	10.187	11.536	128.2	117.7	117.700	0.090	0.098	0.098
	S9	10.046	0.068	10.066	3.082	206.21	185.71	185.710	0.049	0.054	0.054
	S2	3.322	13.680	7.426	14.676	244.38	221.28	221.280	0.060	0.066	0.066
	S10	1.978	1.009	2.280	1.602	355.51	310.41	310.410	0.006	0.007	0.007
	S3	0.621	13.763	4.750	13.949	263.11	237.91	237.910	0.053	0.059	0.059
	S11	0.787	0.482	0.932	0.718	385.098	335.898	335.898	0.002	0.003	0.003
	S4	0.883	13.645	4.977	13.910	245.66	221.784	221.784	0.057	0.063	0.063
	S12	0.694	1.397	1.113	1.605	303.493	265.143	265.143	0.005	0.006	0.006
11	S1	28.540	29.474	37.382	38.036	256.4	235.4	235.400	0.148	0.162	0.162
	S9	37.831	6.639	39.822	17.988	412.42	371.42	371.420	0.097	0.107	0.107
	S2	4.243	41.504	16.694	42.777	488.76	442.56	442.560	0.088	0.097	0.097
	S10	1.144	7.895	3.512	8.238	711.02	620.82	620.820	0.012	0.013	0.013
	S3	0.883	41.726	13.401	41.991	526.22	475.82	475.820	0.080	0.088	0.088
	S11	1.122	11.867	4.682	12.203	770.196	671.796	671.796	0.016	0.018	0.018
	S4	1.398	41.153	13.743	41.572	491.32	443.568	443.568	0.085	0.094	0.094
	S12	7.241	8.247	9.715	10.419	606.986	530.286	530.286	0.017	0.020	0.020
10	S1	61.691	58.044	79.104	76.551	384.6	353.1	353.100	0.206	0.224	0.224
	S9	81.642	18.085	87.068	42.577	618.63	557.13	557.130	0.141	0.156	0.156
	S2	1.028	80.082	25.053	80.390	733.14	663.84	663.840	0.110	0.121	0.121
	S10	12.064	23.656	19.161	27.275	1066.53	931.23	931.230	0.026	0.029	0.029
	S3	0.903	80.585	25.079	80.856	789.33	713.73	713.730	0.102	0.113	0.113
	S11	1.117	34.245	11.390	34.579	1155.294	1007.694	1007.694	0.030	0.034	0.034
	S4	5.931	79.358	29.738	81.137	736.98	665.352	665.352	0.110	0.122	0.122
	S12	18.749	25.640	26.442	31.265	910.479	795.429	795.429	0.034	0.039	0.039
9	S1	102.199	90.834	129.449	121.493	512.8	470.8	457.675	0.252	0.275	0.283
	S9	137.851	32.542	147.613	73.897	824.84	742.84	717.215	0.179	0.199	0.206
	S2	4.313	129.026	43.020	130.320	977.52	885.12	856.245	0.133	0.147	0.152
	S10	23.420	52.464	39.159	59.490	1422.04	1241.64	1185.265	0.042	0.048	0.050
	S3	1.067	127.392	39.284	127.712	1052.44	951.64	920.140	0.121	0.134	0.139
	S11	1.336	73.508	23.389	73.909	1540.392	1343.592	1282.092	0.048	0.055	0.058
	S4	13.792	127.601	52.072	131.739	982.64	887.136	857.291	0.134	0.148	0.154
	S12	35.016	57.064	52.135	67.568	1213.972	1060.572	1012.635	0.056	0.064	0.067
8	S1	149.119	126.750	187.144	171.485	641	588.5	564.875	0.292	0.318	0.331
	S9	204.827	49.091	219.554	110.539	1031.05	928.55	882.425	0.213	0.236	0.249
	S2	12.003	186.872	68.065	190.473	1221.9	1106.4	1054.425	0.156	0.172	0.181
	S10	35.329	91.577	62.802	102.176	1777.55	1552.05	1450.575	0.057	0.066	0.070
	S3	1.387	180.615	55.571	181.031	1315.55	1189.55	1132.850	0.138	0.152	0.160
	S11	1.582	127.223	39.748	127.697	1925.49	1679.49	1568.790	0.066	0.076	0.081
	S4	25.536	184.688	80.943	192.349	1228.3	1108.92	1055.199	0.157	0.173	0.182
	S12	55.405	99.729	85.323	116.350	1517.465	1325.715	1239.428	0.077	0.088	0.094
7	S1	199.553	165.494	249.202	225.360	769.2	706.2	672.075	0.324	0.353	0.371
	S9	281.447	68.028	301.856	152.462	1237.26	1114.26	1047.635	0.244	0.271	0.288
	S2	18.152	251.232	93.522	256.678	1466.28	1327.68	1252.605	0.175	0.193	0.205
	S10	47.246	146.959	91.334	161.132	2133.06	1862.46	1715.885	0.076	0.087	0.094
	S3	1.476	240.622	73.663	241.065	1578.66	1427.46	1345.560	0.153	0.169	0.179
	S11	1.931	195.818	60.677	196.397	2310.588	2015.388	1855.488	0.085	0.097	0.106
	S4	34.190	248.116	108.625	258.373	1473.96	1330.704	1253.107	0.175	0.194	0.206
	S12	80.690	159.942	128.673	184.149	1820.958	1590.858	1466.221	0.101	0.116	0.126

6	S1	253.744	204.977	315.237	281.100	897.4	823.9	784.525	0.351	0.383	0.402
	S9	362.673	89.441	389.505	198.243	1443.47	1299.97	1223.095	0.270	0.300	0.318
	S2	22.291	321.663	118.790	328.350	1710.66	1548.96	1462.335	0.192	0.212	0.225
	S10	55.035	207.834	117.385	224.344	2488.57	2172.87	2003.745	0.090	0.103	0.112
	S3	1.993	309.762	94.921	310.360	1841.77	1665.37	1570.870	0.169	0.186	0.198
	S11	2.014	279.247	85.788	279.851	2695.686	2351.286	2166.786	0.104	0.119	0.129
	S4	47.606	317.010	142.709	331.292	1719.62	1552.488	1462.953	0.193	0.213	0.226
	S12	100.646	225.734	168.366	255.927	2124.451	1856.001	1712.189	0.120	0.138	0.149
5	S1	311.841	247.688	386.147	341.240	1025.6	941.6	902.225	0.377	0.410	0.428
	S9	451.857	124.366	489.167	259.923	1649.68	1485.68	1408.805	0.297	0.329	0.347
	S2	25.415	396.308	144.308	403.933	1955.04	1770.24	1683.615	0.207	0.228	0.240
	S10	66.596	275.889	149.362	295.867	2844.08	2483.28	2314.155	0.104	0.119	0.128
	S3	2.603	384.169	117.853	384.950	2104.88	1903.28	1808.780	0.183	0.202	0.213
	S11	1.921	366.713	111.935	367.290	3080.784	2687.184	2502.684	0.119	0.137	0.147
	S4	64.536	390.289	181.623	409.650	1965.28	1774.272	1684.737	0.208	0.231	0.243
	S12	122.206	299.001	211.907	335.663	2427.944	2121.144	1977.332	0.138	0.158	0.170
4	S1	373.631	292.397	461.350	404.486	1153.8	1059.3	1025.175	0.400	0.436	0.450
	S9	546.117	169.148	596.862	332.983	1855.89	1671.39	1604.765	0.322	0.357	0.372
	S2	27.289	473.880	169.453	482.067	2199.42	1991.52	1916.445	0.219	0.242	0.252
	S10	80.914	352.578	186.688	376.853	3199.59	2793.69	2647.115	0.118	0.135	0.142
	S3	3.485	462.952	142.371	463.997	2367.99	2141.19	2059.290	0.196	0.217	0.225
	S11	2.012	456.518	138.967	457.121	3465.882	3023.082	2863.182	0.132	0.151	0.160
	S4	84.703	466.150	224.548	491.561	2210.94	1996.056	1918.459	0.222	0.246	0.256
	S12	148.913	380.688	263.119	425.362	2731.437	2386.287	2261.650	0.156	0.178	0.188
3	S1	443.159	342.605	545.940	475.552	1282	1177	1153.375	0.426	0.464	0.473
	S9	644.934	219.030	710.643	412.511	2062.1	1857.1	1810.975	0.345	0.383	0.392
	S2	35.145	550.832	200.394	561.375	2443.8	2212.8	2160.825	0.230	0.254	0.260
	S10	99.297	433.548	229.362	463.337	3555.1	3104.1	3002.625	0.130	0.149	0.154
	S3	3.896	543.703	167.006	544.871	2631.1	2379.1	2322.400	0.207	0.229	0.235
	S11	1.896	551.087	167.222	551.656	3850.98	3358.98	3248.280	0.143	0.164	0.170
	S4	106.685	541.756	269.212	573.762	2456.6	2217.84	2164.119	0.234	0.259	0.265
	S12	176.292	467.357	316.498	520.244	3034.93	2651.43	2565.143	0.171	0.196	0.203
2	S1	515.975	394.412	634.299	549.205	1410.2	1294.7	1281.575	0.450	0.490	0.495
	S9	743.274	271.421	824.701	494.404	2268.31	2042.81	2017.185	0.364	0.404	0.409
	S2	47.330	624.606	234.712	638.804	2688.18	2434.08	2405.205	0.238	0.262	0.266
	S10	120.613	513.386	274.629	549.570	3910.61	3414.51	3358.135	0.141	0.161	0.164
	S3	4.102	620.803	190.343	622.034	2894.21	2617.01	2585.510	0.215	0.238	0.241
	S11	1.697	642.147	194.341	642.656	4236.078	3694.878	3633.378	0.152	0.174	0.177
	S4	130.342	614.709	314.755	653.812	2702.26	2439.624	2409.779	0.242	0.268	0.271
	S12	204.114	553.514	370.168	614.748	3338.423	2916.573	2868.636	0.184	0.211	0.214
1	S1	574.701	433.362	704.709	605.772	1538.4	1412.4	1409.775	0.458	0.499	0.500
	S9	821.453	311.152	914.799	557.588	2474.52	2228.52	2223.395	0.370	0.410	0.411
	S2	56.126	683.749	261.250	700.587	2932.56	2655.36	2649.585	0.239	0.264	0.264
	S10	137.870	576.172	310.722	617.533	4266.12	3724.92	3713.645	0.145	0.166	0.166
	S3	4.540	681.684	209.045	683.046	3157.32	2854.92	2848.620	0.216	0.239	0.240
	S11	1.694	712.167	215.344	712.676	4621.176	4030.776	4018.476	0.154	0.177	0.177
	S4	151.895	672.381	353.609	717.950	2947.92	2661.408	2655.439	0.244	0.270	0.270
	S12	227.178	620.044	413.192	688.198	3641.916	3181.716	3172.129	0.189	0.216	0.217

Çizelge B.2: 6 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.252	6.958	10.339	9.433	128.2	122.95	112.45	0.081	0.084	0.092
	S9	10.878	2.027	11.486	5.290	206.21	195.96	175.46	0.056	0.059	0.065
	S2	1.167	9.367	3.977	9.717	244.38	232.83	209.73	0.040	0.042	0.046
	S10	3.190	3.489	4.236	4.446	355.51	332.96	287.86	0.013	0.013	0.015
	S3	0.138	9.398	2.957	9.440	263.11	250.51	225.31	0.036	0.038	0.042
	S11	0.136	4.745	1.560	4.786	385.098	360.498	311.298	0.012	0.013	0.015
	S4	0.970	9.447	3.804	9.738	245.66	233.722	209.846	0.040	0.042	0.046
	S12	2.669	3.728	3.787	4.529	303.493	284.318	245.968	0.015	0.016	0.018
5	S1	29.349	23.133	36.289	31.937	256.4	245.9	230.15	0.142	0.148	0.158
	S9	38.252	10.239	41.324	21.715	412.42	391.92	361.17	0.100	0.105	0.114
	S2	5.845	30.536	15.006	32.289	488.76	465.66	431.01	0.066	0.069	0.075
	S10	12.522	16.210	17.385	19.967	711.02	665.92	598.27	0.028	0.030	0.033
	S3	0.140	30.646	9.334	30.688	526.22	501.02	463.22	0.058	0.061	0.066
	S11	0.096	21.502	6.547	21.531	770.196	720.996	647.196	0.028	0.030	0.033
	S4	4.879	30.522	14.035	31.985	491.32	467.444	431.63	0.065	0.068	0.074
	S12	10.692	17.766	16.021	20.973	606.986	568.636	511.111	0.035	0.037	0.041
4	S1	61.384	46.990	75.481	65.405	384.6	368.85	353.1	0.196	0.205	0.214
	S9	80.263	22.711	87.076	46.790	618.63	587.88	557.13	0.141	0.148	0.156
	S2	14.221	61.563	32.689	65.829	733.14	698.49	663.84	0.090	0.094	0.099
	S10	28.861	35.229	39.429	43.887	1066.53	998.88	931.23	0.041	0.044	0.047
	S3	0.105	61.861	18.663	61.893	789.33	751.53	713.73	0.078	0.082	0.087
	S11	0.294	47.533	14.554	47.621	1155.294	1081.494	1007.694	0.041	0.044	0.047
	S4	10.821	61.423	29.247	64.669	736.98	701.166	665.352	0.088	0.092	0.097
	S12	23.273	38.899	34.943	45.881	910.479	852.954	795.429	0.050	0.054	0.058
3	S1	99.327	74.039	121.539	103.838	512.8	491.8	481.3	0.237	0.247	0.253
	S9	132.369	37.608	143.652	77.319	824.84	783.84	763.34	0.174	0.183	0.188
	S2	24.408	100.672	54.610	107.994	977.52	931.32	908.22	0.110	0.116	0.119
	S10	45.762	65.221	65.328	78.949	1422.04	1331.84	1286.74	0.056	0.059	0.061
	S3	0.219	99.229	29.988	99.295	1052.44	1002.04	976.84	0.094	0.099	0.102
	S11	0.392	87.670	26.693	87.788	1540.392	1441.992	1392.792	0.057	0.061	0.063
	S4	19.509	100.159	49.556	106.012	982.64	934.888	911.012	0.108	0.113	0.116
	S12	39.849	71.875	61.412	83.830	1213.972	1137.272	1098.922	0.069	0.074	0.076
2	S1	140.612	102.089	171.239	144.272	641	614.75	609.5	0.267	0.279	0.281
	S9	190.850	53.436	206.881	110.691	1031.05	979.8	969.55	0.201	0.211	0.213
	S2	35.995	144.744	79.418	155.542	1221.9	1164.15	1152.6	0.127	0.134	0.135
	S10	62.456	102.686	93.262	121.423	1777.55	1664.8	1642.25	0.068	0.073	0.074
	S3	0.216	139.786	42.152	139.851	1315.55	1252.55	1239.95	0.106	0.112	0.113
	S11	0.384	138.035	41.795	138.150	1925.49	1802.49	1777.89	0.072	0.077	0.078
	S4	30.798	143.988	73.994	153.228	1228.3	1168.61	1156.672	0.125	0.131	0.132
	S12	59.277	113.137	93.218	130.920	1517.465	1421.59	1402.415	0.086	0.092	0.093
1	S1	177.508	126.929	215.587	180.181	769.2	737.7	737.7	0.280	0.292	0.292
	S9	247.013	66.862	267.072	140.966	1237.26	1175.76	1175.76	0.216	0.227	0.227
	S2	44.764	186.083	100.589	199.512	1466.28	1396.98	1396.98	0.136	0.143	0.143
	S10	76.472	142.918	119.348	165.859	2133.06	1997.76	1997.76	0.078	0.083	0.083
	S3	0.373	178.053	53.789	178.165	1578.66	1503.06	1503.06	0.113	0.119	0.119
	S11	0.284	190.333	57.384	190.418	2310.588	2162.988	2162.988	0.082	0.088	0.088
	S4	38.327	184.994	93.825	196.492	1473.96	1402.332	1402.332	0.133	0.140	0.140
	S12	78.541	157.212	125.705	180.774	1820.958	1705.908	1705.908	0.099	0.106	0.106

Çizelge B.3: 9 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	8.296	8.432	10.826	10.921	128.2	117.7	104.575	0.085	0.093	0.104
	S9	11.129	1.426	11.557	4.765	206.21	185.71	160.085	0.056	0.062	0.072
	S2	1.039	12.165	4.689	12.477	244.38	221.28	192.405	0.051	0.056	0.065
	S10	0.812	1.459	1.250	1.703	355.51	310.41	254.035	0.005	0.005	0.007
	S3	0.506	11.975	4.098	12.126	263.11	237.91	206.41	0.046	0.051	0.059
	S11	0.529	2.560	1.297	2.719	385.098	335.898	274.398	0.007	0.008	0.010
	S4	0.270	12.141	3.913	12.223	245.66	221.784	191.939	0.050	0.055	0.064
8	S12	1.815	1.428	2.243	1.972	303.493	265.143	217.2055	0.007	0.008	0.010
	S1	30.841	27.549	39.106	36.801	256.4	235.4	211.775	0.153	0.166	0.185
	S9	40.608	9.841	43.560	22.023	412.42	371.42	325.295	0.106	0.117	0.134
	S2	1.162	38.181	12.616	38.530	488.76	442.56	390.585	0.079	0.087	0.099
	S10	7.736	13.175	11.688	15.496	711.02	620.82	519.345	0.022	0.025	0.030
	S3	0.771	37.821	12.117	38.052	526.22	475.82	419.12	0.072	0.080	0.091
	S11	0.752	18.443	6.285	18.669	770.196	671.796	561.096	0.024	0.028	0.033
7	S4	3.812	37.884	15.177	39.028	491.32	443.568	389.847	0.079	0.088	0.100
	S12	9.608	14.288	13.894	17.170	606.986	530.286	443.9985	0.028	0.032	0.039
	S1	66.012	55.532	82.672	75.335	384.6	353.1	318.975	0.215	0.234	0.259
	S9	86.962	23.219	93.927	49.307	618.63	557.13	490.505	0.152	0.169	0.191
	S2	7.663	75.558	30.330	77.857	733.14	663.84	588.765	0.106	0.117	0.132
	S10	22.791	32.132	32.430	38.969	1066.53	931.23	784.655	0.037	0.042	0.050
	S3	0.769	75.160	23.317	75.391	789.33	713.73	631.83	0.096	0.106	0.119
6	S11	0.594	44.963	14.083	45.141	1155.294	1007.694	847.794	0.039	0.045	0.053
	S4	9.717	74.935	32.198	77.850	736.98	665.352	587.755	0.106	0.117	0.132
	S12	22.639	35.323	33.236	42.115	910.479	795.429	670.7915	0.046	0.053	0.063
	S1	108.844	87.852	135.199	120.505	512.8	470.8	418.3	0.264	0.287	0.323
	S9	146.166	39.781	158.100	83.630	824.84	742.84	640.34	0.192	0.213	0.247
	S2	16.444	123.410	53.467	128.344	977.52	885.12	769.62	0.131	0.145	0.167
	S10	38.649	64.538	58.010	76.132	1422.04	1241.64	1016.14	0.054	0.061	0.075
5	S3	0.919	120.585	37.094	120.860	1052.44	951.64	825.64	0.115	0.127	0.146
	S11	0.731	88.856	27.387	89.075	1540.392	1343.592	1097.592	0.058	0.066	0.081
	S4	19.031	122.134	55.671	127.844	982.64	887.136	767.756	0.130	0.144	0.167
	S12	40.640	70.853	61.896	83.045	1213.972	1060.572	868.822	0.068	0.078	0.096
	S1	157.865	123.055	194.781	170.414	641	588.5	525.5	0.304	0.331	0.371
	S9	215.856	58.436	233.386	123.193	1031.05	928.55	805.55	0.226	0.251	0.290
	S2	27.558	179.773	81.490	188.040	1221.9	1106.4	967.8	0.154	0.170	0.194
4	S10	55.118	107.281	87.303	123.816	1777.55	1552.05	1281.45	0.070	0.080	0.097
	S3	1.226	172.076	52.849	172.444	1315.55	1189.55	1038.35	0.131	0.145	0.166
	S11	0.940	147.160	45.088	147.442	1925.49	1679.49	1384.29	0.077	0.088	0.107
	S4	32.157	177.790	85.494	187.437	1228.3	1108.92	965.664	0.153	0.169	0.194
	S12	62.729	117.678	98.033	136.497	1517.465	1325.715	1095.615	0.090	0.103	0.125
	S1	209.793	160.533	257.953	223.471	769.2	706.2	648.45	0.335	0.365	0.398
	S9	294.188	79.283	317.973	167.539	1237.26	1114.26	1001.51	0.257	0.285	0.317
3	S2	37.174	241.741	109.696	252.893	1466.28	1327.68	1200.63	0.172	0.190	0.211
	S10	71.522	165.371	121.133	186.827	2133.06	1862.46	1614.41	0.088	0.100	0.116
	S3	1.284	229.471	70.126	229.856	1578.66	1427.46	1288.86	0.146	0.161	0.178
	S11	1.279	219.449	67.113	219.833	2310.588	2015.388	1744.788	0.095	0.109	0.126
	S4	42.270	238.910	113.943	251.591	1473.96	1330.704	1199.386	0.171	0.189	0.210
	S12	89.322	181.076	143.645	207.872	1820.958	1590.858	1379.933	0.114	0.131	0.151
	S1	264.244	197.803	323.585	277.076	897.4	823.9	776.65	0.361	0.393	0.417
3	S9	375.604	102.218	406.269	214.899	1443.47	1299.97	1207.72	0.281	0.313	0.336
	S2	44.752	307.965	137.142	321.391	1710.66	1548.96	1445.01	0.188	0.207	0.222
	S10	84.033	228.015	152.437	253.225	2488.57	2172.87	1969.92	0.102	0.117	0.129
	S3	1.797	294.073	90.019	294.612	1841.77	1665.37	1551.97	0.160	0.177	0.190

2	S11	1.380	304.726	92.798	305.140	2695.686	2351.286	2129.886	0.113	0.130	0.143
	S4	56.624	303.795	147.762	320.782	1719.62	1552.488	1445.046	0.187	0.207	0.222
	S12	110.662	249.132	185.401	282.330	2124.451	1856.001	1683.426	0.133	0.152	0.168
	S1	319.927	235.870	390.688	331.848	1025.6	941.6	904.85	0.381	0.415	0.432
	S9	460.672	135.749	501.397	273.951	1649.68	1485.68	1413.93	0.304	0.337	0.355
	S2	51.158	374.518	163.513	389.865	1955.04	1770.24	1689.39	0.199	0.220	0.231
	S10	99.511	293.163	187.460	323.016	2844.08	2483.28	2325.43	0.114	0.130	0.139
	S3	2.458	360.496	110.606	361.233	2104.88	1903.28	1815.08	0.172	0.190	0.199
	S11	1.286	389.987	118.282	390.372	3080.784	2687.184	2514.984	0.127	0.145	0.155
	S4	73.987	369.518	184.842	391.714	1965.28	1774.272	1690.706	0.199	0.221	0.232
	S12	132.169	320.041	228.181	359.691	2427.944	2121.144	1986.919	0.148	0.170	0.181
1	S1	367.518	267.825	447.865	378.080	1153.8	1059.3	1033.05	0.388	0.423	0.434
	S9	535.974	169.869	586.934	330.661	1855.89	1671.39	1620.14	0.316	0.351	0.362
	S2	54.715	431.111	184.048	447.526	2199.42	1991.52	1933.77	0.203	0.225	0.231
	S10	114.221	353.726	220.338	387.992	3199.59	2793.69	2680.94	0.121	0.139	0.145
	S3	3.181	417.248	128.356	418.202	2367.99	2141.19	2078.19	0.177	0.195	0.201
	S11	1.392	461.702	139.903	462.120	3465.882	3023.082	2900.082	0.133	0.153	0.159
	S4	89.032	425.218	216.597	451.927	2210.94	1996.056	1936.366	0.204	0.226	0.233
	S12	154.239	385.316	269.834	431.588	2731.437	2386.287	2290.412	0.158	0.181	0.188

Çizelge B.4: 12 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	8.316	10.483	11.460	12.978	128.2	117.7	117.700	0.101	0.110	0.110
	S9	11.301	0.076	11.324	3.467	206.21	185.71	185.710	0.055	0.061	0.061
	S2	3.737	15.390	8.354	16.511	244.38	221.28	221.280	0.068	0.075	0.075
	S10	2.225	1.135	2.566	1.802	355.51	310.41	310.410	0.007	0.008	0.008
	S3	0.699	15.483	5.344	15.693	263.11	237.91	237.910	0.060	0.066	0.066
	S11	0.886	0.542	1.048	0.808	385.098	335.898	335.898	0.003	0.003	0.003
	S4	0.993	15.351	5.599	15.649	245.66	221.784	221.784	0.064	0.071	0.071
11	S12	0.781	1.571	1.252	1.805	303.493	265.143	265.143	0.006	0.007	0.007
	S1	32.108	33.158	42.055	42.791	256.4	235.4	235.400	0.167	0.182	0.182
	S9	42.560	7.469	44.800	20.237	412.42	371.42	371.420	0.109	0.121	0.121
	S2	4.773	46.692	18.780	48.124	488.76	442.56	442.560	0.098	0.109	0.109
	S10	1.287	8.882	3.951	9.268	711.02	620.82	620.820	0.013	0.015	0.015
	S3	0.994	46.942	15.076	47.240	526.22	475.82	475.820	0.090	0.099	0.099
	S11	1.262	13.350	5.267	13.728	770.196	671.796	671.796	0.018	0.020	0.020
10	S4	1.572	46.297	15.461	46.769	491.32	443.568	443.568	0.095	0.105	0.105
	S12	8.146	9.278	10.929	11.721	606.986	530.286	530.286	0.019	0.022	0.022
	S1	69.402	65.300	88.992	86.120	384.6	353.1	353.100	0.231	0.252	0.252
	S9	91.848	20.345	97.951	47.900	618.63	557.13	557.130	0.158	0.176	0.176
	S2	1.157	90.092	28.184	90.439	733.14	663.84	663.840	0.123	0.136	0.136
	S10	13.572	26.613	21.556	30.685	1066.53	931.23	931.230	0.029	0.033	0.033
	S3	1.016	90.658	28.213	90.963	789.33	713.73	713.730	0.115	0.127	0.127
9	S11	1.256	38.525	12.814	38.902	1155.294	1007.694	1007.694	0.034	0.039	0.039
	S4	6.672	89.278	33.455	91.280	736.98	665.352	665.352	0.124	0.137	0.137
	S12	21.093	28.846	29.747	35.173	910.479	795.429	795.429	0.039	0.044	0.044
	S1	114.974	102.188	145.630	136.680	512.8	470.8	457.675	0.284	0.309	0.318
	S9	155.082	36.609	166.065	83.134	824.84	742.84	717.215	0.201	0.224	0.232
	S2	4.852	145.154	48.398	146.610	977.52	885.12	856.245	0.150	0.166	0.171
	S10	26.347	59.022	44.054	66.926	1422.04	1241.64	1185.265	0.047	0.054	0.056
8	S3	1.200	143.315	44.195	143.676	1052.44	951.64	920.140	0.137	0.151	0.156
	S11	1.504	82.697	26.312	83.148	1540.392	1343.592	1282.092	0.054	0.062	0.065
	S4	15.516	143.551	58.581	148.206	982.64	887.136	857.291	0.151	0.167	0.173
	S12	39.393	64.197	58.652	76.014	1213.972	1060.572	1012.635	0.063	0.072	0.075
	S1	167.759	142.593	210.537	192.921	641	588.5	564.875	0.328	0.358	0.373
	S9	230.430	55.227	246.998	124.356	1031.05	928.55	882.425	0.240	0.266	0.280
	S2	13.504	210.231	76.573	214.283	1221.9	1106.4	1054.425	0.175	0.194	0.203
7	S10	39.745	103.025	70.652	114.948	1777.55	1552.05	1450.575	0.065	0.074	0.079
	S3	1.560	203.192	62.518	203.660	1315.55	1189.55	1132.850	0.155	0.171	0.180
	S11	1.779	143.126	44.717	143.659	1925.49	1679.49	1568.790	0.075	0.086	0.092
	S4	28.728	207.774	91.060	216.392	1228.3	1108.92	1055.199	0.176	0.195	0.205
	S12	62.330	112.195	95.989	130.894	1517.465	1325.715	1239.428	0.086	0.099	0.106
	S1	224.498	186.181	280.352	253.530	769.2	706.2	672.075	0.364	0.397	0.417
	S9	316.628	76.532	339.588	171.520	1237.26	1114.26	1047.635	0.274	0.305	0.324
6	S2	20.421	282.636	105.212	288.762	1466.28	1327.68	1252.605	0.197	0.217	0.231
	S10	53.152	165.328	102.750	181.274	2133.06	1862.46	1715.885	0.085	0.097	0.106
	S3	1.661	270.700	82.871	271.198	1578.66	1427.46	1345.560	0.172	0.190	0.202
	S11	2.173	220.295	68.261	220.947	2310.588	2015.388	1855.488	0.096	0.110	0.119
	S4	38.464	279.131	122.203	290.670	1473.96	1330.704	1253.107	0.197	0.218	0.232
	S12	90.777	179.935	144.757	207.168	1820.958	1590.858	1466.221	0.114	0.130	0.141
	S1	285.462	230.599	354.641	316.237	897.4	823.9	784.525	0.395	0.430	0.452
6	S9	408.007	100.621	438.193	223.023	1443.47	1299.97	1223.095	0.304	0.337	0.358
	S2	25.078	361.871	133.639	369.394	1710.66	1548.96	1462.335	0.216	0.238	0.253
	S10	61.914	233.813	132.058	252.387	2488.57	2172.87	2003.745	0.101	0.116	0.126
	S3	2.242	348.483	106.787	349.155	1841.77	1665.37	1570.870	0.190	0.210	0.222

5	S11	2.266	314.153	96.512	314.832	2695.686	2351.286	2166.786	0.117	0.134	0.145
	S4	53.557	356.636	160.547	372.703	1719.62	1552.488	1462.953	0.217	0.240	0.255
	S12	113.227	253.950	189.412	287.918	2124.451	1856.001	1712.189	0.136	0.155	0.168
	S1	350.821	278.649	434.416	383.895	1025.6	941.6	902.225	0.424	0.461	0.481
	S9	508.339	139.912	550.313	292.414	1649.68	1485.68	1408.805	0.334	0.370	0.391
	S2	28.592	445.847	162.346	454.424	1955.04	1770.24	1683.615	0.232	0.257	0.270
	S10	74.920	310.375	168.033	332.851	2844.08	2483.28	2314.155	0.117	0.134	0.144
	S3	2.928	432.191	132.585	433.069	2104.88	1903.28	1808.780	0.206	0.228	0.239
	S11	2.161	412.553	125.927	413.201	3080.784	2687.184	2502.684	0.134	0.154	0.165
	S4	72.603	439.075	204.325	460.856	1965.28	1774.272	1684.737	0.234	0.260	0.274
	S12	137.482	336.376	238.395	377.621	2427.944	2121.144	1977.332	0.156	0.178	0.191
	S1	420.335	328.946	519.019	455.047	1153.8	1059.3	1025.175	0.450	0.490	0.506
4	S9	614.382	190.291	671.469	374.606	1855.89	1671.39	1604.765	0.362	0.402	0.418
	S2	30.700	533.115	190.635	542.325	2199.42	1991.52	1916.445	0.247	0.272	0.283
	S10	91.028	396.651	210.024	423.959	3199.59	2793.69	2647.115	0.133	0.152	0.160
	S3	3.921	520.821	160.167	521.997	2367.99	2141.19	2059.290	0.220	0.244	0.253
	S11	2.264	513.582	156.338	514.261	3465.882	3023.082	2863.182	0.148	0.170	0.180
	S4	95.291	524.419	252.616	553.006	2210.94	1996.056	1918.459	0.250	0.277	0.288
	S12	167.527	428.275	296.009	478.533	2731.437	2386.287	2261.650	0.175	0.201	0.212
	S1	498.554	385.430	614.183	534.997	1282	1177	1153.375	0.479	0.522	0.533
3	S9	725.551	246.409	799.474	464.074	2062.1	1857.1	1810.975	0.388	0.430	0.441
	S2	39.538	619.686	225.444	631.547	2443.8	2212.8	2160.825	0.258	0.285	0.292
	S10	111.710	487.742	258.032	521.254	3555.1	3104.1	3002.625	0.147	0.168	0.174
	S3	4.382	611.665	187.882	612.980	2631.1	2379.1	2322.400	0.233	0.258	0.264
	S11	2.133	619.973	188.125	620.613	3850.98	3358.98	3248.280	0.161	0.185	0.191
	S4	120.021	609.476	302.863	645.482	2456.6	2217.84	2164.119	0.263	0.291	0.298
	S12	198.328	525.776	356.061	585.275	3034.93	2651.43	2565.143	0.193	0.221	0.228
	S1	580.472	443.714	713.586	617.855	1410.2	1294.7	1281.575	0.506	0.551	0.557
2	S9	836.183	305.349	927.788	556.204	2268.31	2042.81	2017.185	0.409	0.454	0.460
	S2	53.246	702.681	264.050	718.655	2688.18	2434.08	2405.205	0.267	0.295	0.299
	S10	135.690	577.559	308.957	618.266	3910.61	3414.51	3358.135	0.158	0.181	0.184
	S3	4.615	698.404	214.136	699.788	2894.21	2617.01	2585.510	0.242	0.267	0.271
	S11	1.909	722.416	218.634	722.988	4236.078	3694.878	3633.378	0.171	0.196	0.199
	S4	146.635	691.547	354.099	735.538	2702.26	2439.624	2409.779	0.272	0.301	0.305
	S12	229.628	622.704	416.439	691.592	3338.423	2916.573	2868.636	0.207	0.237	0.241
	S1	646.538	487.532	792.798	681.494	1538.4	1412.4	1409.775	0.515	0.561	0.562
1	S9	924.135	350.046	1029.148	627.287	2474.52	2228.52	2223.395	0.416	0.462	0.463
	S2	63.141	769.218	293.906	788.160	2932.56	2655.36	2649.585	0.269	0.297	0.297
	S10	155.104	648.193	349.562	694.725	4266.12	3724.92	3713.645	0.163	0.187	0.187
	S3	5.108	766.895	235.176	768.427	3157.32	2854.92	2848.620	0.243	0.269	0.270
	S11	1.906	801.188	242.262	801.760	4621.176	4030.776	4018.476	0.173	0.199	0.200
	S4	170.882	756.429	397.810	807.693	2947.92	2661.408	2655.439	0.274	0.303	0.304
	S12	255.576	697.550	464.841	774.223	3641.916	3181.716	3172.129	0.213	0.243	0.244

Çizelge B.5: 6 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	13.373	11.275	16.755	15.287	128.2	122.95	112.45	0.131	0.136	0.149
	S9	17.627	3.285	18.613	8.573	206.21	195.96	175.46	0.090	0.095	0.106
	S2	1.892	15.179	6.445	15.746	244.38	232.83	209.73	0.064	0.068	0.075
	S10	5.169	5.654	6.865	7.204	355.51	332.96	287.86	0.020	0.022	0.025
	S3	0.223	15.230	4.792	15.297	263.11	250.51	225.31	0.058	0.061	0.068
	S11	0.221	7.690	2.527	7.756	385.098	360.498	311.298	0.020	0.022	0.025
	S4	1.573	15.308	6.165	15.780	245.66	233.722	209.846	0.064	0.068	0.075
5	S12	4.325	6.042	6.137	7.339	303.493	284.318	245.968	0.024	0.026	0.030
	S1	47.561	37.487	58.807	51.755	256.4	245.9	230.15	0.229	0.239	0.256
	S9	61.989	16.593	66.967	35.189	412.42	391.92	361.17	0.162	0.171	0.185
	S2	9.472	49.484	24.317	52.325	488.76	465.66	431.01	0.107	0.112	0.121
	S10	20.293	26.268	28.173	32.356	711.02	665.92	598.27	0.046	0.049	0.054
	S3	0.227	49.663	15.125	49.731	526.22	501.02	463.22	0.095	0.099	0.107
	S11	0.156	34.845	10.609	34.892	770.196	720.996	647.196	0.045	0.048	0.054
4	S4	7.906	49.461	22.744	51.833	491.32	467.444	431.63	0.105	0.111	0.120
	S12	17.326	28.790	25.963	33.987	606.986	568.636	511.111	0.056	0.060	0.066
	S1	99.475	76.148	122.319	105.990	384.6	368.85	353.1	0.318	0.332	0.346
	S9	130.068	36.804	141.109	75.824	618.63	587.88	557.13	0.228	0.240	0.253
	S2	23.045	99.764	52.974	106.677	733.14	698.49	663.84	0.146	0.153	0.161
	S10	46.770	57.089	63.896	71.120	1066.53	998.88	931.23	0.067	0.071	0.076
	S3	0.170	100.248	30.244	100.299	789.33	751.53	713.73	0.127	0.133	0.141
3	S11	0.477	77.029	23.585	77.172	1155.294	1081.494	1007.694	0.067	0.071	0.077
	S4	17.535	99.537	47.396	104.798	736.98	701.166	665.352	0.142	0.149	0.158
	S12	37.714	63.037	56.625	74.352	910.479	852.954	795.429	0.082	0.087	0.093
	S1	160.963	119.983	196.957	168.271	512.8	491.8	481.3	0.384	0.400	0.409
	S9	214.508	60.945	232.791	125.298	824.84	783.84	763.34	0.282	0.297	0.305
	S2	39.554	163.141	88.497	175.007	977.52	931.32	908.22	0.179	0.188	0.193
	S10	74.159	105.692	105.866	127.939	1422.04	1331.84	1286.74	0.090	0.096	0.099
2	S3	0.356	160.804	48.597	160.910	1052.44	1002.04	976.84	0.153	0.161	0.165
	S11	0.635	142.072	43.257	142.263	1540.392	1441.992	1392.792	0.092	0.099	0.102
	S4	31.614	162.311	80.307	171.795	982.64	934.888	911.012	0.175	0.184	0.189
	S12	64.577	116.476	99.520	135.849	1213.972	1137.272	1098.922	0.112	0.119	0.124
	S1	227.866	165.437	277.497	233.797	641	614.75	609.5	0.433	0.451	0.455
	S9	309.278	86.595	335.256	179.378	1031.05	979.8	969.55	0.325	0.342	0.346
	S2	58.330	234.560	128.698	252.059	1221.9	1164.15	1152.6	0.206	0.217	0.219
1	S10	101.212	166.406	151.134	196.770	1777.55	1664.8	1642.25	0.111	0.118	0.120
	S3	0.351	226.527	68.309	226.633	1315.55	1252.55	1239.95	0.172	0.181	0.183
	S11	0.623	223.689	67.730	223.876	1925.49	1802.49	1777.89	0.116	0.124	0.126
	S4	49.909	233.337	119.910	248.309	1228.3	1168.61	1156.672	0.202	0.212	0.215
	S12	96.059	183.341	151.062	212.159	1517.465	1421.59	1402.415	0.140	0.149	0.151
	S1	287.656	205.692	349.364	291.988	769.2	737.7	737.7	0.454	0.474	0.474
	S9	400.291	108.351	432.797	228.439	1237.26	1175.76	1175.76	0.350	0.368	0.368
	S2	72.542	301.553	163.007	323.315	1466.28	1396.98	1396.98	0.221	0.231	0.231
	S10	123.925	231.602	193.406	268.780	2133.06	1997.76	1997.76	0.126	0.135	0.135
	S3	0.604	288.540	87.166	288.721	1578.66	1503.06	1503.06	0.183	0.192	0.192
	S11	0.460	308.439	92.992	308.577	2310.588	2162.988	2162.988	0.134	0.143	0.143
	S4	62.110	299.787	152.046	318.420	1473.96	1402.332	1402.332	0.216	0.227	0.227
	S12	127.278	254.766	203.708	292.950	1820.958	1705.908	1705.908	0.161	0.172	0.172

Çizelge B.6: 9 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	11.061	11.242	14.434	14.561	128.2	117.7	104.575	0.114	0.124	0.139
	S9	14.839	1.902	15.410	6.353	206.21	185.71	160.085	0.075	0.083	0.096
	S2	1.386	16.220	6.252	16.635	244.38	221.28	192.405	0.068	0.075	0.086
	S10	1.083	1.945	1.666	2.270	355.51	310.41	254.035	0.006	0.007	0.009
	S3	0.675	15.966	5.465	16.169	263.11	237.91	206.41	0.061	0.068	0.078
	S11	0.705	3.413	1.729	3.625	385.098	335.898	274.398	0.009	0.011	0.013
	S4	0.361	16.189	5.217	16.297	245.66	221.784	191.939	0.066	0.073	0.085
	S12	2.420	1.904	2.991	2.630	303.493	265.143	217.2055	0.010	0.011	0.014
8	S1	41.121	36.732	52.141	49.068	256.4	235.4	211.775	0.203	0.221	0.246
	S9	54.144	13.121	58.080	29.364	412.42	371.42	325.295	0.141	0.156	0.179
	S2	1.549	50.908	16.821	51.373	488.76	442.56	390.585	0.105	0.116	0.132
	S10	10.315	17.567	15.585	20.661	711.02	620.82	519.345	0.029	0.033	0.040
	S3	1.027	50.428	16.156	50.736	526.22	475.82	419.12	0.096	0.107	0.121
	S11	1.003	24.591	8.380	24.892	770.196	671.796	561.096	0.032	0.037	0.044
	S4	5.083	50.513	20.237	52.037	491.32	443.568	389.847	0.106	0.117	0.133
	S12	12.810	19.050	18.525	22.893	606.986	530.286	443.9985	0.038	0.043	0.052
7	S1	88.016	74.042	110.229	100.447	384.6	353.1	318.975	0.287	0.312	0.346
	S9	115.949	30.958	125.236	65.743	618.63	557.13	490.505	0.202	0.225	0.255
	S2	10.217	100.744	40.440	103.810	733.14	663.84	588.765	0.142	0.156	0.176
	S10	30.388	42.842	43.240	51.959	1066.53	931.23	784.655	0.049	0.056	0.066
	S3	1.026	100.213	31.090	100.521	789.33	713.73	631.83	0.127	0.141	0.159
	S11	0.792	59.950	18.777	60.188	1155.294	1007.694	847.794	0.052	0.060	0.071
	S4	12.956	99.913	42.930	103.800	736.98	665.352	587.755	0.141	0.156	0.177
	S12	30.186	47.098	44.315	56.153	910.479	795.429	670.7915	0.062	0.071	0.084
6	S1	145.125	117.136	180.266	160.673	512.8	470.8	418.3	0.352	0.383	0.431
	S9	194.888	53.041	210.800	111.507	824.84	742.84	640.34	0.256	0.284	0.329
	S2	21.926	164.547	71.290	171.125	977.52	885.12	769.62	0.175	0.193	0.222
	S10	51.532	86.050	77.347	101.510	1422.04	1241.64	1016.14	0.071	0.082	0.100
	S3	1.225	160.780	49.458	161.147	1052.44	951.64	825.64	0.153	0.169	0.195
	S11	0.974	118.474	36.517	118.766	1540.392	1343.592	1097.592	0.077	0.088	0.108
	S4	25.375	162.846	74.228	170.458	982.64	887.136	767.756	0.173	0.192	0.222
	S12	54.187	94.471	82.528	110.727	1213.972	1060.572	868.822	0.091	0.104	0.127
5	S1	210.487	164.073	259.709	227.219	641	588.5	525.5	0.405	0.441	0.494
	S9	287.807	77.915	311.182	164.257	1031.05	928.55	805.55	0.302	0.335	0.386
	S2	36.744	239.697	108.653	250.721	1221.9	1106.4	967.8	0.205	0.227	0.259
	S10	73.491	143.041	116.403	165.088	1777.55	1552.05	1281.45	0.093	0.106	0.129
	S3	1.635	229.435	70.465	229.926	1315.55	1189.55	1038.35	0.175	0.193	0.221
	S11	1.254	196.213	60.117	196.589	1925.49	1679.49	1384.29	0.102	0.117	0.142
	S4	42.876	237.054	113.992	249.917	1228.3	1108.92	965.664	0.203	0.225	0.259
	S12	83.639	156.904	130.710	181.996	1517.465	1325.715	1095.615	0.120	0.137	0.166
4	S1	279.724	214.044	343.938	297.961	769.2	706.2	648.45	0.447	0.487	0.530
	S9	392.251	105.710	423.964	223.386	1237.26	1114.26	1001.51	0.343	0.380	0.423
	S2	49.565	322.321	146.261	337.191	1466.28	1327.68	1200.63	0.230	0.254	0.281
	S10	95.363	220.494	161.511	249.103	2133.06	1862.46	1614.41	0.117	0.134	0.154
	S3	1.712	305.961	93.501	306.475	1578.66	1427.46	1288.86	0.194	0.215	0.238
	S11	1.705	292.599	89.485	293.110	2310.588	2015.388	1744.788	0.127	0.145	0.168
	S4	56.360	318.546	151.924	335.454	1473.96	1330.704	1199.386	0.228	0.252	0.280
	S12	119.096	241.434	191.526	277.163	1820.958	1590.858	1379.933	0.152	0.174	0.201
3	S1	352.325	263.737	431.447	369.435	897.4	823.9	776.65	0.481	0.524	0.556

	S9	500.805	136.291	541.692	286.532	1443.47	1299.97	1207.72	0.375	0.417	0.449
	S2	59.670	410.620	182.856	428.521	1710.66	1548.96	1445.01	0.251	0.277	0.297
	S10	112.044	304.020	203.250	337.633	2488.57	2172.87	1969.92	0.136	0.155	0.171
	S3	2.396	392.098	120.026	392.816	1841.77	1665.37	1551.97	0.213	0.236	0.253
	S11	1.840	406.301	123.731	406.853	2695.686	2351.286	2129.886	0.151	0.173	0.191
	S4	75.498	405.059	197.016	427.709	1719.62	1552.488	1445.046	0.249	0.275	0.296
	S12	147.549	332.175	247.202	376.440	2124.451	1856.001	1683.426	0.177	0.203	0.224
2	S1	426.569	314.494	520.917	442.465	1025.6	941.6	904.85	0.508	0.553	0.576
	S9	614.230	180.999	668.529	365.268	1649.68	1485.68	1413.93	0.405	0.450	0.473
	S2	68.210	499.358	218.018	519.821	1955.04	1770.24	1689.39	0.266	0.294	0.308
	S10	132.682	390.884	249.947	430.688	2844.08	2483.28	2325.43	0.151	0.173	0.185
	S3	3.277	480.661	147.475	481.644	2104.88	1903.28	1815.08	0.229	0.253	0.265
	S11	1.715	519.982	157.709	520.497	3080.784	2687.184	2514.984	0.169	0.194	0.207
	S4	98.650	492.690	246.457	522.285	1965.28	1774.272	1690.706	0.266	0.294	0.309
1	S12	176.226	426.721	304.242	479.588	2427.944	2121.144	1986.919	0.198	0.226	0.241
	S1	490.024	357.100	597.154	504.107	1153.8	1059.3	1033.05	0.518	0.564	0.578
	S9	714.631	226.493	782.579	440.882	1855.89	1671.39	1620.14	0.422	0.468	0.483
	S2	72.953	574.815	245.397	596.701	2199.42	1991.52	1933.77	0.271	0.300	0.309
	S10	152.294	471.634	293.785	517.322	3199.59	2793.69	2680.94	0.162	0.185	0.193
	S3	4.242	556.331	171.141	557.603	2367.99	2141.19	2078.19	0.235	0.260	0.268
	S11	1.856	615.603	186.537	616.160	3465.882	3023.082	2900.082	0.178	0.204	0.212
	S4	118.709	566.957	288.796	602.570	2210.94	1996.056	1936.366	0.273	0.302	0.311
	S12	205.652	513.755	359.778	575.450	2731.437	2386.287	2290.412	0.211	0.241	0.251

Çizelge B.7: 12 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	11.087	13.977	15.280	17.303	128.2	117.7	117.700	0.135	0.147	0.147
	S9	15.068	0.102	15.099	4.622	206.21	185.71	185.710	0.073	0.081	0.081
	S2	4.983	20.520	11.139	22.014	244.38	221.28	221.280	0.090	0.099	0.099
	S10	2.967	1.513	3.421	2.403	355.51	310.41	310.410	0.010	0.011	0.011
	S3	0.932	20.644	7.125	20.924	263.11	237.91	237.910	0.080	0.088	0.088
	S11	1.181	0.723	1.398	1.077	385.098	335.898	335.898	0.004	0.004	0.004
	S4	1.325	20.468	7.465	20.865	245.66	221.784	221.784	0.085	0.094	0.094
11	S12	1.041	2.095	1.670	2.407	303.493	265.143	265.143	0.008	0.009	0.009
	S1	42.810	44.211	56.074	57.054	256.4	235.4	235.400	0.223	0.242	0.242
	S9	56.746	9.959	59.734	26.983	412.42	371.42	371.420	0.145	0.161	0.161
	S2	6.364	62.256	25.041	64.165	488.76	442.56	442.560	0.131	0.145	0.145
	S10	1.716	11.843	5.269	12.358	711.02	620.82	620.820	0.017	0.020	0.020
	S3	1.325	62.589	20.101	62.986	526.22	475.82	475.820	0.120	0.132	0.132
	S11	1.683	17.800	7.023	18.305	770.196	671.796	671.796	0.024	0.027	0.027
10	S4	2.096	61.730	20.615	62.358	491.32	443.568	443.568	0.127	0.141	0.141
	S12	10.861	12.370	14.572	15.629	606.986	530.286	530.286	0.026	0.029	0.029
	S1	92.536	87.066	118.656	114.827	384.6	353.1	353.100	0.309	0.336	0.336
	S9	122.464	27.127	130.602	63.866	618.63	557.13	557.130	0.211	0.234	0.234
	S2	1.542	120.123	37.579	120.586	733.14	663.84	663.840	0.164	0.182	0.182
	S10	18.096	35.484	28.742	40.913	1066.53	931.23	931.230	0.038	0.044	0.044
	S3	1.355	120.878	37.618	121.284	789.33	713.73	713.730	0.154	0.170	0.170
9	S11	1.675	51.367	17.085	51.869	1155.294	1007.694	1007.694	0.045	0.051	0.051
	S4	8.896	119.037	44.607	121.706	736.98	665.352	665.352	0.165	0.183	0.183
	S12	28.124	38.461	39.662	46.898	910.479	795.429	795.429	0.052	0.059	0.059
	S1	153.298	136.251	194.174	182.240	512.8	470.8	457.675	0.379	0.412	0.424
	S9	206.776	48.812	221.420	110.845	824.84	742.84	717.215	0.268	0.298	0.309
	S2	6.469	193.539	64.530	195.480	977.52	885.12	856.245	0.200	0.221	0.228
	S10	35.130	78.696	58.739	89.235	1422.04	1241.64	1185.265	0.063	0.072	0.075
8	S3	1.601	191.087	58.927	191.567	1052.44	951.64	920.140	0.182	0.201	0.208
	S11	2.005	110.262	35.083	110.863	1540.392	1343.592	1282.092	0.072	0.083	0.086
	S4	20.688	191.402	78.108	197.608	982.64	887.136	857.291	0.201	0.223	0.231
	S12	52.524	85.595	78.202	101.352	1213.972	1060.572	1012.635	0.083	0.096	0.100
	S1	223.679	190.124	280.716	257.228	641	588.5	564.875	0.438	0.477	0.497
	S9	307.240	73.636	329.331	165.808	1031.05	928.55	882.425	0.319	0.355	0.373
	S2	18.005	280.309	102.098	285.710	1221.9	1106.4	1054.425	0.234	0.258	0.271
7	S10	52.994	137.366	94.203	153.264	1777.55	1552.05	1450.575	0.086	0.099	0.106
	S3	2.080	270.923	83.357	271.547	1315.55	1189.55	1132.850	0.206	0.228	0.240
	S11	2.373	190.834	59.623	191.546	1925.49	1679.49	1568.790	0.099	0.114	0.122
	S4	38.304	277.032	121.414	288.523	1228.3	1108.92	1055.199	0.235	0.260	0.273
	S12	83.107	149.593	127.985	174.525	1517.465	1325.715	1239.428	0.115	0.132	0.141
	S1	299.330	248.241	373.803	338.040	769.2	706.2	672.075	0.486	0.529	0.556
	S9	422.171	102.042	452.783	228.693	1237.26	1114.26	1047.635	0.366	0.406	0.432
6	S2	27.229	376.848	140.283	385.016	1466.28	1327.68	1252.605	0.263	0.290	0.307
	S10	70.869	220.438	137.001	241.699	2133.06	1862.46	1715.885	0.113	0.130	0.141
	S3	2.214	360.933	110.494	361.598	1578.66	1427.46	1345.560	0.229	0.253	0.269
	S11	2.897	293.726	91.015	294.595	2310.588	2015.388	1855.488	0.127	0.146	0.159
	S4	51.286	372.175	162.938	387.560	1473.96	1330.704	1253.107	0.263	0.291	0.309
	S12	121.035	239.914	193.009	276.224	1820.958	1590.858	1466.221	0.152	0.174	0.188
	S1	380.616	307.465	472.855	421.650	897.4	823.9	784.525	0.527	0.574	0.603
6	S9	544.009	134.162	584.257	297.364	1443.47	1299.97	1223.095	0.405	0.449	0.478
	S2	33.437	482.495	178.185	492.526	1710.66	1548.96	1462.335	0.288	0.318	0.337
	S10	82.552	311.751	176.077	336.516	2488.57	2172.87	2003.745	0.135	0.155	0.168
	S3	2.989	464.644	142.382	465.540	1841.77	1665.37	1570.870	0.253	0.280	0.296

5	S11	3.021	418.870	128.682	419.776	2695.686	2351.286	2166.786	0.156	0.179	0.194
	S4	71.409	475.515	214.063	496.938	1719.62	1552.488	1462.953	0.289	0.320	0.340
	S12	150.969	338.600	252.549	383.891	2124.451	1856.001	1712.189	0.181	0.207	0.224
	S1	467.761	371.532	579.221	511.861	1025.6	941.6	902.225	0.565	0.615	0.642
	S9	677.785	186.550	733.750	389.885	1649.68	1485.68	1408.805	0.445	0.494	0.521
	S2	38.123	594.462	216.461	605.899	1955.04	1770.24	1683.615	0.310	0.342	0.360
	S10	99.894	413.833	224.044	443.801	2844.08	2483.28	2314.155	0.156	0.179	0.192
	S3	3.904	576.254	176.780	577.425	2104.88	1903.28	1808.780	0.274	0.303	0.319
	S11	2.881	550.070	167.902	550.934	3080.784	2687.184	2502.684	0.179	0.205	0.220
	S4	96.804	585.434	272.434	614.475	1965.28	1774.272	1684.737	0.313	0.346	0.365
	S12	183.310	448.501	317.860	503.494	2427.944	2121.144	1977.332	0.207	0.237	0.255
	S1	560.447	438.595	692.026	606.729	1153.8	1059.3	1025.175	0.600	0.653	0.675
4	S9	819.176	253.722	895.292	499.474	1855.89	1671.39	1604.765	0.482	0.536	0.558
	S2	40.934	710.820	254.180	723.100	2199.42	1991.52	1916.445	0.329	0.363	0.377
	S10	121.371	528.868	280.031	565.279	3199.59	2793.69	2647.115	0.177	0.202	0.214
	S3	5.228	694.427	213.556	695.996	2367.99	2141.19	2059.290	0.294	0.325	0.338
	S11	3.018	684.776	208.451	685.682	3465.882	3023.082	2863.182	0.198	0.227	0.239
	S4	127.054	699.226	336.822	737.342	2210.94	1996.056	1918.459	0.333	0.369	0.384
	S12	223.369	571.033	394.679	638.043	2731.437	2386.287	2261.650	0.234	0.267	0.282
	S1	664.738	513.907	818.910	713.329	1282	1177	1153.375	0.639	0.696	0.710
3	S9	967.402	328.545	1065.965	618.766	2062.1	1857.1	1810.975	0.517	0.574	0.589
	S2	52.717	826.248	300.591	842.063	2443.8	2212.8	2160.825	0.345	0.381	0.390
	S10	148.946	650.322	344.043	695.006	3555.1	3104.1	3002.625	0.195	0.224	0.231
	S3	5.843	815.554	250.509	817.307	2631.1	2379.1	2322.400	0.311	0.344	0.352
	S11	2.844	826.630	250.833	827.483	3850.98	3358.98	3248.280	0.215	0.246	0.255
	S4	160.028	812.634	403.818	860.643	2456.6	2217.84	2164.119	0.350	0.388	0.398
	S12	264.437	701.035	474.748	780.366	3034.93	2651.43	2565.143	0.257	0.294	0.304
	S1	773.963	591.618	951.448	823.807	1410.2	1294.7	1281.575	0.675	0.735	0.742
2	S9	1114.911	407.132	1237.051	741.605	2268.31	2042.81	2017.185	0.545	0.606	0.613
	S2	70.995	936.908	352.067	958.207	2688.18	2434.08	2405.205	0.356	0.394	0.398
	S10	180.919	770.079	411.943	824.354	3910.61	3414.51	3358.135	0.211	0.241	0.245
	S3	6.153	931.205	285.514	933.051	2894.21	2617.01	2585.510	0.322	0.357	0.361
	S11	2.545	963.221	291.511	963.985	4236.078	3694.878	3633.378	0.228	0.261	0.265
	S4	195.514	922.063	472.133	980.717	2702.26	2439.624	2409.779	0.363	0.402	0.407
	S12	306.171	830.271	555.253	922.123	3338.423	2916.573	2868.636	0.276	0.316	0.321
	S1	862.051	650.043	1057.064	908.658	1538.4	1412.4	1409.775	0.687	0.748	0.750
1	S9	1232.180	466.728	1372.198	836.382	2474.52	2228.52	2223.395	0.555	0.616	0.617
	S2	84.188	1025.624	391.875	1050.880	2932.56	2655.36	2649.585	0.358	0.396	0.397
	S10	206.805	864.258	466.083	926.299	4266.12	3724.92	3713.645	0.217	0.249	0.249
	S3	6.810	1022.526	313.568	1024.569	3157.32	2854.92	2848.620	0.325	0.359	0.360
	S11	2.541	1068.251	323.016	1069.013	4621.176	4030.776	4018.476	0.231	0.265	0.266
	S4	227.842	1008.572	530.414	1076.925	2947.92	2661.408	2655.439	0.365	0.405	0.406
	S12	340.768	930.067	619.788	1032.297	3641.916	3181.716	3172.129	0.283	0.324	0.325

Çizelge B.8: 6 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	18.543	15.635	23.234	21.198	128.2	122.95	112.45	0.181	0.189	0.207
	S9	24.443	4.555	25.810	11.888	206.21	195.96	175.46	0.125	0.132	0.147
	S2	2.623	21.048	8.938	21.835	244.38	232.83	209.73	0.089	0.094	0.104
	S10	7.167	7.840	9.519	9.990	355.51	332.96	287.86	0.028	0.030	0.035
	S3	0.309	21.119	6.645	21.212	263.11	250.51	225.31	0.081	0.085	0.094
	S11	0.306	10.663	3.505	10.755	385.098	360.498	311.298	0.028	0.030	0.035
	S4	2.181	21.228	8.549	21.882	245.66	233.722	209.846	0.089	0.094	0.104
5	S12	5.997	8.378	8.510	10.177	303.493	284.318	245.968	0.034	0.036	0.041
	S1	65.952	51.982	81.546	71.767	256.4	245.9	230.15	0.318	0.332	0.354
	S9	85.958	23.009	92.860	48.796	412.42	391.92	361.17	0.225	0.237	0.257
	S2	13.135	68.617	33.720	72.558	488.76	465.66	431.01	0.148	0.156	0.168
	S10	28.139	36.426	39.067	44.867	711.02	665.92	598.27	0.063	0.067	0.075
	S3	0.314	68.866	20.974	68.960	526.22	501.02	463.22	0.131	0.138	0.149
	S11	0.216	48.319	14.711	48.383	770.196	720.996	647.196	0.063	0.067	0.075
4	S4	10.963	68.586	31.539	71.875	491.32	467.444	431.63	0.146	0.154	0.167
	S12	24.026	39.921	36.002	47.129	606.986	568.636	511.111	0.078	0.083	0.092
	S1	137.938	105.591	169.615	146.973	384.6	368.85	353.1	0.441	0.460	0.480
	S9	180.360	51.035	195.671	105.143	618.63	587.88	557.13	0.316	0.333	0.351
	S2	31.955	138.339	73.457	147.926	733.14	698.49	663.84	0.202	0.212	0.223
	S10	64.854	79.164	88.603	98.620	1066.53	998.88	931.23	0.092	0.099	0.106
	S3	0.235	139.011	41.938	139.081	789.33	751.53	713.73	0.176	0.185	0.195
3	S11	0.661	106.813	32.705	107.011	1155.294	1081.494	1007.694	0.093	0.099	0.106
	S4	24.315	138.025	65.723	145.320	736.98	701.166	665.352	0.197	0.207	0.218
	S12	52.297	87.412	78.521	103.101	910.479	852.954	795.429	0.113	0.121	0.130
	S1	223.202	166.376	273.114	233.336	512.8	491.8	481.3	0.533	0.555	0.567
	S9	297.450	84.511	322.804	173.746	824.84	783.84	763.34	0.391	0.412	0.423
	S2	54.849	226.222	122.715	242.677	977.52	931.32	908.22	0.248	0.261	0.267
	S10	102.833	146.559	146.801	177.409	1422.04	1331.84	1286.74	0.125	0.133	0.138
2	S3	0.493	222.981	67.387	223.129	1052.44	1002.04	976.84	0.212	0.223	0.228
	S11	0.881	197.007	59.983	197.271	1540.392	1441.992	1392.792	0.128	0.137	0.142
	S4	43.838	225.071	111.359	238.222	982.64	934.888	911.012	0.242	0.255	0.261
	S12	89.547	161.513	138.001	188.377	1213.972	1137.272	1098.922	0.155	0.166	0.171
	S1	315.974	229.406	384.796	324.199	641	614.75	609.5	0.600	0.626	0.631
	S9	428.865	120.079	464.888	248.738	1031.05	979.8	969.55	0.451	0.474	0.479
	S2	80.885	325.257	178.462	349.522	1221.9	1164.15	1152.6	0.286	0.300	0.303
1	S10	140.347	230.750	209.572	272.854	1777.55	1664.8	1642.25	0.153	0.164	0.166
	S3	0.486	314.118	94.722	314.264	1315.55	1252.55	1239.95	0.239	0.251	0.253
	S11	0.864	310.182	93.918	310.441	1925.49	1802.49	1777.89	0.161	0.172	0.175
	S4	69.207	323.560	166.275	344.322	1228.3	1168.61	1156.672	0.280	0.295	0.298
	S12	133.202	254.233	209.472	294.194	1517.465	1421.59	1402.415	0.194	0.207	0.210
	S1	398.883	285.226	484.451	404.891	769.2	737.7	737.7	0.630	0.657	0.657
	S9	555.071	150.247	600.145	316.768	1237.26	1175.76	1175.76	0.485	0.510	0.510
	S2	100.591	418.153	226.037	448.330	1466.28	1396.98	1396.98	0.306	0.321	0.321
	S10	171.843	321.155	268.189	372.708	2133.06	1997.76	1997.76	0.175	0.187	0.187
	S3	0.838	400.109	120.870	400.360	1578.66	1503.06	1503.06	0.254	0.266	0.266
	S11	0.638	427.702	128.948	427.893	2310.588	2162.988	2162.988	0.185	0.198	0.198
	S4	86.125	415.705	210.837	441.542	1473.96	1402.332	1402.332	0.300	0.315	0.315
	S12	176.492	353.276	282.475	406.223	1820.958	1705.908	1705.908	0.223	0.238	0.238

Çizelge B.9: 9 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	13.754	13.979	17.948	18.105	128.2	117.7	104.575	0.141	0.154	0.173
	S9	18.451	2.364	19.161	7.900	206.21	185.71	160.085	0.093	0.103	0.120
	S2	1.723	20.168	7.774	20.685	244.38	221.28	192.405	0.085	0.093	0.108
	S10	1.346	2.419	2.072	2.823	355.51	310.41	254.035	0.008	0.009	0.011
	S3	0.839	19.853	6.795	20.105	263.11	237.91	206.41	0.076	0.085	0.097
	S11	0.877	4.244	2.150	4.507	385.098	335.898	274.398	0.012	0.013	0.016
	S4	0.448	20.129	6.487	20.264	245.66	221.784	191.939	0.082	0.091	0.106
8	S12	3.009	2.367	3.719	3.270	303.493	265.143	217.2055	0.012	0.014	0.017
	S1	51.131	45.674	64.833	61.013	256.4	235.4	211.775	0.253	0.275	0.306
	S9	67.324	16.315	72.218	36.512	412.42	371.42	325.295	0.175	0.194	0.222
	S2	1.926	63.301	20.916	63.879	488.76	442.56	390.585	0.131	0.144	0.164
	S10	12.826	21.843	19.378	25.690	711.02	620.82	519.345	0.036	0.041	0.049
	S3	1.278	62.703	20.088	63.086	526.22	475.82	419.12	0.120	0.133	0.151
	S11	1.247	30.577	10.420	30.951	770.196	671.796	561.096	0.040	0.046	0.055
7	S4	6.320	62.809	25.163	64.705	491.32	443.568	389.847	0.132	0.146	0.166
	S12	15.929	23.688	23.035	28.466	606.986	530.286	443.9985	0.047	0.054	0.064
	S1	109.442	92.066	137.062	124.899	384.6	353.1	318.975	0.356	0.388	0.430
	S9	144.174	38.494	155.722	81.747	618.63	557.13	490.505	0.252	0.280	0.317
	S2	12.704	125.268	50.285	129.080	733.14	663.84	588.765	0.176	0.194	0.219
	S10	37.785	53.271	53.766	64.607	1066.53	931.23	784.655	0.061	0.069	0.082
	S3	1.276	124.608	38.658	124.991	789.33	713.73	631.83	0.158	0.175	0.198
6	S11	0.985	74.544	23.348	74.839	1155.294	1007.694	847.794	0.065	0.074	0.088
	S4	16.110	124.235	53.381	129.068	736.98	665.352	587.755	0.175	0.194	0.220
	S12	37.534	58.563	55.102	69.823	910.479	795.429	670.7915	0.077	0.088	0.104
	S1	180.453	145.650	224.147	199.786	512.8	470.8	418.3	0.437	0.476	0.536
	S9	242.329	65.953	262.114	138.651	824.84	742.84	640.34	0.318	0.353	0.409
	S2	27.263	204.602	88.644	212.781	977.52	885.12	769.62	0.218	0.240	0.276
	S10	64.076	106.997	96.175	126.220	1422.04	1241.64	1016.14	0.089	0.102	0.124
5	S3	1.523	199.918	61.498	200.375	1052.44	951.64	825.64	0.190	0.211	0.243
	S11	1.211	147.314	45.406	147.678	1540.392	1343.592	1097.592	0.096	0.110	0.135
	S4	31.552	202.487	92.298	211.952	982.64	887.136	767.756	0.216	0.239	0.276
	S12	67.378	117.468	102.618	137.681	1213.972	1060.572	868.822	0.113	0.130	0.158
	S1	261.725	204.013	322.929	282.531	641	588.5	525.5	0.504	0.549	0.615
	S9	357.868	96.882	386.932	204.242	1031.05	928.55	805.55	0.375	0.417	0.480
	S2	45.689	298.046	135.103	311.753	1221.9	1106.4	967.8	0.255	0.282	0.322
4	S10	91.381	177.861	144.739	205.275	1777.55	1552.05	1281.45	0.115	0.132	0.160
	S3	2.033	285.286	87.618	285.896	1315.55	1189.55	1038.35	0.217	0.240	0.275
	S11	1.559	243.977	74.752	244.444	1925.49	1679.49	1384.29	0.127	0.146	0.177
	S4	53.314	294.759	141.741	310.753	1228.3	1108.92	965.664	0.253	0.280	0.322
	S12	103.999	195.099	162.529	226.299	1517.465	1325.715	1095.615	0.149	0.171	0.207
	S1	347.817	266.148	427.662	370.493	769.2	706.2	648.45	0.556	0.606	0.660
	S9	487.736	131.443	527.169	277.764	1237.26	1114.26	1001.51	0.426	0.473	0.526
3	S2	61.631	400.784	181.866	419.273	1466.28	1327.68	1200.63	0.286	0.316	0.349
	S10	118.577	274.169	200.827	309.742	2133.06	1862.46	1614.41	0.145	0.166	0.192
	S3	2.129	380.441	116.262	381.080	1578.66	1427.46	1288.86	0.241	0.267	0.296
	S11	2.120	363.826	111.268	364.462	2310.588	2015.388	1744.788	0.158	0.181	0.209
	S4	70.080	396.089	188.907	417.113	1473.96	1330.704	1199.386	0.283	0.313	0.348
	S12	148.087	300.206	238.149	344.632	1820.958	1590.858	1379.933	0.189	0.217	0.250
	S1	438.091	327.938	536.473	459.366	897.4	823.9	776.65	0.598	0.651	0.691
3	S9	622.715	169.468	673.556	356.282	1443.47	1299.97	1207.72	0.467	0.518	0.558
	S2	74.195	510.577	227.368	532.835	1710.66	1548.96	1445.01	0.311	0.344	0.369
	S10	139.318	378.027	252.726	419.823	2488.57	2172.87	1969.92	0.169	0.193	0.213
	S3	2.980	487.545	149.243	488.439	1841.77	1665.37	1551.97	0.265	0.293	0.315

2	S11	2.288	505.206	153.850	505.892	2695.686	2351.286	2129.886	0.188	0.215	0.238
	S4	93.877	503.662	244.975	531.825	1719.62	1552.488	1445.046	0.309	0.343	0.368
	S12	183.467	413.036	307.377	468.076	2124.451	1856.001	1683.426	0.220	0.252	0.278
	S1	530.408	391.050	647.723	550.173	1025.6	941.6	904.85	0.632	0.688	0.716
	S9	763.750	225.059	831.268	454.184	1649.68	1485.68	1413.93	0.504	0.560	0.588
	S2	84.815	620.915	271.089	646.360	1955.04	1770.24	1689.39	0.331	0.365	0.383
	S10	164.980	486.036	310.791	535.530	2844.08	2483.28	2325.43	0.188	0.216	0.230
	S3	4.075	597.668	183.375	598.890	2104.88	1903.28	1815.08	0.285	0.315	0.330
	S11	2.132	646.561	196.100	647.200	3080.784	2687.184	2514.984	0.210	0.241	0.257
	S4	122.664	612.625	306.451	649.424	1965.28	1774.272	1690.706	0.330	0.366	0.384
	S12	219.124	530.597	378.303	596.334	2427.944	2121.144	1986.919	0.246	0.281	0.300
1	S1	609.309	444.028	742.518	626.820	1153.8	1059.3	1033.05	0.644	0.701	0.719
	S9	888.593	281.627	973.081	548.205	1855.89	1671.39	1620.14	0.524	0.582	0.601
	S2	90.711	714.741	305.134	741.955	2199.42	1991.52	1933.77	0.337	0.373	0.384
	S10	189.367	586.443	365.300	643.253	3199.59	2793.69	2680.94	0.201	0.230	0.240
	S3	5.274	691.757	212.801	693.340	2367.99	2141.19	2078.19	0.293	0.324	0.334
	S11	2.308	765.458	231.945	766.150	3465.882	3023.082	2900.082	0.221	0.253	0.264
	S4	147.606	704.970	359.097	749.252	2210.94	1996.056	1936.366	0.339	0.375	0.387
	S12	255.713	638.817	447.358	715.531	2731.437	2386.287	2290.412	0.262	0.300	0.312

Çizelge B.10: 12 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	11.111	14.007	15.313	17.340	128.2	117.7	117.700	0.135	0.147	0.147
	S9	15.100	0.102	15.131	4.632	206.21	185.71	185.710	0.073	0.081	0.081
	S2	4.994	20.563	11.163	22.061	244.38	221.28	221.280	0.090	0.100	0.100
	S10	2.973	1.516	3.428	2.408	355.51	310.41	310.410	0.010	0.011	0.011
	S3	0.934	20.688	7.140	20.968	263.11	237.91	237.910	0.080	0.088	0.088
	S11	1.183	0.724	1.401	1.079	385.098	335.898	335.898	0.004	0.004	0.004
	S4	1.327	20.511	7.481	20.909	245.66	221.784	221.784	0.085	0.094	0.094
11	S12	1.043	2.099	1.673	2.412	303.493	265.143	265.143	0.008	0.009	0.009
	S1	42.901	44.304	56.192	57.175	256.4	235.4	235.400	0.223	0.243	0.243
	S9	56.866	9.980	59.860	27.040	412.42	371.42	371.420	0.145	0.161	0.161
	S2	6.377	62.388	25.094	64.301	488.76	442.56	442.560	0.132	0.145	0.145
	S10	1.719	11.868	5.280	12.384	711.02	620.82	620.820	0.017	0.020	0.020
	S3	1.328	62.721	20.144	63.119	526.22	475.82	475.820	0.120	0.133	0.133
	S11	1.686	17.837	7.037	18.343	770.196	671.796	671.796	0.024	0.027	0.027
10	S4	2.101	61.860	20.659	62.490	491.32	443.568	443.568	0.127	0.141	0.141
	S12	10.884	12.396	14.603	15.662	606.986	530.286	530.286	0.026	0.030	0.030
	S1	92.731	87.250	118.907	115.070	384.6	353.1	353.100	0.309	0.337	0.337
	S9	122.722	27.184	130.878	64.001	618.63	557.13	557.130	0.212	0.235	0.235
	S2	1.546	120.377	37.659	120.840	733.14	663.84	663.840	0.165	0.182	0.182
	S10	18.135	35.559	28.802	40.999	1066.53	931.23	931.230	0.038	0.044	0.044
	S3	1.357	121.133	37.697	121.540	789.33	713.73	713.730	0.154	0.170	0.170
9	S11	1.678	51.475	17.121	51.979	1155.294	1007.694	1007.694	0.045	0.052	0.052
	S4	8.915	119.289	44.702	121.963	736.98	665.352	665.352	0.165	0.183	0.183
	S12	28.184	38.542	39.746	46.997	910.479	795.429	795.429	0.052	0.059	0.059
	S1	153.622	136.539	194.584	182.625	512.8	470.8	457.675	0.379	0.413	0.425
	S9	207.213	48.916	221.888	111.079	824.84	742.84	717.215	0.269	0.299	0.309
	S2	6.482	193.948	64.667	195.893	977.52	885.12	856.245	0.200	0.221	0.229
	S10	35.204	78.863	58.863	89.424	1422.04	1241.64	1185.265	0.063	0.072	0.075
8	S3	1.604	191.491	59.051	191.972	1052.44	951.64	920.140	0.182	0.202	0.209
	S11	2.009	110.495	35.157	111.098	1540.392	1343.592	1282.092	0.072	0.083	0.087
	S4	20.732	191.806	78.273	198.026	982.64	887.136	857.291	0.202	0.223	0.231
	S12	52.635	85.776	78.367	101.567	1213.972	1060.572	1012.635	0.084	0.096	0.100
	S1	224.152	190.526	281.309	257.772	641	588.5	564.875	0.439	0.478	0.498
	S9	307.890	73.791	330.027	166.158	1031.05	928.55	882.425	0.320	0.355	0.374
	S2	18.043	280.901	102.313	286.314	1221.9	1106.4	1054.425	0.234	0.259	0.272
7	S10	53.105	137.656	94.402	153.588	1777.55	1552.05	1450.575	0.086	0.099	0.106
	S3	2.085	271.496	83.533	272.121	1315.55	1189.55	1132.850	0.207	0.229	0.240
	S11	2.378	191.237	59.749	191.951	1925.49	1679.49	1568.790	0.100	0.114	0.122
	S4	38.385	277.617	121.670	289.132	1228.3	1108.92	1055.199	0.235	0.261	0.274
	S12	83.282	149.910	128.255	174.894	1517.465	1325.715	1239.428	0.115	0.132	0.141
	S1	299.963	248.766	374.592	338.754	769.2	706.2	672.075	0.487	0.530	0.557
	S9	423.063	102.258	453.740	229.176	1237.26	1114.26	1047.635	0.367	0.407	0.433
6	S2	27.286	377.644	140.579	385.830	1466.28	1327.68	1252.605	0.263	0.291	0.308
	S10	71.019	220.904	137.290	242.209	2133.06	1862.46	1715.885	0.114	0.130	0.141
	S3	2.219	361.696	110.728	362.362	1578.66	1427.46	1345.560	0.230	0.254	0.269
	S11	2.903	294.347	91.207	295.218	2310.588	2015.388	1855.488	0.128	0.146	0.159
	S4	51.394	372.961	163.282	388.379	1473.96	1330.704	1253.107	0.263	0.292	0.310
	S12	121.291	240.421	193.417	276.808	1820.958	1590.858	1466.221	0.152	0.174	0.189
	S1	381.420	308.115	473.854	422.541	897.4	823.9	784.525	0.528	0.575	0.604
6	S9	545.158	134.445	585.492	297.992	1443.47	1299.97	1223.095	0.406	0.450	0.479
	S2	33.508	483.514	178.562	493.566	1710.66	1548.96	1462.335	0.289	0.319	0.338
	S10	82.727	312.410	176.449	337.227	2488.57	2172.87	2003.745	0.136	0.155	0.168
	S3	2.995	465.625	142.683	466.524	1841.77	1665.37	1570.870	0.253	0.280	0.297

5	S11	3.027	419.755	128.954	420.663	2695.686	2351.286	2166.786	0.156	0.179	0.194
	S4	71.560	476.520	214.515	497.988	1719.62	1552.488	1462.953	0.290	0.321	0.340
	S12	151.288	339.316	253.083	384.702	2124.451	1856.001	1712.189	0.181	0.207	0.225
	S1	468.750	372.317	580.445	512.942	1025.6	941.6	902.225	0.566	0.616	0.643
	S9	679.217	186.944	735.301	390.709	1649.68	1485.68	1408.805	0.446	0.495	0.522
	S2	38.203	595.718	216.919	607.179	1955.04	1770.24	1683.615	0.311	0.343	0.361
	S10	100.105	414.707	224.517	444.739	2844.08	2483.28	2314.155	0.156	0.179	0.192
	S3	3.912	577.472	177.154	578.645	2104.88	1903.28	1808.780	0.275	0.304	0.320
	S11	2.887	551.232	168.257	552.098	3080.784	2687.184	2502.684	0.179	0.205	0.221
	S4	97.009	586.670	273.010	615.773	1965.28	1774.272	1684.737	0.313	0.347	0.366
	S12	183.697	449.449	318.531	504.558	2427.944	2121.144	1977.332	0.208	0.238	0.255
	S1	561.631	439.522	693.488	608.011	1153.8	1059.3	1025.175	0.601	0.655	0.676
4	S9	820.907	254.258	897.184	500.530	1855.89	1671.39	1604.765	0.483	0.537	0.559
	S2	41.020	712.322	254.717	724.628	2199.42	1991.52	1916.445	0.329	0.364	0.378
	S10	121.628	529.985	280.623	566.473	3199.59	2793.69	2647.115	0.177	0.203	0.214
	S3	5.239	695.895	214.007	697.466	2367.99	2141.19	2059.290	0.295	0.326	0.339
	S11	3.025	686.223	208.892	687.130	3465.882	3023.082	2863.182	0.198	0.227	0.240
	S4	127.323	700.703	337.534	738.900	2210.94	1996.056	1918.459	0.334	0.370	0.385
	S12	223.841	572.239	395.513	639.391	2731.437	2386.287	2261.650	0.234	0.268	0.283
	S1	666.143	514.993	820.641	714.836	1282	1177	1153.375	0.640	0.697	0.712
3	S9	969.446	329.239	1068.217	620.073	2062.1	1857.1	1810.975	0.518	0.575	0.590
	S2	52.828	827.994	301.227	843.842	2443.8	2212.8	2160.825	0.345	0.381	0.391
	S10	149.261	651.696	344.769	696.474	3555.1	3104.1	3002.625	0.196	0.224	0.232
	S3	5.856	817.277	251.039	819.034	2631.1	2379.1	2322.400	0.311	0.344	0.353
	S11	2.850	828.377	251.363	829.232	3850.98	3358.98	3248.280	0.215	0.247	0.255
	S4	160.366	814.351	404.671	862.461	2456.6	2217.84	2164.119	0.351	0.389	0.399
	S12	264.996	702.516	475.751	782.015	3034.93	2651.43	2565.143	0.258	0.295	0.305
	S1	775.598	592.868	953.458	825.548	1410.2	1294.7	1281.575	0.676	0.736	0.744
2	S9	1117.267	407.992	1239.664	743.172	2268.31	2042.81	2017.185	0.547	0.607	0.615
	S2	71.145	938.888	352.811	960.231	2688.18	2434.08	2405.205	0.357	0.394	0.399
	S10	181.302	771.706	412.813	826.096	3910.61	3414.51	3358.135	0.211	0.242	0.246
	S3	6.166	933.172	286.118	935.022	2894.21	2617.01	2585.510	0.323	0.357	0.362
	S11	2.550	965.256	292.127	966.021	4236.078	3694.878	3633.378	0.228	0.261	0.266
	S4	195.927	924.011	473.130	982.789	2702.26	2439.624	2409.779	0.364	0.403	0.408
	S12	306.818	832.026	556.426	924.071	3338.423	2916.573	2868.636	0.277	0.317	0.322
	S1	863.873	651.416	1059.297	910.578	1538.4	1412.4	1409.775	0.689	0.750	0.751
1	S9	1234.783	467.715	1375.097	838.149	2474.52	2228.52	2223.395	0.556	0.617	0.618
	S2	84.366	1027.791	392.703	1053.100	2932.56	2655.36	2649.585	0.359	0.397	0.397
	S10	207.242	866.084	467.067	928.256	4266.12	3724.92	3713.645	0.218	0.249	0.250
	S3	6.825	1024.687	314.230	1026.734	3157.32	2854.92	2848.620	0.325	0.360	0.360
	S11	2.546	1070.508	323.699	1071.272	4621.176	4030.776	4018.476	0.232	0.266	0.267
	S4	228.324	1010.703	531.534	1079.200	2947.92	2661.408	2655.439	0.366	0.405	0.406
	S12	341.488	932.032	621.097	1034.478	3641.916	3181.716	3172.129	0.284	0.325	0.326

Çizelge B.11: 6 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	26.745	22.550	33.510	30.574	128.2	122.95	112.45	0.261	0.273	0.298
	S9	35.255	6.570	37.225	17.146	206.21	195.96	175.46	0.181	0.190	0.212
	S2	3.784	30.358	12.891	31.493	244.38	232.83	209.73	0.129	0.135	0.150
	S10	10.338	11.307	13.730	14.408	355.51	332.96	287.86	0.041	0.043	0.050
	S3	0.446	30.461	9.584	30.594	263.11	250.51	225.31	0.116	0.122	0.136
	S11	0.441	15.380	5.055	15.512	385.098	360.498	311.298	0.040	0.043	0.050
	S4	3.145	30.617	12.330	31.560	245.66	233.722	209.846	0.128	0.135	0.150
5	S12	8.649	12.084	12.275	14.679	303.493	284.318	245.968	0.048	0.052	0.060
	S1	95.122	74.974	117.614	103.510	256.4	245.9	230.15	0.459	0.478	0.511
	S9	123.977	33.186	133.933	70.379	412.42	391.92	361.17	0.325	0.342	0.371
	S2	18.945	98.967	48.635	104.651	488.76	465.66	431.01	0.214	0.225	0.243
	S10	40.586	52.537	56.347	64.713	711.02	665.92	598.27	0.091	0.097	0.108
	S3	0.453	99.326	30.251	99.462	526.22	501.02	463.22	0.189	0.199	0.215
	S11	0.311	69.690	21.218	69.784	770.196	720.996	647.196	0.091	0.097	0.108
4	S4	15.812	98.922	45.489	103.665	491.32	467.444	431.63	0.211	0.222	0.240
	S12	34.652	57.579	51.926	67.975	606.986	568.636	511.111	0.112	0.120	0.133
	S1	198.949	152.295	244.638	211.980	384.6	368.85	353.1	0.636	0.663	0.693
	S9	260.135	73.608	282.217	151.648	618.63	587.88	557.13	0.456	0.480	0.507
	S2	46.089	199.528	105.948	213.355	733.14	698.49	663.84	0.291	0.305	0.321
	S10	93.539	114.178	127.793	142.240	1066.53	998.88	931.23	0.133	0.142	0.153
	S3	0.339	200.496	60.488	200.598	789.33	751.53	713.73	0.254	0.267	0.281
3	S11	0.953	154.057	47.170	154.343	1155.294	1081.494	1007.694	0.134	0.143	0.153
	S4	35.070	199.075	94.792	209.596	736.98	701.166	665.352	0.284	0.299	0.315
	S12	75.428	126.075	113.251	148.703	910.479	852.954	795.429	0.163	0.174	0.187
	S1	321.925	239.966	393.915	336.543	512.8	491.8	481.3	0.768	0.801	0.818
	S9	429.015	121.891	465.582	250.595	824.84	783.84	763.34	0.564	0.594	0.610
	S2	79.109	326.282	176.993	350.015	977.52	931.32	908.22	0.358	0.376	0.385
	S10	148.317	211.383	211.732	255.878	1422.04	1331.84	1286.74	0.180	0.192	0.199
2	S3	0.711	321.607	97.193	321.821	1052.44	1002.04	976.84	0.306	0.321	0.329
	S11	1.271	284.144	86.514	284.525	1540.392	1441.992	1392.792	0.185	0.197	0.204
	S4	63.228	324.622	160.614	343.590	982.64	934.888	911.012	0.350	0.368	0.377
	S12	129.154	232.951	199.039	271.697	1213.972	1137.272	1098.922	0.224	0.239	0.247
	S1	455.732	330.875	554.994	467.594	641	614.75	609.5	0.866	0.903	0.911
	S9	618.555	173.190	670.512	358.757	1031.05	979.8	969.55	0.650	0.684	0.692
	S2	116.660	469.121	257.397	504.119	1221.9	1164.15	1152.6	0.413	0.433	0.437
1	S10	202.424	332.812	302.267	393.539	1777.55	1664.8	1642.25	0.221	0.236	0.240
	S3	0.702	453.055	136.618	453.265	1315.55	1252.55	1239.95	0.345	0.362	0.366
	S11	1.246	447.377	135.459	447.751	1925.49	1802.49	1777.89	0.233	0.248	0.252
	S4	99.818	466.673	239.819	496.619	1228.3	1168.61	1156.672	0.404	0.425	0.429
	S12	192.119	366.682	302.123	424.318	1517.465	1421.59	1402.415	0.280	0.298	0.303
	S1	575.312	411.383	698.727	583.977	769.2	737.7	737.7	0.908	0.947	0.947
	S9	800.583	216.703	865.593	456.877	1237.26	1175.76	1175.76	0.700	0.736	0.736
	S2	145.083	603.105	326.015	646.630	1466.28	1396.98	1396.98	0.441	0.463	0.463
	S10	247.851	463.204	386.812	537.559	2133.06	1997.76	1997.76	0.252	0.269	0.269
	S3	1.208	577.080	174.332	577.442	1578.66	1503.06	1503.06	0.366	0.384	0.384
	S11	0.920	616.878	185.983	617.154	2310.588	2162.988	2162.988	0.267	0.285	0.285
	S4	124.219	599.574	304.091	636.840	1473.96	1402.332	1402.332	0.432	0.454	0.454
	S12	254.556	509.532	407.416	585.899	1820.958	1705.908	1705.908	0.322	0.343	0.343

Çizelge B.12: 9 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	19.838	20.162	25.886	26.113	128.2	117.7	104.575	0.204	0.222	0.250
	S9	26.613	3.410	27.636	11.394	206.21	185.71	160.085	0.134	0.149	0.173
	S2	2.485	29.088	11.212	29.834	244.38	221.28	192.405	0.122	0.135	0.155
	S10	1.942	3.488	2.988	4.071	355.51	310.41	254.035	0.011	0.013	0.016
	S3	1.210	28.634	9.800	28.997	263.11	237.91	206.41	0.110	0.122	0.140
	S11	1.265	6.121	3.101	6.501	385.098	335.898	274.398	0.017	0.019	0.024
	S4	0.647	29.033	9.356	29.227	245.66	221.784	191.939	0.119	0.132	0.152
8	S12	4.340	3.414	5.364	4.716	303.493	265.143	217.2055	0.018	0.020	0.025
	S1	73.747	65.875	93.510	87.999	256.4	235.4	211.775	0.365	0.397	0.442
	S9	97.101	23.532	104.161	52.662	412.42	371.42	325.295	0.253	0.280	0.320
	S2	2.777	91.299	30.167	92.132	488.76	442.56	390.585	0.189	0.208	0.236
	S10	18.498	31.504	27.950	37.054	711.02	620.82	519.345	0.052	0.060	0.071
	S3	1.843	90.437	28.974	90.990	526.22	475.82	419.12	0.173	0.191	0.217
	S11	1.799	44.101	15.029	44.641	770.196	671.796	561.096	0.058	0.066	0.080
7	S4	9.116	90.590	36.292	93.324	491.32	443.568	389.847	0.190	0.210	0.239
	S12	22.974	34.165	33.224	41.057	606.986	530.286	443.9985	0.068	0.077	0.092
	S1	157.849	132.788	197.685	180.143	384.6	353.1	318.975	0.514	0.560	0.620
	S9	207.943	55.521	224.599	117.904	618.63	557.13	490.505	0.363	0.403	0.458
	S2	18.323	180.676	72.526	186.173	733.14	663.84	588.765	0.254	0.280	0.316
	S10	54.498	76.834	77.548	93.183	1066.53	931.23	784.655	0.087	0.100	0.119
	S3	1.840	179.723	55.757	180.275	789.33	713.73	631.83	0.228	0.253	0.285
6	S11	1.420	107.515	33.675	107.941	1155.294	1007.694	847.794	0.093	0.107	0.127
	S4	23.236	179.185	76.991	186.156	736.98	665.352	587.755	0.253	0.280	0.317
	S12	54.135	84.465	79.475	100.706	910.479	795.429	670.7915	0.111	0.127	0.150
	S1	260.268	210.072	323.290	288.152	512.8	470.8	418.3	0.630	0.687	0.773
	S9	349.512	95.124	378.050	199.978	824.84	742.84	640.34	0.458	0.509	0.590
	S2	39.322	295.100	127.852	306.896	977.52	885.12	769.62	0.314	0.347	0.399
	S10	92.417	154.323	138.714	182.048	1422.04	1241.64	1016.14	0.128	0.147	0.179
5	S3	2.196	288.343	88.699	289.002	1052.44	951.64	825.64	0.275	0.304	0.350
	S11	1.747	212.472	65.489	212.997	1540.392	1343.592	1097.592	0.138	0.159	0.194
	S4	45.507	292.049	133.122	305.701	982.64	887.136	767.756	0.311	0.345	0.398
	S12	97.179	169.425	148.007	198.579	1213.972	1060.572	868.822	0.164	0.187	0.229
	S1	377.488	294.250	465.763	407.496	641	588.5	525.5	0.727	0.791	0.886
	S9	516.155	139.734	558.075	294.580	1031.05	928.55	805.55	0.541	0.601	0.693
	S2	65.897	429.875	194.859	449.644	1221.9	1106.4	967.8	0.368	0.406	0.465
4	S10	131.800	256.530	208.759	296.070	1777.55	1552.05	1281.45	0.167	0.191	0.231
	S3	2.932	411.470	126.373	412.350	1315.55	1189.55	1038.35	0.313	0.347	0.397
	S11	2.248	351.889	107.815	352.564	1925.49	1679.49	1384.29	0.183	0.210	0.255
	S4	76.895	425.134	204.435	448.202	1228.3	1108.92	965.664	0.365	0.404	0.464
	S12	149.999	281.393	234.417	326.393	1517.465	1325.715	1095.615	0.215	0.246	0.298
	S1	501.659	383.868	616.820	534.365	769.2	706.2	648.45	0.802	0.873	0.951
	S9	703.466	189.581	760.340	400.621	1237.26	1114.26	1001.51	0.615	0.682	0.759
3	S2	88.890	578.053	262.306	604.720	1466.28	1327.68	1200.63	0.412	0.455	0.504
	S10	171.024	395.436	289.655	446.743	2133.06	1862.46	1614.41	0.209	0.240	0.277
	S3	3.071	548.713	167.685	549.634	1578.66	1427.46	1288.86	0.348	0.385	0.426
	S11	3.058	524.749	160.482	525.666	2310.588	2015.388	1744.788	0.228	0.261	0.301
	S4	101.077	571.282	272.462	601.605	1473.96	1330.704	1199.386	0.408	0.452	0.502
	S12	213.588	432.989	343.484	497.065	1820.958	1590.858	1379.933	0.273	0.312	0.360
	S1	631.862	472.988	773.759	662.547	897.4	823.9	776.65	0.862	0.939	0.996
	S9	898.147	244.424	971.474	513.868	1443.47	1299.97	1207.72	0.673	0.747	0.804
	S2	107.012	736.409	327.935	768.512	1710.66	1548.96	1445.01	0.449	0.496	0.532
	S10	200.940	545.232	364.509	605.514	2488.57	2172.87	1969.92	0.243	0.279	0.307
	S3	4.298	703.190	215.255	704.479	1841.77	1665.37	1551.97	0.383	0.423	0.454

2	S11	3.300	728.663	221.899	729.653	2695.686	2351.286	2129.886	0.271	0.310	0.343
	S4	135.399	726.436	353.330	767.056	1719.62	1552.488	1445.046	0.446	0.494	0.531
	S12	264.615	595.725	443.333	675.110	2124.451	1856.001	1683.426	0.318	0.364	0.401
	S1	765.012	564.015	934.216	793.518	1025.6	941.6	904.85	0.911	0.992	1.032
	S9	1101.563	324.605	1198.944	655.073	1649.68	1485.68	1413.93	0.727	0.807	0.848
	S2	122.329	895.551	390.994	932.249	1955.04	1770.24	1689.39	0.477	0.527	0.552
	S10	237.952	701.013	448.256	772.399	2844.08	2483.28	2325.43	0.272	0.311	0.332
	S3	5.877	862.021	264.483	863.784	2104.88	1903.28	1815.08	0.410	0.454	0.476
	S11	3.075	932.539	282.837	933.462	3080.784	2687.184	2514.984	0.303	0.347	0.371
	S4	176.919	883.593	441.997	936.669	1965.28	1774.272	1690.706	0.477	0.528	0.554
	S12	316.044	765.283	545.629	860.097	2427.944	2121.144	1986.919	0.354	0.405	0.433
1	S1	878.812	640.424	1070.939	904.068	1153.8	1059.3	1033.05	0.928	1.011	1.037
	S9	1281.624	406.193	1403.482	790.680	1855.89	1671.39	1620.14	0.756	0.840	0.866
	S2	130.834	1030.877	440.097	1070.127	2199.42	1991.52	1933.77	0.487	0.537	0.553
	S10	273.126	845.831	526.875	927.769	3199.59	2793.69	2680.94	0.290	0.332	0.346
	S3	7.607	997.727	306.925	1000.009	2367.99	2141.19	2078.19	0.422	0.467	0.481
	S11	3.329	1104.026	334.536	1105.024	3465.882	3023.082	2900.082	0.319	0.366	0.381
	S4	212.893	1016.784	517.928	1080.652	2210.94	1996.056	1936.366	0.489	0.541	0.558
	S12	368.817	921.371	645.228	1032.016	2731.437	2386.287	2290.412	0.378	0.432	0.451

Çizelge B.13: 12 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	16.025	20.202	22.086	25.010	128.2	117.7	117.700	0.195	0.212	0.212
	S9	21.779	0.147	21.823	6.681	206.21	185.71	185.710	0.106	0.118	0.118
	S2	7.203	29.658	16.100	31.819	244.38	221.28	221.280	0.130	0.144	0.144
	S10	4.288	2.187	4.944	3.473	355.51	310.41	310.410	0.014	0.016	0.016
	S3	1.347	29.838	10.298	30.242	263.11	237.91	237.910	0.115	0.127	0.127
	S11	1.707	1.045	2.020	1.557	385.098	335.898	335.898	0.005	0.006	0.006
	S4	1.914	29.583	10.789	30.157	245.66	221.784	221.784	0.123	0.136	0.136
11	S12	1.505	3.028	2.413	3.479	303.493	265.143	265.143	0.011	0.013	0.013
	S1	61.876	63.900	81.046	82.463	256.4	235.4	235.400	0.322	0.350	0.350
	S9	82.018	14.394	86.337	39.000	412.42	371.42	371.420	0.209	0.232	0.232
	S2	9.198	89.982	36.192	92.742	488.76	442.56	442.560	0.190	0.210	0.210
	S10	2.480	17.117	7.615	17.861	711.02	620.82	620.820	0.025	0.029	0.029
	S3	1.915	90.463	29.054	91.038	526.22	475.82	475.820	0.173	0.191	0.191
	S11	2.432	25.727	10.150	26.457	770.196	671.796	671.796	0.034	0.039	0.039
10	S4	3.030	89.221	29.796	90.130	491.32	443.568	443.568	0.183	0.203	0.203
	S12	15.698	17.879	21.062	22.589	606.986	530.286	530.286	0.037	0.043	0.043
	S1	133.747	125.842	171.500	165.966	384.6	353.1	353.100	0.446	0.486	0.486
	S9	177.003	39.208	188.766	92.309	618.63	557.13	557.130	0.305	0.339	0.339
	S2	2.229	173.620	54.315	174.289	733.14	663.84	663.840	0.238	0.263	0.263
	S10	26.156	51.287	41.542	59.134	1066.53	931.23	931.230	0.055	0.064	0.064
	S3	1.958	174.711	54.371	175.299	789.33	713.73	713.730	0.222	0.246	0.246
9	S11	2.421	74.243	24.694	74.969	1155.294	1007.694	1007.694	0.065	0.074	0.074
	S4	12.858	172.051	64.473	175.908	736.98	665.352	665.352	0.239	0.264	0.264
	S12	40.649	55.589	57.326	67.784	910.479	795.429	795.429	0.074	0.085	0.085
	S1	221.571	196.931	280.650	263.402	512.8	470.8	457.675	0.547	0.596	0.613
	S9	298.865	70.551	320.030	160.211	824.84	742.84	717.215	0.388	0.431	0.446
	S2	9.350	279.732	93.269	282.537	977.52	885.12	856.245	0.289	0.319	0.330
	S10	50.775	113.744	84.898	128.976	1422.04	1241.64	1185.265	0.091	0.104	0.109
8	S3	2.313	276.189	85.170	276.883	1052.44	951.64	920.140	0.263	0.291	0.301
	S11	2.897	159.368	50.708	160.237	1540.392	1343.592	1282.092	0.104	0.119	0.125
	S4	29.901	276.644	112.894	285.614	982.64	887.136	857.291	0.291	0.322	0.333
	S12	75.915	123.716	113.030	146.490	1213.972	1060.572	1012.635	0.121	0.138	0.145
	S1	323.296	274.797	405.735	371.786	641	588.5	564.875	0.633	0.689	0.718
	S9	444.071	106.430	476.000	239.651	1031.05	928.55	882.425	0.462	0.513	0.539
	S2	26.024	405.145	147.567	412.952	1221.9	1106.4	1054.425	0.338	0.373	0.392
7	S10	76.594	198.543	136.157	221.521	1777.55	1552.05	1450.575	0.125	0.143	0.153
	S3	3.007	391.580	120.481	392.482	1315.55	1189.55	1132.850	0.298	0.330	0.346
	S11	3.429	275.823	86.176	276.852	1925.49	1679.49	1568.790	0.144	0.165	0.176
	S4	55.363	400.409	175.486	417.018	1228.3	1108.92	1055.199	0.340	0.376	0.395
	S12	120.119	216.216	184.983	252.251	1517.465	1325.715	1239.428	0.166	0.190	0.204
	S1	432.638	358.797	540.277	488.588	769.2	706.2	672.075	0.702	0.765	0.804
	S9	610.187	147.487	654.433	330.543	1237.26	1114.26	1047.635	0.529	0.587	0.625
6	S2	39.355	544.679	202.758	556.485	1466.28	1327.68	1252.605	0.380	0.419	0.444
	S10	102.431	318.611	198.015	349.340	2133.06	1862.46	1715.885	0.164	0.188	0.204
	S3	3.200	521.677	159.703	522.637	1578.66	1427.46	1345.560	0.331	0.366	0.388
	S11	4.187	424.539	131.549	425.795	2310.588	2015.388	1855.488	0.184	0.211	0.229
	S4	74.126	537.924	235.503	560.162	1473.96	1330.704	1253.107	0.380	0.421	0.447
	S12	174.939	346.760	278.967	399.242	1820.958	1590.858	1466.221	0.219	0.251	0.272
	S1	550.125	444.396	683.444	609.434	897.4	823.9	784.525	0.762	0.830	0.871
6	S9	786.286	193.911	844.460	429.797	1443.47	1299.97	1223.095	0.585	0.650	0.690
	S2	48.328	697.376	257.541	711.874	1710.66	1548.96	1462.335	0.416	0.460	0.487
	S10	119.317	450.591	254.494	486.386	2488.57	2172.87	2003.745	0.195	0.224	0.243
	S3	4.320	671.575	205.793	672.871	1841.77	1665.37	1570.870	0.365	0.404	0.428

5	S11	4.367	605.416	185.991	606.726	2695.686	2351.286	2166.786	0.225	0.258	0.280
	S4	103.211	687.288	309.397	718.252	1719.62	1552.488	1462.953	0.418	0.463	0.491
	S12	218.204	489.398	365.023	554.859	2124.451	1856.001	1712.189	0.261	0.299	0.324
	S1	676.081	536.996	837.180	739.820	1025.6	941.6	902.225	0.816	0.889	0.928
	S9	979.640	269.630	1060.529	563.522	1649.68	1485.68	1408.805	0.643	0.714	0.753
	S2	55.101	859.209	312.864	875.739	1955.04	1770.24	1683.615	0.448	0.495	0.520
	S10	144.382	598.136	323.823	641.450	2844.08	2483.28	2314.155	0.226	0.258	0.277
	S3	5.642	832.892	255.510	834.584	2104.88	1903.28	1808.780	0.396	0.438	0.461
	S11	4.164	795.046	242.678	796.296	3080.784	2687.184	2502.684	0.258	0.296	0.318
	S4	139.916	846.159	393.764	888.134	1965.28	1774.272	1684.737	0.452	0.501	0.527
	S12	264.947	648.243	459.420	727.728	2427.944	2121.144	1977.332	0.300	0.343	0.368
	S1	810.045	633.926	1000.223	876.939	1153.8	1059.3	1025.175	0.867	0.944	0.976
4	S9	1184.000	366.718	1294.015	721.918	1855.89	1671.39	1604.765	0.697	0.774	0.806
	S2	59.164	1027.387	367.380	1045.136	2199.42	1991.52	1916.445	0.475	0.525	0.545
	S10	175.425	764.401	404.745	817.029	3199.59	2793.69	2647.115	0.255	0.292	0.309
	S3	7.556	1003.694	308.664	1005.961	2367.99	2141.19	2059.290	0.425	0.470	0.488
	S11	4.362	989.745	301.286	991.053	3465.882	3023.082	2863.182	0.286	0.328	0.346
	S4	183.639	1010.629	486.827	1065.721	2210.94	1996.056	1918.459	0.482	0.534	0.556
	S12	322.847	825.345	570.451	922.199	2731.437	2386.287	2261.650	0.338	0.386	0.408
	S1	960.783	742.778	1183.616	1031.013	1282	1177	1153.375	0.923	1.006	1.026
3	S9	1398.239	474.865	1540.698	894.336	2062.1	1857.1	1810.975	0.747	0.830	0.851
	S2	76.195	1194.222	434.461	1217.080	2443.8	2212.8	2160.825	0.498	0.550	0.563
	S10	215.280	939.946	497.264	1004.530	3555.1	3104.1	3002.625	0.283	0.324	0.335
	S3	8.446	1178.765	362.075	1181.298	2631.1	2379.1	2322.400	0.449	0.497	0.509
	S11	4.111	1194.774	362.543	1196.007	3850.98	3358.98	3248.280	0.311	0.356	0.368
	S4	231.297	1174.545	583.660	1243.934	2456.6	2217.84	2164.119	0.506	0.561	0.575
	S12	382.206	1013.244	686.179	1127.906	3034.93	2651.43	2565.143	0.372	0.425	0.440
	S1	1118.651	855.098	1375.180	1190.694	1410.2	1294.7	1281.575	0.975	1.062	1.073
2	S9	1611.442	588.451	1787.977	1071.883	2268.31	2042.81	2017.185	0.788	0.875	0.886
	S2	102.613	1354.165	508.862	1384.949	2688.18	2434.08	2405.205	0.515	0.569	0.576
	S10	261.493	1113.037	595.404	1191.485	3910.61	3414.51	3358.135	0.305	0.349	0.355
	S3	8.893	1345.922	412.670	1348.590	2894.21	2617.01	2585.510	0.466	0.515	0.522
	S11	3.678	1392.196	421.337	1393.300	4236.078	3694.878	3633.378	0.329	0.377	0.383
	S4	282.587	1332.709	682.399	1417.485	2702.26	2439.624	2409.779	0.525	0.581	0.588
	S12	442.526	1200.037	802.537	1332.795	3338.423	2916.573	2868.636	0.399	0.457	0.465
	S1	1245.970	939.543	1527.833	1313.334	1538.4	1412.4	1409.775	0.993	1.082	1.084
1	S9	1780.937	674.588	1983.313	1208.869	2474.52	2228.52	2223.395	0.801	0.890	0.892
	S2	121.682	1482.390	566.399	1518.895	2932.56	2655.36	2649.585	0.518	0.572	0.573
	S10	298.907	1249.159	673.655	1338.831	4266.12	3724.92	3713.645	0.314	0.359	0.361
	S3	9.843	1477.913	453.217	1480.866	3157.32	2854.92	2848.620	0.469	0.519	0.520
	S11	3.672	1544.002	466.873	1545.104	4621.176	4030.776	4018.476	0.334	0.383	0.384
	S4	329.313	1457.744	766.636	1556.538	2947.92	2661.408	2655.439	0.528	0.585	0.586
	S12	492.530	1344.277	895.813	1492.036	3641.916	3181.716	3172.129	0.410	0.469	0.470

Çizelge B.14: 6 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	3.374	2.845	4.227	3.857	128.2	122.95	112.45	0.033	0.034	0.038
	S9	4.448	0.829	4.696	2.163	206.21	195.96	175.46	0.023	0.024	0.027
	S2	0.477	3.830	1.626	3.973	244.38	232.83	209.73	0.016	0.017	0.019
	S10	1.304	1.426	1.732	1.818	355.51	332.96	287.86	0.005	0.005	0.006
	S3	0.056	3.843	1.209	3.860	263.11	250.51	225.31	0.015	0.015	0.017
	S11	0.056	1.940	0.638	1.957	385.098	360.498	311.298	0.005	0.005	0.006
	S4	0.397	3.862	1.556	3.981	245.66	233.722	209.846	0.016	0.017	0.019
5	S12	1.091	1.524	1.549	1.852	303.493	284.318	245.968	0.006	0.007	0.008
	S1	12.000	9.458	14.837	13.058	256.4	245.9	230.15	0.058	0.060	0.064
	S9	15.640	4.187	16.896	8.879	412.42	391.92	361.17	0.041	0.043	0.047
	S2	2.390	12.485	6.136	13.202	488.76	465.66	431.01	0.027	0.028	0.031
	S10	5.120	6.628	7.108	8.164	711.02	665.92	598.27	0.011	0.012	0.014
	S3	0.057	12.530	3.816	12.547	526.22	501.02	463.22	0.024	0.025	0.027
	S11	0.039	8.792	2.677	8.803	770.196	720.996	647.196	0.011	0.012	0.014
4	S4	1.995	12.479	5.739	13.078	491.32	467.444	431.63	0.027	0.028	0.030
	S12	4.372	7.264	6.551	8.575	606.986	568.636	511.111	0.014	0.015	0.017
	S1	25.098	19.213	30.862	26.742	384.6	368.85	353.1	0.080	0.084	0.087
	S9	32.817	9.286	35.603	19.131	618.63	587.88	557.13	0.058	0.061	0.064
	S2	5.814	25.171	13.366	26.916	733.14	698.49	663.84	0.037	0.039	0.041
	S10	11.800	14.404	16.122	17.944	1066.53	998.88	931.23	0.017	0.018	0.019
	S3	0.043	25.293	7.631	25.306	789.33	751.53	713.73	0.032	0.034	0.035
3	S11	0.120	19.435	5.951	19.471	1155.294	1081.494	1007.694	0.017	0.018	0.019
	S4	4.424	25.114	11.958	26.441	736.98	701.166	665.352	0.036	0.038	0.040
	S12	9.516	15.905	14.287	18.759	910.479	852.954	795.429	0.021	0.022	0.024
	S1	40.612	30.273	49.694	42.456	512.8	491.8	481.3	0.097	0.101	0.103
	S9	54.122	15.377	58.735	31.614	824.84	783.84	763.34	0.071	0.075	0.077
	S2	9.980	41.162	22.328	44.156	977.52	931.32	908.22	0.045	0.047	0.049
	S10	18.711	26.667	26.711	32.280	1422.04	1331.84	1286.74	0.023	0.024	0.025
2	S3	0.090	40.572	12.261	40.599	1052.44	1002.04	976.84	0.039	0.041	0.042
	S11	0.160	35.846	10.914	35.894	1540.392	1441.992	1392.792	0.023	0.025	0.026
	S4	7.977	40.952	20.262	43.345	982.64	934.888	911.012	0.044	0.046	0.048
	S12	16.293	29.388	25.110	34.276	1213.972	1137.272	1098.922	0.028	0.030	0.031
	S1	57.492	41.741	70.015	58.989	641	614.75	609.5	0.109	0.114	0.115
	S9	78.033	21.849	84.588	45.259	1031.05	979.8	969.55	0.082	0.086	0.087
	S2	14.717	59.181	32.472	63.597	1221.9	1164.15	1152.6	0.052	0.055	0.055
1	S10	25.537	41.986	38.132	49.646	1777.55	1664.8	1642.25	0.028	0.030	0.030
	S3	0.089	57.155	17.235	57.181	1315.55	1252.55	1239.95	0.043	0.046	0.046
	S11	0.157	56.438	17.089	56.486	1925.49	1802.49	1777.89	0.029	0.031	0.032
	S4	12.592	58.873	30.254	62.650	1228.3	1168.61	1156.672	0.051	0.054	0.054
	S12	24.237	46.258	38.114	53.529	1517.465	1421.59	1402.415	0.035	0.038	0.038
	S1	72.578	51.898	88.147	73.671	769.2	737.7	737.7	0.115	0.119	0.119
	S9	100.997	27.338	109.198	57.637	1237.26	1175.76	1175.76	0.088	0.093	0.093
	S2	18.303	76.084	41.128	81.575	1466.28	1396.98	1396.98	0.056	0.058	0.058
	S10	31.267	58.435	48.798	67.815	2133.06	1997.76	1997.76	0.032	0.034	0.034
	S3	0.152	72.801	21.993	72.847	1578.66	1503.06	1503.06	0.046	0.048	0.048
	S11	0.116	77.822	23.463	77.856	2310.588	2162.988	2162.988	0.034	0.036	0.036
	S4	15.671	75.639	38.362	80.340	1473.96	1402.332	1402.332	0.055	0.057	0.057
	S12	32.113	64.279	51.397	73.913	1820.958	1705.908	1705.908	0.041	0.043	0.043

Çizelge B.15: 9 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	2.774	2.820	3.620	3.652	128.2	117.7	104.575	0.028	0.031	0.035
	S9	3.722	0.477	3.865	1.593	206.21	185.71	160.085	0.019	0.021	0.024
	S2	0.348	4.068	1.568	4.172	244.38	221.28	192.405	0.017	0.019	0.022
	S10	0.272	0.488	0.418	0.569	355.51	310.41	254.035	0.002	0.002	0.002
	S3	0.169	4.004	1.371	4.055	263.11	237.91	206.41	0.015	0.017	0.020
	S11	0.177	0.856	0.434	0.909	385.098	335.898	274.398	0.002	0.003	0.003
	S4	0.090	4.060	1.308	4.087	245.66	221.784	191.939	0.017	0.018	0.021
8	S12	0.607	0.478	0.750	0.660	303.493	265.143	217.2055	0.002	0.003	0.003
	S1	10.313	9.213	13.077	12.306	256.4	235.4	211.775	0.051	0.056	0.062
	S9	13.579	3.291	14.567	7.365	412.42	371.42	325.295	0.035	0.039	0.045
	S2	0.388	12.768	4.219	12.885	488.76	442.56	390.585	0.026	0.029	0.033
	S10	2.587	4.406	3.909	5.182	711.02	620.82	519.345	0.007	0.008	0.010
	S3	0.258	12.648	4.052	12.725	526.22	475.82	419.12	0.024	0.027	0.030
	S11	0.252	6.167	2.102	6.243	770.196	671.796	561.096	0.008	0.009	0.011
7	S4	1.275	12.669	5.075	13.051	491.32	443.568	389.847	0.027	0.029	0.033
	S12	3.213	4.778	4.646	5.742	606.986	530.286	443.9985	0.009	0.011	0.013
	S1	22.075	18.570	27.646	25.193	384.6	353.1	318.975	0.072	0.078	0.087
	S9	29.080	7.765	31.410	16.489	618.63	557.13	490.505	0.051	0.056	0.064
	S2	2.563	25.267	10.143	26.036	733.14	663.84	588.765	0.036	0.039	0.044
	S10	7.621	10.745	10.845	13.031	1066.53	931.23	784.655	0.012	0.014	0.017
	S3	0.257	25.134	7.797	25.211	789.33	713.73	631.83	0.032	0.035	0.040
6	S11	0.199	15.036	4.709	15.095	1155.294	1007.694	847.794	0.013	0.015	0.018
	S4	3.250	25.059	10.767	26.034	736.98	665.352	587.755	0.035	0.039	0.044
	S12	7.571	11.812	11.114	14.084	910.479	795.429	670.7915	0.015	0.018	0.021
	S1	36.398	29.378	45.211	40.297	512.8	470.8	418.3	0.088	0.096	0.108
	S9	48.879	13.303	52.869	27.966	824.84	742.84	640.34	0.064	0.071	0.083
	S2	5.499	41.269	17.880	42.919	977.52	885.12	769.62	0.044	0.048	0.056
	S10	12.924	21.582	19.399	25.459	1422.04	1241.64	1016.14	0.018	0.021	0.025
5	S3	0.307	40.324	12.404	40.416	1052.44	951.64	825.64	0.038	0.042	0.049
	S11	0.244	29.714	9.159	29.787	1540.392	1343.592	1097.592	0.019	0.022	0.027
	S4	6.364	40.842	18.617	42.752	982.64	887.136	767.756	0.044	0.048	0.056
	S12	13.590	23.694	20.698	27.771	1213.972	1060.572	868.822	0.023	0.026	0.032
	S1	52.791	41.150	65.136	56.987	641	588.5	525.5	0.102	0.111	0.124
	S9	72.183	19.541	78.046	41.196	1031.05	928.55	805.55	0.076	0.084	0.097
	S2	9.216	60.117	27.251	62.882	1221.9	1106.4	967.8	0.051	0.057	0.065
4	S10	18.432	35.875	29.194	41.405	1777.55	1552.05	1281.45	0.023	0.027	0.032
	S3	0.410	57.543	17.673	57.666	1315.55	1189.55	1038.35	0.044	0.048	0.056
	S11	0.314	49.211	15.078	49.305	1925.49	1679.49	1384.29	0.026	0.029	0.036
	S4	10.754	59.454	28.590	62.680	1228.3	1108.92	965.664	0.051	0.057	0.065
	S12	20.977	39.352	32.783	45.645	1517.465	1325.715	1095.615	0.030	0.034	0.042
	S1	70.156	53.683	86.261	74.730	769.2	706.2	648.45	0.112	0.122	0.133
	S9	98.378	26.513	106.332	56.026	1237.26	1114.26	1001.51	0.086	0.095	0.106
3	S2	12.431	80.840	36.683	84.569	1466.28	1327.68	1200.63	0.058	0.064	0.070
	S10	23.917	55.301	40.508	62.476	2133.06	1862.46	1614.41	0.029	0.034	0.039
	S3	0.430	76.736	23.450	76.865	1578.66	1427.46	1288.86	0.049	0.054	0.060
	S11	0.428	73.385	22.443	73.513	2310.588	2015.388	1744.788	0.032	0.036	0.042
	S4	14.135	79.893	38.103	84.133	1473.96	1330.704	1199.386	0.057	0.063	0.070
	S12	29.870	60.553	48.036	69.514	1820.958	1590.858	1379.933	0.038	0.044	0.050
	S1	88.365	66.146	108.208	92.656	897.4	823.9	776.65	0.121	0.131	0.139
3	S9	125.604	34.182	135.859	71.863	1443.47	1299.97	1207.72	0.094	0.105	0.112
	S2	14.965	102.985	45.861	107.475	1710.66	1548.96	1445.01	0.063	0.069	0.074
	S10	28.101	76.250	50.976	84.680	2488.57	2172.87	1969.92	0.034	0.039	0.043
	S3	0.601	98.340	30.103	98.520	1841.77	1665.37	1551.97	0.053	0.059	0.063

2	S11	0.462	101.902	31.032	102.040	2695.686	2351.286	2129.886	0.038	0.043	0.048
	S4	18.935	101.591	49.412	107.271	1719.62	1552.488	1445.046	0.062	0.069	0.074
	S12	37.006	83.311	61.999	94.413	2124.451	1856.001	1683.426	0.044	0.051	0.056
	S1	106.985	78.876	130.648	110.972	1025.6	941.6	904.85	0.127	0.139	0.144
	S9	154.051	45.395	167.670	91.611	1649.68	1485.68	1413.93	0.102	0.113	0.119
	S2	17.107	125.241	54.680	130.373	1955.04	1770.24	1689.39	0.067	0.074	0.077
	S10	33.277	98.035	62.688	108.018	2844.08	2483.28	2325.43	0.038	0.043	0.046
	S3	0.822	120.552	36.987	120.798	2104.88	1903.28	1815.08	0.057	0.063	0.067
	S11	0.430	130.414	39.554	130.543	3080.784	2687.184	2514.984	0.042	0.049	0.052
	S4	24.742	123.569	61.812	130.991	1965.28	1774.272	1690.706	0.067	0.074	0.077
	S12	44.198	107.023	76.305	120.283	2427.944	2121.144	1986.919	0.050	0.057	0.061
1	S1	122.900	89.562	149.768	126.432	1153.8	1059.3	1033.05	0.130	0.141	0.145
	S9	179.232	56.805	196.274	110.575	1855.89	1671.39	1620.14	0.106	0.117	0.121
	S2	18.297	144.166	61.547	149.655	2199.42	1991.52	1933.77	0.068	0.075	0.077
	S10	38.196	118.288	73.682	129.746	3199.59	2793.69	2680.94	0.041	0.046	0.048
	S3	1.064	139.530	42.923	139.849	2367.99	2141.19	2078.19	0.059	0.065	0.067
	S11	0.466	154.396	46.784	154.535	3465.882	3023.082	2900.082	0.045	0.051	0.053
	S4	29.773	142.195	72.431	151.127	2210.94	1996.056	1936.366	0.068	0.076	0.078
	S12	51.578	128.852	90.234	144.325	2731.437	2386.287	2290.412	0.053	0.060	0.063

Çizelge B.16: 12 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	2.781	3.506	3.832	4.340	128.2	117.7	117.700	0.034	0.037	0.037
	S9	3.779	0.026	3.787	1.159	206.21	185.71	185.710	0.018	0.020	0.020
	S2	1.250	5.146	2.794	5.521	244.38	221.28	221.280	0.023	0.025	0.025
	S10	0.744	0.380	0.858	0.603	355.51	310.41	310.410	0.002	0.003	0.003
	S3	0.234	5.178	1.787	5.248	263.11	237.91	237.910	0.020	0.022	0.022
	S11	0.296	0.181	0.351	0.270	385.098	335.898	335.898	0.001	0.001	0.001
	S4	0.332	5.133	1.872	5.233	245.66	221.784	221.784	0.021	0.024	0.024
11	S12	0.261	0.525	0.419	0.604	303.493	265.143	265.143	0.002	0.002	0.002
	S1	10.737	11.088	14.063	14.309	256.4	235.4	235.400	0.056	0.061	0.061
	S9	14.232	2.498	14.981	6.767	412.42	371.42	371.420	0.036	0.040	0.040
	S2	1.596	15.614	6.280	16.093	488.76	442.56	442.560	0.033	0.036	0.036
	S10	0.430	2.970	1.321	3.099	711.02	620.82	620.820	0.004	0.005	0.005
	S3	0.332	15.698	5.042	15.797	526.22	475.82	475.820	0.030	0.033	0.033
	S11	0.422	4.464	1.761	4.591	770.196	671.796	671.796	0.006	0.007	0.007
10	S4	0.526	15.482	5.170	15.640	491.32	443.568	443.568	0.032	0.035	0.035
	S12	2.724	3.103	3.655	3.920	606.986	530.286	530.286	0.006	0.007	0.007
	S1	23.208	21.837	29.759	28.799	384.6	353.1	353.100	0.077	0.084	0.084
	S9	30.714	6.804	32.755	16.018	618.63	557.13	557.130	0.053	0.059	0.059
	S2	0.387	30.127	9.425	30.243	733.14	663.84	663.840	0.041	0.046	0.046
	S10	4.539	8.900	7.208	10.261	1066.53	931.23	931.230	0.010	0.011	0.011
	S3	0.340	30.317	9.435	30.419	789.33	713.73	713.730	0.039	0.043	0.043
9	S11	0.420	12.883	4.285	13.009	1155.294	1007.694	1007.694	0.011	0.013	0.013
	S4	2.231	29.855	11.188	30.524	736.98	665.352	665.352	0.041	0.046	0.046
	S12	7.054	9.646	9.947	11.762	910.479	795.429	795.429	0.013	0.015	0.015
	S1	38.448	34.172	48.699	45.707	512.8	470.8	457.675	0.095	0.103	0.106
	S9	51.860	12.242	55.533	27.800	824.84	742.84	717.215	0.067	0.075	0.077
	S2	1.622	48.540	16.184	49.027	977.52	885.12	856.245	0.050	0.055	0.057
	S10	8.811	19.737	14.732	22.381	1422.04	1241.64	1185.265	0.016	0.018	0.019
8	S3	0.401	47.925	14.779	48.046	1052.44	951.64	920.140	0.046	0.050	0.052
	S11	0.503	27.654	8.799	27.805	1540.392	1343.592	1282.092	0.018	0.021	0.022
	S4	5.189	48.004	19.590	49.561	982.64	887.136	857.291	0.050	0.056	0.058
	S12	13.173	21.468	19.613	25.420	1213.972	1060.572	1012.635	0.021	0.024	0.025
	S1	56.100	47.684	70.405	64.514	641	588.5	564.875	0.110	0.120	0.125
	S9	77.057	18.468	82.598	41.585	1031.05	928.55	882.425	0.080	0.089	0.094
	S2	4.516	70.303	25.606	71.657	1221.9	1106.4	1054.425	0.059	0.065	0.068
7	S10	13.291	34.452	23.627	38.439	1777.55	1552.05	1450.575	0.022	0.025	0.026
	S3	0.522	67.949	20.906	68.105	1315.55	1189.55	1132.850	0.052	0.057	0.060
	S11	0.595	47.862	14.954	48.040	1925.49	1679.49	1568.790	0.025	0.029	0.031
	S4	9.607	69.481	30.451	72.363	1228.3	1108.92	1055.199	0.059	0.065	0.069
	S12	20.844	37.519	32.099	43.772	1517.465	1325.715	1239.428	0.029	0.033	0.035
	S1	75.073	62.260	93.751	84.782	769.2	706.2	672.075	0.122	0.133	0.139
	S9	105.882	25.593	113.560	57.357	1237.26	1114.26	1047.635	0.092	0.102	0.108
6	S2	6.829	94.515	35.183	96.564	1466.28	1327.68	1252.605	0.066	0.073	0.077
	S10	17.774	55.287	34.360	60.619	2133.06	1862.46	1715.885	0.028	0.033	0.035
	S3	0.555	90.524	27.712	90.690	1578.66	1427.46	1345.560	0.057	0.064	0.067
	S11	0.727	73.668	22.827	73.886	2310.588	2015.388	1855.488	0.032	0.037	0.040
	S4	12.863	93.343	40.865	97.202	1473.96	1330.704	1253.107	0.066	0.073	0.078
	S12	30.356	60.171	48.407	69.278	1820.958	1590.858	1466.221	0.038	0.044	0.047
	S1	95.460	77.114	118.594	105.751	897.4	823.9	784.525	0.132	0.144	0.151
6	S9	136.440	33.648	146.534	74.580	1443.47	1299.97	1223.095	0.102	0.113	0.120
	S2	8.386	121.012	44.690	123.527	1710.66	1548.96	1462.335	0.072	0.080	0.084
	S10	20.704	78.188	44.161	84.400	2488.57	2172.87	2003.745	0.034	0.039	0.042
	S3	0.750	116.534	35.710	116.759	1841.77	1665.37	1570.870	0.063	0.070	0.074

5	S11	0.758	105.054	32.274	105.282	2695.686	2351.286	2166.786	0.039	0.045	0.049
	S4	17.910	119.261	53.688	124.634	1719.62	1552.488	1462.953	0.072	0.080	0.085
	S12	37.864	84.922	63.340	96.281	2124.451	1856.001	1712.189	0.045	0.052	0.056
	S1	117.316	93.182	145.271	128.377	1025.6	941.6	902.225	0.142	0.154	0.161
	S9	169.991	46.787	184.027	97.785	1649.68	1485.68	1408.805	0.112	0.124	0.131
	S2	9.561	149.094	54.289	151.962	1955.04	1770.24	1683.615	0.078	0.086	0.090
	S10	25.054	103.791	56.191	111.307	2844.08	2483.28	2314.155	0.039	0.045	0.048
	S3	0.979	144.527	44.337	144.821	2104.88	1903.28	1808.780	0.069	0.076	0.080
	S11	0.723	137.960	42.111	138.176	3080.784	2687.184	2502.684	0.045	0.051	0.055
	S4	24.279	146.829	68.328	154.113	1965.28	1774.272	1684.737	0.078	0.087	0.091
	S12	45.975	112.486	79.720	126.278	2427.944	2121.144	1977.332	0.052	0.060	0.064
	S1	140.562	110.001	173.563	152.170	1153.8	1059.3	1025.175	0.150	0.164	0.169
4	S9	205.452	63.634	224.543	125.270	1855.89	1671.39	1604.765	0.121	0.134	0.140
	S2	10.266	178.276	63.749	181.356	2199.42	1991.52	1916.445	0.082	0.091	0.095
	S10	30.440	132.642	70.233	141.774	3199.59	2793.69	2647.115	0.044	0.051	0.054
	S3	1.311	174.165	53.561	174.558	2367.99	2141.19	2059.290	0.074	0.082	0.085
	S11	0.757	171.745	52.280	171.972	3465.882	3023.082	2863.182	0.050	0.057	0.060
	S4	31.866	175.369	84.476	184.928	2210.94	1996.056	1918.459	0.084	0.093	0.096
	S12	56.022	143.217	98.987	160.024	2731.437	2386.287	2261.650	0.059	0.067	0.071
	S1	166.719	128.890	205.386	178.906	1282	1177	1153.375	0.160	0.174	0.178
3	S9	242.628	82.400	267.348	155.189	2062.1	1857.1	1810.975	0.130	0.144	0.148
	S2	13.222	207.226	75.389	211.193	2443.8	2212.8	2160.825	0.086	0.095	0.098
	S10	37.356	163.103	86.287	174.310	3555.1	3104.1	3002.625	0.049	0.056	0.058
	S3	1.466	204.544	62.829	204.984	2631.1	2379.1	2322.400	0.078	0.086	0.088
	S11	0.713	207.322	62.910	207.536	3850.98	3358.98	3248.280	0.054	0.062	0.064
	S4	40.136	203.812	101.279	215.852	2456.6	2217.84	2164.119	0.088	0.097	0.100
	S12	66.322	175.822	119.069	195.719	3034.93	2651.43	2565.143	0.064	0.074	0.076
	S1	194.113	148.380	238.627	206.614	1410.2	1294.7	1281.575	0.169	0.184	0.186
2	S9	279.624	102.110	310.257	185.998	2268.31	2042.81	2017.185	0.137	0.152	0.154
	S2	17.806	234.980	88.300	240.322	2688.18	2434.08	2405.205	0.089	0.099	0.100
	S10	45.375	193.139	103.317	206.751	3910.61	3414.51	3358.135	0.053	0.061	0.062
	S3	1.543	233.550	71.608	234.013	2894.21	2617.01	2585.510	0.081	0.089	0.091
	S11	0.638	241.580	73.112	241.771	4236.078	3694.878	3633.378	0.057	0.065	0.067
	S4	49.036	231.257	118.413	245.968	2702.26	2439.624	2409.779	0.091	0.101	0.102
	S12	76.789	208.235	139.259	231.272	3338.423	2916.573	2868.636	0.069	0.079	0.081
	S1	216.206	163.033	265.116	227.895	1538.4	1412.4	1409.775	0.172	0.188	0.188
1	S9	309.035	117.057	344.153	209.768	2474.52	2228.52	2223.395	0.139	0.154	0.155
	S2	21.115	257.230	98.284	263.565	2932.56	2655.36	2649.585	0.090	0.099	0.099
	S10	51.868	216.759	116.895	232.319	4266.12	3724.92	3713.645	0.054	0.062	0.063
	S3	1.708	256.454	78.644	256.966	3157.32	2854.92	2848.620	0.081	0.090	0.090
	S11	0.637	267.922	81.014	268.113	4621.176	4030.776	4018.476	0.058	0.067	0.067
	S4	57.144	252.954	133.030	270.097	2947.92	2661.408	2655.439	0.092	0.101	0.102
	S12	85.466	233.264	155.445	258.904	3641.916	3181.716	3172.129	0.071	0.081	0.082

Çizelge B.17: 6 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	3.374	2.845	4.227	3.857	128.2	122.95	112.45	0.033	0.034	0.038
	S9	4.448	0.829	4.696	2.163	206.21	195.96	175.46	0.023	0.024	0.027
	S2	0.477	3.830	1.626	3.973	244.38	232.83	209.73	0.016	0.017	0.019
	S10	1.304	1.426	1.732	1.818	355.51	332.96	287.86	0.005	0.005	0.006
	S3	0.056	3.843	1.209	3.860	263.11	250.51	225.31	0.015	0.015	0.017
	S11	0.056	1.940	0.638	1.957	385.098	360.498	311.298	0.005	0.005	0.006
	S4	0.397	3.862	1.556	3.981	245.66	233.722	209.846	0.016	0.017	0.019
5	S12	1.091	1.524	1.549	1.852	303.493	284.318	245.968	0.006	0.007	0.008
	S1	12.000	9.458	14.837	13.058	256.4	245.9	230.15	0.058	0.060	0.064
	S9	15.640	4.187	16.896	8.879	412.42	391.92	361.17	0.041	0.043	0.047
	S2	2.390	12.485	6.136	13.202	488.76	465.66	431.01	0.027	0.028	0.031
	S10	5.120	6.628	7.108	8.164	711.02	665.92	598.27	0.011	0.012	0.014
	S3	0.057	12.530	3.816	12.547	526.22	501.02	463.22	0.024	0.025	0.027
	S11	0.039	8.792	2.677	8.803	770.196	720.996	647.196	0.011	0.012	0.014
4	S4	1.995	12.479	5.739	13.078	491.32	467.444	431.63	0.027	0.028	0.030
	S12	4.372	7.264	6.551	8.575	606.986	568.636	511.111	0.014	0.015	0.017
	S1	25.098	19.213	30.862	26.742	384.6	368.85	353.1	0.080	0.084	0.087
	S9	32.817	9.286	35.603	19.131	618.63	587.88	557.13	0.058	0.061	0.064
	S2	5.814	25.171	13.366	26.916	733.14	698.49	663.84	0.037	0.039	0.041
	S10	11.800	14.404	16.122	17.944	1066.53	998.88	931.23	0.017	0.018	0.019
	S3	0.043	25.293	7.631	25.306	789.33	751.53	713.73	0.032	0.034	0.035
3	S11	0.120	19.435	5.951	19.471	1155.294	1081.494	1007.694	0.017	0.018	0.019
	S4	4.424	25.114	11.958	26.441	736.98	701.166	665.352	0.036	0.038	0.040
	S12	9.516	15.905	14.287	18.759	910.479	852.954	795.429	0.021	0.022	0.024
	S1	40.612	30.273	49.694	42.456	512.8	491.8	481.3	0.097	0.101	0.103
	S9	54.122	15.377	58.735	31.614	824.84	783.84	763.34	0.071	0.075	0.077
	S2	9.980	41.162	22.328	44.156	977.52	931.32	908.22	0.045	0.047	0.049
	S10	18.711	26.667	26.711	32.280	1422.04	1331.84	1286.74	0.023	0.024	0.025
2	S3	0.090	40.572	12.261	40.599	1052.44	1002.04	976.84	0.039	0.041	0.042
	S11	0.160	35.846	10.914	35.894	1540.392	1441.992	1392.792	0.023	0.025	0.026
	S4	7.977	40.952	20.262	43.345	982.64	934.888	911.012	0.044	0.046	0.048
	S12	16.293	29.388	25.110	34.276	1213.972	1137.272	1098.922	0.028	0.030	0.031
	S1	57.492	41.741	70.015	58.989	641	614.75	609.5	0.109	0.114	0.115
	S9	78.033	21.849	84.588	45.259	1031.05	979.8	969.55	0.082	0.086	0.087
	S2	14.717	59.181	32.472	63.597	1221.9	1164.15	1152.6	0.052	0.055	0.055
1	S10	25.537	41.986	38.132	49.646	1777.55	1664.8	1642.25	0.028	0.030	0.030
	S3	0.089	57.155	17.235	57.181	1315.55	1252.55	1239.95	0.043	0.046	0.046
	S11	0.157	56.438	17.089	56.486	1925.49	1802.49	1777.89	0.029	0.031	0.032
	S4	12.592	58.873	30.254	62.650	1228.3	1168.61	1156.672	0.051	0.054	0.054
	S12	24.237	46.258	38.114	53.529	1517.465	1421.59	1402.415	0.035	0.038	0.038
	S1	72.578	51.898	88.147	73.671	769.2	737.7	737.7	0.115	0.119	0.119
	S9	100.997	27.338	109.198	57.637	1237.26	1175.76	1175.76	0.088	0.093	0.093
	S2	18.303	76.084	41.128	81.575	1466.28	1396.98	1396.98	0.056	0.058	0.058
	S10	31.267	58.435	48.798	67.815	2133.06	1997.76	1997.76	0.032	0.034	0.034
	S3	0.152	72.801	21.993	72.847	1578.66	1503.06	1503.06	0.046	0.048	0.048
	S11	0.116	77.822	23.463	77.856	2310.588	2162.988	2162.988	0.034	0.036	0.036
	S4	15.671	75.639	38.362	80.340	1473.96	1402.332	1402.332	0.055	0.057	0.057
	S12	32.113	64.279	51.397	73.913	1820.958	1705.908	1705.908	0.041	0.043	0.043

Çizelge B.18: 9 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	3.121	3.172	4.073	4.108	128.2	117.7	104.575	0.032	0.035	0.039
	S9	4.187	0.537	4.348	1.793	206.21	185.71	160.085	0.021	0.023	0.027
	S2	0.391	4.576	1.764	4.694	244.38	221.28	192.405	0.019	0.021	0.024
	S10	0.306	0.549	0.470	0.640	355.51	310.41	254.035	0.002	0.002	0.003
	S3	0.190	4.505	1.542	4.562	263.11	237.91	206.41	0.017	0.019	0.022
	S11	0.199	0.963	0.488	1.023	385.098	335.898	274.398	0.003	0.003	0.004
	S4	0.102	4.568	1.472	4.598	245.66	221.784	191.939	0.019	0.021	0.024
8	S12	0.683	0.537	0.844	0.742	303.493	265.143	217.2055	0.003	0.003	0.004
	S1	11.603	10.364	14.712	13.845	256.4	235.4	211.775	0.057	0.062	0.069
	S9	15.277	3.702	16.388	8.285	412.42	371.42	325.295	0.040	0.044	0.050
	S2	0.437	14.364	4.746	14.495	488.76	442.56	390.585	0.030	0.033	0.037
	S10	2.910	4.957	4.397	5.830	711.02	620.82	519.345	0.008	0.009	0.011
	S3	0.290	14.228	4.558	14.315	526.22	475.82	419.12	0.027	0.030	0.034
	S11	0.283	6.938	2.365	7.023	770.196	671.796	561.096	0.009	0.010	0.013
7	S4	1.434	14.252	5.710	14.683	491.32	443.568	389.847	0.030	0.033	0.038
	S12	3.615	5.375	5.227	6.459	606.986	530.286	443.9985	0.011	0.012	0.015
	S1	24.834	20.891	31.102	28.342	384.6	353.1	318.975	0.081	0.088	0.098
	S9	32.715	8.735	35.336	18.550	618.63	557.13	490.505	0.057	0.063	0.072
	S2	2.883	28.426	11.410	29.290	733.14	663.84	588.765	0.040	0.044	0.050
	S10	8.574	12.088	12.200	14.660	1066.53	931.23	784.655	0.014	0.016	0.019
	S3	0.289	28.276	8.772	28.362	789.33	713.73	631.83	0.036	0.040	0.045
6	S11	0.224	16.915	5.298	16.982	1155.294	1007.694	847.794	0.015	0.017	0.020
	S4	3.656	28.191	12.113	29.288	736.98	665.352	587.755	0.040	0.044	0.050
	S12	8.517	13.289	12.504	15.844	910.479	795.429	670.7915	0.017	0.020	0.024
	S1	40.948	33.050	50.863	45.335	512.8	470.8	418.3	0.099	0.108	0.122
	S9	54.988	14.966	59.478	31.462	824.84	742.84	640.34	0.072	0.080	0.093
	S2	6.187	46.428	20.115	48.284	977.52	885.12	769.62	0.049	0.055	0.063
	S10	14.540	24.280	21.824	28.641	1422.04	1241.64	1016.14	0.020	0.023	0.028
5	S3	0.346	45.365	13.955	45.468	1052.44	951.64	825.64	0.043	0.048	0.055
	S11	0.275	33.428	10.303	33.510	1540.392	1343.592	1097.592	0.022	0.025	0.031
	S4	7.160	45.948	20.944	48.095	982.64	887.136	767.756	0.049	0.054	0.063
	S12	15.289	26.656	23.286	31.242	1213.972	1060.572	868.822	0.026	0.029	0.036
	S1	59.390	46.294	73.278	64.111	641	588.5	525.5	0.114	0.125	0.139
	S9	81.206	21.984	87.801	46.346	1031.05	928.55	805.55	0.085	0.095	0.109
	S2	10.368	67.632	30.657	70.742	1221.9	1106.4	967.8	0.058	0.064	0.073
4	S10	20.736	40.360	32.844	46.580	1777.55	1552.05	1281.45	0.026	0.030	0.036
	S3	0.461	64.736	19.882	64.874	1315.55	1189.55	1038.35	0.049	0.055	0.062
	S11	0.354	55.362	16.962	55.468	1925.49	1679.49	1384.29	0.029	0.033	0.040
	S4	12.098	66.886	32.163	70.515	1228.3	1108.92	965.664	0.057	0.064	0.073
	S12	23.599	44.271	36.881	51.351	1517.465	1325.715	1095.615	0.034	0.039	0.047
	S1	78.925	60.393	97.043	84.071	769.2	706.2	648.45	0.126	0.137	0.150
	S9	110.675	29.827	119.623	63.029	1237.26	1114.26	1001.51	0.097	0.107	0.119
3	S2	13.985	90.944	41.268	95.140	1466.28	1327.68	1200.63	0.065	0.072	0.079
	S10	26.907	62.213	45.571	70.286	2133.06	1862.46	1614.41	0.033	0.038	0.044
	S3	0.483	86.328	26.382	86.473	1578.66	1427.46	1288.86	0.055	0.061	0.067
	S11	0.481	82.558	25.248	82.702	2310.588	2015.388	1744.788	0.036	0.041	0.047
	S4	15.902	89.879	42.866	94.650	1473.96	1330.704	1199.386	0.064	0.071	0.079
	S12	33.604	68.122	54.040	78.203	1820.958	1590.858	1379.933	0.043	0.049	0.057
	S1	99.410	74.415	121.734	104.238	897.4	823.9	776.65	0.136	0.148	0.157
3	S9	141.304	38.455	152.841	80.846	1443.47	1299.97	1207.72	0.106	0.118	0.127
	S2	16.836	115.858	51.594	120.909	1710.66	1548.96	1445.01	0.071	0.078	0.084
	S10	31.614	85.781	57.348	95.265	2488.57	2172.87	1969.92	0.038	0.044	0.048
3	S3	0.676	110.632	33.866	110.835	1841.77	1665.37	1551.97	0.060	0.067	0.071

2	S11	0.519	114.640	34.911	114.795	2695.686	2351.286	2129.886	0.043	0.049	0.054
	S4	21.302	114.289	55.589	120.680	1719.62	1552.488	1445.046	0.070	0.078	0.084
	S12	41.632	93.725	69.749	106.214	2124.451	1856.001	1683.426	0.050	0.057	0.063
	S1	120.358	88.736	146.979	124.843	1025.6	941.6	904.85	0.143	0.156	0.162
	S9	173.308	51.070	188.628	103.062	1649.68	1485.68	1413.93	0.114	0.127	0.133
	S2	19.246	140.896	61.515	146.670	1955.04	1770.24	1689.39	0.075	0.083	0.087
	S10	37.437	110.290	70.524	121.521	2844.08	2483.28	2325.43	0.043	0.049	0.052
	S3	0.925	135.621	41.611	135.898	2104.88	1903.28	1815.08	0.065	0.071	0.075
	S11	0.484	146.715	44.498	146.860	3080.784	2687.184	2514.984	0.048	0.055	0.058
	S4	27.834	139.015	69.539	147.365	1965.28	1774.272	1690.706	0.075	0.083	0.087
	S12	49.723	120.401	85.843	135.318	2427.944	2121.144	1986.919	0.056	0.064	0.068
1	S1	138.262	100.757	168.490	142.236	1153.8	1059.3	1033.05	0.146	0.159	0.163
	S9	201.636	63.906	220.808	124.397	1855.89	1671.39	1620.14	0.119	0.132	0.136
	S2	20.584	162.187	69.240	168.362	2199.42	1991.52	1933.77	0.077	0.085	0.087
	S10	42.971	133.074	82.893	145.965	3199.59	2793.69	2680.94	0.046	0.052	0.054
	S3	1.197	156.971	48.288	157.330	2367.99	2141.19	2078.19	0.066	0.073	0.076
	S11	0.524	173.695	52.632	173.852	3465.882	3023.082	2900.082	0.050	0.058	0.060
	S4	33.494	159.969	81.485	170.018	2210.94	1996.056	1936.366	0.077	0.085	0.088
	S12	58.026	144.958	101.513	162.366	2731.437	2386.287	2290.412	0.059	0.068	0.071

Çizelge B.19: 12 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	3.128	3.944	4.311	4.882	128.2	117.7	117.700	0.038	0.041	0.041
	S2	4.252	0.029	4.260	1.304	206.21	185.71	185.710	0.021	0.023	0.023
	S5	1.406	5.790	3.143	6.212	244.38	221.28	221.280	0.025	0.028	0.028
	S6	0.837	0.427	0.965	0.678	355.51	310.41	310.410	0.003	0.003	0.003
	S9	0.263	5.825	2.010	5.904	263.11	237.91	237.910	0.022	0.025	0.025
	S10	0.333	0.204	0.394	0.304	385.098	335.898	335.898	0.001	0.001	0.001
	S13	0.374	5.775	2.106	5.887	245.66	221.784	221.784	0.024	0.027	0.027
11	S14	0.294	0.591	0.471	0.679	303.493	265.143	265.143	0.002	0.003	0.003
	S1	12.079	12.474	15.821	16.098	256.4	235.4	235.400	0.063	0.068	0.068
	S2	16.011	2.810	16.854	7.613	412.42	371.42	371.420	0.041	0.045	0.045
	S5	1.796	17.566	7.065	18.104	488.76	442.56	442.560	0.037	0.041	0.041
	S6	0.484	3.342	1.487	3.487	711.02	620.82	620.820	0.005	0.006	0.006
	S9	0.374	17.660	5.672	17.772	526.22	475.82	475.820	0.034	0.037	0.037
	S10	0.475	5.022	1.981	5.165	770.196	671.796	671.796	0.007	0.008	0.008
10	S13	0.592	17.417	5.817	17.595	491.32	443.568	443.568	0.036	0.040	0.040
	S14	3.065	3.490	4.112	4.410	606.986	530.286	530.286	0.007	0.008	0.008
	S1	26.109	24.566	33.479	32.399	384.6	353.1	353.100	0.087	0.095	0.095
	S2	34.554	7.654	36.850	18.020	618.63	557.13	557.130	0.060	0.066	0.066
	S5	0.435	33.893	10.603	34.024	733.14	663.84	663.840	0.046	0.051	0.051
	S6	5.106	10.012	8.110	11.544	1066.53	931.23	931.230	0.011	0.012	0.012
	S9	0.382	34.106	10.614	34.221	789.33	713.73	713.730	0.043	0.048	0.048
9	S10	0.473	14.493	4.821	14.635	1155.294	1007.694	1007.694	0.013	0.015	0.015
	S13	2.510	33.587	12.586	34.340	736.98	665.352	665.352	0.047	0.052	0.052
	S14	7.935	10.852	11.191	13.232	910.479	795.429	795.429	0.015	0.017	0.017
	S1	43.254	38.444	54.787	51.420	512.8	470.8	457.675	0.107	0.116	0.120
	S2	58.343	13.773	62.475	31.275	824.84	742.84	717.215	0.076	0.084	0.087
	S5	1.825	54.608	18.208	55.155	977.52	885.12	856.245	0.056	0.062	0.064
	S6	9.912	22.205	16.573	25.178	1422.04	1241.64	1185.265	0.018	0.020	0.021
8	S9	0.452	53.916	16.626	54.052	1052.44	951.64	920.140	0.051	0.057	0.059
	S10	0.566	31.111	9.899	31.281	1540.392	1343.592	1282.092	0.020	0.023	0.024
	S13	5.837	54.005	22.039	55.756	982.64	887.136	857.291	0.057	0.063	0.065
	S14	14.820	24.151	22.065	28.597	1213.972	1060.572	1012.635	0.024	0.027	0.028
	S1	63.112	53.644	79.205	72.578	641	588.5	564.875	0.124	0.135	0.140
	S2	86.689	20.777	92.922	46.783	1031.05	928.55	882.425	0.090	0.100	0.105
	S5	5.080	79.090	28.807	80.614	1221.9	1106.4	1054.425	0.066	0.073	0.076
7	S6	14.952	38.758	26.580	43.244	1777.55	1552.05	1450.575	0.024	0.028	0.030
	S9	0.587	76.442	23.520	76.618	1315.55	1189.55	1132.850	0.058	0.064	0.068
	S10	0.669	53.845	16.823	54.046	1925.49	1679.49	1568.790	0.028	0.032	0.034
	S13	10.808	78.166	34.257	81.408	1228.3	1108.92	1055.199	0.066	0.073	0.077
	S14	23.449	42.208	36.111	49.243	1517.465	1325.715	1239.428	0.032	0.037	0.040
	S1	84.457	70.042	105.470	95.379	769.2	706.2	672.075	0.137	0.149	0.157
	S2	119.117	28.792	127.755	64.527	1237.26	1114.26	1047.635	0.103	0.115	0.122
6	S5	7.683	106.329	39.581	108.634	1466.28	1327.68	1252.605	0.074	0.082	0.087
	S6	19.996	62.198	38.655	68.196	2133.06	1862.46	1715.885	0.032	0.037	0.040
	S9	0.625	101.839	31.176	102.026	1578.66	1427.46	1345.560	0.065	0.071	0.076
	S10	0.817	82.876	25.680	83.121	2310.588	2015.388	1855.488	0.036	0.041	0.045
	S13	14.471	105.011	45.974	109.352	1473.96	1330.704	1253.107	0.074	0.082	0.087
	S14	34.151	67.693	54.458	77.938	1820.958	1590.858	1466.221	0.043	0.049	0.053
	S1	107.392	86.753	133.418	118.970	897.4	823.9	784.525	0.149	0.162	0.170
6	S2	153.495	37.854	164.851	83.903	1443.47	1299.97	1223.095	0.114	0.127	0.135
	S5	9.434	136.138	50.276	138.968	1710.66	1548.96	1462.335	0.081	0.090	0.095
	S6	23.292	87.962	49.681	94.950	2488.57	2172.87	2003.745	0.038	0.044	0.047
	S9	0.843	131.101	40.174	131.354	1841.77	1665.37	1570.870	0.071	0.079	0.084

	S10	0.852	118.186	36.308	118.442	2695.686	2351.286	2166.786	0.044	0.050	0.055
	S13	20.148	134.169	60.399	140.213	1719.62	1552.488	1462.953	0.082	0.090	0.096
	S14	42.597	95.538	71.258	108.316	2124.451	1856.001	1712.189	0.051	0.058	0.063
5	S1	131.981	104.829	163.430	144.424	1025.6	941.6	902.225	0.159	0.174	0.181
	S2	191.240	52.636	207.031	110.008	1649.68	1485.68	1408.805	0.125	0.139	0.147
	S5	10.757	167.730	61.076	170.957	1955.04	1770.24	1683.615	0.087	0.097	0.102
	S6	28.185	116.765	63.215	125.220	2844.08	2483.28	2314.155	0.044	0.050	0.054
	S9	1.102	162.593	49.879	162.923	2104.88	1903.28	1808.780	0.077	0.086	0.090
	S10	0.813	155.205	47.374	155.448	3080.784	2687.184	2502.684	0.050	0.058	0.062
	S13	27.314	165.183	76.868	173.377	1965.28	1774.272	1684.737	0.088	0.098	0.103
	S14	51.722	126.547	89.686	142.063	2427.944	2121.144	1977.332	0.059	0.067	0.072
4	S1	158.133	123.752	195.258	171.191	1153.8	1059.3	1025.175	0.169	0.184	0.190
	S2	231.134	71.589	252.611	140.929	1855.89	1671.39	1604.765	0.136	0.151	0.157
	S5	11.550	200.561	71.718	204.026	2199.42	1991.52	1916.445	0.093	0.102	0.106
	S6	34.245	149.222	79.012	159.496	3199.59	2793.69	2647.115	0.050	0.057	0.060
	S9	1.475	195.936	60.256	196.378	2367.99	2141.19	2059.290	0.083	0.092	0.095
	S10	0.852	193.213	58.815	193.468	3465.882	3023.082	2863.182	0.056	0.064	0.068
	S13	35.849	197.290	95.036	208.044	2210.94	1996.056	1918.459	0.094	0.104	0.108
	S14	63.025	161.119	111.360	180.027	2731.437	2386.287	2261.650	0.066	0.075	0.080
3	S1	187.559	145.001	231.059	201.269	1282	1177	1153.375	0.180	0.196	0.200
	S2	272.957	92.701	300.767	174.587	2062.1	1857.1	1810.975	0.146	0.162	0.166
	S5	14.874	233.130	84.813	237.592	2443.8	2212.8	2160.825	0.097	0.107	0.110
	S6	42.026	183.491	97.073	196.099	3555.1	3104.1	3002.625	0.055	0.063	0.065
	S9	1.649	230.112	70.682	230.607	2631.1	2379.1	2322.400	0.088	0.097	0.099
	S10	0.803	233.237	70.774	233.478	3850.98	3358.98	3248.280	0.061	0.070	0.072
	S13	45.153	229.288	113.939	242.834	2456.6	2217.84	2164.119	0.099	0.109	0.112
	S14	74.612	197.800	133.952	220.184	3034.93	2651.43	2565.143	0.073	0.083	0.086
2	S1	218.377	166.928	268.455	232.441	1410.2	1294.7	1281.575	0.190	0.207	0.209
	S2	314.577	114.874	349.039	209.247	2268.31	2042.81	2017.185	0.154	0.171	0.173
	S5	20.032	264.353	99.337	270.362	2688.18	2434.08	2405.205	0.101	0.111	0.112
	S6	51.047	217.281	116.232	232.595	3910.61	3414.51	3358.135	0.059	0.068	0.069
	S9	1.736	262.744	80.559	263.264	2894.21	2617.01	2585.510	0.091	0.101	0.102
	S10	0.718	271.777	82.251	271.992	4236.078	3694.878	3633.378	0.064	0.074	0.075
	S13	55.165	260.164	133.214	276.714	2702.26	2439.624	2409.779	0.102	0.113	0.115
	S14	86.388	234.265	156.667	260.181	3338.423	2916.573	2868.636	0.078	0.089	0.091
1	S1	243.232	183.412	298.255	256.382	1538.4	1412.4	1409.775	0.194	0.211	0.212
	S2	347.665	131.689	387.172	235.989	2474.52	2228.52	2223.395	0.156	0.174	0.174
	S5	23.754	289.384	110.569	296.510	2932.56	2655.36	2649.585	0.101	0.112	0.112
	S6	58.351	243.854	131.507	261.359	4266.12	3724.92	3713.645	0.061	0.070	0.070
	S9	1.922	288.510	88.475	289.087	3157.32	2854.92	2848.620	0.092	0.101	0.101
	S10	0.717	301.412	91.140	301.627	4621.176	4030.776	4018.476	0.065	0.075	0.075
	S13	64.287	284.573	149.659	303.859	2947.92	2661.408	2655.439	0.103	0.114	0.114
	S14	96.149	262.422	174.876	291.267	3641.916	3181.716	3172.129	0.080	0.092	0.092

Çizelge B.20: 6 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	6.326	5.334	7.927	7.232	128.2	122.95	112.45	0.062	0.064	0.070
	S9	8.339	1.554	8.805	4.056	206.21	195.96	175.46	0.043	0.045	0.050
	S2	0.895	7.181	3.049	7.449	244.38	232.83	209.73	0.030	0.032	0.036
	S10	2.445	2.675	3.248	3.408	355.51	332.96	287.86	0.010	0.010	0.012
	S3	0.106	7.205	2.267	7.237	263.11	250.51	225.31	0.028	0.029	0.032
	S11	0.104	3.638	1.196	3.669	385.098	360.498	311.298	0.010	0.010	0.012
	S4	0.744	7.242	2.917	7.465	245.66	233.722	209.846	0.030	0.032	0.036
5	S12	2.046	2.858	2.903	3.472	303.493	284.318	245.968	0.011	0.012	0.014
	S1	22.500	17.734	27.820	24.484	256.4	245.9	230.15	0.109	0.113	0.121
	S9	29.325	7.850	31.680	16.647	412.42	391.92	361.17	0.077	0.081	0.088
	S2	4.481	23.410	11.504	24.754	488.76	465.66	431.01	0.051	0.053	0.057
	S10	9.600	12.427	13.328	15.307	711.02	665.92	598.27	0.022	0.023	0.026
	S3	0.107	23.494	7.155	23.526	526.22	501.02	463.22	0.045	0.047	0.051
	S11	0.074	16.484	5.019	16.506	770.196	720.996	647.196	0.021	0.023	0.026
4	S4	3.740	23.399	10.760	24.521	491.32	467.444	431.63	0.050	0.052	0.057
	S12	8.197	13.620	12.282	16.079	606.986	568.636	511.111	0.026	0.028	0.031
	S1	47.059	36.024	57.866	50.141	384.6	368.85	353.1	0.150	0.157	0.164
	S9	61.532	17.411	66.755	35.871	618.63	587.88	557.13	0.108	0.114	0.120
	S2	10.902	47.196	25.061	50.467	733.14	698.49	663.84	0.069	0.072	0.076
	S10	22.126	27.008	30.228	33.645	1066.53	998.88	931.23	0.032	0.034	0.036
	S3	0.080	47.425	14.308	47.449	789.33	751.53	713.73	0.060	0.063	0.066
3	S11	0.225	36.441	11.158	36.508	1155.294	1081.494	1007.694	0.032	0.034	0.036
	S4	8.295	47.089	22.422	49.577	736.98	701.166	665.352	0.067	0.071	0.075
	S12	17.842	29.822	26.788	35.174	910.479	852.954	795.429	0.039	0.041	0.044
	S1	76.148	56.761	93.176	79.605	512.8	491.8	481.3	0.182	0.189	0.194
	S9	101.479	28.832	110.128	59.275	824.84	783.84	763.34	0.134	0.140	0.144
	S2	18.712	77.178	41.866	82.792	977.52	931.32	908.22	0.085	0.089	0.091
	S10	35.083	50.000	50.083	60.525	1422.04	1331.84	1286.74	0.043	0.045	0.047
2	S3	0.168	76.073	22.990	76.123	1052.44	1002.04	976.84	0.072	0.076	0.078
	S11	0.301	67.211	20.464	67.301	1540.392	1441.992	1392.792	0.044	0.047	0.048
	S4	14.956	76.786	37.992	81.272	982.64	934.888	911.012	0.083	0.087	0.089
	S12	30.550	55.102	47.080	64.267	1213.972	1137.272	1098.922	0.053	0.057	0.058
	S1	107.798	78.265	131.277	110.604	641	614.75	609.5	0.205	0.214	0.215
	S9	146.312	40.966	158.602	84.860	1031.05	979.8	969.55	0.154	0.162	0.164
	S2	27.595	110.965	60.884	119.243	1221.9	1164.15	1152.6	0.098	0.102	0.103
1	S10	47.881	78.723	71.498	93.087	1777.55	1664.8	1642.25	0.052	0.056	0.057
	S3	0.166	107.165	32.315	107.215	1315.55	1252.55	1239.95	0.081	0.086	0.086
	S11	0.295	105.822	32.041	105.910	1925.49	1802.49	1777.89	0.055	0.059	0.060
	S4	23.611	110.386	56.727	117.469	1228.3	1168.61	1156.672	0.096	0.101	0.102
	S12	45.444	86.734	71.464	100.367	1517.465	1421.59	1402.415	0.066	0.071	0.072
	S1	136.084	97.308	165.276	138.133	769.2	737.7	737.7	0.215	0.224	0.224
	S9	189.369	51.259	204.746	108.069	1237.26	1175.76	1175.76	0.165	0.174	0.174
	S2	34.318	142.658	77.115	152.953	1466.28	1396.98	1396.98	0.104	0.109	0.109
	S10	58.626	109.566	91.496	127.153	2133.06	1997.76	1997.76	0.060	0.064	0.064
	S3	0.286	136.502	41.236	136.587	1578.66	1503.06	1503.06	0.087	0.091	0.091
	S11	0.218	145.915	43.992	145.981	2310.588	2162.988	2162.988	0.063	0.067	0.067
	S4	29.383	141.822	71.929	150.637	1473.96	1402.332	1402.332	0.102	0.107	0.107
	S12	60.212	120.524	96.370	138.588	1820.958	1705.908	1705.908	0.076	0.081	0.081

Çizelge B.21: 9 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	4.692	4.769	6.123	6.177	128.2	117.7	104.575	0.048	0.052	0.059
	S9	6.295	0.807	6.537	2.695	206.21	185.71	160.085	0.032	0.035	0.041
	S2	0.588	6.881	2.652	7.057	244.38	221.28	192.405	0.029	0.032	0.037
	S10	0.459	0.825	0.707	0.963	355.51	310.41	254.035	0.003	0.003	0.004
	S3	0.286	6.773	2.318	6.859	263.11	237.91	206.41	0.026	0.029	0.033
	S11	0.299	1.448	0.734	1.538	385.098	335.898	274.398	0.004	0.005	0.006
	S4	0.153	6.867	2.213	6.913	245.66	221.784	191.939	0.028	0.031	0.036
8	S12	1.027	0.808	1.269	1.116	303.493	265.143	217.2055	0.004	0.005	0.006
	S1	17.444	15.582	22.119	20.815	256.4	235.4	211.775	0.086	0.094	0.104
	S9	22.968	5.566	24.638	12.457	412.42	371.42	325.295	0.060	0.066	0.076
	S2	0.657	21.596	7.136	21.793	488.76	442.56	390.585	0.045	0.049	0.056
	S10	4.376	7.452	6.611	8.765	711.02	620.82	519.345	0.012	0.014	0.017
	S3	0.436	21.392	6.853	21.523	526.22	475.82	419.12	0.041	0.045	0.051
	S11	0.426	10.432	3.555	10.559	770.196	671.796	561.096	0.014	0.016	0.019
7	S4	2.156	21.428	8.585	22.075	491.32	443.568	389.847	0.045	0.050	0.057
	S12	5.434	8.081	7.859	9.712	606.986	530.286	443.9985	0.016	0.018	0.022
	S1	37.337	31.409	46.760	42.611	384.6	353.1	318.975	0.122	0.132	0.147
	S9	49.187	13.133	53.126	27.889	618.63	557.13	490.505	0.086	0.095	0.108
	S2	4.334	42.737	17.155	44.037	733.14	663.84	588.765	0.060	0.066	0.075
	S10	12.891	18.174	18.343	22.041	1066.53	931.23	784.655	0.021	0.024	0.028
	S3	0.435	42.511	13.189	42.642	789.33	713.73	631.83	0.054	0.060	0.067
6	S11	0.336	25.431	7.965	25.532	1155.294	1007.694	847.794	0.022	0.025	0.030
	S4	5.496	42.384	18.211	44.033	736.98	665.352	587.755	0.060	0.066	0.075
	S12	12.805	19.979	18.799	23.821	910.479	795.429	670.7915	0.026	0.030	0.036
	S1	61.563	49.690	76.470	68.159	512.8	470.8	418.3	0.149	0.162	0.183
	S9	82.673	22.500	89.423	47.302	824.84	742.84	640.34	0.108	0.120	0.140
	S2	9.301	69.802	30.242	72.593	977.52	885.12	769.62	0.074	0.082	0.094
	S10	21.860	36.503	32.811	43.061	1422.04	1241.64	1016.14	0.030	0.035	0.042
5	S3	0.520	68.204	20.981	68.360	1052.44	951.64	825.64	0.065	0.072	0.083
	S11	0.413	50.258	15.491	50.382	1540.392	1343.592	1097.592	0.033	0.037	0.046
	S4	10.764	69.081	31.488	72.310	982.64	887.136	767.756	0.074	0.082	0.094
	S12	22.987	40.076	35.009	46.972	1213.972	1060.572	868.822	0.039	0.044	0.054
	S1	89.291	69.601	110.171	96.388	641	588.5	525.5	0.172	0.187	0.210
	S9	122.091	33.052	132.006	69.679	1031.05	928.55	805.55	0.128	0.142	0.164
	S2	15.587	101.682	46.092	106.358	1221.9	1106.4	967.8	0.087	0.096	0.110
4	S10	31.176	60.679	49.379	70.032	1777.55	1552.05	1281.45	0.039	0.045	0.055
	S3	0.693	97.329	29.892	97.537	1315.55	1189.55	1038.35	0.074	0.082	0.094
	S11	0.532	83.235	25.502	83.395	1925.49	1679.49	1384.29	0.043	0.050	0.060
	S4	18.189	100.560	48.357	106.017	1228.3	1108.92	965.664	0.086	0.096	0.110
	S12	35.481	66.560	55.449	77.204	1517.465	1325.715	1095.615	0.051	0.058	0.070
	S1	118.662	90.799	145.902	126.398	769.2	706.2	648.45	0.190	0.207	0.225
	S9	166.397	44.843	179.850	94.762	1237.26	1114.26	1001.51	0.145	0.161	0.180
3	S2	21.026	136.732	62.045	143.040	1466.28	1327.68	1200.63	0.098	0.108	0.119
	S10	40.454	93.536	68.515	105.672	2133.06	1862.46	1614.41	0.050	0.057	0.065
	S3	0.726	129.792	39.664	130.010	1578.66	1427.46	1288.86	0.082	0.091	0.101
	S11	0.723	124.123	37.960	124.340	2310.588	2015.388	1744.788	0.054	0.062	0.071
	S4	23.909	135.130	64.448	142.303	1473.96	1330.704	1199.386	0.097	0.107	0.119
	S12	50.522	102.419	81.247	117.575	1820.958	1590.858	1379.933	0.065	0.074	0.085
	S1	149.460	111.880	183.024	156.718	897.4	823.9	776.65	0.204	0.222	0.236
3	S9	212.446	57.816	229.791	121.550	1443.47	1299.97	1207.72	0.159	0.177	0.190
	S2	25.313	174.189	77.569	181.783	1710.66	1548.96	1445.01	0.106	0.117	0.126
	S10	47.530	128.968	86.220	143.227	2488.57	2172.87	1969.92	0.058	0.066	0.073
	S3	1.017	166.331	50.916	166.636	1841.77	1665.37	1551.97	0.090	0.100	0.107

2	S11	0.781	172.357	52.488	172.591	2695.686	2351.286	2129.886	0.064	0.073	0.081
	S4	32.027	171.830	83.576	181.438	1719.62	1552.488	1445.046	0.106	0.117	0.126
	S12	62.592	140.912	104.865	159.689	2124.451	1856.001	1683.426	0.075	0.086	0.095
	S1	180.955	133.411	220.978	187.698	1025.6	941.6	904.85	0.215	0.235	0.244
	S9	260.562	76.782	283.596	154.950	1649.68	1485.68	1413.93	0.172	0.191	0.201
	S2	28.936	211.832	92.485	220.513	1955.04	1770.24	1689.39	0.113	0.125	0.131
	S10	56.285	165.817	106.030	182.702	2844.08	2483.28	2325.43	0.064	0.074	0.079
	S3	1.390	203.901	62.560	204.318	2104.88	1903.28	1815.08	0.097	0.107	0.113
	S11	0.727	220.581	66.902	220.800	3080.784	2687.184	2514.984	0.072	0.082	0.088
	S4	41.848	209.004	104.549	221.558	1965.28	1774.272	1690.706	0.113	0.125	0.131
	S12	74.757	181.019	129.062	203.446	2427.944	2121.144	1986.919	0.084	0.096	0.102
1	S1	207.873	151.485	253.318	213.847	1153.8	1059.3	1033.05	0.220	0.239	0.245
	S9	303.153	96.080	331.977	187.026	1855.89	1671.39	1620.14	0.179	0.199	0.205
	S2	30.947	243.842	104.100	253.126	2199.42	1991.52	1933.77	0.115	0.127	0.131
	S10	64.605	200.072	124.626	219.453	3199.59	2793.69	2680.94	0.069	0.079	0.082
	S3	1.799	236.001	72.600	236.541	2367.99	2141.19	2078.19	0.100	0.110	0.114
	S11	0.787	261.145	79.131	261.381	3465.882	3023.082	2900.082	0.075	0.086	0.090
	S4	50.357	240.509	122.510	255.616	2210.94	1996.056	1936.366	0.116	0.128	0.132
	S12	87.240	217.940	152.621	244.111	2731.437	2386.287	2290.412	0.089	0.102	0.107

Çizelge B.22: 12 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	4.519	5.697	6.228	7.052	128.2	117.7	117.700	0.055	0.060	0.060
	S9	6.141	0.042	6.154	1.884	206.21	185.71	185.710	0.030	0.033	0.033
	S2	2.031	8.363	4.540	8.972	244.38	221.28	221.280	0.037	0.041	0.041
	S10	1.209	0.617	1.394	0.979	355.51	310.41	310.410	0.004	0.004	0.004
	S3	0.380	8.414	2.904	8.528	263.11	237.91	237.910	0.032	0.036	0.036
	S11	0.481	0.295	0.570	0.439	385.098	335.898	335.898	0.001	0.002	0.002
	S4	0.540	8.342	3.042	8.504	245.66	221.784	221.784	0.035	0.038	0.038
11	S12	0.424	0.854	0.680	0.981	303.493	265.143	265.143	0.003	0.004	0.004
	S1	17.448	18.018	22.853	23.253	256.4	235.4	235.400	0.091	0.099	0.099
	S9	23.127	4.059	24.345	10.997	412.42	371.42	371.420	0.059	0.066	0.066
	S2	2.594	25.373	10.205	26.151	488.76	442.56	442.560	0.054	0.059	0.059
	S10	0.699	4.827	2.147	5.036	711.02	620.82	620.820	0.007	0.008	0.008
	S3	0.540	25.509	8.192	25.670	526.22	475.82	475.820	0.049	0.054	0.054
	S11	0.686	7.254	2.862	7.460	770.196	671.796	671.796	0.010	0.011	0.011
10	S4	0.854	25.158	8.402	25.415	491.32	443.568	443.568	0.052	0.057	0.057
	S12	4.427	5.042	5.939	6.370	606.986	530.286	530.286	0.010	0.012	0.012
	S1	37.714	35.485	48.359	46.799	384.6	353.1	353.100	0.126	0.137	0.137
	S9	49.911	11.056	53.228	26.029	618.63	557.13	557.130	0.086	0.096	0.096
	S2	0.629	48.957	15.316	49.145	733.14	663.84	663.840	0.067	0.074	0.074
	S10	7.375	14.462	11.714	16.674	1066.53	931.23	931.230	0.016	0.018	0.018
	S3	0.552	49.265	15.331	49.430	789.33	713.73	713.730	0.063	0.069	0.069
9	S11	0.683	20.935	6.963	21.140	1155.294	1007.694	1007.694	0.018	0.021	0.021
	S4	3.626	48.514	18.180	49.602	736.98	665.352	665.352	0.067	0.075	0.075
	S12	11.462	15.675	16.165	19.114	910.479	795.429	795.429	0.021	0.024	0.024
	S1	62.478	55.530	79.137	74.273	512.8	470.8	457.675	0.154	0.168	0.173
	S9	84.273	19.894	90.241	45.176	824.84	742.84	717.215	0.109	0.121	0.126
	S2	2.636	78.878	26.300	79.669	977.52	885.12	856.245	0.082	0.090	0.093
	S10	14.317	32.073	23.939	36.368	1422.04	1241.64	1185.265	0.026	0.029	0.031
8	S3	0.652	77.879	24.016	78.074	1052.44	951.64	920.140	0.074	0.082	0.085
	S11	0.817	44.938	14.298	45.183	1540.392	1343.592	1282.092	0.029	0.034	0.035
	S4	8.431	78.007	31.834	80.537	982.64	887.136	857.291	0.082	0.091	0.094
	S12	21.406	34.885	31.872	41.307	1213.972	1060.572	1012.635	0.034	0.039	0.041
	S1	91.162	77.486	114.408	104.835	641	588.5	564.875	0.178	0.194	0.203
	S9	125.218	30.011	134.221	67.576	1031.05	928.55	882.425	0.130	0.145	0.152
	S2	7.338	114.242	41.611	116.443	1221.9	1106.4	1054.425	0.095	0.105	0.110
7	S10	21.598	55.984	38.393	62.464	1777.55	1552.05	1450.575	0.035	0.040	0.043
	S3	0.848	110.416	33.973	110.671	1315.55	1189.55	1132.850	0.084	0.093	0.098
	S11	0.967	77.776	24.300	78.066	1925.49	1679.49	1568.790	0.041	0.046	0.050
	S4	15.611	112.906	49.483	117.589	1228.3	1108.92	1055.199	0.096	0.106	0.111
	S12	33.871	60.968	52.161	71.129	1517.465	1325.715	1239.428	0.047	0.054	0.057
	S1	121.994	101.172	152.346	137.770	769.2	706.2	672.075	0.198	0.216	0.227
	S9	172.058	41.588	184.535	93.205	1237.26	1114.26	1047.635	0.149	0.166	0.176
6	S2	11.097	153.587	57.173	156.916	1466.28	1327.68	1252.605	0.107	0.118	0.125
	S10	28.883	89.841	55.835	98.506	2133.06	1862.46	1715.885	0.046	0.053	0.057
	S3	0.902	147.101	45.033	147.371	1578.66	1427.46	1345.560	0.093	0.103	0.110
	S11	1.181	119.710	37.094	120.064	2310.588	2015.388	1855.488	0.052	0.060	0.065
	S4	20.902	151.682	66.406	157.953	1473.96	1330.704	1253.107	0.107	0.119	0.126
	S12	49.329	97.778	78.662	112.577	1820.958	1590.858	1466.221	0.062	0.071	0.077
	S1	155.122	125.309	192.715	171.846	897.4	823.9	784.525	0.215	0.234	0.246
6	S9	221.714	54.678	238.118	121.193	1443.47	1299.97	1223.095	0.165	0.183	0.195
	S2	13.628	196.644	72.621	200.732	1710.66	1548.96	1462.335	0.117	0.130	0.137
	S10	33.645	127.056	71.761	137.149	2488.57	2172.87	2003.745	0.055	0.063	0.068
	S3	1.218	189.368	58.029	189.734	1841.77	1665.37	1570.870	0.103	0.114	0.121

5	S11	1.231	170.713	52.445	171.082	2695.686	2351.286	2166.786	0.063	0.073	0.079
	S4	29.103	193.799	87.243	202.530	1719.62	1552.488	1462.953	0.118	0.130	0.138
	S12	61.528	137.999	102.928	156.457	2124.451	1856.001	1712.189	0.074	0.084	0.091
	S1	190.639	151.420	236.065	208.612	1025.6	941.6	902.225	0.230	0.251	0.262
	S9	276.236	76.029	299.045	158.900	1649.68	1485.68	1408.805	0.181	0.201	0.212
	S2	15.537	242.277	88.220	246.938	1955.04	1770.24	1683.615	0.126	0.139	0.147
	S10	40.712	168.660	91.310	180.874	2844.08	2483.28	2314.155	0.064	0.073	0.078
	S3	1.591	234.856	72.048	235.333	2104.88	1903.28	1808.780	0.112	0.124	0.130
	S11	1.174	224.185	68.430	224.537	3080.784	2687.184	2502.684	0.073	0.084	0.090
	S4	39.453	238.597	111.032	250.433	1965.28	1774.272	1684.737	0.127	0.141	0.149
	S12	74.709	182.790	129.546	205.202	2427.944	2121.144	1977.332	0.085	0.097	0.104
	S1	228.414	178.752	282.039	247.276	1153.8	1059.3	1025.175	0.244	0.266	0.275
4	S9	333.860	103.406	364.882	203.564	1855.89	1671.39	1604.765	0.197	0.218	0.227
	S2	16.683	289.699	103.592	294.704	2199.42	1991.52	1916.445	0.134	0.148	0.154
	S10	49.466	215.543	114.129	230.383	3199.59	2793.69	2647.115	0.072	0.082	0.087
	S3	2.131	283.018	87.036	283.658	2367.99	2141.19	2059.290	0.120	0.132	0.138
	S11	1.230	279.085	84.956	279.454	3465.882	3023.082	2863.182	0.081	0.092	0.098
	S4	51.782	284.974	137.274	300.508	2210.94	1996.056	1918.459	0.136	0.151	0.157
	S12	91.035	232.728	160.854	260.039	2731.437	2386.287	2261.650	0.095	0.109	0.115
	S1	270.918	209.446	333.752	290.722	1282	1177	1153.375	0.260	0.284	0.289
3	S9	394.271	133.901	434.441	252.182	2062.1	1857.1	1810.975	0.211	0.234	0.240
	S2	21.485	336.743	122.508	343.188	2443.8	2212.8	2160.825	0.140	0.155	0.159
	S10	60.704	265.043	140.217	283.254	3555.1	3104.1	3002.625	0.080	0.091	0.094
	S3	2.381	332.384	102.097	333.099	2631.1	2379.1	2322.400	0.127	0.140	0.143
	S11	1.159	336.898	102.229	337.246	3850.98	3358.98	3248.280	0.088	0.100	0.104
	S4	65.220	331.194	164.578	350.760	2456.6	2217.84	2164.119	0.143	0.158	0.162
	S12	107.773	285.711	193.486	318.043	3034.93	2651.43	2565.143	0.105	0.120	0.124
	S1	315.433	241.118	387.769	335.748	1410.2	1294.7	1281.575	0.275	0.300	0.303
2	S9	454.389	165.929	504.168	302.246	2268.31	2042.81	2017.185	0.222	0.247	0.250
	S2	28.934	381.843	143.487	390.523	2688.18	2434.08	2405.205	0.145	0.160	0.162
	S10	73.735	313.850	167.890	335.971	3910.61	3414.51	3358.135	0.086	0.098	0.100
	S3	2.508	379.518	116.363	380.271	2894.21	2617.01	2585.510	0.131	0.145	0.147
	S11	1.037	392.567	118.807	392.878	4236.078	3694.878	3633.378	0.093	0.106	0.108
	S4	79.683	375.793	192.421	399.697	2702.26	2439.624	2409.779	0.148	0.164	0.166
	S12	124.782	338.382	226.297	375.817	3338.423	2916.573	2868.636	0.113	0.129	0.131
	S1	351.334	264.929	430.813	370.329	1538.4	1412.4	1409.775	0.280	0.305	0.306
1	S9	502.183	190.218	559.248	340.873	2474.52	2228.52	2223.395	0.226	0.251	0.252
	S2	34.311	417.999	159.711	428.293	2932.56	2655.36	2649.585	0.146	0.161	0.162
	S10	84.285	352.234	189.955	377.519	4266.12	3724.92	3713.645	0.088	0.101	0.102
	S3	2.776	416.737	127.797	417.570	3157.32	2854.92	2848.620	0.132	0.146	0.147
	S11	1.036	435.372	131.647	435.683	4621.176	4030.776	4018.476	0.094	0.108	0.108
	S4	92.859	411.050	216.173	438.907	2947.92	2661.408	2655.439	0.149	0.165	0.165
	S12	138.882	379.055	252.598	420.719	3641.916	3181.716	3172.129	0.116	0.132	0.133

Çizelge B.23: 6 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	9.928	8.371	12.439	11.349	128.2	122.95	112.45	0.097	0.101	0.111
	S9	13.087	2.439	13.818	6.365	206.21	195.96	175.46	0.067	0.071	0.079
	S2	1.405	11.269	4.785	11.690	244.38	232.83	209.73	0.048	0.050	0.056
	S10	3.837	4.197	5.097	5.349	355.51	332.96	287.86	0.015	0.016	0.019
	S3	0.166	11.307	3.558	11.357	263.11	250.51	225.31	0.043	0.045	0.050
	S11	0.164	5.709	1.876	5.758	385.098	360.498	311.298	0.015	0.016	0.018
	S4	1.168	11.365	4.577	11.715	245.66	233.722	209.846	0.048	0.050	0.056
5	S12	3.211	4.486	4.556	5.449	303.493	284.318	245.968	0.018	0.019	0.022
	S1	35.310	27.831	43.659	38.424	256.4	245.9	230.15	0.170	0.178	0.190
	S9	46.021	12.319	49.717	26.125	412.42	391.92	361.17	0.121	0.127	0.138
	S2	7.032	36.737	18.054	38.847	488.76	465.66	431.01	0.079	0.083	0.090
	S10	15.066	19.502	20.916	24.022	711.02	665.92	598.27	0.034	0.036	0.040
	S3	0.168	36.870	11.229	36.921	526.22	501.02	463.22	0.070	0.074	0.080
	S11	0.116	25.870	7.876	25.904	770.196	720.996	647.196	0.034	0.036	0.040
4	S4	5.870	36.721	16.886	38.481	491.32	467.444	431.63	0.078	0.082	0.089
	S12	12.863	21.374	19.275	25.233	606.986	568.636	511.111	0.042	0.044	0.049
	S1	73.851	56.533	90.811	78.689	384.6	368.85	353.1	0.236	0.246	0.257
	S9	96.564	27.324	104.761	56.293	618.63	587.88	557.13	0.169	0.178	0.188
	S2	17.109	74.066	39.329	79.199	733.14	698.49	663.84	0.108	0.113	0.119
	S10	34.722	42.384	47.438	52.801	1066.53	998.88	931.23	0.050	0.053	0.057
	S3	0.126	74.426	22.454	74.463	789.33	751.53	713.73	0.094	0.099	0.104
3	S11	0.354	57.187	17.510	57.293	1155.294	1081.494	1007.694	0.050	0.053	0.057
	S4	13.018	73.898	35.188	77.804	736.98	701.166	665.352	0.106	0.111	0.117
	S12	28.000	46.800	42.040	55.200	910.479	852.954	795.429	0.061	0.065	0.069
	S1	119.501	89.077	146.224	124.927	512.8	491.8	481.3	0.285	0.297	0.304
	S9	159.254	45.247	172.828	93.023	824.84	783.84	763.34	0.210	0.220	0.226
	S2	29.366	121.119	65.701	129.928	977.52	931.32	908.22	0.133	0.140	0.143
	S10	55.057	78.467	78.597	94.984	1422.04	1331.84	1286.74	0.067	0.071	0.074
2	S3	0.264	119.383	36.079	119.462	1052.44	1002.04	976.84	0.114	0.119	0.122
	S11	0.472	105.477	32.115	105.618	1540.392	1441.992	1392.792	0.069	0.073	0.076
	S4	23.471	120.502	59.621	127.543	982.64	934.888	911.012	0.130	0.136	0.140
	S12	47.943	86.473	73.885	100.856	1213.972	1137.272	1098.922	0.083	0.089	0.092
	S1	169.171	122.823	206.018	173.575	641	614.75	609.5	0.321	0.335	0.338
	S9	229.612	64.290	248.899	133.173	1031.05	979.8	969.55	0.241	0.254	0.257
	S2	43.305	174.141	95.548	187.133	1221.9	1164.15	1152.6	0.153	0.161	0.162
1	S10	75.141	123.542	112.204	146.085	1777.55	1664.8	1642.25	0.082	0.088	0.089
	S3	0.260	168.177	50.714	168.256	1315.55	1252.55	1239.95	0.128	0.134	0.136
	S11	0.463	166.070	50.283	166.209	1925.49	1802.49	1777.89	0.086	0.092	0.093
	S4	37.053	173.233	89.023	184.349	1228.3	1168.61	1156.672	0.150	0.158	0.159
	S12	71.316	136.115	112.151	157.510	1517.465	1421.59	1402.415	0.104	0.111	0.112
	S1	213.560	152.709	259.373	216.777	769.2	737.7	737.7	0.337	0.352	0.352
	S9	297.183	80.442	321.315	169.596	1237.26	1175.76	1175.76	0.260	0.273	0.273
	S2	53.856	223.877	121.019	240.034	1466.28	1396.98	1396.98	0.164	0.172	0.172
	S10	92.004	171.945	143.587	199.546	2133.06	1997.76	1997.76	0.094	0.100	0.100
	S3	0.448	214.216	64.713	214.351	1578.66	1503.06	1503.06	0.136	0.143	0.143
	S11	0.342	228.990	69.038	229.092	2310.588	2162.988	2162.988	0.099	0.106	0.106
	S4	46.111	222.567	112.881	236.400	1473.96	1402.332	1402.332	0.160	0.169	0.169
	S12	94.493	189.142	151.236	217.490	1820.958	1705.908	1705.908	0.119	0.127	0.127

Çizelge B.24: 9 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	7.364	7.484	9.609	9.693	128.2	117.7	104.575	0.076	0.082	0.093
	S9	9.879	1.266	10.259	4.230	206.21	185.71	160.085	0.050	0.055	0.064
	S2	0.923	10.798	4.162	11.075	244.38	221.28	192.405	0.045	0.050	0.058
	S10	0.721	1.295	1.109	1.511	355.51	310.41	254.035	0.004	0.005	0.006
	S3	0.449	10.629	3.638	10.764	263.11	237.91	206.41	0.041	0.045	0.052
	S11	0.470	2.272	1.151	2.413	385.098	335.898	274.398	0.006	0.007	0.009
	S4	0.240	10.777	3.473	10.849	245.66	221.784	191.939	0.044	0.049	0.057
8	S12	1.611	1.268	1.991	1.751	303.493	265.143	217.2055	0.007	0.008	0.009
	S1	27.375	24.454	34.711	32.666	256.4	235.4	211.775	0.135	0.147	0.164
	S9	36.045	8.735	38.665	19.549	412.42	371.42	325.295	0.094	0.104	0.119
	S2	1.031	33.891	11.198	34.200	488.76	442.56	390.585	0.070	0.077	0.088
	S10	6.867	11.695	10.375	13.755	711.02	620.82	519.345	0.019	0.022	0.026
	S3	0.684	33.571	10.755	33.776	526.22	475.82	419.12	0.064	0.071	0.081
	S11	0.668	16.371	5.579	16.571	770.196	671.796	561.096	0.022	0.025	0.030
7	S4	3.384	33.628	13.472	34.643	491.32	443.568	389.847	0.071	0.078	0.089
	S12	8.528	12.682	12.333	15.241	606.986	530.286	443.9985	0.025	0.029	0.034
	S1	58.595	49.292	73.382	66.870	384.6	353.1	318.975	0.191	0.208	0.230
	S9	77.190	20.610	83.373	43.767	618.63	557.13	490.505	0.135	0.150	0.170
	S2	6.802	67.068	26.922	69.109	733.14	663.84	588.765	0.094	0.104	0.117
	S10	20.230	28.521	28.786	34.590	1066.53	931.23	784.655	0.032	0.037	0.044
	S3	0.683	66.715	20.697	66.919	789.33	713.73	631.83	0.085	0.094	0.106
6	S11	0.527	39.910	12.500	40.069	1155.294	1007.694	847.794	0.035	0.040	0.047
	S4	8.625	66.515	28.580	69.102	736.98	665.352	587.755	0.094	0.104	0.118
	S12	20.095	31.354	29.502	37.383	910.479	795.429	670.7915	0.041	0.047	0.056
	S1	96.614	77.980	120.008	106.964	512.8	470.8	418.3	0.234	0.255	0.287
	S9	129.742	35.311	140.335	74.233	824.84	742.84	640.34	0.170	0.189	0.219
	S2	14.597	109.543	47.460	113.922	977.52	885.12	769.62	0.117	0.129	0.148
	S10	34.306	57.286	51.492	67.578	1422.04	1241.64	1016.14	0.048	0.054	0.067
5	S3	0.815	107.035	32.926	107.280	1052.44	951.64	825.64	0.102	0.113	0.130
	S11	0.649	78.871	24.310	79.066	1540.392	1343.592	1097.592	0.051	0.059	0.072
	S4	16.893	108.411	49.416	113.478	982.64	887.136	767.756	0.115	0.128	0.148
	S12	36.074	62.892	54.941	73.714	1213.972	1060.572	868.822	0.061	0.070	0.085
	S1	140.127	109.228	172.895	151.266	641	588.5	525.5	0.270	0.294	0.329
	S9	191.601	51.870	207.162	109.350	1031.05	928.55	805.55	0.201	0.223	0.257
	S2	24.462	159.573	72.333	166.911	1221.9	1106.4	967.8	0.137	0.151	0.172
4	S10	48.925	95.226	77.493	109.904	1777.55	1552.05	1281.45	0.062	0.071	0.086
	S3	1.088	152.741	46.910	153.067	1315.55	1189.55	1038.35	0.116	0.129	0.147
	S11	0.835	130.624	40.022	130.874	1925.49	1679.49	1384.29	0.068	0.078	0.095
	S4	28.544	157.813	75.888	166.376	1228.3	1108.92	965.664	0.135	0.150	0.172
	S12	55.681	104.455	87.017	121.160	1517.465	1325.715	1095.615	0.080	0.091	0.111
	S1	186.220	142.495	228.968	198.361	769.2	706.2	648.45	0.298	0.324	0.353
	S9	261.132	70.374	282.244	148.714	1237.26	1114.26	1001.51	0.228	0.253	0.282
3	S2	32.997	214.578	97.370	224.477	1466.28	1327.68	1200.63	0.153	0.169	0.187
	S10	63.486	146.789	107.522	165.834	2133.06	1862.46	1614.41	0.078	0.089	0.103
	S3	1.140	203.687	62.246	204.029	1578.66	1427.46	1288.86	0.129	0.143	0.158
	S11	1.135	194.791	59.572	195.131	2310.588	2015.388	1744.788	0.084	0.097	0.112
	S4	37.521	212.064	101.140	223.321	1473.96	1330.704	1199.386	0.152	0.168	0.186
	S12	79.285	160.729	127.504	184.515	1820.958	1590.858	1379.933	0.101	0.116	0.134
	S1	234.552	175.577	287.225	245.942	897.4	823.9	776.65	0.320	0.349	0.370
3	S9	333.399	90.732	360.619	190.752	1443.47	1299.97	1207.72	0.250	0.277	0.299
	S2	39.724	273.361	121.732	285.278	1710.66	1548.96	1445.01	0.167	0.184	0.197
	S10	74.590	202.394	135.309	224.771	2488.57	2172.87	1969.92	0.090	0.103	0.114
	S3	1.595	261.030	79.904	261.508	1841.77	1665.37	1551.97	0.142	0.157	0.169

2	S11	1.225	270.485	82.371	270.853	2695.686	2351.286	2129.886	0.100	0.115	0.127
	S4	50.261	269.659	131.159	284.737	1719.62	1552.488	1445.046	0.166	0.183	0.197
	S12	98.227	221.138	164.569	250.606	2124.451	1856.001	1683.426	0.118	0.135	0.149
	S1	283.978	209.367	346.788	294.560	1025.6	941.6	904.85	0.338	0.368	0.383
	S9	408.909	120.496	445.057	243.168	1649.68	1485.68	1413.93	0.270	0.300	0.315
	S2	45.409	332.435	145.140	346.058	1955.04	1770.24	1689.39	0.177	0.195	0.205
	S10	88.330	260.222	166.396	286.720	2844.08	2483.28	2325.43	0.101	0.115	0.123
	S3	2.182	319.989	98.178	320.643	2104.88	1903.28	1815.08	0.152	0.168	0.177
	S11	1.141	346.166	104.991	346.508	3080.784	2687.184	2514.984	0.112	0.129	0.138
	S4	65.674	327.997	164.072	347.699	1965.28	1774.272	1690.706	0.177	0.196	0.206
	S12	117.318	284.079	202.542	319.274	2427.944	2121.144	1986.919	0.131	0.151	0.161
1	S1	326.222	237.730	397.541	335.597	1153.8	1059.3	1033.05	0.345	0.375	0.385
	S9	475.749	150.782	520.983	293.507	1855.89	1671.39	1620.14	0.281	0.312	0.322
	S2	48.567	382.669	163.367	397.239	2199.42	1991.52	1933.77	0.181	0.199	0.205
	S10	101.386	313.979	195.580	344.395	3199.59	2793.69	2680.94	0.108	0.123	0.128
	S3	2.824	370.364	113.933	371.211	2367.99	2141.19	2078.19	0.157	0.173	0.179
	S11	1.236	409.823	124.182	410.193	3465.882	3023.082	2900.082	0.118	0.136	0.141
	S4	79.027	377.438	192.259	401.146	2210.94	1996.056	1936.366	0.181	0.201	0.207
	S12	136.908	342.020	239.514	383.092	2731.437	2386.287	2290.412	0.140	0.161	0.167

Çizelge B.25: 12 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	5.949	7.499	8.198	9.284	128.2	117.7	117.700	0.072	0.079	0.079
	S9	8.085	0.055	8.101	2.480	206.21	185.71	185.710	0.039	0.044	0.044
	S2	2.674	11.009	5.976	11.811	244.38	221.28	221.280	0.048	0.053	0.053
	S10	1.592	0.812	1.835	1.289	355.51	310.41	310.410	0.005	0.006	0.006
	S3	0.500	11.076	3.823	11.226	263.11	237.91	237.910	0.043	0.047	0.047
	S11	0.634	0.388	0.750	0.578	385.098	335.898	335.898	0.002	0.002	0.002
	S4	0.711	10.982	4.005	11.195	245.66	221.784	221.784	0.046	0.050	0.050
11	S12	0.559	1.124	0.896	1.292	303.493	265.143	265.143	0.004	0.005	0.005
	S1	22.969	23.720	30.085	30.611	256.4	235.4	235.400	0.119	0.130	0.130
	S9	30.446	5.343	32.049	14.477	412.42	371.42	371.420	0.078	0.086	0.086
	S2	3.414	33.402	13.435	34.426	488.76	442.56	442.560	0.070	0.078	0.078
	S10	0.921	6.354	2.827	6.630	711.02	620.82	620.820	0.009	0.011	0.011
	S3	0.711	33.581	10.785	33.794	526.22	475.82	475.820	0.064	0.071	0.071
	S11	0.903	9.550	3.768	9.821	770.196	671.796	671.796	0.013	0.015	0.015
10	S4	1.125	33.120	11.061	33.457	491.32	443.568	443.568	0.068	0.075	0.075
	S12	5.827	6.637	7.818	8.385	606.986	530.286	530.286	0.014	0.016	0.016
	S1	49.648	46.714	63.662	61.608	384.6	353.1	353.100	0.166	0.180	0.180
	S9	65.705	14.554	70.071	34.266	618.63	557.13	557.130	0.113	0.126	0.126
	S2	0.828	64.449	20.162	64.697	733.14	663.84	663.840	0.088	0.097	0.097
	S10	9.709	19.038	15.421	21.951	1066.53	931.23	931.230	0.021	0.024	0.024
	S3	0.727	64.854	20.183	65.072	789.33	713.73	713.730	0.082	0.091	0.091
9	S11	0.899	27.560	9.166	27.829	1155.294	1007.694	1007.694	0.024	0.028	0.028
	S4	4.773	63.867	23.933	65.299	736.98	665.352	665.352	0.089	0.098	0.098
	S12	15.089	20.635	21.280	25.162	910.479	795.429	795.429	0.028	0.032	0.032
	S1	82.249	73.102	104.179	97.777	512.8	470.8	457.675	0.203	0.221	0.228
	S9	110.941	26.189	118.798	59.471	824.84	742.84	717.215	0.144	0.160	0.166
	S2	3.471	103.839	34.622	104.880	977.52	885.12	856.245	0.107	0.118	0.122
	S10	18.848	42.223	31.515	47.877	1422.04	1241.64	1185.265	0.034	0.039	0.040
8	S3	0.859	102.523	31.616	102.781	1052.44	951.64	920.140	0.098	0.108	0.112
	S11	1.076	59.159	18.823	59.481	1540.392	1343.592	1282.092	0.039	0.044	0.046
	S4	11.100	102.692	41.907	106.022	982.64	887.136	857.291	0.108	0.120	0.124
	S12	28.180	45.924	41.958	54.378	1213.972	1060.572	1012.635	0.045	0.051	0.054
	S1	120.010	102.007	150.612	138.010	641	588.5	564.875	0.235	0.256	0.267
	S9	164.843	39.508	176.695	88.960	1031.05	928.55	882.425	0.171	0.190	0.200
	S2	9.660	150.393	54.778	153.291	1221.9	1106.4	1054.425	0.125	0.139	0.145
7	S10	28.432	73.701	50.543	82.230	1777.55	1552.05	1450.575	0.046	0.053	0.057
	S3	1.116	145.358	44.723	145.692	1315.55	1189.55	1132.850	0.111	0.122	0.129
	S11	1.273	102.388	31.989	102.769	1925.49	1679.49	1568.790	0.053	0.061	0.066
	S4	20.551	148.635	65.142	154.800	1228.3	1108.92	1055.199	0.126	0.140	0.147
	S12	44.589	80.261	68.667	93.638	1517.465	1325.715	1239.428	0.062	0.071	0.076
	S1	160.599	133.188	200.555	181.368	769.2	706.2	672.075	0.261	0.284	0.298
	S9	226.506	54.748	242.930	122.700	1237.26	1114.26	1047.635	0.196	0.218	0.232
6	S2	14.609	202.189	75.266	206.572	1466.28	1327.68	1252.605	0.141	0.156	0.165
	S10	38.023	118.271	73.505	129.678	2133.06	1862.46	1715.885	0.061	0.070	0.076
	S3	1.188	193.650	59.283	194.007	1578.66	1427.46	1345.560	0.123	0.136	0.144
	S11	1.554	157.592	48.832	158.058	2310.588	2015.388	1855.488	0.068	0.078	0.085
	S4	27.516	199.682	87.421	207.936	1473.96	1330.704	1253.107	0.141	0.156	0.166
	S12	64.939	128.720	103.555	148.202	1820.958	1590.858	1466.221	0.081	0.093	0.101
	S1	204.211	164.963	253.700	226.227	897.4	823.9	784.525	0.283	0.308	0.323
6	S9	291.876	71.981	313.470	159.544	1443.47	1299.97	1223.095	0.217	0.241	0.256
	S2	17.940	258.871	95.601	264.253	1710.66	1548.96	1462.335	0.154	0.171	0.181
	S10	44.291	167.263	94.470	180.550	2488.57	2172.87	2003.745	0.073	0.083	0.090
	S3	1.604	249.294	76.392	249.775	1841.77	1665.37	1570.870	0.136	0.150	0.159

5	S11	1.621	224.735	69.041	225.221	2695.686	2351.286	2166.786	0.084	0.096	0.104
	S4	38.313	255.127	114.851	266.621	1719.62	1552.488	1462.953	0.155	0.172	0.182
	S12	80.999	181.668	135.499	205.968	2124.451	1856.001	1712.189	0.097	0.111	0.120
	S1	250.967	199.337	310.768	274.627	1025.6	941.6	902.225	0.303	0.330	0.344
	S9	363.650	100.089	393.677	209.184	1649.68	1485.68	1408.805	0.239	0.265	0.279
	S2	20.454	318.945	116.137	325.081	1955.04	1770.24	1683.615	0.166	0.184	0.193
	S10	53.596	222.033	120.205	238.111	2844.08	2483.28	2314.155	0.084	0.096	0.103
	S3	2.095	309.176	94.847	309.804	2104.88	1903.28	1808.780	0.147	0.163	0.171
	S11	1.546	295.127	90.084	295.591	3080.784	2687.184	2502.684	0.096	0.110	0.118
	S4	51.938	314.101	146.168	329.682	1965.28	1774.272	1684.737	0.168	0.186	0.196
	S12	98.351	240.633	170.540	270.138	2427.944	2121.144	1977.332	0.111	0.127	0.137
	S1	300.695	235.318	371.290	325.527	1153.8	1059.3	1025.175	0.322	0.351	0.362
4	S9	439.510	136.129	480.348	267.981	1855.89	1671.39	1604.765	0.259	0.287	0.299
	S2	21.962	381.374	136.374	387.963	2199.42	1991.52	1916.445	0.176	0.195	0.202
	S10	65.119	283.752	150.244	303.287	3199.59	2793.69	2647.115	0.095	0.109	0.115
	S3	2.805	372.579	114.579	373.420	2367.99	2141.19	2059.290	0.158	0.174	0.181
	S11	1.619	367.401	111.840	367.887	3465.882	3023.082	2863.182	0.106	0.122	0.128
	S4	68.168	375.153	180.714	395.604	2210.94	1996.056	1918.459	0.179	0.198	0.206
	S12	119.844	306.374	211.756	342.327	2731.437	2386.287	2261.650	0.125	0.143	0.151
	S1	356.650	275.725	439.368	382.720	1282	1177	1153.375	0.343	0.373	0.381
3	S9	519.037	176.273	571.919	331.985	2062.1	1857.1	1810.975	0.277	0.308	0.316
	S2	28.284	443.304	161.275	451.790	2443.8	2212.8	2160.825	0.185	0.204	0.209
	S10	79.914	348.915	184.588	372.889	3555.1	3104.1	3002.625	0.105	0.120	0.124
	S3	3.135	437.567	134.405	438.507	2631.1	2379.1	2322.400	0.167	0.184	0.189
	S11	1.526	443.509	134.579	443.967	3850.98	3358.98	3248.280	0.115	0.132	0.137
	S4	85.859	436.000	216.659	461.758	2456.6	2217.84	2164.119	0.188	0.208	0.213
	S12	141.878	376.124	254.715	418.687	3034.93	2651.43	2565.143	0.138	0.158	0.163
	S1	415.252	317.419	510.477	441.995	1410.2	1294.7	1281.575	0.362	0.394	0.398
2	S9	598.180	218.437	663.711	397.891	2268.31	2042.81	2017.185	0.293	0.325	0.329
	S2	38.091	502.676	188.894	514.104	2688.18	2434.08	2405.205	0.191	0.211	0.214
	S10	97.068	413.168	221.018	442.288	3910.61	3414.51	3358.135	0.113	0.130	0.132
	S3	3.301	499.617	153.186	500.607	2894.21	2617.01	2585.510	0.173	0.191	0.194
	S11	1.366	516.794	156.404	517.204	4236.078	3694.878	3633.378	0.122	0.140	0.142
	S4	104.898	494.712	253.312	526.181	2702.26	2439.624	2409.779	0.195	0.216	0.218
	S12	164.269	445.463	297.908	494.744	3338.423	2916.573	2868.636	0.148	0.170	0.172
	S1	462.514	348.765	567.143	487.520	1538.4	1412.4	1409.775	0.369	0.402	0.402
1	S9	661.097	250.412	736.221	448.742	2474.52	2228.52	2223.395	0.298	0.330	0.331
	S2	45.169	550.275	210.252	563.825	2932.56	2655.36	2649.585	0.192	0.212	0.213
	S10	110.957	463.698	250.066	496.984	4266.12	3724.92	3713.645	0.116	0.133	0.134
	S3	3.654	548.613	168.238	549.709	3157.32	2854.92	2848.620	0.174	0.193	0.193
	S11	1.363	573.145	173.307	573.554	4621.176	4030.776	4018.476	0.124	0.142	0.143
	S4	122.244	541.126	284.581	577.799	2947.92	2661.408	2655.439	0.196	0.217	0.218
	S12	182.831	499.006	332.533	553.855	3641.916	3181.716	3172.129	0.152	0.174	0.175

Çizelge B.26: 6 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	16.841	14.199	21.100	19.251	128.2	122.95	112.45	0.165	0.172	0.188
	S9	22.199	4.137	23.440	10.796	206.21	195.96	175.46	0.114	0.120	0.134
	S2	2.382	19.115	8.117	19.830	244.38	232.83	209.73	0.081	0.085	0.095
	S10	6.509	7.120	8.645	9.072	355.51	332.96	287.86	0.026	0.027	0.032
	S3	0.281	19.180	6.035	19.264	263.11	250.51	225.31	0.073	0.077	0.086
	S11	0.278	9.684	3.183	9.767	385.098	360.498	311.298	0.025	0.027	0.031
	S4	1.980	19.278	7.764	19.873	245.66	233.722	209.846	0.081	0.085	0.095
5	S12	5.446	7.609	7.729	9.243	303.493	284.318	245.968	0.030	0.033	0.038
	S1	59.895	47.208	74.058	65.177	256.4	245.9	230.15	0.289	0.301	0.322
	S9	78.064	20.896	84.333	44.315	412.42	391.92	361.17	0.204	0.215	0.233
	S2	11.929	62.316	30.624	65.895	488.76	465.66	431.01	0.135	0.142	0.153
	S10	25.555	33.081	35.480	40.747	711.02	665.92	598.27	0.057	0.061	0.068
	S3	0.285	62.542	19.048	62.627	526.22	501.02	463.22	0.119	0.125	0.135
	S11	0.196	43.882	13.360	43.940	770.196	720.996	647.196	0.057	0.061	0.068
4	S4	9.956	62.288	28.643	65.275	491.32	467.444	431.63	0.133	0.140	0.151
	S12	21.819	36.256	32.696	42.801	606.986	568.636	511.111	0.071	0.075	0.084
	S1	125.271	95.895	154.040	133.476	384.6	368.85	353.1	0.401	0.418	0.436
	S9	163.798	46.348	177.703	95.488	618.63	587.88	557.13	0.287	0.302	0.319
	S2	29.021	125.636	66.712	134.342	733.14	698.49	663.84	0.183	0.192	0.202
	S10	58.898	71.894	80.467	89.563	1066.53	998.88	931.23	0.084	0.090	0.096
	S3	0.214	126.245	38.087	126.309	789.33	751.53	713.73	0.160	0.168	0.177
3	S11	0.600	97.005	29.701	97.185	1155.294	1081.494	1007.694	0.084	0.090	0.096
	S4	22.082	125.350	59.687	131.975	736.98	701.166	665.352	0.179	0.188	0.198
	S12	47.495	79.385	71.310	93.633	910.479	852.954	795.429	0.103	0.110	0.118
	S1	202.705	151.098	248.035	211.909	512.8	491.8	481.3	0.484	0.504	0.515
	S9	270.136	76.750	293.161	157.791	824.84	783.84	763.34	0.355	0.374	0.384
	S2	49.812	205.449	111.447	220.392	977.52	931.32	908.22	0.225	0.237	0.243
	S10	93.390	133.101	133.320	161.118	1422.04	1331.84	1286.74	0.113	0.121	0.125
2	S3	0.448	202.505	61.199	202.639	1052.44	1002.04	976.84	0.193	0.202	0.207
	S11	0.800	178.916	54.475	179.156	1540.392	1441.992	1392.792	0.116	0.124	0.129
	S4	39.813	204.403	101.133	216.347	982.64	934.888	911.012	0.220	0.231	0.237
	S12	81.324	146.681	125.328	171.078	1213.972	1137.272	1098.922	0.141	0.150	0.156
	S1	286.959	208.340	349.461	294.428	641	614.75	609.5	0.545	0.568	0.573
	S9	389.483	109.052	422.198	225.897	1031.05	979.8	969.55	0.409	0.431	0.435
	S2	73.457	295.389	162.074	317.426	1221.9	1164.15	1152.6	0.260	0.273	0.275
1	S10	127.459	209.560	190.327	247.798	1777.55	1664.8	1642.25	0.139	0.149	0.151
	S3	0.442	285.273	86.024	285.405	1315.55	1252.55	1239.95	0.217	0.228	0.230
	S11	0.785	281.698	85.294	281.933	1925.49	1802.49	1777.89	0.146	0.156	0.159
	S4	62.852	293.848	151.006	312.703	1228.3	1168.61	1156.672	0.255	0.268	0.270
	S12	120.971	230.887	190.237	267.178	1517.465	1421.59	1402.415	0.176	0.188	0.191
	S1	362.254	259.034	439.964	367.710	769.2	737.7	737.7	0.572	0.596	0.596
	S9	504.099	136.450	545.034	287.680	1237.26	1175.76	1175.76	0.441	0.464	0.464
	S2	91.354	379.754	205.280	407.161	1466.28	1396.98	1396.98	0.278	0.291	0.291
	S10	156.063	291.664	243.562	338.482	2133.06	1997.76	1997.76	0.159	0.169	0.169
	S3	0.761	363.367	109.771	363.595	1578.66	1503.06	1503.06	0.230	0.242	0.242
	S11	0.579	388.427	117.107	388.600	2310.588	2162.988	2162.988	0.168	0.180	0.180
	S4	78.217	377.531	191.476	400.996	1473.96	1402.332	1402.332	0.272	0.286	0.286
	S12	160.285	320.835	256.536	368.920	1820.958	1705.908	1705.908	0.203	0.216	0.216

Çizelge B.27: 9 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	12.491	12.695	16.300	16.443	128.2	117.7	104.575	0.128	0.140	0.157
	S9	16.757	2.147	17.401	7.174	206.21	185.71	160.085	0.084	0.094	0.109
	S2	1.565	18.316	7.060	18.785	244.38	221.28	192.405	0.077	0.085	0.098
	S10	1.223	2.197	1.882	2.563	355.51	310.41	254.035	0.007	0.008	0.010
	S3	0.762	18.030	6.171	18.258	263.11	237.91	206.41	0.069	0.077	0.088
	S11	0.797	3.854	1.953	4.093	385.098	335.898	274.398	0.011	0.012	0.015
	S4	0.407	18.281	5.891	18.403	245.66	221.784	191.939	0.075	0.083	0.096
8	S12	2.733	2.150	3.378	2.970	303.493	265.143	217.2055	0.011	0.013	0.016
	S1	46.436	41.480	58.880	55.410	256.4	235.4	211.775	0.230	0.250	0.278
	S9	61.141	14.817	65.587	33.159	412.42	371.42	325.295	0.159	0.177	0.202
	S2	1.749	57.488	18.995	58.013	488.76	442.56	390.585	0.119	0.131	0.149
	S10	11.648	19.837	17.599	23.331	711.02	620.82	519.345	0.033	0.038	0.045
	S3	1.160	56.945	18.244	57.293	526.22	475.82	419.12	0.109	0.120	0.137
	S11	1.133	27.769	9.464	28.109	770.196	671.796	561.096	0.036	0.042	0.050
7	S4	5.740	57.041	22.852	58.763	491.32	443.568	389.847	0.120	0.132	0.151
	S12	14.466	21.512	20.920	25.852	606.986	530.286	443.9985	0.043	0.049	0.058
	S1	99.392	83.612	124.476	113.430	384.6	353.1	318.975	0.324	0.353	0.390
	S9	130.935	34.960	141.422	74.240	618.63	557.13	490.505	0.229	0.254	0.288
	S2	11.538	113.765	45.667	117.226	733.14	663.84	588.765	0.160	0.177	0.199
	S10	34.315	48.379	48.829	58.674	1066.53	931.23	784.655	0.055	0.063	0.075
	S3	1.158	113.165	35.108	113.513	789.33	713.73	631.83	0.144	0.159	0.180
6	S11	0.894	67.699	21.204	67.967	1155.294	1007.694	847.794	0.059	0.067	0.080
	S4	14.631	112.827	48.479	117.216	736.98	665.352	587.755	0.159	0.176	0.199
	S12	34.087	53.185	50.042	63.411	910.479	795.429	670.7915	0.070	0.080	0.095
	S1	163.882	132.275	203.564	181.440	512.8	470.8	418.3	0.397	0.432	0.487
	S9	220.076	59.896	238.045	125.919	824.84	742.84	640.34	0.289	0.320	0.372
	S2	24.760	185.814	80.504	193.242	977.52	885.12	769.62	0.198	0.218	0.251
	S10	58.192	97.172	87.343	114.630	1422.04	1241.64	1016.14	0.081	0.092	0.113
5	S3	1.383	181.560	55.851	181.975	1052.44	951.64	825.64	0.173	0.191	0.220
	S11	1.100	133.787	41.236	134.117	1540.392	1343.592	1097.592	0.087	0.100	0.122
	S4	28.654	183.893	83.822	192.489	982.64	887.136	767.756	0.196	0.217	0.251
	S12	61.190	106.681	93.195	125.038	1213.972	1060.572	868.822	0.103	0.118	0.144
	S1	237.691	185.279	293.275	256.586	641	588.5	525.5	0.458	0.498	0.558
	S9	325.005	87.985	351.401	185.487	1031.05	928.55	805.55	0.341	0.378	0.436
	S2	41.493	270.677	122.696	283.125	1221.9	1106.4	967.8	0.232	0.256	0.293
4	S10	82.990	161.528	131.448	186.425	1777.55	1552.05	1281.45	0.105	0.120	0.145
	S3	1.846	259.089	79.572	259.642	1315.55	1189.55	1038.35	0.197	0.218	0.250
	S11	1.416	221.572	67.887	221.997	1925.49	1679.49	1384.29	0.115	0.132	0.160
	S4	48.418	267.692	128.725	282.217	1228.3	1108.92	965.664	0.230	0.254	0.292
	S12	94.449	177.184	147.604	205.518	1517.465	1325.715	1095.615	0.135	0.155	0.188
	S1	315.878	241.708	388.390	336.471	769.2	706.2	648.45	0.505	0.550	0.599
	S9	442.948	119.373	478.760	252.257	1237.26	1114.26	1001.51	0.387	0.430	0.478
3	S2	55.971	363.980	165.165	380.771	1466.28	1327.68	1200.63	0.260	0.287	0.317
	S10	107.688	248.992	182.386	281.299	2133.06	1862.46	1614.41	0.132	0.151	0.174
	S3	1.934	345.506	105.585	346.086	1578.66	1427.46	1288.86	0.219	0.242	0.269
	S11	1.925	330.416	101.050	330.994	2310.588	2015.388	1744.788	0.143	0.164	0.190
	S4	63.645	359.717	171.560	378.810	1473.96	1330.704	1199.386	0.257	0.285	0.316
	S12	134.489	272.638	216.280	312.985	1820.958	1590.858	1379.933	0.172	0.197	0.227
	S1	397.862	297.824	487.209	417.183	897.4	823.9	776.65	0.543	0.591	0.627
2	S9	565.532	153.906	611.704	323.565	1443.47	1299.97	1207.72	0.424	0.471	0.506
	S2	67.382	463.691	206.489	483.905	1710.66	1548.96	1445.01	0.283	0.312	0.335
	S10	126.525	343.314	229.519	381.271	2488.57	2172.87	1969.92	0.153	0.175	0.194
	S3	2.706	442.774	135.538	443.586	1841.77	1665.37	1551.97	0.241	0.266	0.286

2	S11	2.078	458.814	139.722	459.437	2695.686	2351.286	2129.886	0.170	0.195	0.216
	S4	85.256	457.412	222.480	482.988	1719.62	1552.488	1445.046	0.281	0.311	0.334
	S12	166.619	375.108	279.151	425.093	2124.451	1856.001	1683.426	0.200	0.229	0.253
	S1	481.701	355.141	588.244	499.651	1025.6	941.6	904.85	0.574	0.625	0.650
	S9	693.616	204.392	754.934	412.477	1649.68	1485.68	1413.93	0.458	0.508	0.534
	S2	77.026	563.897	246.195	587.005	1955.04	1770.24	1689.39	0.300	0.332	0.347
	S10	149.830	441.404	282.251	486.353	2844.08	2483.28	2325.43	0.171	0.196	0.209
	S3	3.700	542.785	166.536	543.895	2104.88	1903.28	1815.08	0.258	0.286	0.300
	S11	1.936	587.188	178.092	587.769	3080.784	2687.184	2514.984	0.191	0.219	0.234
	S4	111.400	556.368	278.310	589.788	1965.28	1774.272	1690.706	0.300	0.332	0.349
	S12	199.002	481.872	343.564	541.573	2427.944	2121.144	1986.919	0.223	0.255	0.273
1	S1	553.357	403.253	674.333	569.260	1153.8	1059.3	1033.05	0.584	0.637	0.653
	S9	806.994	255.766	883.724	497.864	1855.89	1671.39	1620.14	0.476	0.529	0.545
	S2	82.382	649.107	277.114	673.822	2199.42	1991.52	1933.77	0.306	0.338	0.348
	S10	171.978	532.591	331.755	584.184	3199.59	2793.69	2680.94	0.183	0.209	0.218
	S3	4.790	628.234	193.260	629.671	2367.99	2141.19	2078.19	0.266	0.294	0.303
	S11	2.096	695.167	210.646	695.796	3465.882	3023.082	2900.082	0.201	0.230	0.240
	S4	134.051	640.234	326.121	680.449	2210.94	1996.056	1936.366	0.308	0.341	0.351
	S12	232.232	580.155	406.278	649.825	2731.437	2386.287	2290.412	0.238	0.272	0.284

Çizelge B.28: 12 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	10.090	12.721	13.907	15.748	128.2	117.7	117.700	0.123	0.134	0.134
	S9	13.714	0.093	13.741	4.207	206.21	185.71	185.710	0.067	0.074	0.074
	S2	4.535	18.675	10.138	20.035	244.38	221.28	221.280	0.082	0.091	0.091
	S10	2.700	1.377	3.113	2.187	355.51	310.41	310.410	0.009	0.010	0.010
	S3	0.848	18.788	6.485	19.043	263.11	237.91	237.910	0.072	0.080	0.080
	S11	1.075	0.658	1.272	0.980	385.098	335.898	335.898	0.003	0.004	0.004
	S4	1.205	18.628	6.794	18.989	245.66	221.784	221.784	0.077	0.086	0.086
11	S12	0.948	1.907	1.519	2.191	303.493	265.143	265.143	0.007	0.008	0.008
	S1	38.961	40.236	51.032	51.924	256.4	235.4	235.400	0.203	0.221	0.221
	S9	51.644	9.063	54.363	24.557	412.42	371.42	371.420	0.132	0.146	0.146
	S2	5.792	56.659	22.789	58.396	488.76	442.56	442.560	0.119	0.132	0.132
	S10	1.562	10.778	4.795	11.247	711.02	620.82	620.820	0.016	0.018	0.018
	S3	1.206	56.962	18.294	57.323	526.22	475.82	475.820	0.109	0.120	0.120
	S11	1.531	16.199	6.391	16.659	770.196	671.796	671.796	0.022	0.025	0.025
10	S4	1.908	56.179	18.762	56.752	491.32	443.568	443.568	0.116	0.128	0.128
	S12	9.885	11.258	13.262	14.223	606.986	530.286	530.286	0.023	0.027	0.027
	S1	84.216	79.238	107.987	104.503	384.6	353.1	353.100	0.281	0.306	0.306
	S9	111.453	24.688	118.859	58.124	618.63	557.13	557.130	0.192	0.213	0.213
	S2	1.404	109.323	34.200	109.744	733.14	663.84	663.840	0.150	0.165	0.165
	S10	16.469	32.294	26.157	37.234	1066.53	931.23	931.230	0.035	0.040	0.040
	S3	1.233	110.010	34.236	110.380	789.33	713.73	713.730	0.140	0.155	0.155
9	S11	1.524	46.748	15.549	47.206	1155.294	1007.694	1007.694	0.041	0.047	0.047
	S4	8.096	108.335	40.597	110.763	736.98	665.352	665.352	0.150	0.166	0.166
	S12	25.596	35.003	36.096	42.681	910.479	795.429	795.429	0.047	0.054	0.054
	S1	139.515	124.000	176.715	165.855	512.8	470.8	457.675	0.345	0.375	0.386
	S9	188.185	44.424	201.512	100.879	824.84	742.84	717.215	0.244	0.271	0.281
	S2	5.887	176.138	58.728	177.904	977.52	885.12	856.245	0.182	0.201	0.208
	S10	31.971	71.621	53.457	81.212	1422.04	1241.64	1185.265	0.057	0.065	0.069
8	S3	1.457	173.907	53.629	174.344	1052.44	951.64	920.140	0.166	0.183	0.189
	S11	1.824	100.348	31.929	100.896	1540.392	1343.592	1282.092	0.066	0.075	0.079
	S4	18.828	174.193	71.086	179.841	982.64	887.136	857.291	0.183	0.203	0.210
	S12	47.801	77.900	71.171	92.240	1213.972	1060.572	1012.635	0.076	0.087	0.091
	S1	203.568	173.030	255.477	234.101	641	588.5	564.875	0.399	0.434	0.452
	S9	279.616	67.015	299.721	150.900	1031.05	928.55	882.425	0.291	0.323	0.340
	S2	16.386	255.106	92.918	260.022	1221.9	1106.4	1054.425	0.213	0.235	0.247
7	S10	48.229	125.015	85.733	139.484	1777.55	1552.05	1450.575	0.078	0.090	0.096
	S3	1.893	246.564	75.863	247.132	1315.55	1189.55	1132.850	0.188	0.208	0.218
	S11	2.159	173.676	54.262	174.324	1925.49	1679.49	1568.790	0.091	0.104	0.111
	S4	34.860	252.124	110.498	262.582	1228.3	1108.92	1055.199	0.214	0.237	0.249
	S12	75.635	136.144	116.478	158.834	1517.465	1325.715	1239.428	0.105	0.120	0.128
	S1	272.417	225.922	340.194	307.647	769.2	706.2	672.075	0.442	0.482	0.506
	S9	384.213	92.867	412.074	208.131	1237.26	1114.26	1047.635	0.333	0.370	0.393
6	S2	24.780	342.966	127.670	350.400	1466.28	1327.68	1252.605	0.239	0.264	0.280
	S10	64.498	200.618	124.683	219.967	2133.06	1862.46	1715.885	0.103	0.118	0.128
	S3	2.015	328.482	100.560	329.086	1578.66	1427.46	1345.560	0.208	0.231	0.245
	S11	2.637	267.317	82.832	268.108	2310.588	2015.388	1855.488	0.116	0.133	0.144
	S4	46.675	338.712	148.288	352.715	1473.96	1330.704	1253.107	0.239	0.265	0.281
	S12	110.153	218.343	175.656	251.389	1820.958	1590.858	1466.221	0.138	0.158	0.171
	S1	346.394	279.821	430.341	383.739	897.4	823.9	784.525	0.480	0.522	0.549
6	S9	495.097	122.099	531.727	270.628	1443.47	1299.97	1223.095	0.368	0.409	0.435
	S2	30.431	439.113	162.165	448.243	1710.66	1548.96	1462.335	0.262	0.289	0.307
	S10	75.130	283.721	160.246	306.260	2488.57	2172.87	2003.745	0.123	0.141	0.153
	S3	2.720	422.868	129.581	423.684	1841.77	1665.37	1570.870	0.230	0.254	0.270

5	S11	2.749	381.209	117.112	382.034	2695.686	2351.286	2166.786	0.142	0.162	0.176
	S4	64.988	432.762	194.817	452.258	1719.62	1552.488	1462.953	0.263	0.291	0.309
	S12	137.395	308.157	229.842	349.375	2124.451	1856.001	1712.189	0.164	0.188	0.204
	S1	425.705	338.128	527.143	465.839	1025.6	941.6	902.225	0.514	0.560	0.584
	S9	616.846	169.777	667.779	354.831	1649.68	1485.68	1408.805	0.405	0.449	0.474
	S2	34.695	541.014	196.999	551.423	1955.04	1770.24	1683.615	0.282	0.311	0.328
	S10	90.912	376.625	203.900	403.899	2844.08	2483.28	2314.155	0.142	0.163	0.175
	S3	3.553	524.443	160.886	525.509	2104.88	1903.28	1808.780	0.250	0.276	0.291
	S11	2.622	500.613	152.806	501.400	3080.784	2687.184	2502.684	0.163	0.187	0.200
	S4	88.100	532.797	247.939	559.227	1965.28	1774.272	1684.737	0.285	0.315	0.332
	S12	166.828	408.176	289.281	458.225	2427.944	2121.144	1977.332	0.189	0.216	0.232
	S1	510.057	399.161	629.806	552.178	1153.8	1059.3	1025.175	0.546	0.595	0.614
4	S9	745.524	230.910	814.797	454.567	1855.89	1671.39	1604.765	0.439	0.487	0.508
	S2	37.253	646.910	231.326	658.086	2199.42	1991.52	1916.445	0.299	0.330	0.343
	S10	110.459	481.317	254.854	514.455	3199.59	2793.69	2647.115	0.161	0.184	0.194
	S3	4.758	631.992	194.355	633.419	2367.99	2141.19	2059.290	0.267	0.296	0.308
	S11	2.747	623.208	189.709	624.032	3465.882	3023.082	2863.182	0.180	0.206	0.218
	S4	115.631	636.358	306.538	671.047	2210.94	1996.056	1918.459	0.304	0.336	0.350
	S12	203.286	519.691	359.193	580.677	2731.437	2386.287	2261.650	0.213	0.243	0.257
	S1	604.972	467.702	745.282	649.193	1282	1177	1153.375	0.581	0.633	0.646
3	S9	880.423	299.006	970.124	563.133	2062.1	1857.1	1810.975	0.470	0.522	0.536
	S2	47.977	751.960	273.565	766.353	2443.8	2212.8	2160.825	0.314	0.346	0.355
	S10	135.554	591.852	313.110	632.518	3555.1	3104.1	3002.625	0.178	0.204	0.211
	S3	5.318	742.227	227.986	743.823	2631.1	2379.1	2322.400	0.283	0.313	0.320
	S11	2.588	752.308	228.281	753.084	3850.98	3358.98	3248.280	0.196	0.224	0.232
	S4	145.639	739.571	367.511	783.262	2456.6	2217.84	2164.119	0.319	0.353	0.362
	S12	240.662	638.005	432.063	710.203	3034.93	2651.43	2565.143	0.234	0.268	0.277
	S1	704.376	538.426	865.903	749.739	1410.2	1294.7	1281.575	0.614	0.669	0.676
2	S9	1014.669	370.527	1125.827	674.928	2268.31	2042.81	2017.185	0.496	0.551	0.558
	S2	64.612	852.671	320.413	872.054	2688.18	2434.08	2405.205	0.324	0.358	0.363
	S10	164.653	700.841	374.905	750.237	3910.61	3414.51	3358.135	0.192	0.220	0.223
	S3	5.600	847.480	259.844	849.160	2894.21	2617.01	2585.510	0.293	0.324	0.328
	S11	2.316	876.618	265.302	877.313	4236.078	3694.878	3633.378	0.207	0.237	0.241
	S4	177.935	839.161	429.683	892.541	2702.26	2439.624	2409.779	0.330	0.366	0.370
	S12	278.643	755.622	505.330	839.215	3338.423	2916.573	2868.636	0.251	0.288	0.293
	S1	784.544	591.597	962.023	826.961	1538.4	1412.4	1409.775	0.625	0.681	0.682
1	S9	1121.394	424.765	1248.824	761.183	2474.52	2228.52	2223.395	0.505	0.560	0.562
	S2	76.619	933.410	356.642	956.396	2932.56	2655.36	2649.585	0.326	0.360	0.361
	S10	188.211	786.552	424.177	843.016	4266.12	3724.92	3713.645	0.198	0.226	0.227
	S3	6.198	930.591	285.375	932.450	3157.32	2854.92	2848.620	0.295	0.327	0.327
	S11	2.312	972.205	293.974	972.898	4621.176	4030.776	4018.476	0.211	0.241	0.242
	S4	207.357	917.891	482.724	980.098	2947.92	2661.408	2655.439	0.332	0.368	0.369
	S12	310.129	846.444	564.063	939.483	3641.916	3181.716	3172.129	0.258	0.295	0.296

Çizelge B.29: 6 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.342	7.033	10.451	9.536	128.2	122.95	112.45	0.082	0.085	0.093
	S9	10.995	2.049	11.610	5.348	206.21	195.96	175.46	0.056	0.059	0.066
	S2	1.180	9.468	4.021	9.822	244.38	232.83	209.73	0.040	0.042	0.047
	S10	3.224	3.527	4.282	4.494	355.51	332.96	287.86	0.013	0.013	0.016
	S3	0.139	9.500	2.989	9.542	263.11	250.51	225.31	0.036	0.038	0.042
	S11	0.138	4.797	1.577	4.838	385.098	360.498	311.298	0.013	0.013	0.016
	S4	0.981	9.549	3.846	9.843	245.66	233.722	209.846	0.040	0.042	0.047
5	S12	2.698	3.769	3.828	4.578	303.493	284.318	245.968	0.015	0.016	0.019
	S1	29.667	23.383	36.682	32.283	256.4	245.9	230.15	0.143	0.149	0.159
	S9	38.667	10.350	41.772	21.950	412.42	391.92	361.17	0.101	0.107	0.116
	S2	5.909	30.866	15.169	32.639	488.76	465.66	431.01	0.067	0.070	0.076
	S10	12.658	16.386	17.574	20.183	711.02	665.92	598.27	0.028	0.030	0.034
	S3	0.141	30.978	9.435	31.021	526.22	501.02	463.22	0.059	0.062	0.067
	S11	0.097	21.735	6.618	21.765	770.196	720.996	647.196	0.028	0.030	0.034
4	S4	4.932	30.852	14.187	32.332	491.32	467.444	431.63	0.066	0.069	0.075
	S12	10.808	17.958	16.195	21.200	606.986	568.636	511.111	0.035	0.037	0.041
	S1	62.049	47.499	76.299	66.114	384.6	368.85	353.1	0.198	0.207	0.216
	S9	81.132	22.957	88.020	47.297	618.63	587.88	557.13	0.142	0.150	0.158
	S2	14.375	62.230	33.044	66.542	733.14	698.49	663.84	0.091	0.095	0.100
	S10	29.174	35.611	39.857	44.363	1066.53	998.88	931.23	0.042	0.044	0.048
	S3	0.106	62.532	18.865	62.564	789.33	751.53	713.73	0.079	0.083	0.088
3	S11	0.297	48.048	14.712	48.137	1155.294	1081.494	1007.694	0.042	0.045	0.048
	S4	10.938	62.089	29.564	65.370	736.98	701.166	665.352	0.089	0.093	0.098
	S12	23.525	39.321	35.321	46.378	910.479	852.954	795.429	0.051	0.054	0.058
	S1	100.404	74.842	122.856	104.963	512.8	491.8	481.3	0.240	0.250	0.255
	S9	133.804	38.016	145.208	78.157	824.84	783.84	763.34	0.176	0.185	0.190
	S2	24.673	101.763	55.202	109.165	977.52	931.32	908.22	0.112	0.117	0.120
	S10	46.258	65.927	66.036	79.805	1422.04	1331.84	1286.74	0.056	0.060	0.062
2	S3	0.222	100.305	30.313	100.371	1052.44	1002.04	976.84	0.095	0.100	0.103
	S11	0.396	88.621	26.982	88.739	1540.392	1441.992	1392.792	0.058	0.062	0.064
	S4	19.720	101.245	50.093	107.161	982.64	934.888	911.012	0.109	0.115	0.118
	S12	40.281	72.654	62.078	84.738	1213.972	1137.272	1098.922	0.070	0.075	0.077
	S1	142.136	103.195	173.095	145.836	641	614.75	609.5	0.270	0.282	0.284
	S9	192.919	54.016	209.123	111.891	1031.05	979.8	969.55	0.203	0.213	0.216
	S2	36.385	146.312	80.278	157.228	1221.9	1164.15	1152.6	0.129	0.135	0.136
1	S10	63.133	103.799	94.273	122.739	1777.55	1664.8	1642.25	0.069	0.074	0.075
	S3	0.219	141.301	42.609	141.367	1315.55	1252.55	1239.95	0.107	0.113	0.114
	S11	0.389	139.531	42.248	139.647	1925.49	1802.49	1777.89	0.073	0.077	0.079
	S4	31.132	145.549	74.796	154.888	1228.3	1168.61	1156.672	0.126	0.133	0.134
	S12	59.919	114.363	94.228	132.339	1517.465	1421.59	1402.415	0.087	0.093	0.094
	S1	179.432	128.305	217.923	182.134	769.2	737.7	737.7	0.283	0.295	0.295
	S9	249.690	67.586	269.966	142.493	1237.26	1175.76	1175.76	0.218	0.230	0.230
	S2	45.249	188.100	101.679	201.675	1466.28	1396.98	1396.98	0.138	0.144	0.144
	S10	77.301	144.467	120.641	167.657	2133.06	1997.76	1997.76	0.079	0.084	0.084
	S3	0.377	179.983	54.372	180.096	1578.66	1503.06	1503.06	0.114	0.120	0.120
	S11	0.287	192.395	58.006	192.481	2310.588	2162.988	2162.988	0.083	0.089	0.089
	S4	38.742	186.999	94.842	198.621	1473.96	1402.332	1402.332	0.135	0.142	0.142
	S12	79.392	158.916	127.067	182.734	1820.958	1705.908	1705.908	0.100	0.107	0.107

Çizelge B.30: 9 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	8.386	8.523	10.943	11.039	128.2	117.7	104.575	0.086	0.094	0.106
	S9	11.250	1.442	11.682	4.817	206.21	185.71	160.085	0.057	0.063	0.073
	S2	1.051	12.297	4.740	12.612	244.38	221.28	192.405	0.052	0.057	0.066
	S10	0.821	1.475	1.263	1.721	355.51	310.41	254.035	0.005	0.006	0.007
	S3	0.512	12.104	4.143	12.258	263.11	237.91	206.41	0.047	0.052	0.059
	S11	0.535	2.588	1.311	2.748	385.098	335.898	274.398	0.007	0.008	0.010
	S4	0.273	12.273	3.955	12.355	245.66	221.784	191.939	0.050	0.056	0.064
8	S12	1.835	1.443	2.268	1.994	303.493	265.143	217.2055	0.007	0.009	0.010
	S1	31.175	27.848	39.529	37.200	256.4	235.4	211.775	0.154	0.168	0.187
	S9	41.048	9.948	44.032	22.262	412.42	371.42	325.295	0.107	0.119	0.135
	S2	1.174	38.595	12.753	38.947	488.76	442.56	390.585	0.080	0.088	0.100
	S10	7.820	13.318	11.815	15.664	711.02	620.82	519.345	0.022	0.025	0.030
	S3	0.779	38.231	12.248	38.464	526.22	475.82	419.12	0.073	0.081	0.092
	S11	0.761	18.643	6.353	18.871	770.196	671.796	561.096	0.025	0.028	0.034
7	S4	3.853	38.295	15.342	39.451	491.32	443.568	389.847	0.080	0.089	0.101
	S12	9.712	14.443	14.045	17.356	606.986	530.286	443.9985	0.029	0.033	0.039
	S1	66.728	56.134	83.568	76.152	384.6	353.1	318.975	0.217	0.237	0.262
	S9	87.904	23.470	94.945	49.842	618.63	557.13	490.505	0.153	0.170	0.194
	S2	7.746	76.377	30.659	78.701	733.14	663.84	588.765	0.107	0.119	0.134
	S10	23.038	32.480	32.782	39.391	1066.53	931.23	784.655	0.037	0.042	0.050
	S3	0.778	75.974	23.570	76.208	789.33	713.73	631.83	0.097	0.107	0.121
6	S11	0.601	45.450	14.235	45.630	1155.294	1007.694	847.794	0.039	0.045	0.054
	S4	9.823	75.747	32.547	78.694	736.98	665.352	587.755	0.107	0.118	0.134
	S12	22.885	35.706	33.596	42.571	910.479	795.429	670.7915	0.047	0.054	0.063
	S1	110.023	88.804	136.664	121.811	512.8	470.8	418.3	0.267	0.290	0.327
	S9	147.750	40.212	159.813	84.537	824.84	742.84	640.34	0.194	0.215	0.250
	S2	16.623	124.748	54.047	129.734	977.52	885.12	769.62	0.133	0.147	0.169
	S10	39.068	65.237	58.639	76.957	1422.04	1241.64	1016.14	0.054	0.062	0.076
5	S3	0.928	121.892	37.496	122.170	1052.44	951.64	825.64	0.116	0.128	0.148
	S11	0.739	89.819	27.684	90.040	1540.392	1343.592	1097.592	0.058	0.067	0.082
	S4	19.237	123.458	56.275	129.229	982.64	887.136	767.756	0.132	0.146	0.168
	S12	41.081	71.621	62.567	83.945	1213.972	1060.572	868.822	0.069	0.079	0.097
	S1	159.576	124.388	196.892	172.261	641	588.5	525.5	0.307	0.335	0.375
	S9	218.195	59.070	235.916	124.528	1031.05	928.55	805.55	0.229	0.254	0.293
	S2	27.857	181.721	82.373	190.078	1221.9	1106.4	967.8	0.156	0.172	0.196
4	S10	55.716	108.443	88.249	125.158	1777.55	1552.05	1281.45	0.070	0.081	0.098
	S3	1.239	173.941	53.422	174.313	1315.55	1189.55	1038.35	0.133	0.147	0.168
	S11	0.950	148.754	45.577	149.040	1925.49	1679.49	1384.29	0.077	0.089	0.108
	S4	32.506	179.717	86.421	189.469	1228.3	1108.92	965.664	0.154	0.171	0.196
	S12	63.409	118.954	99.095	137.976	1517.465	1325.715	1095.615	0.091	0.104	0.126
	S1	212.067	162.273	260.749	225.893	769.2	706.2	648.45	0.339	0.369	0.402
	S9	297.377	80.142	321.419	169.355	1237.26	1114.26	1001.51	0.260	0.288	0.321
3	S2	37.577	244.361	110.885	255.634	1466.28	1327.68	1200.63	0.174	0.193	0.213
	S10	72.297	167.163	122.446	188.852	2133.06	1862.46	1614.41	0.089	0.101	0.117
	S3	1.298	231.958	70.886	232.347	1578.66	1427.46	1288.86	0.147	0.163	0.180
	S11	1.293	221.828	67.841	222.215	2310.588	2015.388	1744.788	0.096	0.110	0.127
	S4	42.728	241.499	115.178	254.317	1473.96	1330.704	1199.386	0.173	0.191	0.212
	S12	90.290	183.038	145.201	210.125	1820.958	1590.858	1379.933	0.115	0.132	0.152
	S1	267.108	199.947	327.092	280.079	897.4	823.9	776.65	0.364	0.397	0.421
3	S9	379.674	103.326	410.672	217.228	1443.47	1299.97	1207.72	0.285	0.316	0.340
	S2	45.237	311.303	138.628	324.874	1710.66	1548.96	1445.01	0.190	0.210	0.225
	S10	84.943	230.486	154.089	255.969	2488.57	2172.87	1969.92	0.103	0.118	0.130
	S3	1.817	297.260	90.995	297.805	1841.77	1665.37	1551.97	0.162	0.179	0.192

2	S11	1.395	308.028	93.804	308.447	2695.686	2351.286	2129.886	0.114	0.131	0.145
	S4	57.237	307.087	149.363	324.258	1719.62	1552.488	1445.046	0.189	0.209	0.224
	S12	111.861	251.831	187.410	285.390	2124.451	1856.001	1683.426	0.134	0.154	0.170
	S1	323.394	238.427	394.922	335.445	1025.6	941.6	904.85	0.385	0.419	0.436
	S9	465.665	137.220	506.831	276.920	1649.68	1485.68	1413.93	0.307	0.341	0.358
	S2	51.712	378.577	165.285	394.090	1955.04	1770.24	1689.39	0.202	0.223	0.233
	S10	100.590	296.340	189.492	326.517	2844.08	2483.28	2325.43	0.115	0.131	0.140
	S3	2.484	364.403	111.805	365.148	2104.88	1903.28	1815.08	0.173	0.192	0.201
	S11	1.300	394.213	119.564	394.603	3080.784	2687.184	2514.984	0.128	0.147	0.157
	S4	74.789	373.522	186.846	395.959	1965.28	1774.272	1690.706	0.201	0.223	0.234
	S12	133.601	323.509	230.654	363.589	2427.944	2121.144	1986.919	0.150	0.171	0.183
1	S1	371.501	270.727	452.719	382.177	1153.8	1059.3	1033.05	0.392	0.427	0.438
	S9	541.782	171.710	593.295	334.245	1855.89	1671.39	1620.14	0.320	0.355	0.366
	S2	55.307	435.783	186.042	452.376	2199.42	1991.52	1933.77	0.206	0.227	0.234
	S10	115.459	357.559	222.726	392.196	3199.59	2793.69	2680.94	0.123	0.140	0.146
	S3	3.216	421.770	129.747	422.735	2367.99	2141.19	2078.19	0.179	0.197	0.203
	S11	1.407	466.706	141.419	467.128	3465.882	3023.082	2900.082	0.135	0.155	0.161
	S4	89.996	429.826	218.944	456.825	2210.94	1996.056	1936.366	0.207	0.229	0.236
	S12	155.910	389.492	272.758	436.265	2731.437	2386.287	2290.412	0.160	0.183	0.190

Çizelge B.31: 12 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	8.406	10.597	11.585	13.118	128.2	117.7	117.700	0.102	0.111	0.111
	S9	11.424	0.077	11.447	3.504	206.21	185.71	185.710	0.056	0.062	0.062
	S2	3.778	15.556	8.445	16.690	244.38	221.28	221.280	0.068	0.075	0.075
	S10	2.249	1.147	2.593	1.822	355.51	310.41	310.410	0.007	0.008	0.008
	S3	0.707	15.651	5.402	15.863	263.11	237.91	237.910	0.060	0.067	0.067
	S11	0.895	0.548	1.060	0.816	385.098	335.898	335.898	0.003	0.003	0.003
	S4	1.004	15.517	5.659	15.818	245.66	221.784	221.784	0.064	0.071	0.071
11	S12	0.789	1.588	1.266	1.825	303.493	265.143	265.143	0.006	0.007	0.007
	S1	32.456	33.518	42.511	43.254	256.4	235.4	235.400	0.169	0.184	0.184
	S9	43.021	7.550	45.286	20.456	412.42	371.42	371.420	0.110	0.122	0.122
	S2	4.825	47.198	18.984	48.645	488.76	442.56	442.560	0.100	0.110	0.110
	S10	1.301	8.978	3.994	9.369	711.02	620.82	620.820	0.013	0.015	0.015
	S3	1.004	47.450	15.239	47.752	526.22	475.82	475.820	0.091	0.100	0.100
	S11	1.276	13.495	5.324	13.877	770.196	671.796	671.796	0.018	0.021	0.021
10	S4	1.589	46.799	15.629	47.276	491.32	443.568	443.568	0.096	0.107	0.107
	S12	8.234	9.378	11.048	11.848	606.986	530.286	530.286	0.020	0.022	0.022
	S1	70.154	66.008	89.956	87.054	384.6	353.1	353.100	0.234	0.255	0.255
	S9	92.843	20.566	99.013	48.419	618.63	557.13	557.130	0.160	0.178	0.178
	S2	1.169	91.068	28.490	91.419	733.14	663.84	663.840	0.125	0.138	0.138
	S10	13.719	26.901	21.790	31.017	1066.53	931.23	931.230	0.029	0.033	0.033
	S3	1.027	91.641	28.519	91.949	789.33	713.73	713.730	0.116	0.129	0.129
9	S11	1.270	38.943	12.952	39.323	1155.294	1007.694	1007.694	0.034	0.039	0.039
	S4	6.744	90.245	33.818	92.269	736.98	665.352	665.352	0.125	0.139	0.139
	S12	21.322	29.158	30.069	35.555	910.479	795.429	795.429	0.039	0.045	0.045
	S1	116.220	103.296	147.208	138.161	512.8	470.8	457.675	0.287	0.313	0.322
	S9	156.763	37.006	167.865	84.035	824.84	742.84	717.215	0.204	0.226	0.234
	S2	4.904	146.727	48.922	148.198	977.52	885.12	856.245	0.152	0.167	0.173
	S10	26.633	59.662	44.531	67.652	1422.04	1241.64	1185.265	0.048	0.054	0.057
8	S3	1.213	144.869	44.674	145.233	1052.44	951.64	920.140	0.138	0.153	0.158
	S11	1.520	83.593	26.598	84.049	1540.392	1343.592	1282.092	0.055	0.063	0.066
	S4	15.684	145.107	59.216	149.812	982.64	887.136	857.291	0.152	0.169	0.175
	S12	39.820	64.892	59.287	76.838	1213.972	1060.572	1012.635	0.063	0.072	0.076
	S1	169.577	144.139	212.819	195.012	641	588.5	564.875	0.332	0.362	0.377
	S9	232.928	55.825	249.675	125.704	1031.05	928.55	882.425	0.242	0.269	0.283
	S2	13.650	212.510	77.403	216.605	1221.9	1106.4	1054.425	0.177	0.196	0.205
7	S10	40.176	104.141	71.418	116.194	1777.55	1552.05	1450.575	0.065	0.075	0.080
	S3	1.577	205.394	63.195	205.867	1315.55	1189.55	1132.850	0.156	0.173	0.182
	S11	1.799	144.677	45.202	145.216	1925.49	1679.49	1568.790	0.075	0.086	0.093
	S4	29.040	210.025	92.047	218.737	1228.3	1108.92	1055.199	0.178	0.197	0.207
	S12	63.006	113.411	97.029	132.313	1517.465	1325.715	1239.428	0.087	0.100	0.107
	S1	226.931	188.199	283.390	256.278	769.2	706.2	672.075	0.368	0.401	0.422
	S9	320.060	77.361	343.268	173.379	1237.26	1114.26	1047.635	0.277	0.308	0.328
6	S2	20.643	285.699	106.352	291.892	1466.28	1327.68	1252.605	0.199	0.220	0.233
	S10	53.728	167.120	103.864	183.238	2133.06	1862.46	1715.885	0.086	0.098	0.107
	S3	1.679	273.634	83.769	274.137	1578.66	1427.46	1345.560	0.174	0.192	0.204
	S11	2.196	222.682	69.001	223.341	2310.588	2015.388	1855.488	0.097	0.111	0.120
	S4	38.881	282.156	123.528	293.820	1473.96	1330.704	1253.107	0.199	0.221	0.234
	S12	91.760	181.885	146.326	209.413	1820.958	1590.858	1466.221	0.115	0.132	0.143
	S1	288.555	233.098	358.485	319.665	897.4	823.9	784.525	0.399	0.435	0.457
6	S9	412.428	101.712	442.942	225.440	1443.47	1299.97	1223.095	0.307	0.341	0.362
	S2	25.350	365.793	135.087	373.397	1710.66	1548.96	1462.335	0.218	0.241	0.255
	S10	62.585	236.347	133.489	255.123	2488.57	2172.87	2003.745	0.103	0.117	0.127
	S3	2.266	352.259	107.944	352.939	1841.77	1665.37	1570.870	0.192	0.212	0.225

5	S11	2.290	317.557	97.557	318.244	2695.686	2351.286	2166.786	0.118	0.135	0.147
	S4	54.137	360.501	162.287	376.742	1719.62	1552.488	1462.953	0.219	0.243	0.258
	S12	114.454	256.702	191.464	291.038	2124.451	1856.001	1712.189	0.137	0.157	0.170
	S1	354.623	281.669	439.124	388.056	1025.6	941.6	902.225	0.428	0.466	0.487
	S9	513.848	141.428	556.277	295.583	1649.68	1485.68	1408.805	0.337	0.374	0.395
	S2	28.902	450.679	164.105	459.349	1955.04	1770.24	1683.615	0.235	0.259	0.273
	S10	75.732	313.738	169.854	336.458	2844.08	2483.28	2314.155	0.118	0.135	0.145
	S3	2.960	436.874	134.022	437.762	2104.88	1903.28	1808.780	0.208	0.230	0.242
	S11	2.184	417.023	127.291	417.679	3080.784	2687.184	2502.684	0.136	0.155	0.167
	S4	73.390	443.833	206.540	465.850	1965.28	1774.272	1684.737	0.237	0.263	0.277
	S12	138.972	340.021	240.978	381.713	2427.944	2121.144	1977.332	0.157	0.180	0.193
4	S1	424.891	332.511	524.644	459.978	1153.8	1059.3	1025.175	0.455	0.495	0.512
	S9	621.040	192.353	678.746	378.665	1855.89	1671.39	1604.765	0.366	0.406	0.423
	S2	31.033	538.892	192.701	548.202	2199.42	1991.52	1916.445	0.249	0.275	0.286
	S10	92.015	400.949	212.300	428.554	3199.59	2793.69	2647.115	0.134	0.153	0.162
	S3	3.963	526.465	161.903	527.654	2367.99	2141.19	2059.290	0.223	0.246	0.256
	S11	2.288	519.148	158.033	519.834	3465.882	3023.082	2863.182	0.150	0.172	0.182
	S4	96.323	530.102	255.354	558.999	2210.94	1996.056	1918.459	0.253	0.280	0.291
	S12	169.342	432.916	299.217	483.718	2731.437	2386.287	2261.650	0.177	0.203	0.214
3	S1	503.957	389.607	620.839	540.794	1282	1177	1153.375	0.484	0.527	0.538
	S9	733.414	249.079	808.138	469.104	2062.1	1857.1	1810.975	0.392	0.435	0.446
	S2	39.966	626.402	227.887	638.392	2443.8	2212.8	2160.825	0.261	0.288	0.295
	S10	112.920	493.027	260.828	526.903	3555.1	3104.1	3002.625	0.148	0.170	0.175
	S3	4.430	618.294	189.918	619.623	2631.1	2379.1	2322.400	0.235	0.260	0.267
	S11	2.156	626.691	190.164	627.338	3850.98	3358.98	3248.280	0.163	0.187	0.193
	S4	121.321	616.081	306.146	652.477	2456.6	2217.84	2164.119	0.266	0.294	0.301
	S12	200.477	531.474	359.920	591.617	3034.93	2651.43	2565.143	0.195	0.223	0.231
2	S1	586.763	448.522	721.319	624.551	1410.2	1294.7	1281.575	0.512	0.557	0.563
	S9	845.245	308.658	937.843	562.232	2268.31	2042.81	2017.185	0.413	0.459	0.465
	S2	53.823	710.296	266.912	726.443	2688.18	2434.08	2405.205	0.270	0.298	0.302
	S10	137.160	583.818	312.305	624.966	3910.61	3414.51	3358.135	0.160	0.183	0.186
	S3	4.665	705.972	216.457	707.372	2894.21	2617.01	2585.510	0.244	0.270	0.274
	S11	1.929	730.245	221.003	730.824	4236.078	3694.878	3633.378	0.173	0.198	0.201
	S4	148.224	699.042	357.937	743.509	2702.26	2439.624	2409.779	0.275	0.305	0.309
	S12	232.117	629.452	420.952	699.087	3338.423	2916.573	2868.636	0.209	0.240	0.244
1	S1	653.545	492.816	801.390	688.879	1538.4	1412.4	1409.775	0.521	0.567	0.568
	S9	934.150	353.840	1040.302	634.085	2474.52	2228.52	2223.395	0.420	0.467	0.468
	S2	63.825	777.554	297.092	796.702	2932.56	2655.36	2649.585	0.272	0.300	0.301
	S10	156.785	655.218	353.350	702.253	4266.12	3724.92	3713.645	0.165	0.189	0.189
	S3	5.163	775.206	237.725	776.754	3157.32	2854.92	2848.620	0.246	0.272	0.273
	S11	1.926	809.871	244.888	810.449	4621.176	4030.776	4018.476	0.175	0.201	0.202
	S4	172.734	764.627	402.121	816.447	2947.92	2661.408	2655.439	0.277	0.307	0.307
	S12	258.346	705.110	469.878	782.613	3641.916	3181.716	3172.129	0.215	0.246	0.247

Çizelge B.32: 6 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.342	7.033	10.451	9.536	128.2	122.95	112.45	0.092	0.096	0.105
	S9	10.995	2.049	11.610	5.348	206.21	195.96	175.46	0.063	0.067	0.074
	S2	1.180	9.468	4.021	9.822	244.38	232.83	209.73	0.045	0.047	0.053
	S10	3.224	3.527	4.282	4.494	355.51	332.96	287.86	0.014	0.015	0.018
	S3	0.139	9.500	2.989	9.542	263.11	250.51	225.31	0.041	0.043	0.048
	S11	0.138	4.797	1.577	4.838	385.098	360.498	311.298	0.014	0.015	0.017
	S4	0.981	9.549	3.846	9.843	245.66	233.722	209.846	0.045	0.047	0.053
5	S12	2.698	3.769	3.828	4.578	303.493	284.318	245.968	0.017	0.018	0.021
	S1	29.667	23.383	36.682	32.283	256.4	245.9	230.15	0.161	0.168	0.179
	S9	38.667	10.350	41.772	21.950	412.42	391.92	361.17	0.114	0.120	0.130
	S2	5.909	30.866	15.169	32.639	488.76	465.66	431.01	0.075	0.079	0.085
	S10	12.658	16.386	17.574	20.183	711.02	665.92	598.27	0.032	0.034	0.038
	S3	0.141	30.978	9.435	31.021	526.22	501.02	463.22	0.066	0.070	0.075
	S11	0.097	21.735	6.618	21.765	770.196	720.996	647.196	0.032	0.034	0.038
4	S4	4.932	30.852	14.187	32.332	491.32	467.444	431.63	0.074	0.078	0.084
	S12	10.808	17.958	16.195	21.200	606.986	568.636	511.111	0.039	0.042	0.047
	S1	62.049	47.499	76.299	66.114	384.6	368.85	353.1	0.223	0.233	0.243
	S9	81.132	22.957	88.020	47.297	618.63	587.88	557.13	0.160	0.168	0.178
	S2	14.375	62.230	33.044	66.542	733.14	698.49	663.84	0.102	0.107	0.113
	S10	29.174	35.611	39.857	44.363	1066.53	998.88	931.23	0.047	0.050	0.054
	S3	0.106	62.532	18.865	62.564	789.33	751.53	713.73	0.089	0.094	0.099
3	S11	0.297	48.048	14.712	48.137	1155.294	1081.494	1007.694	0.047	0.050	0.054
	S4	10.938	62.089	29.564	65.370	736.98	701.166	665.352	0.100	0.105	0.111
	S12	23.525	39.321	35.321	46.378	910.479	852.954	795.429	0.057	0.061	0.066
	S1	100.404	74.842	122.856	104.963	512.8	491.8	481.3	0.270	0.281	0.287
	S9	133.804	38.016	145.208	78.157	824.84	783.84	763.34	0.198	0.208	0.214
	S2	24.673	101.763	55.202	109.165	977.52	931.32	908.22	0.126	0.132	0.135
	S10	46.258	65.927	66.036	79.805	1422.04	1331.84	1286.74	0.063	0.067	0.070
2	S3	0.222	100.305	30.313	100.371	1052.44	1002.04	976.84	0.107	0.113	0.116
	S11	0.396	88.621	26.982	88.739	1540.392	1441.992	1392.792	0.065	0.069	0.072
	S4	19.720	101.245	50.093	107.161	982.64	934.888	911.012	0.123	0.129	0.132
	S12	40.281	72.654	62.078	84.738	1213.972	1137.272	1098.922	0.079	0.084	0.087
	S1	142.136	103.195	173.095	145.836	641	614.75	609.5	0.304	0.317	0.319
	S9	192.919	54.016	209.123	111.891	1031.05	979.8	969.55	0.228	0.240	0.243
	S2	36.385	146.312	80.278	157.228	1221.9	1164.15	1152.6	0.145	0.152	0.153
1	S10	63.133	103.799	94.273	122.739	1777.55	1664.8	1642.25	0.078	0.083	0.084
	S3	0.219	141.301	42.609	141.367	1315.55	1252.55	1239.95	0.121	0.127	0.128
	S11	0.389	139.531	42.248	139.647	1925.49	1802.49	1777.89	0.082	0.087	0.088
	S4	31.132	145.549	74.796	154.888	1228.3	1168.61	1156.672	0.142	0.149	0.151
	S12	59.919	114.363	94.228	132.339	1517.465	1421.59	1402.415	0.098	0.105	0.106
	S1	179.432	128.305	217.923	182.134	769.2	737.7	737.7	0.319	0.332	0.332
	S9	249.690	67.586	269.966	142.493	1237.26	1175.76	1175.76	0.245	0.258	0.258
	S2	45.249	188.100	101.679	201.675	1466.28	1396.98	1396.98	0.155	0.162	0.162
	S10	77.301	144.467	120.641	167.657	2133.06	1997.76	1997.76	0.088	0.094	0.094
	S3	0.377	179.983	54.372	180.096	1578.66	1503.06	1503.06	0.128	0.135	0.135
	S11	0.287	192.395	58.006	192.481	2310.588	2162.988	2162.988	0.094	0.100	0.100
	S4	38.742	186.999	94.842	198.621	1473.96	1402.332	1402.332	0.152	0.159	0.159
	S12	79.392	158.916	127.067	182.734	1820.958	1705.908	1705.908	0.113	0.121	0.121

Çizelge B.33: 9 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	8.386	8.523	10.943	11.039	128.2	117.7	104.575	0.097	0.106	0.119
	S9	11.250	1.442	11.682	4.817	206.21	185.71	160.085	0.064	0.071	0.082
	S2	1.051	12.297	4.740	12.612	244.38	221.28	192.405	0.058	0.064	0.074
	S10	0.821	1.475	1.263	1.721	355.51	310.41	254.035	0.005	0.006	0.008
	S3	0.512	12.104	4.143	12.258	263.11	237.91	206.41	0.052	0.058	0.067
	S11	0.535	2.588	1.311	2.748	385.098	335.898	274.398	0.008	0.009	0.011
	S4	0.273	12.273	3.955	12.355	245.66	221.784	191.939	0.057	0.063	0.072
8	S12	1.835	1.443	2.268	1.994	303.493	265.143	217.2055	0.008	0.010	0.012
	S1	31.175	27.848	39.529	37.200	256.4	235.4	211.775	0.173	0.189	0.210
	S9	41.048	9.948	44.032	22.262	412.42	371.42	325.295	0.120	0.133	0.152
	S2	1.174	38.595	12.753	38.947	488.76	442.56	390.585	0.090	0.099	0.112
	S10	7.820	13.318	11.815	15.664	711.02	620.82	519.345	0.025	0.028	0.034
	S3	0.779	38.231	12.248	38.464	526.22	475.82	419.12	0.082	0.091	0.103
	S11	0.761	18.643	6.353	18.871	770.196	671.796	561.096	0.028	0.032	0.038
7	S4	3.853	38.295	15.342	39.451	491.32	443.568	389.847	0.090	0.100	0.114
	S12	9.712	14.443	14.045	17.356	606.986	530.286	443.9985	0.032	0.037	0.044
	S1	66.728	56.134	83.568	76.152	384.6	353.1	318.975	0.244	0.266	0.295
	S9	87.904	23.470	94.945	49.842	618.63	557.13	490.505	0.173	0.192	0.218
	S2	7.746	76.377	30.659	78.701	733.14	663.84	588.765	0.121	0.133	0.150
	S10	23.038	32.480	32.782	39.391	1066.53	931.23	784.655	0.042	0.048	0.056
	S3	0.778	75.974	23.570	76.208	789.33	713.73	631.83	0.109	0.120	0.136
6	S11	0.601	45.450	14.235	45.630	1155.294	1007.694	847.794	0.044	0.051	0.061
	S4	9.823	75.747	32.547	78.694	736.98	665.352	587.755	0.120	0.133	0.151
	S12	22.885	35.706	33.596	42.571	910.479	795.429	670.7915	0.053	0.060	0.071
	S1	110.023	88.804	136.664	121.811	512.8	470.8	418.3	0.300	0.327	0.368
	S9	147.750	40.212	159.813	84.537	824.84	742.84	640.34	0.218	0.242	0.281
	S2	16.623	124.748	54.047	129.734	977.52	885.12	769.62	0.149	0.165	0.190
	S10	39.068	65.237	58.639	76.957	1422.04	1241.64	1016.14	0.061	0.070	0.085
5	S3	0.928	121.892	37.496	122.170	1052.44	951.64	825.64	0.131	0.144	0.166
	S11	0.739	89.819	27.684	90.040	1540.392	1343.592	1097.592	0.066	0.075	0.092
	S4	19.237	123.458	56.275	129.229	982.64	887.136	767.756	0.148	0.164	0.189
	S12	41.081	71.621	62.567	83.945	1213.972	1060.572	868.822	0.078	0.089	0.109
	S1	159.576	124.388	196.892	172.261	641	588.5	525.5	0.346	0.376	0.422
	S9	218.195	59.070	235.916	124.528	1031.05	928.55	805.55	0.257	0.286	0.329
	S2	27.857	181.721	82.373	190.078	1221.9	1106.4	967.8	0.175	0.193	0.221
4	S10	55.716	108.443	88.249	125.158	1777.55	1552.05	1281.45	0.079	0.091	0.110
	S3	1.239	173.941	53.422	174.313	1315.55	1189.55	1038.35	0.149	0.165	0.189
	S11	0.950	148.754	45.577	149.040	1925.49	1679.49	1384.29	0.087	0.100	0.121
	S4	32.506	179.717	86.421	189.469	1228.3	1108.92	965.664	0.174	0.192	0.221
	S12	63.409	118.954	99.095	137.976	1517.465	1325.715	1095.615	0.102	0.117	0.142
	S1	212.067	162.273	260.749	225.893	769.2	706.2	648.45	0.381	0.415	0.452
	S9	297.377	80.142	321.419	169.355	1237.26	1114.26	1001.51	0.292	0.325	0.361
3	S2	37.577	244.361	110.885	255.634	1466.28	1327.68	1200.63	0.196	0.217	0.240
	S10	72.297	167.163	122.446	188.852	2133.06	1862.46	1614.41	0.100	0.114	0.132
	S3	1.298	231.958	70.886	232.347	1578.66	1427.46	1288.86	0.166	0.183	0.203
	S11	1.293	221.828	67.841	222.215	2310.588	2015.388	1744.788	0.108	0.124	0.143
	S4	42.728	241.499	115.178	254.317	1473.96	1330.704	1199.386	0.194	0.215	0.239
	S12	90.290	183.038	145.201	210.125	1820.958	1590.858	1379.933	0.130	0.149	0.171
	S1	267.108	199.947	327.092	280.079	897.4	823.9	776.65	0.410	0.447	0.474
2	S9	379.674	103.326	410.672	217.228	1443.47	1299.97	1207.72	0.320	0.355	0.383
	S2	45.237	311.303	138.628	324.874	1710.66	1548.96	1445.01	0.214	0.236	0.253
	S10	84.943	230.486	154.089	255.969	2488.57	2172.87	1969.92	0.116	0.133	0.146
	S3	1.817	297.260	90.995	297.805	1841.77	1665.37	1551.97	0.182	0.201	0.216

2	S11	1.395	308.028	93.804	308.447	2695.686	2351.286	2129.886	0.129	0.148	0.163
	S4	57.237	307.087	149.363	324.258	1719.62	1552.488	1445.046	0.212	0.235	0.252
	S12	111.861	251.831	187.410	285.390	2124.451	1856.001	1683.426	0.151	0.173	0.191
	S1	323.394	238.427	394.922	335.445	1025.6	941.6	904.85	0.433	0.472	0.491
	S9	465.665	137.220	506.831	276.920	1649.68	1485.68	1413.93	0.346	0.384	0.403
	S2	51.712	378.577	165.285	394.090	1955.04	1770.24	1689.39	0.227	0.250	0.262
	S10	100.590	296.340	189.492	326.517	2844.08	2483.28	2325.43	0.129	0.148	0.158
	S3	2.484	364.403	111.805	365.148	2104.88	1903.28	1815.08	0.195	0.216	0.226
	S11	1.300	394.213	119.564	394.603	3080.784	2687.184	2514.984	0.144	0.165	0.177
	S4	74.789	373.522	186.846	395.959	1965.28	1774.272	1690.706	0.227	0.251	0.263
	S12	133.601	323.509	230.654	363.589	2427.944	2121.144	1986.919	0.168	0.193	0.206
	S1	371.501	270.727	452.719	382.177	1153.8	1059.3	1033.05	0.441	0.481	0.493
1	S9	541.782	171.710	593.295	334.245	1855.89	1671.39	1620.14	0.360	0.399	0.412
	S2	55.307	435.783	186.042	452.376	2199.42	1991.52	1933.77	0.231	0.256	0.263
	S10	115.459	357.559	222.726	392.196	3199.59	2793.69	2680.94	0.138	0.158	0.165
	S3	3.216	421.770	129.747	422.735	2367.99	2141.19	2078.19	0.201	0.222	0.229
	S11	1.407	466.706	141.419	467.128	3465.882	3023.082	2900.082	0.152	0.174	0.181
	S4	89.996	429.826	218.944	456.825	2210.94	1996.056	1936.366	0.232	0.257	0.265
	S12	155.910	389.492	272.758	436.265	2731.437	2386.287	2290.412	0.180	0.206	0.214

Çizelge B.34: 12 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	8.406	10.597	11.585	13.118	128.2	117.7	117.700	0.115	0.125	0.125
	S9	11.424	0.077	11.447	3.504	206.21	185.71	185.710	0.062	0.069	0.069
	S2	3.778	15.556	8.445	16.690	244.38	221.28	221.280	0.077	0.085	0.085
	S10	2.249	1.147	2.593	1.822	355.51	310.41	310.410	0.008	0.009	0.009
	S3	0.707	15.651	5.402	15.863	263.11	237.91	237.910	0.068	0.075	0.075
	S11	0.895	0.548	1.060	0.816	385.098	335.898	335.898	0.003	0.004	0.004
	S4	1.004	15.517	5.659	15.818	245.66	221.784	221.784	0.072	0.080	0.080
11	S12	0.789	1.588	1.266	1.825	303.493	265.143	265.143	0.007	0.008	0.008
	S1	32.456	33.518	42.511	43.254	256.4	235.4	235.400	0.190	0.207	0.207
	S9	43.021	7.550	45.286	20.456	412.42	371.42	371.420	0.124	0.137	0.137
	S2	4.825	47.198	18.984	48.645	488.76	442.56	442.560	0.112	0.124	0.124
	S10	1.301	8.978	3.994	9.369	711.02	620.82	620.820	0.015	0.017	0.017
	S3	1.004	47.450	15.239	47.752	526.22	475.82	475.820	0.102	0.113	0.113
	S11	1.276	13.495	5.324	13.877	770.196	671.796	671.796	0.020	0.023	0.023
10	S4	1.589	46.799	15.629	47.276	491.32	443.568	443.568	0.108	0.120	0.120
	S12	8.234	9.378	11.048	11.848	606.986	530.286	530.286	0.022	0.025	0.025
	S1	70.154	66.008	89.956	87.054	384.6	353.1	353.100	0.263	0.287	0.287
	S9	92.843	20.566	99.013	48.419	618.63	557.13	557.130	0.180	0.200	0.200
	S2	1.169	91.068	28.490	91.419	733.14	663.84	663.840	0.140	0.155	0.155
	S10	13.719	26.901	21.790	31.017	1066.53	931.23	931.230	0.033	0.037	0.037
	S3	1.027	91.641	28.519	91.949	789.33	713.73	713.730	0.131	0.145	0.145
9	S11	1.270	38.943	12.952	39.323	1155.294	1007.694	1007.694	0.038	0.044	0.044
	S4	6.744	90.245	33.818	92.269	736.98	665.352	665.352	0.141	0.156	0.156
	S12	21.322	29.158	30.069	35.555	910.479	795.429	795.429	0.044	0.050	0.050
	S1	116.220	103.296	147.208	138.161	512.8	470.8	457.675	0.323	0.352	0.362
	S9	156.763	37.006	167.865	84.035	824.84	742.84	717.215	0.229	0.254	0.263
	S2	4.904	146.727	48.922	148.198	977.52	885.12	856.245	0.171	0.188	0.195
	S10	26.633	59.662	44.531	67.652	1422.04	1241.64	1185.265	0.054	0.061	0.064
8	S3	1.213	144.869	44.674	145.233	1052.44	951.64	920.140	0.155	0.172	0.178
	S11	1.520	83.593	26.598	84.049	1540.392	1343.592	1282.092	0.061	0.070	0.074
	S4	15.684	145.107	59.216	149.812	982.64	887.136	857.291	0.172	0.190	0.197
	S12	39.820	64.892	59.287	76.838	1213.972	1060.572	1012.635	0.071	0.082	0.085
	S1	169.577	144.139	212.819	195.012	641	588.5	564.875	0.374	0.407	0.424
	S9	232.928	55.825	249.675	125.704	1031.05	928.55	882.425	0.272	0.302	0.318
	S2	13.650	212.510	77.403	216.605	1221.9	1106.4	1054.425	0.199	0.220	0.231
7	S10	40.176	104.141	71.418	116.194	1777.55	1552.05	1450.575	0.074	0.084	0.090
	S3	1.577	205.394	63.195	205.867	1315.55	1189.55	1132.850	0.176	0.195	0.204
	S11	1.799	144.677	45.202	145.216	1925.49	1679.49	1568.790	0.085	0.097	0.104
	S4	29.040	210.025	92.047	218.737	1228.3	1108.92	1055.199	0.200	0.222	0.233
	S12	63.006	113.411	97.029	132.313	1517.465	1325.715	1239.428	0.098	0.112	0.120
	S1	226.931	188.199	283.390	256.278	769.2	706.2	672.075	0.414	0.451	0.474
	S9	320.060	77.361	343.268	173.379	1237.26	1114.26	1047.635	0.312	0.347	0.369
6	S2	20.643	285.699	106.352	291.892	1466.28	1327.68	1252.605	0.224	0.247	0.262
	S10	53.728	167.120	103.864	183.238	2133.06	1862.46	1715.885	0.097	0.111	0.120
	S3	1.679	273.634	83.769	274.137	1578.66	1427.46	1345.560	0.195	0.216	0.229
	S11	2.196	222.682	69.001	223.341	2310.588	2015.388	1855.488	0.109	0.125	0.135
	S4	38.881	282.156	123.528	293.820	1473.96	1330.704	1253.107	0.224	0.248	0.264
	S12	91.760	181.885	146.326	209.413	1820.958	1590.858	1466.221	0.129	0.148	0.161
	S1	288.555	233.098	358.485	319.665	897.4	823.9	784.525	0.449	0.489	0.514
6	S9	412.428	101.712	442.942	225.440	1443.47	1299.97	1223.095	0.345	0.383	0.407
	S2	25.350	365.793	135.087	373.397	1710.66	1548.96	1462.335	0.246	0.271	0.287
	S10	62.585	236.347	133.489	255.123	2488.57	2172.87	2003.745	0.115	0.132	0.143
	S3	2.266	352.259	107.944	352.939	1841.77	1665.37	1570.870	0.216	0.238	0.253

5	S11	2.290	317.557	97.557	318.244	2695.686	2351.286	2166.786	0.133	0.152	0.165
	S4	54.137	360.501	162.287	376.742	1719.62	1552.488	1462.953	0.246	0.273	0.290
	S12	114.454	256.702	191.464	291.038	2124.451	1856.001	1712.189	0.154	0.176	0.191
	S1	354.623	281.669	439.124	388.056	1025.6	941.6	902.225	0.482	0.525	0.548
	S9	513.848	141.428	556.277	295.583	1649.68	1485.68	1408.805	0.379	0.421	0.444
	S2	28.902	450.679	164.105	459.349	1955.04	1770.24	1683.615	0.264	0.292	0.307
	S10	75.732	313.738	169.854	336.458	2844.08	2483.28	2314.155	0.133	0.152	0.164
	S3	2.960	436.874	134.022	437.762	2104.88	1903.28	1808.780	0.234	0.259	0.272
	S11	2.184	417.023	127.291	417.679	3080.784	2687.184	2502.684	0.153	0.175	0.188
	S4	73.390	443.833	206.540	465.850	1965.28	1774.272	1684.737	0.267	0.295	0.311
	S12	138.972	340.021	240.978	381.713	2427.944	2121.144	1977.332	0.177	0.202	0.217
	S1	424.891	332.511	524.644	459.978	1153.8	1059.3	1025.175	0.512	0.557	0.576
4	S9	621.040	192.353	678.746	378.665	1855.89	1671.39	1604.765	0.411	0.457	0.476
	S2	31.033	538.892	192.701	548.202	2199.42	1991.52	1916.445	0.280	0.310	0.322
	S10	92.015	400.949	212.300	428.554	3199.59	2793.69	2647.115	0.151	0.173	0.182
	S3	3.963	526.465	161.903	527.654	2367.99	2141.19	2059.290	0.251	0.277	0.288
	S11	2.288	519.148	158.033	519.834	3465.882	3023.082	2863.182	0.169	0.193	0.204
	S4	96.323	530.102	255.354	558.999	2210.94	1996.056	1918.459	0.284	0.315	0.328
	S12	169.342	432.916	299.217	483.718	2731.437	2386.287	2261.650	0.199	0.228	0.241
3	S1	503.957	389.607	620.839	540.794	1282	1177	1153.375	0.545	0.593	0.606
	S9	733.414	249.079	808.138	469.104	2062.1	1857.1	1810.975	0.441	0.490	0.502
	S2	39.966	626.402	227.887	638.392	2443.8	2212.8	2160.825	0.294	0.325	0.332
	S10	112.920	493.027	260.828	526.903	3555.1	3104.1	3002.625	0.167	0.191	0.197
	S3	4.430	618.294	189.918	619.623	2631.1	2379.1	2322.400	0.265	0.293	0.300
	S11	2.156	626.691	190.164	627.338	3850.98	3358.98	3248.280	0.183	0.210	0.217
	S4	121.321	616.081	306.146	652.477	2456.6	2217.84	2164.119	0.299	0.331	0.339
	S12	200.477	531.474	359.920	591.617	3034.93	2651.43	2565.143	0.219	0.251	0.259
2	S1	586.763	448.522	721.319	624.551	1410.2	1294.7	1281.575	0.575	0.627	0.633
	S9	845.245	308.658	937.843	562.232	2268.31	2042.81	2017.185	0.465	0.516	0.523
	S2	53.823	710.296	266.912	726.443	2688.18	2434.08	2405.205	0.304	0.336	0.340
	S10	137.160	583.818	312.305	624.966	3910.61	3414.51	3358.135	0.180	0.206	0.209
	S3	4.665	705.972	216.457	707.372	2894.21	2617.01	2585.510	0.275	0.304	0.308
	S11	1.929	730.245	221.003	730.824	4236.078	3694.878	3633.378	0.194	0.223	0.226
	S4	148.224	699.042	357.937	743.509	2702.26	2439.624	2409.779	0.310	0.343	0.347
	S12	232.117	629.452	420.952	699.087	3338.423	2916.573	2868.636	0.236	0.270	0.274
1	S1	653.545	492.816	801.390	688.879	1538.4	1412.4	1409.775	0.586	0.638	0.640
	S9	934.150	353.840	1040.302	634.085	2474.52	2228.52	2223.395	0.473	0.525	0.526
	S2	63.825	777.554	297.092	796.702	2932.56	2655.36	2649.585	0.306	0.338	0.338
	S10	156.785	655.218	353.350	702.253	4266.12	3724.92	3713.645	0.185	0.212	0.213
	S3	5.163	775.206	237.725	776.754	3157.32	2854.92	2848.620	0.277	0.306	0.307
	S11	1.926	809.871	244.888	810.449	4621.176	4030.776	4018.476	0.197	0.226	0.227
	S4	172.734	764.627	402.121	816.447	2947.92	2661.408	2655.439	0.312	0.345	0.346
	S12	258.346	705.110	469.878	782.613	3641.916	3181.716	3172.129	0.242	0.277	0.278

Çizelge B.35: 6 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	13.270	11.188	16.626	15.169	128.2	122.95	112.45	0.130	0.135	0.148
	S9	17.492	3.260	18.470	8.507	206.21	195.96	175.46	0.090	0.094	0.105
	S2	1.877	15.062	6.396	15.625	244.38	232.83	209.73	0.064	0.067	0.075
	S10	5.129	5.610	6.812	7.149	355.51	332.96	287.86	0.020	0.021	0.025
	S3	0.221	15.113	4.755	15.180	263.11	250.51	225.31	0.058	0.061	0.067
	S11	0.219	7.631	2.508	7.696	385.098	360.498	311.298	0.020	0.021	0.025
	S4	1.561	15.191	6.118	15.659	245.66	233.722	209.846	0.064	0.067	0.075
5	S12	4.291	5.995	6.090	7.283	303.493	284.318	245.968	0.024	0.026	0.030
	S1	47.195	37.199	58.355	51.357	256.4	245.9	230.15	0.228	0.237	0.254
	S9	61.512	16.465	66.451	34.919	412.42	391.92	361.17	0.161	0.170	0.184
	S2	9.400	49.103	24.130	51.923	488.76	465.66	431.01	0.106	0.112	0.120
	S10	20.137	26.066	27.957	32.107	711.02	665.92	598.27	0.045	0.048	0.054
	S3	0.225	49.281	15.009	49.348	526.22	501.02	463.22	0.094	0.098	0.107
	S11	0.154	34.577	10.528	34.623	770.196	720.996	647.196	0.045	0.048	0.053
4	S4	7.845	49.081	22.569	51.434	491.32	467.444	431.63	0.105	0.110	0.119
	S12	17.193	28.568	25.763	33.726	606.986	568.636	511.111	0.056	0.059	0.066
	S1	98.709	75.562	121.378	105.175	384.6	368.85	353.1	0.316	0.329	0.344
	S9	129.067	36.521	140.023	75.241	618.63	587.88	557.13	0.226	0.238	0.251
	S2	22.867	98.997	52.566	105.857	733.14	698.49	663.84	0.144	0.152	0.159
	S10	46.410	56.650	63.405	70.573	1066.53	998.88	931.23	0.066	0.071	0.076
	S3	0.168	99.477	30.011	99.527	789.33	751.53	713.73	0.126	0.132	0.139
3	S11	0.473	76.436	23.404	76.578	1155.294	1081.494	1007.694	0.066	0.071	0.076
	S4	17.400	98.772	47.032	103.992	736.98	701.166	665.352	0.141	0.148	0.156
	S12	37.424	62.552	56.190	73.780	910.479	852.954	795.429	0.081	0.086	0.093
	S1	159.724	119.060	195.442	166.977	512.8	491.8	481.3	0.381	0.397	0.406
	S9	212.857	60.477	231.000	124.334	824.84	783.84	763.34	0.280	0.295	0.303
	S2	39.250	161.886	87.816	173.661	977.52	931.32	908.22	0.178	0.186	0.191
	S10	73.588	104.879	105.052	126.955	1422.04	1331.84	1286.74	0.089	0.095	0.099
2	S3	0.353	159.567	48.223	159.673	1052.44	1002.04	976.84	0.152	0.159	0.163
	S11	0.630	140.979	42.924	141.168	1540.392	1441.992	1392.792	0.092	0.098	0.101
	S4	31.371	161.062	79.689	170.474	982.64	934.888	911.012	0.173	0.182	0.187
	S12	64.080	115.580	98.754	134.804	1213.972	1137.272	1098.922	0.111	0.119	0.123
	S1	226.113	164.165	275.363	231.999	641	614.75	609.5	0.430	0.448	0.452
	S9	306.899	85.929	332.677	177.998	1031.05	979.8	969.55	0.323	0.340	0.343
	S2	57.881	232.756	127.708	250.121	1221.9	1164.15	1152.6	0.205	0.215	0.217
1	S10	100.433	165.126	149.971	195.256	1777.55	1664.8	1642.25	0.110	0.117	0.119
	S3	0.348	224.785	67.783	224.889	1315.55	1252.55	1239.95	0.171	0.180	0.181
	S11	0.618	221.968	67.209	222.153	1925.49	1802.49	1777.89	0.115	0.123	0.125
	S4	49.525	231.542	118.987	246.399	1228.3	1168.61	1156.672	0.201	0.211	0.213
	S12	95.320	181.931	149.900	210.527	1517.465	1421.59	1402.415	0.139	0.148	0.150
	S1	285.444	204.109	346.676	289.742	769.2	737.7	737.7	0.451	0.470	0.470
	S9	397.212	107.518	429.468	226.681	1237.26	1175.76	1175.76	0.347	0.365	0.365
	S2	71.984	299.233	161.753	320.828	1466.28	1396.98	1396.98	0.219	0.230	0.230
	S10	122.972	229.820	191.918	266.712	2133.06	1997.76	1997.76	0.125	0.134	0.134
	S3	0.599	286.320	86.495	286.500	1578.66	1503.06	1503.06	0.181	0.191	0.191
	S11	0.457	306.066	92.276	306.203	2310.588	2162.988	2162.988	0.133	0.142	0.142
	S4	61.632	297.481	150.876	315.971	1473.96	1402.332	1402.332	0.214	0.225	0.225
	S12	126.299	252.806	202.141	290.696	1820.958	1705.908	1705.908	0.160	0.170	0.170

Çizelge B.36: 9 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	12.579	12.785	16.414	16.558	128.2	117.7	104.575	0.129	0.141	0.158
	S9	16.875	2.162	17.524	7.225	206.21	185.71	160.085	0.085	0.094	0.109
	S2	1.576	18.445	7.109	18.918	244.38	221.28	192.405	0.077	0.085	0.098
	S10	1.231	2.212	1.895	2.581	355.51	310.41	254.035	0.007	0.008	0.010
	S3	0.767	18.157	6.214	18.387	263.11	237.91	206.41	0.070	0.077	0.089
	S11	0.802	3.882	1.967	4.122	385.098	335.898	274.398	0.011	0.012	0.015
	S4	0.410	18.410	5.933	18.533	245.66	221.784	191.939	0.075	0.084	0.097
8	S12	2.752	2.165	3.401	2.991	303.493	265.143	217.2055	0.011	0.013	0.016
	S1	46.763	41.771	59.294	55.800	256.4	235.4	211.775	0.231	0.252	0.280
	S9	61.572	14.921	66.048	33.393	412.42	371.42	325.295	0.160	0.178	0.203
	S2	1.761	57.893	19.129	58.421	488.76	442.56	390.585	0.120	0.132	0.150
	S10	11.730	19.977	17.723	23.496	711.02	620.82	519.345	0.033	0.038	0.045
	S3	1.168	57.346	18.372	57.696	526.22	475.82	419.12	0.110	0.121	0.138
	S11	1.141	27.964	9.530	28.307	770.196	671.796	561.096	0.037	0.042	0.050
7	S4	5.780	57.443	23.013	59.177	491.32	443.568	389.847	0.120	0.133	0.152
	S12	14.568	21.664	21.067	26.034	606.986	530.286	443.9985	0.043	0.049	0.059
	S1	100.092	84.200	125.352	114.228	384.6	353.1	318.975	0.326	0.355	0.393
	S9	131.856	35.206	142.418	74.762	618.63	557.13	490.505	0.230	0.256	0.290
	S2	11.619	114.566	45.989	118.051	733.14	663.84	588.765	0.161	0.178	0.201
	S10	34.557	48.720	49.173	59.087	1066.53	931.23	784.655	0.055	0.063	0.075
	S3	1.167	113.962	35.355	114.312	789.33	713.73	631.83	0.145	0.160	0.181
6	S11	0.901	68.175	21.353	68.445	1155.294	1007.694	847.794	0.059	0.068	0.081
	S4	14.734	113.621	48.820	118.041	736.98	665.352	587.755	0.160	0.177	0.201
	S12	34.327	53.559	50.395	63.857	910.479	795.429	670.7915	0.070	0.080	0.095
	S1	165.035	133.206	204.997	182.716	512.8	470.8	418.3	0.400	0.435	0.490
	S9	221.625	60.318	239.720	126.805	824.84	742.84	640.34	0.291	0.323	0.374
	S2	24.934	187.122	81.070	194.602	977.52	885.12	769.62	0.199	0.220	0.253
	S10	58.601	97.856	87.958	115.436	1422.04	1241.64	1016.14	0.081	0.093	0.114
5	S3	1.393	182.837	56.244	183.255	1052.44	951.64	825.64	0.174	0.193	0.222
	S11	1.108	134.728	41.526	135.060	1540.392	1343.592	1097.592	0.088	0.101	0.123
	S4	28.856	185.187	84.412	193.844	982.64	887.136	767.756	0.197	0.219	0.252
	S12	61.621	107.432	93.850	125.918	1213.972	1060.572	868.822	0.104	0.119	0.145
	S1	239.364	186.583	295.339	258.392	641	588.5	525.5	0.461	0.502	0.562
	S9	327.292	88.605	353.874	186.792	1031.05	928.55	805.55	0.343	0.381	0.439
	S2	41.785	272.582	123.560	285.117	1221.9	1106.4	967.8	0.233	0.258	0.295
4	S10	83.574	162.665	132.373	187.737	1777.55	1552.05	1281.45	0.106	0.121	0.147
	S3	1.859	260.912	80.132	261.469	1315.55	1189.55	1038.35	0.199	0.220	0.252
	S11	1.426	223.132	68.365	223.559	1925.49	1679.49	1384.29	0.116	0.133	0.161
	S4	48.759	269.576	129.631	284.203	1228.3	1108.92	965.664	0.231	0.256	0.294
	S12	95.114	178.430	148.643	206.964	1517.465	1325.715	1095.615	0.136	0.156	0.189
	S1	318.100	243.409	391.123	338.839	769.2	706.2	648.45	0.508	0.554	0.603
	S9	446.065	120.213	482.129	254.032	1237.26	1114.26	1001.51	0.390	0.433	0.481
3	S2	56.365	366.541	166.327	383.451	1466.28	1327.68	1200.63	0.262	0.289	0.319
	S10	108.446	250.744	183.669	283.278	2133.06	1862.46	1614.41	0.133	0.152	0.175
	S3	1.947	347.937	106.328	348.521	1578.66	1427.46	1288.86	0.221	0.244	0.270
	S11	1.939	332.741	101.761	333.323	2310.588	2015.388	1744.788	0.144	0.165	0.191
	S4	64.093	362.248	172.767	381.476	1473.96	1330.704	1199.386	0.259	0.287	0.318
	S12	135.435	274.557	217.802	315.187	1820.958	1590.858	1379.933	0.173	0.198	0.228
	S1	400.662	299.920	490.638	420.118	897.4	823.9	776.65	0.547	0.596	0.632
2	S9	569.512	154.989	616.008	325.842	1443.47	1299.97	1207.72	0.427	0.474	0.510
	S2	67.856	466.954	207.942	487.311	1710.66	1548.96	1445.01	0.285	0.315	0.337
	S10	127.415	345.730	231.134	383.954	2488.57	2172.87	1969.92	0.154	0.177	0.195
	S3	2.725	445.890	136.492	446.708	1841.77	1665.37	1551.97	0.243	0.268	0.288

2	S11	2.093	462.042	140.705	462.670	2695.686	2351.286	2129.886	0.172	0.197	0.217
	S4	85.856	460.630	224.045	486.387	1719.62	1552.488	1445.046	0.283	0.313	0.337
	S12	167.792	377.747	281.116	428.085	2124.451	1856.001	1683.426	0.202	0.231	0.254
	S1	485.091	357.640	592.383	503.167	1025.6	941.6	904.85	0.578	0.629	0.655
	S9	698.497	205.831	760.246	415.380	1649.68	1485.68	1413.93	0.461	0.512	0.538
	S2	77.568	567.865	247.928	591.136	1955.04	1770.24	1689.39	0.302	0.334	0.350
	S10	150.884	444.510	284.237	489.775	2844.08	2483.28	2325.43	0.172	0.197	0.211
	S3	3.726	546.604	167.708	547.722	2104.88	1903.28	1815.08	0.260	0.288	0.302
	S11	1.950	591.320	179.346	591.905	3080.784	2687.184	2514.984	0.192	0.220	0.235
	S4	112.183	560.283	280.268	593.938	1965.28	1774.272	1690.706	0.302	0.335	0.351
	S12	200.402	485.263	345.981	545.384	2427.944	2121.144	1986.919	0.225	0.257	0.274
1	S1	557.251	406.091	679.078	573.266	1153.8	1059.3	1033.05	0.589	0.641	0.657
	S9	812.673	257.566	889.943	501.367	1855.89	1671.39	1620.14	0.480	0.532	0.549
	S2	82.961	653.675	279.064	678.563	2199.42	1991.52	1933.77	0.309	0.341	0.351
	S10	173.188	536.338	334.089	588.295	3199.59	2793.69	2680.94	0.184	0.211	0.219
	S3	4.824	632.655	194.620	634.102	2367.99	2141.19	2078.19	0.268	0.296	0.305
	S11	2.111	700.059	212.128	700.692	3465.882	3023.082	2900.082	0.202	0.232	0.242
	S4	134.995	644.739	328.416	685.237	2210.94	1996.056	1936.366	0.310	0.343	0.354
	S12	233.866	584.238	409.137	654.397	2731.437	2386.287	2290.412	0.240	0.274	0.286

Çizelge B.37: 12 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	12.608	15.895	17.377	19.677	128.2	117.7	117.700	0.153	0.167	0.167
	S9	17.136	0.116	17.170	5.257	206.21	185.71	185.710	0.083	0.092	0.092
	S2	5.667	23.335	12.667	25.035	244.38	221.28	221.280	0.102	0.113	0.113
	S10	3.374	1.721	3.890	2.733	355.51	310.41	310.410	0.011	0.013	0.013
	S3	1.060	23.476	8.103	23.794	263.11	237.91	237.910	0.090	0.100	0.100
	S11	1.343	0.822	1.589	1.225	385.098	335.898	335.898	0.004	0.005	0.005
	S4	1.506	23.276	8.489	23.728	245.66	221.784	221.784	0.097	0.107	0.107
11	S12	1.184	2.382	1.899	2.737	303.493	265.143	265.143	0.009	0.010	0.010
	S1	48.684	50.276	63.766	64.881	256.4	235.4	235.400	0.253	0.276	0.276
	S9	64.531	11.325	67.929	30.684	412.42	371.42	371.420	0.165	0.183	0.183
	S2	7.237	70.797	28.476	72.968	488.76	442.56	442.560	0.149	0.165	0.165
	S10	1.951	13.468	5.991	14.053	711.02	620.82	620.820	0.020	0.023	0.023
	S3	1.507	71.176	22.859	71.627	526.22	475.82	475.820	0.136	0.151	0.151
	S11	1.914	20.242	7.986	20.816	770.196	671.796	671.796	0.027	0.031	0.031
10	S4	2.384	70.198	23.443	70.913	491.32	443.568	443.568	0.144	0.160	0.160
	S12	12.351	14.067	16.571	17.773	606.986	530.286	530.286	0.029	0.034	0.034
	S1	105.231	99.011	134.934	130.581	384.6	353.1	353.100	0.351	0.382	0.382
	S9	139.265	30.849	148.519	72.628	618.63	557.13	557.130	0.240	0.267	0.267
	S2	1.754	136.603	42.735	137.129	733.14	663.84	663.840	0.187	0.207	0.207
	S10	20.579	40.352	32.685	46.526	1066.53	931.23	931.230	0.044	0.050	0.050
	S3	1.540	137.461	42.779	137.923	789.33	713.73	713.730	0.175	0.193	0.193
9	S11	1.905	58.414	19.429	58.985	1155.294	1007.694	1007.694	0.051	0.059	0.059
	S4	10.117	135.368	50.727	138.403	736.98	665.352	665.352	0.188	0.208	0.208
	S12	31.983	43.737	45.104	53.332	910.479	795.429	795.429	0.059	0.067	0.067
	S1	174.330	154.943	220.813	207.242	512.8	470.8	457.675	0.431	0.469	0.482
	S9	235.144	55.509	251.797	126.052	824.84	742.84	717.215	0.305	0.339	0.351
	S2	7.356	220.091	73.383	222.298	977.52	885.12	856.245	0.227	0.251	0.260
	S10	39.949	89.493	66.797	101.477	1422.04	1241.64	1185.265	0.071	0.082	0.086
8	S3	1.820	217.303	67.011	217.849	1052.44	951.64	920.140	0.207	0.229	0.237
	S11	2.280	125.389	39.896	126.073	1540.392	1343.592	1282.092	0.082	0.094	0.098
	S4	23.526	217.661	88.824	224.718	982.64	887.136	857.291	0.229	0.253	0.262
	S12	59.729	97.338	88.931	115.257	1213.972	1060.572	1012.635	0.095	0.109	0.114
	S1	254.366	216.208	319.228	292.518	641	588.5	564.875	0.498	0.542	0.565
	S9	349.391	83.738	374.513	188.555	1031.05	928.55	882.425	0.363	0.403	0.424
	S2	20.475	318.765	116.105	324.907	1221.9	1106.4	1054.425	0.266	0.294	0.308
7	S10	60.264	156.212	107.127	174.291	1777.55	1552.05	1450.575	0.098	0.112	0.120
	S3	2.366	308.092	94.793	308.801	1315.55	1189.55	1132.850	0.235	0.260	0.273
	S11	2.698	217.015	67.802	217.824	1925.49	1679.49	1568.790	0.113	0.130	0.139
	S4	43.559	315.038	138.071	328.106	1228.3	1108.92	1055.199	0.267	0.296	0.311
	S12	94.508	170.116	145.543	198.469	1517.465	1325.715	1239.428	0.131	0.150	0.160
	S1	340.396	282.298	425.085	384.417	769.2	706.2	672.075	0.553	0.602	0.632
	S9	480.089	116.041	514.902	260.068	1237.26	1114.26	1047.635	0.416	0.462	0.491
6	S2	30.964	428.548	159.528	437.838	1466.28	1327.68	1252.605	0.299	0.330	0.350
	S10	80.592	250.680	155.796	274.858	2133.06	1862.46	1715.885	0.129	0.148	0.160
	S3	2.518	410.450	125.653	411.206	1578.66	1427.46	1345.560	0.260	0.288	0.306
	S11	3.294	334.023	103.501	335.011	2310.588	2015.388	1855.488	0.145	0.166	0.181
	S4	58.322	423.234	185.292	440.730	1473.96	1330.704	1253.107	0.299	0.331	0.352
	S12	137.640	272.828	219.489	314.120	1820.958	1590.858	1466.221	0.173	0.197	0.214
	S1	432.833	349.647	537.727	479.497	897.4	823.9	784.525	0.599	0.653	0.685
6	S9	618.643	152.567	664.413	338.160	1443.47	1299.97	1223.095	0.460	0.511	0.543
	S2	38.024	548.689	202.631	560.096	1710.66	1548.96	1462.335	0.327	0.362	0.383
	S10	93.878	354.521	200.234	382.684	2488.57	2172.87	2003.745	0.154	0.176	0.191
	S3	3.399	528.389	161.916	529.409	1841.77	1665.37	1570.870	0.287	0.318	0.337

5	S11	3.436	476.336	146.336	477.366	2695.686	2351.286	2166.786	0.177	0.203	0.220
	S4	81.205	540.752	243.431	565.114	1719.62	1552.488	1462.953	0.329	0.364	0.386
	S12	171.681	385.054	287.197	436.558	2124.451	1856.001	1712.189	0.205	0.235	0.255
	S1	531.934	422.503	658.685	582.084	1025.6	941.6	902.225	0.642	0.700	0.730
	S9	770.772	212.143	834.415	443.374	1649.68	1485.68	1408.805	0.506	0.562	0.592
	S2	43.353	676.018	246.158	689.024	1955.04	1770.24	1683.615	0.352	0.389	0.409
	S10	113.598	470.608	254.781	504.687	2844.08	2483.28	2314.155	0.177	0.203	0.218
	S3	4.439	655.312	201.033	656.643	2104.88	1903.28	1808.780	0.312	0.345	0.363
	S11	3.276	625.535	190.937	626.518	3080.784	2687.184	2502.684	0.203	0.233	0.250
	S4	110.085	665.750	309.810	698.776	1965.28	1774.272	1684.737	0.356	0.394	0.415
	S12	208.458	510.032	361.468	572.569	2427.944	2121.144	1977.332	0.236	0.270	0.290
	S1	637.336	498.767	786.966	689.968	1153.8	1059.3	1025.175	0.682	0.743	0.768
4	S9	931.560	288.530	1018.119	567.998	1855.89	1671.39	1604.765	0.549	0.609	0.634
	S2	46.549	808.338	289.051	822.303	2199.42	1991.52	1916.445	0.374	0.413	0.429
	S10	138.022	601.424	318.450	642.831	3199.59	2793.69	2647.115	0.201	0.230	0.243
	S3	5.945	789.697	242.854	791.481	2367.99	2141.19	2059.290	0.334	0.370	0.384
	S11	3.432	778.722	237.049	779.752	3465.882	3023.082	2863.182	0.225	0.258	0.272
	S4	144.485	795.154	383.031	838.499	2210.94	1996.056	1918.459	0.379	0.420	0.437
	S12	254.013	649.374	448.826	725.578	2731.437	2386.287	2261.650	0.266	0.304	0.321
3	S1	755.935	584.411	931.258	811.192	1282	1177	1153.375	0.726	0.791	0.807
	S9	1100.121	373.619	1212.207	703.655	2062.1	1857.1	1810.975	0.588	0.653	0.669
	S2	59.949	939.603	341.830	957.587	2443.8	2212.8	2160.825	0.392	0.433	0.443
	S10	169.380	739.541	391.242	790.355	3555.1	3104.1	3002.625	0.222	0.255	0.263
	S3	6.645	927.441	284.877	929.435	2631.1	2379.1	2322.400	0.353	0.391	0.400
	S11	3.234	940.037	285.245	941.007	3850.98	3358.98	3248.280	0.244	0.280	0.290
	S4	181.982	924.121	459.218	978.716	2456.6	2217.84	2164.119	0.398	0.441	0.452
	S12	300.716	797.211	539.879	887.426	3034.93	2651.43	2565.143	0.292	0.335	0.346
2	S1	880.144	672.784	1081.979	936.827	1410.2	1294.7	1281.575	0.767	0.836	0.844
	S9	1267.868	462.987	1406.764	843.348	2268.31	2042.81	2017.185	0.620	0.689	0.697
	S2	80.735	1065.444	400.368	1089.665	2688.18	2434.08	2405.205	0.405	0.448	0.453
	S10	205.740	875.727	468.458	937.449	3910.61	3414.51	3358.135	0.240	0.275	0.279
	S3	6.997	1058.959	324.685	1061.058	2894.21	2617.01	2585.510	0.367	0.405	0.410
	S11	2.894	1095.367	331.504	1096.235	4236.078	3694.878	3633.378	0.259	0.297	0.302
	S4	222.337	1048.563	536.905	1115.264	2702.26	2439.624	2409.779	0.413	0.457	0.463
	S12	348.175	944.178	631.429	1048.630	3338.423	2916.573	2868.636	0.314	0.360	0.366
1	S1	980.318	739.223	1202.085	1033.319	1538.4	1412.4	1409.775	0.781	0.851	0.853
	S9	1401.225	530.760	1560.452	951.127	2474.52	2228.52	2223.395	0.631	0.700	0.702
	S2	95.738	1166.331	445.637	1195.052	2932.56	2655.36	2649.585	0.408	0.450	0.451
	S10	235.177	982.827	530.025	1053.380	4266.12	3724.92	3713.645	0.247	0.283	0.284
	S3	7.744	1162.808	356.587	1165.132	3157.32	2854.92	2848.620	0.369	0.408	0.409
	S11	2.889	1214.806	367.331	1215.673	4621.176	4030.776	4018.476	0.263	0.302	0.303
	S4	259.100	1146.940	603.182	1224.670	2947.92	2661.408	2655.439	0.415	0.460	0.461
	S12	387.518	1057.664	704.817	1173.920	3641.916	3181.716	3172.129	0.322	0.369	0.370

Çizelge B.38: 6 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	18.436	15.544	23.099	21.075	128.2	122.95	112.45	0.180	0.188	0.205
	S9	24.302	4.529	25.660	11.819	206.21	195.96	175.46	0.124	0.131	0.146
	S2	2.608	20.926	8.886	21.709	244.38	232.83	209.73	0.089	0.093	0.104
	S10	7.126	7.794	9.464	9.932	355.51	332.96	287.86	0.028	0.030	0.035
	S3	0.308	20.997	6.607	21.089	263.11	250.51	225.31	0.080	0.084	0.094
	S11	0.304	10.602	3.484	10.693	385.098	360.498	311.298	0.028	0.030	0.034
	S4	2.168	21.105	8.499	21.755	245.66	233.722	209.846	0.089	0.093	0.104
5	S12	5.962	8.330	8.461	10.118	303.493	284.318	245.968	0.033	0.036	0.041
	S1	65.570	51.681	81.074	71.352	256.4	245.9	230.15	0.316	0.330	0.352
	S9	85.461	22.876	92.323	48.514	412.42	391.92	361.17	0.224	0.236	0.256
	S2	13.059	68.220	33.525	72.138	488.76	465.66	431.01	0.148	0.155	0.167
	S10	27.977	36.215	38.841	44.608	711.02	665.92	598.27	0.063	0.067	0.075
	S3	0.312	68.467	20.853	68.561	526.22	501.02	463.22	0.130	0.137	0.148
	S11	0.215	48.039	14.626	48.103	770.196	720.996	647.196	0.062	0.067	0.074
4	S4	10.900	68.189	31.356	71.459	491.32	467.444	431.63	0.145	0.153	0.166
	S12	23.887	39.691	35.794	46.856	606.986	568.636	511.111	0.077	0.082	0.092
	S1	137.140	104.981	168.634	146.123	384.6	368.85	353.1	0.438	0.457	0.478
	S9	179.317	50.740	194.539	104.535	618.63	587.88	557.13	0.314	0.331	0.349
	S2	31.771	137.539	73.032	147.070	733.14	698.49	663.84	0.201	0.211	0.222
	S10	64.479	78.706	88.090	98.049	1066.53	998.88	931.23	0.092	0.098	0.105
	S3	0.234	138.207	41.696	138.277	789.33	751.53	713.73	0.175	0.184	0.194
3	S11	0.657	106.195	32.516	106.392	1155.294	1081.494	1007.694	0.092	0.098	0.106
	S4	24.174	137.227	65.342	144.479	736.98	701.166	665.352	0.196	0.206	0.217
	S12	51.995	86.906	78.066	102.505	910.479	852.954	795.429	0.113	0.120	0.129
	S1	221.911	165.414	271.535	231.987	512.8	491.8	481.3	0.530	0.552	0.564
	S9	295.730	84.022	320.937	172.741	824.84	783.84	763.34	0.389	0.409	0.420
	S2	54.531	224.914	122.006	241.273	977.52	931.32	908.22	0.247	0.259	0.266
	S10	102.238	145.711	145.952	176.383	1422.04	1331.84	1286.74	0.124	0.132	0.137
2	S3	0.490	221.691	66.998	221.838	1052.44	1002.04	976.84	0.211	0.221	0.227
	S11	0.876	195.867	59.636	196.130	1540.392	1441.992	1392.792	0.127	0.136	0.141
	S4	43.585	223.769	110.715	236.845	982.64	934.888	911.012	0.241	0.253	0.260
	S12	89.029	160.579	137.202	187.287	1213.972	1137.272	1098.922	0.154	0.165	0.170
	S1	314.146	228.080	382.570	322.323	641	614.75	609.5	0.597	0.622	0.628
	S9	426.384	119.384	462.199	247.299	1031.05	979.8	969.55	0.448	0.472	0.477
	S2	80.417	323.376	177.429	347.501	1221.9	1164.15	1152.6	0.284	0.299	0.301
1	S10	139.536	229.415	208.360	271.275	1777.55	1664.8	1642.25	0.153	0.163	0.165
	S3	0.484	312.301	94.174	312.446	1315.55	1252.55	1239.95	0.238	0.249	0.252
	S11	0.859	308.388	93.375	308.645	1925.49	1802.49	1777.89	0.160	0.171	0.174
	S4	68.807	321.689	165.313	342.331	1228.3	1168.61	1156.672	0.279	0.293	0.296
	S12	132.432	252.762	208.261	292.492	1517.465	1421.59	1402.415	0.193	0.206	0.209
	S1	396.576	283.576	481.649	402.549	769.2	737.7	737.7	0.626	0.653	0.653
	S9	551.860	149.378	596.674	314.936	1237.26	1175.76	1175.76	0.482	0.507	0.507
	S2	100.009	415.734	224.729	445.737	1466.28	1396.98	1396.98	0.304	0.319	0.319
	S10	170.849	319.297	266.638	370.552	2133.06	1997.76	1997.76	0.174	0.185	0.185
	S3	0.833	397.794	120.171	398.044	1578.66	1503.06	1503.06	0.252	0.265	0.265
	S11	0.634	425.228	128.203	425.418	2310.588	2162.988	2162.988	0.184	0.197	0.197
	S4	85.627	413.300	209.617	438.989	1473.96	1402.332	1402.332	0.298	0.313	0.313
	S12	175.471	351.232	280.841	403.874	1820.958	1705.908	1705.908	0.222	0.237	0.237

Çizelge B.39: 9 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	13.675	13.898	17.844	18.001	128.2	117.7	104.575	0.140	0.153	0.172
	S9	18.345	2.351	19.050	7.854	206.21	185.71	160.085	0.092	0.103	0.119
	S2	1.713	20.051	7.729	20.565	244.38	221.28	192.405	0.084	0.093	0.107
	S10	1.339	2.405	2.060	2.806	355.51	310.41	254.035	0.008	0.009	0.011
	S3	0.834	19.738	6.756	19.988	263.11	237.91	206.41	0.076	0.084	0.097
	S11	0.872	4.220	2.138	4.481	385.098	335.898	274.398	0.012	0.013	0.016
	S4	0.446	20.013	6.450	20.147	245.66	221.784	191.939	0.082	0.091	0.105
8	S12	2.992	2.354	3.698	3.251	303.493	265.143	217.2055	0.012	0.014	0.017
	S1	50.836	45.409	64.458	60.660	256.4	235.4	211.775	0.251	0.274	0.304
	S9	66.934	16.221	71.801	36.301	412.42	371.42	325.295	0.174	0.193	0.221
	S2	1.915	62.935	20.795	63.509	488.76	442.56	390.585	0.130	0.144	0.163
	S10	12.751	21.716	19.266	25.542	711.02	620.82	519.345	0.036	0.041	0.049
	S3	1.270	62.341	19.972	62.722	526.22	475.82	419.12	0.119	0.132	0.150
	S11	1.240	30.400	10.360	30.772	770.196	671.796	561.096	0.040	0.046	0.055
7	S4	6.284	62.445	25.017	64.330	491.32	443.568	389.847	0.131	0.145	0.165
	S12	15.837	23.551	22.902	28.302	606.986	530.286	443.9985	0.047	0.053	0.064
	S1	108.809	91.534	136.269	124.177	384.6	353.1	318.975	0.354	0.386	0.427
	S9	143.340	38.272	154.822	81.274	618.63	557.13	490.505	0.250	0.278	0.316
	S2	12.631	124.544	49.994	128.333	733.14	663.84	588.765	0.175	0.193	0.218
	S10	37.566	52.963	53.455	64.233	1066.53	931.23	784.655	0.060	0.069	0.082
	S3	1.268	123.887	38.434	124.268	789.33	713.73	631.83	0.157	0.174	0.197
6	S11	0.979	74.113	23.213	74.406	1155.294	1007.694	847.794	0.064	0.074	0.088
	S4	16.017	123.517	53.072	128.322	736.98	665.352	587.755	0.174	0.193	0.218
	S12	37.317	58.224	54.784	69.419	910.479	795.429	670.7915	0.076	0.087	0.103
	S1	179.409	144.808	222.851	198.630	512.8	470.8	418.3	0.435	0.473	0.533
	S9	240.927	65.571	260.598	137.849	824.84	742.84	640.34	0.316	0.351	0.407
	S2	27.106	203.419	88.131	211.551	977.52	885.12	769.62	0.216	0.239	0.275
	S10	63.705	106.379	95.619	125.490	1422.04	1241.64	1016.14	0.088	0.101	0.123
5	S3	1.514	198.762	61.142	199.216	1052.44	951.64	825.64	0.189	0.209	0.241
	S11	1.204	146.462	45.143	146.823	1540.392	1343.592	1097.592	0.095	0.109	0.134
	S4	31.369	201.316	91.764	210.727	982.64	887.136	767.756	0.214	0.238	0.274
	S12	66.988	116.789	102.024	136.885	1213.972	1060.572	868.822	0.113	0.129	0.158
	S1	260.211	202.833	321.061	280.896	641	588.5	525.5	0.501	0.546	0.611
	S9	355.798	96.322	384.694	203.061	1031.05	928.55	805.55	0.373	0.414	0.478
	S2	45.424	296.322	134.321	309.950	1221.9	1106.4	967.8	0.254	0.280	0.320
4	S10	90.853	176.832	143.902	204.088	1777.55	1552.05	1281.45	0.115	0.131	0.159
	S3	2.021	283.636	87.112	284.242	1315.55	1189.55	1038.35	0.216	0.239	0.274
	S11	1.550	242.565	74.319	243.030	1925.49	1679.49	1384.29	0.126	0.145	0.176
	S4	53.005	293.054	140.922	308.956	1228.3	1108.92	965.664	0.252	0.279	0.320
	S12	103.398	193.971	161.589	224.990	1517.465	1325.715	1095.615	0.148	0.170	0.205
	S1	345.805	264.609	425.188	368.350	769.2	706.2	648.45	0.553	0.602	0.656
	S9	484.915	130.683	524.120	276.157	1237.26	1114.26	1001.51	0.424	0.470	0.523
3	S2	61.274	398.465	180.814	416.848	1466.28	1327.68	1200.63	0.284	0.314	0.347
	S10	117.891	272.583	199.666	307.950	2133.06	1862.46	1614.41	0.144	0.165	0.191
	S3	2.117	378.241	115.589	378.876	1578.66	1427.46	1288.86	0.240	0.265	0.294
	S11	2.108	361.722	110.624	362.354	2310.588	2015.388	1744.788	0.157	0.180	0.208
	S4	69.675	393.798	187.814	414.701	1473.96	1330.704	1199.386	0.281	0.312	0.346
	S12	147.231	298.470	236.772	342.639	1820.958	1590.858	1379.933	0.188	0.215	0.248
	S1	435.557	326.042	533.370	456.709	897.4	823.9	776.65	0.594	0.647	0.687
3	S9	619.114	168.487	669.660	354.221	1443.47	1299.97	1207.72	0.464	0.515	0.554
	S2	73.766	507.623	226.053	529.753	1710.66	1548.96	1445.01	0.310	0.342	0.367
	S10	138.512	375.841	251.265	417.395	2488.57	2172.87	1969.92	0.168	0.192	0.212
	S3	2.963	484.725	148.380	485.614	1841.77	1665.37	1551.97	0.264	0.292	0.313

2	S11	2.275	502.284	152.960	502.966	2695.686	2351.286	2129.886	0.187	0.214	0.236
	S4	93.334	500.749	243.559	528.749	1719.62	1552.488	1445.046	0.307	0.341	0.366
	S12	182.405	410.647	305.599	465.369	2124.451	1856.001	1683.426	0.219	0.251	0.276
	S1	527.340	388.789	643.977	546.991	1025.6	941.6	904.85	0.628	0.684	0.712
	S9	759.333	223.757	826.460	451.557	1649.68	1485.68	1413.93	0.501	0.556	0.585
	S2	84.324	617.324	269.521	642.621	1955.04	1770.24	1689.39	0.329	0.363	0.380
	S10	164.026	483.225	308.993	532.432	2844.08	2483.28	2325.43	0.187	0.214	0.229
	S3	4.051	594.211	182.314	595.426	2104.88	1903.28	1815.08	0.283	0.313	0.328
	S11	2.120	642.821	194.966	643.457	3080.784	2687.184	2514.984	0.209	0.239	0.256
	S4	121.954	609.081	304.678	645.667	1965.28	1774.272	1690.706	0.329	0.364	0.382
	S12	217.856	527.528	376.115	592.884	2427.944	2121.144	1986.919	0.244	0.280	0.298
1	S1	605.785	441.459	738.223	623.195	1153.8	1059.3	1033.05	0.640	0.697	0.715
	S9	883.453	279.998	967.452	545.034	1855.89	1671.39	1620.14	0.521	0.579	0.597
	S2	90.187	710.607	303.369	737.663	2199.42	1991.52	1933.77	0.335	0.370	0.381
	S10	188.272	583.051	363.187	639.532	3199.59	2793.69	2680.94	0.200	0.229	0.239
	S3	5.244	687.756	211.571	689.329	2367.99	2141.19	2078.19	0.291	0.322	0.332
	S11	2.295	761.030	230.604	761.719	3465.882	3023.082	2900.082	0.220	0.252	0.263
	S4	146.752	700.893	357.020	744.918	2210.94	1996.056	1936.366	0.337	0.373	0.385
	S12	254.234	635.122	444.771	711.392	2731.437	2386.287	2290.412	0.260	0.298	0.311

Çizelge B.40: 12 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	11.301	14.247	15.575	17.637	128.2	117.7	117.700	0.138	0.150	0.150
	S9	15.359	0.104	15.390	4.712	206.21	185.71	185.710	0.075	0.083	0.083
	S2	5.079	20.916	11.354	22.439	244.38	221.28	221.280	0.092	0.101	0.101
	S10	3.024	1.542	3.487	2.450	355.51	310.41	310.410	0.010	0.011	0.011
	S3	0.950	21.043	7.263	21.328	263.11	237.91	237.910	0.081	0.090	0.090
	S11	1.204	0.737	1.425	1.098	385.098	335.898	335.898	0.004	0.004	0.004
	S4	1.350	20.863	7.609	21.268	245.66	221.784	221.784	0.087	0.096	0.096
11	S12	1.061	2.135	1.702	2.454	303.493	265.143	265.143	0.008	0.009	0.009
	S1	43.637	45.064	57.156	58.155	256.4	235.4	235.400	0.227	0.247	0.247
	S9	57.842	10.151	60.887	27.504	412.42	371.42	371.420	0.148	0.164	0.164
	S2	6.487	63.458	25.524	65.404	488.76	442.56	442.560	0.134	0.148	0.148
	S10	1.749	12.071	5.370	12.596	711.02	620.82	620.820	0.018	0.020	0.020
	S3	1.350	63.797	20.489	64.202	526.22	475.82	475.820	0.122	0.135	0.135
	S11	1.715	18.143	7.158	18.658	770.196	671.796	671.796	0.024	0.028	0.028
10	S4	2.137	62.921	21.013	63.562	491.32	443.568	443.568	0.129	0.143	0.143
	S12	11.071	12.609	14.854	15.930	606.986	530.286	530.286	0.026	0.030	0.030
	S1	94.322	88.747	120.946	117.044	384.6	353.1	353.100	0.314	0.343	0.343
	S9	124.827	27.651	133.123	65.099	618.63	557.13	557.130	0.215	0.239	0.239
	S2	1.572	122.442	38.305	122.913	733.14	663.84	663.840	0.168	0.185	0.185
	S10	18.446	36.169	29.296	41.703	1066.53	931.23	931.230	0.039	0.045	0.045
	S3	1.381	123.211	38.344	123.625	789.33	713.73	713.730	0.157	0.173	0.173
9	S11	1.707	52.358	17.415	52.870	1155.294	1007.694	1007.694	0.046	0.052	0.052
	S4	9.068	121.335	45.468	124.055	736.98	665.352	665.352	0.168	0.186	0.186
	S12	28.667	39.203	40.428	47.803	910.479	795.429	795.429	0.053	0.060	0.060
	S1	156.257	138.881	197.922	185.758	512.8	470.8	457.675	0.386	0.420	0.432
	S9	210.768	49.755	225.694	112.985	824.84	742.84	717.215	0.274	0.304	0.315
	S2	6.594	197.275	65.776	199.253	977.52	885.12	856.245	0.204	0.225	0.233
	S10	35.808	80.215	59.872	90.958	1422.04	1241.64	1185.265	0.064	0.073	0.077
8	S3	1.632	194.776	60.064	195.265	1052.44	951.64	920.140	0.186	0.205	0.212
	S11	2.043	112.390	35.760	113.003	1540.392	1343.592	1282.092	0.073	0.084	0.088
	S4	21.087	195.097	79.616	201.423	982.64	887.136	857.291	0.205	0.227	0.235
	S12	53.537	87.248	79.712	103.309	1213.972	1060.572	1012.635	0.085	0.097	0.102
	S1	227.997	193.794	286.135	262.193	641	588.5	564.875	0.446	0.486	0.507
	S9	313.171	75.057	335.688	169.008	1031.05	928.55	882.425	0.326	0.362	0.380
	S2	18.353	285.719	104.068	291.225	1221.9	1106.4	1054.425	0.238	0.263	0.276
7	S10	54.016	140.018	96.022	156.223	1777.55	1552.05	1450.575	0.088	0.101	0.108
	S3	2.120	276.153	84.966	276.789	1315.55	1189.55	1132.850	0.210	0.233	0.244
	S11	2.418	194.518	60.774	195.243	1925.49	1679.49	1568.790	0.101	0.116	0.124
	S4	39.044	282.379	123.757	294.092	1228.3	1108.92	1055.199	0.239	0.265	0.279
	S12	84.711	152.481	130.455	177.894	1517.465	1325.715	1239.428	0.117	0.134	0.144
	S1	305.108	253.033	381.018	344.565	769.2	706.2	672.075	0.495	0.540	0.567
	S9	430.320	104.012	461.523	233.108	1237.26	1114.26	1047.635	0.373	0.414	0.441
6	S2	27.754	384.122	142.991	392.448	1466.28	1327.68	1252.605	0.268	0.296	0.313
	S10	72.237	224.693	139.645	246.364	2133.06	1862.46	1715.885	0.115	0.132	0.144
	S3	2.257	367.900	112.627	368.578	1578.66	1427.46	1345.560	0.233	0.258	0.274
	S11	2.953	299.396	92.772	300.282	2310.588	2015.388	1855.488	0.130	0.149	0.162
	S4	52.276	379.359	166.083	395.041	1473.96	1330.704	1253.107	0.268	0.297	0.315
	S12	123.372	244.545	196.735	281.556	1820.958	1590.858	1466.221	0.155	0.177	0.192
	S1	387.963	313.400	481.983	429.789	897.4	823.9	784.525	0.537	0.585	0.614
6	S9	554.510	136.751	595.535	303.104	1443.47	1299.97	1223.095	0.413	0.458	0.487
	S2	34.083	491.808	181.625	502.033	1710.66	1548.96	1462.335	0.293	0.324	0.343
	S10	84.146	317.769	179.476	343.012	2488.57	2172.87	2003.745	0.138	0.158	0.171
	S3	3.047	473.613	145.131	474.527	1841.77	1665.37	1570.870	0.258	0.285	0.302

5	S11	3.079	426.955	131.166	427.879	2695.686	2351.286	2166.786	0.159	0.182	0.197
	S4	72.787	484.694	218.195	506.530	1719.62	1552.488	1462.953	0.295	0.326	0.346
	S12	153.883	345.136	257.424	391.301	2124.451	1856.001	1712.189	0.184	0.211	0.229
	S1	476.791	378.704	590.402	521.741	1025.6	941.6	902.225	0.576	0.627	0.654
	S9	690.869	190.151	747.914	397.411	1649.68	1485.68	1408.805	0.453	0.503	0.531
	S2	38.859	605.937	220.640	617.595	1955.04	1770.24	1683.615	0.316	0.349	0.367
	S10	101.822	421.821	228.368	452.368	2844.08	2483.28	2314.155	0.159	0.182	0.195
	S3	3.979	587.378	180.192	588.571	2104.88	1903.28	1808.780	0.280	0.309	0.325
	S11	2.937	560.688	171.143	561.569	3080.784	2687.184	2502.684	0.182	0.209	0.224
	S4	98.673	596.734	277.693	626.336	1965.28	1774.272	1684.737	0.319	0.353	0.372
	S12	186.848	457.159	323.995	513.213	2427.944	2121.144	1977.332	0.211	0.242	0.260
	S1	571.265	447.061	705.384	618.441	1153.8	1059.3	1025.175	0.611	0.666	0.688
4	S9	834.988	258.619	912.574	509.116	1855.89	1671.39	1604.765	0.492	0.546	0.569
	S2	41.724	724.541	259.086	737.058	2199.42	1991.52	1916.445	0.335	0.370	0.385
	S10	123.714	539.076	285.437	576.190	3199.59	2793.69	2647.115	0.180	0.206	0.218
	S3	5.329	707.832	217.678	709.431	2367.99	2141.19	2059.290	0.300	0.331	0.345
	S11	3.077	697.994	212.475	698.917	3465.882	3023.082	2863.182	0.202	0.231	0.244
	S4	129.507	712.723	343.324	751.575	2210.94	1996.056	1918.459	0.340	0.377	0.392
	S12	227.681	582.055	402.297	650.359	2731.437	2386.287	2261.650	0.238	0.273	0.288
	S1	677.570	523.827	834.718	727.098	1282	1177	1153.375	0.651	0.709	0.724
3	S9	986.075	334.887	1086.541	630.710	2062.1	1857.1	1810.975	0.527	0.585	0.600
	S2	53.735	842.197	306.394	858.317	2443.8	2212.8	2160.825	0.351	0.388	0.397
	S10	151.821	662.875	350.684	708.422	3555.1	3104.1	3002.625	0.199	0.228	0.236
	S3	5.956	831.297	255.345	833.083	2631.1	2379.1	2322.400	0.317	0.350	0.359
	S11	2.899	842.587	255.675	843.456	3850.98	3358.98	3248.280	0.219	0.251	0.260
	S4	163.117	828.321	411.613	877.256	2456.6	2217.84	2164.119	0.357	0.396	0.405
	S12	269.542	714.567	483.912	795.430	3034.93	2651.43	2565.143	0.262	0.300	0.310
	S1	788.902	603.038	969.814	839.709	1410.2	1294.7	1281.575	0.688	0.749	0.757
2	S9	1136.432	414.991	1260.930	755.921	2268.31	2042.81	2017.185	0.556	0.617	0.625
	S2	72.365	954.993	358.863	976.703	2688.18	2434.08	2405.205	0.363	0.401	0.406
	S10	184.412	784.943	419.895	840.267	3910.61	3414.51	3358.135	0.215	0.246	0.250
	S3	6.272	949.180	291.026	951.061	2894.21	2617.01	2585.510	0.329	0.363	0.368
	S11	2.594	981.814	297.138	982.592	4236.078	3694.878	3633.378	0.232	0.266	0.270
	S4	199.288	939.862	481.246	999.648	2702.26	2439.624	2409.779	0.370	0.410	0.415
	S12	312.081	846.298	565.971	939.922	3338.423	2916.573	2868.636	0.282	0.322	0.328
	S1	878.691	662.591	1077.468	926.198	1538.4	1412.4	1409.775	0.700	0.763	0.764
1	S9	1255.964	475.738	1398.685	852.527	2474.52	2228.52	2223.395	0.565	0.628	0.629
	S2	85.813	1045.421	399.440	1071.165	2932.56	2655.36	2649.585	0.365	0.403	0.404
	S10	210.797	880.941	475.079	944.180	4266.12	3724.92	3713.645	0.221	0.253	0.254
	S3	6.942	1042.264	319.621	1044.346	3157.32	2854.92	2848.620	0.331	0.366	0.367
	S11	2.590	1088.872	329.251	1089.648	4621.176	4030.776	4018.476	0.236	0.270	0.271
	S4	232.240	1028.040	540.652	1097.712	2947.92	2661.408	2655.439	0.372	0.412	0.413
	S12	347.346	948.020	631.751	1052.223	3641.916	3181.716	3172.129	0.289	0.331	0.332

Çizelge B.41: 6 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	26.628	22.451	33.363	30.440	128.2	122.95	112.45	0.260	0.271	0.297
	S9	35.100	6.541	37.062	17.071	206.21	195.96	175.46	0.180	0.189	0.211
	S2	3.767	30.225	12.835	31.355	244.38	232.83	209.73	0.128	0.135	0.150
	S10	10.292	11.258	13.669	14.345	355.51	332.96	287.86	0.040	0.043	0.050
	S3	0.444	30.327	9.542	30.460	263.11	250.51	225.31	0.116	0.122	0.135
	S11	0.439	15.312	5.033	15.444	385.098	360.498	311.298	0.040	0.043	0.050
	S4	3.131	30.483	12.276	31.422	245.66	233.722	209.846	0.128	0.134	0.150
5	S12	8.612	12.031	12.221	14.614	303.493	284.318	245.968	0.048	0.051	0.059
	S1	94.705	74.645	117.099	103.057	256.4	245.9	230.15	0.457	0.476	0.509
	S9	123.434	33.040	133.346	70.070	412.42	391.92	361.17	0.323	0.340	0.369
	S2	18.862	98.533	48.422	104.192	488.76	465.66	431.01	0.213	0.224	0.242
	S10	40.408	52.307	56.100	64.429	711.02	665.92	598.27	0.091	0.097	0.108
	S3	0.451	98.890	30.118	99.025	526.22	501.02	463.22	0.188	0.198	0.214
	S11	0.310	69.385	21.125	69.478	770.196	720.996	647.196	0.090	0.096	0.107
4	S4	15.743	98.488	45.289	103.211	491.32	467.444	431.63	0.210	0.221	0.239
	S12	34.500	57.327	51.698	67.677	606.986	568.636	511.111	0.111	0.119	0.132
	S1	198.077	151.628	243.565	211.051	384.6	368.85	353.1	0.633	0.660	0.690
	S9	258.995	73.285	280.980	150.983	618.63	587.88	557.13	0.454	0.478	0.504
	S2	45.887	198.653	105.483	212.419	733.14	698.49	663.84	0.290	0.304	0.320
	S10	93.129	113.677	127.232	141.616	1066.53	998.88	931.23	0.133	0.142	0.152
	S3	0.338	199.617	60.223	199.718	789.33	751.53	713.73	0.253	0.266	0.280
3	S11	0.949	153.382	46.963	153.667	1155.294	1081.494	1007.694	0.133	0.142	0.152
	S4	34.916	198.202	94.377	208.677	736.98	701.166	665.352	0.283	0.298	0.314
	S12	75.098	125.522	112.754	148.051	910.479	852.954	795.429	0.163	0.174	0.186
	S1	320.514	238.913	392.188	335.067	512.8	491.8	481.3	0.765	0.797	0.815
	S9	427.134	121.356	463.541	249.496	824.84	783.84	763.34	0.562	0.591	0.607
	S2	78.762	324.852	176.217	348.480	977.52	931.32	908.22	0.356	0.374	0.384
	S10	147.667	210.456	210.804	254.756	1422.04	1331.84	1286.74	0.179	0.191	0.198
2	S3	0.708	320.197	96.767	320.410	1052.44	1002.04	976.84	0.304	0.320	0.328
	S11	1.265	282.898	86.134	283.278	1540.392	1441.992	1392.792	0.184	0.196	0.203
	S4	62.951	323.198	159.910	342.084	982.64	934.888	911.012	0.348	0.366	0.375
	S12	128.588	231.930	198.167	270.506	1213.972	1137.272	1098.922	0.223	0.238	0.246
	S1	453.734	329.424	552.561	465.544	641	614.75	609.5	0.862	0.899	0.907
	S9	615.843	172.431	667.572	357.184	1031.05	979.8	969.55	0.647	0.681	0.689
	S2	116.149	467.064	256.268	501.909	1221.9	1164.15	1152.6	0.411	0.431	0.435
1	S10	201.536	331.353	300.942	391.813	1777.55	1664.8	1642.25	0.220	0.235	0.239
	S3	0.698	451.068	136.019	451.278	1315.55	1252.55	1239.95	0.343	0.360	0.364
	S11	1.241	445.416	134.865	445.788	1925.49	1802.49	1777.89	0.232	0.247	0.251
	S4	99.380	464.627	238.768	494.441	1228.3	1168.61	1156.672	0.403	0.423	0.427
	S12	191.276	365.074	300.799	422.457	1517.465	1421.59	1402.415	0.278	0.297	0.301
	S1	572.790	409.580	695.664	581.416	769.2	737.7	737.7	0.904	0.943	0.943
	S9	797.073	215.753	861.798	454.874	1237.26	1175.76	1175.76	0.697	0.733	0.733
	S2	144.447	600.461	324.585	643.795	1466.28	1396.98	1396.98	0.439	0.461	0.461
	S10	246.764	461.173	385.116	535.202	2133.06	1997.76	1997.76	0.251	0.268	0.268
	S3	1.203	574.549	173.567	574.910	1578.66	1503.06	1503.06	0.364	0.382	0.382
	S11	0.916	614.173	185.168	614.448	2310.588	2162.988	2162.988	0.266	0.284	0.284
	S4	123.675	596.945	302.758	634.048	1473.96	1402.332	1402.332	0.430	0.452	0.452
	S12	253.440	507.298	405.629	583.330	1820.958	1705.908	1705.908	0.320	0.342	0.342

Çizelge B.42: 9 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	19.751	20.074	25.773	25.999	128.2	117.7	104.575	0.203	0.221	0.249
	S9	26.496	3.395	27.515	11.344	206.21	185.71	160.085	0.133	0.148	0.172
	S2	2.475	28.961	11.163	29.703	244.38	221.28	192.405	0.122	0.134	0.154
	S10	1.933	3.473	2.975	4.053	355.51	310.41	254.035	0.011	0.013	0.016
	S3	1.205	28.508	9.757	28.870	263.11	237.91	206.41	0.110	0.121	0.140
	S11	1.259	6.094	3.088	6.472	385.098	335.898	274.398	0.017	0.019	0.024
	S4	0.644	28.905	9.315	29.099	245.66	221.784	191.939	0.118	0.131	0.152
8	S12	4.321	3.400	5.341	4.696	303.493	265.143	217.2055	0.018	0.020	0.025
	S1	73.424	65.587	93.100	87.614	256.4	235.4	211.775	0.363	0.395	0.440
	S9	96.676	23.428	103.704	52.431	412.42	371.42	325.295	0.251	0.279	0.319
	S2	2.765	90.899	30.035	91.728	488.76	442.56	390.585	0.188	0.207	0.235
	S10	18.417	31.366	27.827	36.891	711.02	620.82	519.345	0.052	0.059	0.071
	S3	1.834	90.041	28.847	90.591	526.22	475.82	419.12	0.172	0.190	0.216
	S11	1.791	43.908	14.963	44.445	770.196	671.796	561.096	0.058	0.066	0.079
7	S4	9.076	90.192	36.133	92.915	491.32	443.568	389.847	0.189	0.209	0.238
	S12	22.874	34.015	33.078	40.877	606.986	530.286	443.9985	0.067	0.077	0.092
	S1	157.157	132.206	196.819	179.353	384.6	353.1	318.975	0.512	0.557	0.617
	S9	207.031	55.277	223.615	117.387	618.63	557.13	490.505	0.361	0.401	0.456
	S2	18.243	179.883	72.208	185.356	733.14	663.84	588.765	0.253	0.279	0.315
	S10	54.259	76.497	77.208	92.774	1066.53	931.23	784.655	0.087	0.100	0.118
	S3	1.832	178.935	55.512	179.484	789.33	713.73	631.83	0.227	0.251	0.284
6	S11	1.414	107.044	33.527	107.468	1155.294	1007.694	847.794	0.093	0.107	0.127
	S4	23.134	178.400	76.654	185.340	736.98	665.352	587.755	0.251	0.279	0.315
	S12	53.898	84.095	79.126	100.264	910.479	795.429	670.7915	0.110	0.126	0.149
	S1	259.127	209.151	321.872	286.889	512.8	470.8	418.3	0.628	0.684	0.769
	S9	347.980	94.707	376.392	199.101	824.84	742.84	640.34	0.456	0.507	0.588
	S2	39.150	293.806	127.291	305.550	977.52	885.12	769.62	0.313	0.345	0.397
	S10	92.012	153.647	138.106	181.250	1422.04	1241.64	1016.14	0.127	0.146	0.178
5	S3	2.187	287.079	88.310	287.735	1052.44	951.64	825.64	0.273	0.302	0.348
	S11	1.740	211.541	65.202	212.063	1540.392	1343.592	1097.592	0.138	0.158	0.193
	S4	45.307	290.768	132.538	304.360	982.64	887.136	767.756	0.310	0.343	0.396
	S12	96.753	168.682	147.358	197.708	1213.972	1060.572	868.822	0.163	0.186	0.228
	S1	375.833	292.959	463.721	405.709	641	588.5	525.5	0.723	0.788	0.882
	S9	513.892	139.121	555.629	293.288	1031.05	928.55	805.55	0.539	0.598	0.690
	S2	65.608	427.990	194.005	447.672	1221.9	1106.4	967.8	0.366	0.405	0.463
4	S10	131.222	255.406	207.843	294.772	1777.55	1552.05	1281.45	0.166	0.190	0.230
	S3	2.919	409.666	125.819	410.542	1315.55	1189.55	1038.35	0.312	0.345	0.395
	S11	2.238	350.346	107.342	351.018	1925.49	1679.49	1384.29	0.182	0.209	0.254
	S4	76.558	423.269	203.538	446.237	1228.3	1108.92	965.664	0.363	0.402	0.462
	S12	149.341	280.159	233.389	324.962	1517.465	1325.715	1095.615	0.214	0.245	0.297
	S1	499.460	382.184	614.115	532.022	769.2	706.2	648.45	0.798	0.870	0.947
	S9	700.381	188.750	757.006	398.865	1237.26	1114.26	1001.51	0.612	0.679	0.756
3	S2	88.500	575.519	261.156	602.069	1466.28	1327.68	1200.63	0.411	0.453	0.501
	S10	170.275	393.702	288.385	444.784	2133.06	1862.46	1614.41	0.209	0.239	0.276
	S3	3.058	546.307	166.950	547.224	1578.66	1427.46	1288.86	0.347	0.383	0.425
	S11	3.044	522.448	159.779	523.361	2310.588	2015.388	1744.788	0.227	0.260	0.300
	S4	100.634	568.778	271.267	598.968	1473.96	1330.704	1199.386	0.406	0.450	0.499
	S12	212.651	431.091	341.978	494.886	1820.958	1590.858	1379.933	0.272	0.311	0.359
	S1	629.092	470.914	770.366	659.642	897.4	823.9	776.65	0.858	0.935	0.992
	S9	894.209	243.353	967.215	511.615	1443.47	1299.97	1207.72	0.670	0.744	0.801
	S2	106.543	733.180	326.497	765.143	1710.66	1548.96	1445.01	0.447	0.494	0.530
	S10	200.059	542.841	362.911	602.859	2488.57	2172.87	1969.92	0.242	0.277	0.306
	S3	4.279	700.107	214.311	701.390	1841.77	1665.37	1551.97	0.381	0.421	0.452

2	S11	3.286	725.468	220.926	726.453	2695.686	2351.286	2129.886	0.269	0.309	0.341
	S4	134.806	723.251	351.781	763.692	1719.62	1552.488	1445.046	0.444	0.492	0.528
	S12	263.455	593.113	441.389	672.150	2124.451	1856.001	1683.426	0.316	0.362	0.399
	S1	761.657	561.542	930.120	790.039	1025.6	941.6	904.85	0.907	0.988	1.028
	S9	1096.733	323.181	1193.687	652.201	1649.68	1485.68	1413.93	0.724	0.803	0.844
	S2	121.793	891.624	389.280	928.162	1955.04	1770.24	1689.39	0.475	0.524	0.549
	S10	236.909	697.940	446.290	769.012	2844.08	2483.28	2325.43	0.270	0.310	0.331
	S3	5.851	858.241	263.323	859.996	2104.88	1903.28	1815.08	0.409	0.452	0.474
	S11	3.061	928.451	281.596	929.369	3080.784	2687.184	2514.984	0.302	0.346	0.370
	S4	176.143	879.719	440.059	932.562	1965.28	1774.272	1690.706	0.475	0.526	0.552
	S12	314.658	761.928	543.236	856.325	2427.944	2121.144	1986.919	0.353	0.404	0.431
1	S1	874.958	637.616	1066.243	900.104	1153.8	1059.3	1033.05	0.924	1.007	1.032
	S9	1276.005	404.412	1397.328	787.213	1855.89	1671.39	1620.14	0.753	0.836	0.862
	S2	130.260	1026.357	438.167	1065.435	2199.42	1991.52	1933.77	0.484	0.535	0.551
	S10	271.928	842.123	524.565	923.701	3199.59	2793.69	2680.94	0.289	0.331	0.345
	S3	7.574	993.352	305.579	995.624	2367.99	2141.19	2078.19	0.420	0.465	0.479
	S11	3.314	1099.185	333.070	1100.179	3465.882	3023.082	2900.082	0.317	0.364	0.379
	S4	211.959	1012.326	515.657	1075.914	2210.94	1996.056	1936.366	0.487	0.539	0.556
	S12	367.200	917.331	642.399	1027.491	2731.437	2386.287	2290.412	0.376	0.431	0.449

Çizelge B.43: 12 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	15.955	20.114	21.989	24.900	128.2	117.7	117.700	0.194	0.212	0.212
	S9	21.684	0.147	21.728	6.652	206.21	185.71	185.710	0.105	0.117	0.117
	S2	7.171	29.528	16.029	31.679	244.38	221.28	221.280	0.130	0.143	0.143
	S10	4.269	2.177	4.922	3.458	355.51	310.41	310.410	0.014	0.016	0.016
	S3	1.341	29.707	10.253	30.110	263.11	237.91	237.910	0.114	0.127	0.127
	S11	1.699	1.040	2.011	1.550	385.098	335.898	335.898	0.005	0.006	0.006
	S4	1.906	29.453	10.742	30.025	245.66	221.784	221.784	0.122	0.135	0.135
11	S12	1.498	3.015	2.402	3.464	303.493	265.143	265.143	0.011	0.013	0.013
	S1	61.605	63.620	80.691	82.102	256.4	235.4	235.400	0.320	0.349	0.349
	S9	81.659	14.331	85.958	38.829	412.42	371.42	371.420	0.208	0.231	0.231
	S2	9.158	89.588	36.034	92.335	488.76	442.56	442.560	0.189	0.209	0.209
	S10	2.469	17.042	7.582	17.783	711.02	620.82	620.820	0.025	0.029	0.029
	S3	1.906	90.066	28.926	90.638	526.22	475.82	475.820	0.172	0.190	0.190
	S11	2.421	25.614	10.106	26.341	770.196	671.796	671.796	0.034	0.039	0.039
10	S4	3.017	88.830	29.666	89.735	491.32	443.568	443.568	0.183	0.202	0.202
	S12	15.630	17.801	20.970	22.490	606.986	530.286	530.286	0.037	0.042	0.042
	S1	133.161	125.290	170.748	165.238	384.6	353.1	353.100	0.444	0.484	0.484
	S9	176.227	39.036	187.938	91.904	618.63	557.13	557.130	0.304	0.337	0.337
	S2	2.220	172.859	54.077	173.525	733.14	663.84	663.840	0.237	0.261	0.261
	S10	26.041	51.062	41.359	58.874	1066.53	931.23	931.230	0.055	0.063	0.063
	S3	1.949	173.945	54.133	174.530	789.33	713.73	713.730	0.221	0.245	0.245
9	S11	2.410	73.918	24.585	74.641	1155.294	1007.694	1007.694	0.065	0.074	0.074
	S4	12.802	171.297	64.191	175.137	736.98	665.352	665.352	0.238	0.263	0.263
	S12	40.471	55.346	57.075	67.487	910.479	795.429	795.429	0.074	0.085	0.085
	S1	220.599	196.067	279.419	262.247	512.8	470.8	457.675	0.545	0.593	0.611
	S9	297.555	70.242	318.627	159.508	824.84	742.84	717.215	0.386	0.429	0.444
	S2	9.309	278.506	92.860	281.298	977.52	885.12	856.245	0.288	0.318	0.329
	S10	50.552	113.245	84.526	128.411	1422.04	1241.64	1185.265	0.090	0.103	0.108
8	S3	2.303	274.978	84.797	275.669	1052.44	951.64	920.140	0.262	0.290	0.300
	S11	2.885	158.669	50.485	159.534	1540.392	1343.592	1282.092	0.104	0.119	0.124
	S4	29.770	275.431	112.399	284.362	982.64	887.136	857.291	0.289	0.321	0.332
	S12	75.582	123.173	112.534	145.848	1213.972	1060.572	1012.635	0.120	0.138	0.144
	S1	321.878	273.592	403.956	370.156	641	588.5	564.875	0.630	0.686	0.715
	S9	442.124	105.963	473.913	238.600	1031.05	928.55	882.425	0.460	0.510	0.537
	S2	25.910	403.369	146.920	411.142	1221.9	1106.4	1054.425	0.336	0.372	0.390
7	S10	76.259	197.672	135.560	220.550	1777.55	1552.05	1450.575	0.124	0.142	0.152
	S3	2.994	389.863	119.952	390.761	1315.55	1189.55	1132.850	0.297	0.328	0.345
	S11	3.414	274.614	85.798	275.638	1925.49	1679.49	1568.790	0.143	0.164	0.176
	S4	55.121	398.653	174.717	415.190	1228.3	1108.92	1055.199	0.338	0.374	0.393
	S12	119.592	215.268	184.172	251.145	1517.465	1325.715	1239.428	0.166	0.189	0.203
	S1	430.741	357.224	537.908	486.446	769.2	706.2	672.075	0.699	0.762	0.800
	S9	607.511	146.840	651.563	329.094	1237.26	1114.26	1047.635	0.527	0.585	0.622
6	S2	39.182	542.291	201.869	554.045	1466.28	1327.68	1252.605	0.378	0.417	0.442
	S10	101.982	317.214	197.146	347.808	2133.06	1862.46	1715.885	0.163	0.187	0.203
	S3	3.186	519.389	159.003	520.345	1578.66	1427.46	1345.560	0.330	0.365	0.387
	S11	4.169	422.677	130.972	423.928	2310.588	2015.388	1855.488	0.183	0.210	0.228
	S4	73.801	535.566	234.471	557.706	1473.96	1330.704	1253.107	0.378	0.419	0.445
	S12	174.172	345.240	277.744	397.492	1820.958	1590.858	1466.221	0.218	0.250	0.271
	S1	547.713	442.448	680.447	606.762	897.4	823.9	784.525	0.758	0.826	0.867
6	S9	782.839	193.061	840.757	427.912	1443.47	1299.97	1223.095	0.582	0.647	0.687
	S2	48.117	694.318	256.412	708.753	1710.66	1548.96	1462.335	0.414	0.458	0.485
	S10	118.794	448.615	253.378	484.253	2488.57	2172.87	2003.745	0.195	0.223	0.242
	S3	4.301	668.630	204.890	669.921	1841.77	1665.37	1570.870	0.364	0.402	0.426

5	S11	4.347	602.761	185.176	604.065	2695.686	2351.286	2166.786	0.224	0.257	0.279
	S4	102.758	684.275	308.041	715.102	1719.62	1552.488	1462.953	0.416	0.461	0.489
	S12	217.247	487.252	363.422	552.426	2124.451	1856.001	1712.189	0.260	0.298	0.323
	S1	673.117	534.641	833.509	736.576	1025.6	941.6	902.225	0.813	0.885	0.924
	S9	975.345	268.448	1055.880	561.052	1649.68	1485.68	1408.805	0.640	0.711	0.749
	S2	54.859	855.442	311.492	871.900	1955.04	1770.24	1683.615	0.446	0.493	0.518
	S10	143.749	595.513	322.403	638.638	2844.08	2483.28	2314.155	0.225	0.257	0.276
	S3	5.618	829.240	254.390	830.925	2104.88	1903.28	1808.780	0.395	0.437	0.459
	S11	4.146	791.561	241.614	792.804	3080.784	2687.184	2502.684	0.257	0.295	0.317
	S4	139.303	842.449	392.037	884.240	1965.28	1774.272	1684.737	0.450	0.498	0.525
	S12	263.786	645.401	457.406	724.537	2427.944	2121.144	1977.332	0.298	0.342	0.366
	S1	806.493	631.146	995.837	873.094	1153.8	1059.3	1025.175	0.863	0.940	0.971
4	S9	1178.808	365.110	1288.341	718.752	1855.89	1671.39	1604.765	0.694	0.771	0.803
	S2	58.904	1022.882	365.769	1040.553	2199.42	1991.52	1916.445	0.473	0.522	0.543
	S10	174.655	761.050	402.970	813.446	3199.59	2793.69	2647.115	0.254	0.291	0.307
	S3	7.523	999.293	307.311	1001.550	2367.99	2141.19	2059.290	0.423	0.468	0.486
	S11	4.343	985.405	299.965	986.708	3465.882	3023.082	2863.182	0.285	0.326	0.345
	S4	182.833	1006.198	484.693	1061.048	2210.94	1996.056	1918.459	0.480	0.532	0.553
	S12	321.432	821.726	567.950	918.156	2731.437	2386.287	2261.650	0.336	0.385	0.406
	S1	956.570	739.522	1178.427	1026.493	1282	1177	1153.375	0.919	1.001	1.022
3	S9	1392.108	472.783	1533.943	890.415	2062.1	1857.1	1810.975	0.744	0.826	0.847
	S2	75.861	1188.986	432.556	1211.744	2443.8	2212.8	2160.825	0.496	0.548	0.561
	S10	214.336	935.825	495.083	1000.126	3555.1	3104.1	3002.625	0.281	0.322	0.333
	S3	8.409	1173.596	360.487	1176.119	2631.1	2379.1	2322.400	0.447	0.494	0.506
	S11	4.093	1189.536	360.953	1190.763	3850.98	3358.98	3248.280	0.309	0.355	0.367
	S4	230.282	1169.395	581.101	1238.480	2456.6	2217.84	2164.119	0.504	0.558	0.572
	S12	380.530	1008.802	683.170	1122.961	3034.93	2651.43	2565.143	0.370	0.424	0.438
	S1	1113.746	851.349	1369.150	1185.473	1410.2	1294.7	1281.575	0.971	1.058	1.068
2	S9	1604.377	585.870	1780.138	1067.183	2268.31	2042.81	2017.185	0.785	0.871	0.882
	S2	102.163	1348.228	506.631	1378.876	2688.18	2434.08	2405.205	0.513	0.566	0.573
	S10	260.346	1108.157	592.793	1186.260	3910.61	3414.51	3358.135	0.303	0.347	0.353
	S3	8.854	1340.020	410.860	1342.677	2894.21	2617.01	2585.510	0.464	0.513	0.519
	S11	3.662	1386.092	419.490	1387.191	4236.078	3694.878	3633.378	0.327	0.375	0.382
	S4	281.348	1326.865	679.407	1411.269	2702.26	2439.624	2409.779	0.522	0.578	0.586
	S12	440.586	1194.775	799.018	1326.951	3338.423	2916.573	2868.636	0.397	0.455	0.463
	S1	1240.507	935.423	1521.134	1307.575	1538.4	1412.4	1409.775	0.989	1.077	1.079
1	S9	1773.128	671.630	1974.617	1203.569	2474.52	2228.52	2223.395	0.798	0.886	0.888
	S2	121.148	1475.891	563.915	1512.235	2932.56	2655.36	2649.585	0.516	0.570	0.571
	S10	297.597	1243.682	670.701	1332.961	4266.12	3724.92	3713.645	0.312	0.358	0.359
	S3	9.800	1471.433	451.230	1474.373	3157.32	2854.92	2848.620	0.467	0.516	0.518
	S11	3.656	1537.232	464.826	1538.329	4621.176	4030.776	4018.476	0.333	0.382	0.383
	S4	327.869	1451.353	763.275	1549.713	2947.92	2661.408	2655.439	0.526	0.582	0.584
	S12	490.371	1338.382	891.885	1485.494	3641.916	3181.716	3172.129	0.408	0.467	0.468

Model 2

Çizelge B.44: 6 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.030	4.058	1.248	4.067	355.51	332.96	287.86	0.011	0.012	0.014
	S11	3.313	3.643	4.406	4.637	385.098	360.498	311.298	0.012	0.013	0.015
	S4	8.388	5.529	10.046	8.046	245.66	233.722	209.846	0.041	0.043	0.048
	S12	1.203	2.443	1.936	2.804	303.493	284.318	245.968	0.009	0.010	0.011
5	S10	0.029	4.832	1.479	4.841	711.02	665.92	598.27	0.007	0.007	0.008
	S11	7.931	11.432	11.361	13.812	770.196	720.996	647.196	0.018	0.019	0.021
	S4	14.723	14.164	18.972	18.581	491.32	467.444	431.63	0.039	0.041	0.044
	S12	4.112	8.611	6.696	9.845	606.986	568.636	511.111	0.016	0.017	0.019
4	S10	0.186	5.878	1.950	5.934	1066.53	998.88	931.23	0.006	0.006	0.006
	S11	12.296	19.136	18.037	22.825	1155.294	1081.494	1007.694	0.020	0.021	0.023
	S4	21.217	22.750	28.042	29.115	736.98	701.166	665.352	0.040	0.042	0.044
	S12	6.950	14.831	11.399	16.916	910.479	852.954	795.429	0.019	0.020	0.021
3	S10	0.242	4.768	1.672	4.840	1422.04	1331.84	1286.74	0.003	0.004	0.004
	S11	16.454	28.273	24.935	33.209	1540.392	1441.992	1392.792	0.022	0.023	0.024
	S4	26.787	31.399	36.207	39.435	982.64	934.888	911.012	0.040	0.042	0.043
	S12	10.025	22.329	16.724	25.337	1213.972	1137.272	1098.922	0.021	0.022	0.023
2	S10	1.012	1.993	1.610	2.297	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	19.883	37.655	31.179	43.620	1925.49	1802.49	1777.89	0.023	0.024	0.025
	S4	30.922	39.405	42.743	48.681	1228.3	1168.61	1156.672	0.040	0.042	0.042
	S12	12.938	30.080	21.962	33.961	1517.465	1421.59	1402.415	0.022	0.024	0.024
1	S10	1.375	1.055	1.691	1.467	2133.06	1997.76	1997.76	0.001	0.001	0.001
	S11	21.939	45.174	35.491	51.756	2310.588	2162.988	2162.988	0.022	0.024	0.024
	S4	33.243	45.406	46.865	55.379	1473.96	1402.332	1402.332	0.038	0.039	0.039
	S12	15.151	36.599	26.131	41.145	1820.958	1705.908	1705.908	0.023	0.024	0.024

Çizelge B.45: 9 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.191	6.476	2.134	6.533	355.51	310.41	254.035	0.018	0.021	0.026
	S11	5.144	4.257	6.421	5.800	385.098	335.898	274.398	0.017	0.019	0.023
	S4	12.478	8.534	15.038	12.277	245.66	221.784	191.939	0.061	0.068	0.078
	S12	1.079	2.941	1.961	3.264	303.493	265.143	217.2055	0.011	0.012	0.015
8	S10	0.445	7.641	2.737	7.774	711.02	620.82	519.345	0.011	0.013	0.015
	S11	12.557	15.119	17.093	18.886	770.196	671.796	561.096	0.025	0.028	0.034
	S4	21.891	22.472	28.632	29.039	491.32	443.568	389.847	0.059	0.065	0.074
	S12	4.889	11.624	8.376	13.091	606.986	530.286	443.9985	0.022	0.025	0.029
7	S10	0.578	9.521	3.434	9.694	1066.53	931.23	784.655	0.009	0.010	0.012
	S11	19.848	26.241	27.720	32.195	1155.294	1007.694	847.794	0.028	0.032	0.038
	S4	32.042	36.719	43.058	46.332	736.98	665.352	587.755	0.063	0.070	0.079
	S12	8.703	20.658	14.900	23.269	910.479	795.429	670.7915	0.026	0.029	0.035
6	S10	1.975	7.639	4.266	8.231	1422.04	1241.64	1072.515	0.006	0.007	0.008
	S11	27.488	41.130	39.827	49.376	1540.392	1343.592	1159.092	0.032	0.037	0.043
	S4	41.547	52.233	57.217	64.697	982.64	887.136	797.601	0.066	0.073	0.081
	S12	13.405	32.798	23.244	36.819	1213.972	1060.572	916.7595	0.030	0.035	0.040
5	S10	4.264	2.921	5.141	4.200	1777.55	1552.05	1382.925	0.003	0.003	0.004
	S11	35.080	58.743	52.703	69.267	1925.49	1679.49	1494.99	0.036	0.041	0.046
	S4	50.191	68.661	70.790	83.719	1228.3	1108.92	1019.385	0.068	0.075	0.082
	S12	18.676	47.009	32.778	52.612	1517.465	1325.715	1181.9025	0.035	0.040	0.045
4	S10	6.952	3.830	8.101	5.916	2133.06	1862.46	1715.885	0.004	0.004	0.005
	S11	42.267	77.569	65.538	90.249	2310.588	2015.388	1855.488	0.039	0.045	0.049
	S4	58.554	84.505	83.905	102.071	1473.96	1330.704	1253.107	0.069	0.077	0.081
	S12	24.408	63.338	43.409	70.661	1820.958	1590.858	1466.2205	0.039	0.044	0.048
3	S10	11.049	12.042	14.662	15.356	2488.57	2172.87	2071.395	0.006	0.007	0.007
	S11	48.678	98.256	78.155	112.859	2695.686	2351.286	2240.586	0.042	0.048	0.050
	S4	63.843	99.347	93.647	118.499	1719.62	1552.488	1498.767	0.069	0.076	0.079
	S12	28.832	79.258	52.610	87.907	2124.451	1856.001	1769.7135	0.041	0.047	0.050
2	S10	14.784	19.616	20.669	24.051	2844.08	2483.28	2426.905	0.008	0.010	0.010
	S11	53.580	116.318	88.476	132.392	3080.784	2687.184	2625.684	0.043	0.049	0.050
	S4	66.245	111.992	99.843	131.866	1965.28	1774.272	1744.427	0.067	0.074	0.076
	S12	32.216	92.589	59.993	102.254	2427.944	2121.144	2073.2065	0.042	0.048	0.049
1	S10	16.735	26.571	24.706	31.591	3199.59	2793.69	2782.415	0.010	0.011	0.011
	S11	56.386	128.875	95.048	145.790	3465.882	3023.082	3010.782	0.042	0.048	0.048
	S4	66.785	120.901	103.055	140.936	2210.94	1996.056	1990.087	0.064	0.071	0.071
	S12	35.394	103.188	66.350	113.806	2731.437	2386.287	2376.6995	0.042	0.048	0.048

Çizelge B.46: 12 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.430	8.622	3.017	8.751	355.51	310.41	310.41	0.025	0.028	0.028
	S11	6.645	3.589	7.722	5.583	385.098	335.898	335.898	0.020	0.023	0.023
	S4	16.194	11.750	19.719	16.608	245.66	221.784	221.784	0.080	0.089	0.089
	S12	0.363	2.728	1.182	2.837	303.493	265.143	265.143	0.009	0.011	0.011
11	S10	1.133	9.898	4.102	10.238	711.02	620.82	620.82	0.014	0.016	0.016
	S11	16.442	16.038	21.253	20.970	770.196	671.796	671.796	0.028	0.032	0.032
	S4	28.069	31.104	37.400	39.525	491.32	443.568	443.568	0.080	0.089	0.089
	S12	4.465	13.057	8.382	14.396	606.986	530.286	530.286	0.024	0.027	0.027
10	S10	1.683	12.267	5.363	12.772	1066.53	931.23	931.23	0.012	0.014	0.014
	S11	26.183	28.924	34.860	36.778	1155.294	1007.694	1007.694	0.032	0.036	0.036
	S4	41.163	50.995	56.462	63.344	736.98	665.352	665.352	0.086	0.095	0.095
	S12	8.589	23.952	15.774	26.528	910.479	795.429	795.429	0.029	0.033	0.033
9	S10	4.140	9.315	6.935	10.557	1422.04	1241.64	1185.265	0.007	0.009	0.009
	S11	36.656	47.472	50.898	58.469	1540.392	1343.592	1282.092	0.038	0.044	0.046
	S4	53.657	73.132	75.596	89.229	982.64	887.136	857.291	0.091	0.101	0.104
	S12	14.105	39.456	25.942	43.688	1213.972	1060.572	1012.6345	0.036	0.041	0.043
8	S10	8.016	2.380	8.730	4.785	1777.55	1552.05	1450.575	0.005	0.006	0.006
	S11	47.523	70.697	68.732	84.954	1925.49	1679.49	1568.79	0.044	0.051	0.054
	S4	65.542	97.442	94.774	117.105	1228.3	1108.92	1055.199	0.095	0.106	0.111
	S12	20.696	58.467	38.236	64.676	1517.465	1325.715	1239.4275	0.043	0.049	0.052
7	S10	12.836	8.397	15.355	12.247	2133.06	1862.46	1715.885	0.007	0.008	0.009
	S11	58.603	97.758	87.931	115.339	2310.588	2015.388	1855.488	0.050	0.057	0.062
	S4	78.096	122.477	114.839	145.906	1473.96	1330.704	1253.107	0.099	0.110	0.116
	S12	28.792	82.576	53.565	91.214	1820.958	1590.858	1466.2205	0.050	0.057	0.062
6	S10	20.939	22.165	27.588	28.446	2488.57	2172.87	2003.745	0.011	0.013	0.014
	S11	69.720	131.655	109.217	152.571	2695.686	2351.286	2166.786	0.057	0.065	0.070
	S4	86.619	148.664	131.218	174.649	1719.62	1552.488	1462.953	0.102	0.112	0.119
	S12	35.181	108.161	67.629	118.715	2124.451	1856.001	1712.1885	0.056	0.064	0.069
5	S10	29.647	37.724	40.964	46.618	2844.08	2483.28	2314.155	0.016	0.019	0.020
	S11	80.276	166.386	130.191	190.469	3080.784	2687.184	2502.684	0.062	0.071	0.076
	S4	91.659	174.983	144.154	202.481	1965.28	1774.272	1684.737	0.103	0.114	0.120
	S12	41.870	134.448	82.205	147.009	2427.944	2121.144	1977.3315	0.061	0.069	0.074
4	S10	37.243	54.399	53.562	65.572	3199.59	2793.69	2647.115	0.020	0.023	0.025
	S11	89.851	199.146	149.595	226.102	3465.882	3023.082	2863.182	0.065	0.075	0.079
	S4	94.511	199.659	154.409	228.013	2210.94	1996.056	1918.459	0.103	0.114	0.119
	S12	49.979	161.292	98.366	176.285	2731.437	2386.287	2261.6495	0.065	0.074	0.078
3	S10	44.059	69.786	64.995	83.004	3555.1	3104.1	3002.625	0.023	0.027	0.028
	S11	98.033	229.408	166.856	258.818	3850.98	3358.98	3248.28	0.067	0.077	0.080
	S4	95.319	221.195	161.678	249.790	2456.6	2217.84	2164.119	0.102	0.113	0.115
	S12	57.183	185.477	112.826	202.632	3034.93	2651.43	2565.1425	0.067	0.076	0.079
2	S10	49.478	83.735	74.598	98.578	3910.61	3414.51	3358.135	0.025	0.029	0.029
	S11	104.192	254.478	180.536	285.736	4236.078	3694.878	3633.378	0.067	0.077	0.079
	S4	94.986	238.750	166.611	267.246	2702.26	2439.624	2409.779	0.099	0.110	0.111
	S12	63.423	206.293	125.311	225.320	3338.423	2916.573	2868.6355	0.067	0.077	0.079
1	S10	52.438	93.489	80.484	109.221	4266.12	3724.92	3713.645	0.026	0.029	0.029
	S11	107.628	271.048	188.943	303.336	4621.176	4030.776	4018.476	0.066	0.075	0.075
	S4	92.865	250.670	168.066	278.529	2947.92	2661.408	2655.439	0.094	0.105	0.105
	S12	67.654	219.829	133.603	240.125	3641.916	3181.716	3172.1285	0.066	0.075	0.076

Çizelge B.47: 6 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.030	4.058	1.248	4.067	355.51	332.96	287.86	0.011	0.012	0.014
	S11	3.313	3.643	4.406	4.637	385.098	360.498	311.298	0.012	0.013	0.015
	S4	8.388	5.529	10.046	8.046	245.66	233.722	209.846	0.041	0.043	0.048
	S12	1.203	2.443	1.936	2.804	303.493	284.318	245.968	0.009	0.010	0.011
5	S10	0.029	4.832	1.479	4.841	711.02	665.92	598.27	0.007	0.007	0.008
	S11	7.931	11.432	11.361	13.812	770.196	720.996	647.196	0.018	0.019	0.021
	S4	14.723	14.164	18.972	18.581	491.32	467.444	431.63	0.039	0.041	0.044
	S12	4.112	8.611	6.696	9.845	606.986	568.636	511.111	0.016	0.017	0.019
4	S10	0.186	5.878	1.950	5.934	1066.53	998.88	931.23	0.006	0.006	0.006
	S11	12.296	19.136	18.037	22.825	1155.294	1081.494	1007.694	0.020	0.021	0.023
	S4	21.217	22.750	28.042	29.115	736.98	701.166	665.352	0.040	0.042	0.044
	S12	6.950	14.831	11.399	16.916	910.479	852.954	795.429	0.019	0.020	0.021
3	S10	0.242	4.768	1.672	4.840	1422.04	1331.84	1286.74	0.003	0.004	0.004
	S11	16.454	28.273	24.935	33.209	1540.392	1441.992	1392.792	0.022	0.023	0.024
	S4	26.787	31.399	36.207	39.435	982.64	934.888	911.012	0.040	0.042	0.043
	S12	10.025	22.329	16.724	25.337	1213.972	1137.272	1098.922	0.021	0.022	0.023
2	S10	1.012	1.993	1.610	2.297	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	19.883	37.655	31.179	43.620	1925.49	1802.49	1777.89	0.023	0.024	0.025
	S4	30.922	39.405	42.743	48.681	1228.3	1168.61	1156.672	0.040	0.042	0.042
	S12	12.938	30.080	21.962	33.961	1517.465	1421.59	1402.415	0.022	0.024	0.024
1	S10	1.375	1.055	1.691	1.467	2133.06	1997.76	1997.76	0.001	0.001	0.001
	S11	21.939	45.174	35.491	51.756	2310.588	2162.988	2162.988	0.022	0.024	0.024
	S4	33.243	45.406	46.865	55.379	1473.96	1402.332	1402.332	0.038	0.039	0.039
	S12	15.151	36.599	26.131	41.145	1820.958	1705.908	1705.908	0.023	0.024	0.024

Çizelge B.48: 9 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}, k_{E\beta} = N_E / N_{G+\beta Q0}, k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.191	6.476	2.134	6.533	355.51	310.41	254.035	0.018	0.021	0.026
	S11	5.144	4.257	6.421	5.800	385.098	335.898	274.398	0.017	0.019	0.023
	S4	12.478	8.534	15.038	12.277	245.66	221.784	191.939	0.061	0.068	0.078
	S12	1.079	2.941	1.961	3.264	303.493	265.143	217.2055	0.011	0.012	0.015
8	S10	0.445	7.641	2.737	7.774	711.02	620.82	519.345	0.011	0.013	0.015
	S11	12.557	15.119	17.093	18.886	770.196	671.796	561.096	0.025	0.028	0.034
	S4	21.891	22.472	28.632	29.039	491.32	443.568	389.847	0.059	0.065	0.074
	S12	4.889	11.624	8.376	13.091	606.986	530.286	443.9985	0.022	0.025	0.029
7	S10	0.578	9.521	3.434	9.694	1066.53	931.23	784.655	0.009	0.010	0.012
	S11	19.848	26.241	27.720	32.195	1155.294	1007.694	847.794	0.028	0.032	0.038
	S4	32.042	36.719	43.058	46.332	736.98	665.352	587.755	0.063	0.070	0.079
	S12	8.703	20.658	14.900	23.269	910.479	795.429	670.7915	0.026	0.029	0.035
6	S10	1.975	7.639	4.266	8.231	1422.04	1241.64	1072.515	0.006	0.007	0.008
	S11	27.488	41.130	39.827	49.376	1540.392	1343.592	1159.092	0.032	0.037	0.043
	S4	41.547	52.233	57.217	64.697	982.64	887.136	797.601	0.066	0.073	0.081
	S12	13.405	32.798	23.244	36.819	1213.972	1060.572	916.7595	0.030	0.035	0.040
5	S10	4.264	2.921	5.141	4.200	1777.55	1552.05	1382.925	0.003	0.003	0.004
	S11	35.080	58.743	52.703	69.267	1925.49	1679.49	1494.99	0.036	0.041	0.046
	S4	50.191	68.661	70.790	83.719	1228.3	1108.92	1019.385	0.068	0.075	0.082
	S12	18.676	47.009	32.778	52.612	1517.465	1325.715	1181.9025	0.035	0.040	0.045
4	S10	6.952	3.830	8.101	5.916	2133.06	1862.46	1715.885	0.004	0.004	0.005
	S11	42.267	77.569	65.538	90.249	2310.588	2015.388	1855.488	0.039	0.045	0.049
	S4	58.554	84.505	83.905	102.071	1473.96	1330.704	1253.107	0.069	0.077	0.081
	S12	24.408	63.338	43.409	70.661	1820.958	1590.858	1466.2205	0.039	0.044	0.048
3	S10	11.049	12.042	14.662	15.356	2488.57	2172.87	2071.395	0.006	0.007	0.007
	S11	48.678	98.256	78.155	112.859	2695.686	2351.286	2240.586	0.042	0.048	0.050
	S4	63.843	99.347	93.647	118.499	1719.62	1552.488	1498.767	0.069	0.076	0.079
	S12	28.832	79.258	52.610	87.907	2124.451	1856.001	1769.7135	0.041	0.047	0.050
2	S10	14.784	19.616	20.669	24.051	2844.08	2483.28	2426.905	0.008	0.010	0.010
	S11	53.580	116.318	88.476	132.392	3080.784	2687.184	2625.684	0.043	0.049	0.050
	S4	66.245	111.992	99.843	131.866	1965.28	1774.272	1744.427	0.067	0.074	0.076
	S12	32.216	92.589	59.993	102.254	2427.944	2121.144	2073.2065	0.042	0.048	0.049
1	S10	16.735	26.571	24.706	31.591	3199.59	2793.69	2782.415	0.010	0.011	0.011
	S11	56.386	128.875	95.048	145.790	3465.882	3023.082	3010.782	0.042	0.048	0.048
	S4	66.785	120.901	103.055	140.936	2210.94	1996.056	1990.087	0.064	0.071	0.071
	S12	35.394	103.188	66.350	113.806	2731.437	2386.287	2376.6995	0.042	0.048	0.048

Çizelge B.49: 12 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.484	9.700	3.394	9.845	355.51	310.41	310.41	0.028	0.032	0.032
	S11	7.476	4.038	8.687	6.281	385.098	335.898	335.898	0.023	0.026	0.026
	S4	18.218	13.219	22.184	18.684	245.66	221.784	221.784	0.090	0.100	0.100
	S12	0.409	3.069	1.329	3.192	303.493	265.143	265.143	0.011	0.012	0.012
11	S10	1.275	11.135	4.615	11.518	711.02	620.82	620.82	0.016	0.019	0.019
	S11	18.497	18.043	23.910	23.592	770.196	671.796	671.796	0.031	0.036	0.036
	S4	31.578	34.992	42.075	44.466	491.32	443.568	443.568	0.091	0.100	0.100
	S12	5.023	14.689	9.430	16.196	606.986	530.286	530.286	0.027	0.031	0.031
10	S10	1.893	13.800	6.033	14.368	1066.53	931.23	931.23	0.013	0.015	0.015
	S11	29.455	32.539	39.217	41.376	1155.294	1007.694	1007.694	0.036	0.041	0.041
	S4	46.309	57.369	63.519	71.261	736.98	665.352	665.352	0.097	0.107	0.107
	S12	9.662	26.945	17.746	29.844	910.479	795.429	795.429	0.033	0.038	0.038
9	S10	4.658	10.480	7.801	11.877	1422.04	1241.64	1185.265	0.008	0.010	0.010
	S11	41.238	53.406	57.260	65.778	1540.392	1343.592	1282.092	0.043	0.049	0.051
	S4	60.364	82.273	85.046	100.382	982.64	887.136	857.291	0.102	0.113	0.117
	S12	15.868	44.388	29.184	49.149	1213.972	1060.572	1012.6345	0.040	0.046	0.049
8	S10	9.018	2.677	9.821	5.383	1777.55	1552.05	1450.575	0.006	0.006	0.007
	S11	53.464	79.534	77.324	95.573	1925.49	1679.49	1568.79	0.050	0.057	0.061
	S4	73.734	109.622	106.621	131.743	1228.3	1108.92	1055.199	0.107	0.119	0.125
	S12	23.283	65.775	43.015	72.760	1517.465	1325.715	1239.4275	0.048	0.055	0.059
7	S10	14.440	9.446	17.274	13.778	2133.06	1862.46	1715.885	0.008	0.009	0.010
	S11	65.929	109.978	98.922	129.756	2310.588	2015.388	1855.488	0.056	0.064	0.070
	S4	87.858	137.787	129.194	164.144	1473.96	1330.704	1253.107	0.111	0.123	0.131
	S12	32.392	92.898	60.261	102.616	1820.958	1590.858	1466.2205	0.056	0.065	0.070
6	S10	23.556	24.935	31.037	32.002	2488.57	2172.87	2003.745	0.013	0.015	0.016
	S11	78.435	148.112	122.869	171.642	2695.686	2351.286	2166.786	0.064	0.073	0.079
	S4	97.447	167.247	147.621	196.481	1719.62	1552.488	1462.953	0.114	0.127	0.134
	S12	39.579	121.681	76.083	133.554	2124.451	1856.001	1712.1885	0.063	0.072	0.078
5	S10	33.353	42.439	46.085	52.445	2844.08	2483.28	2314.155	0.018	0.021	0.023
	S11	90.310	187.184	146.465	214.277	3080.784	2687.184	2502.684	0.070	0.080	0.086
	S4	103.116	196.856	162.173	227.791	1965.28	1774.272	1684.737	0.116	0.128	0.135
	S12	47.104	151.254	92.480	165.386	2427.944	2121.144	1977.3315	0.068	0.078	0.084
4	S10	41.898	61.199	60.258	73.768	3199.59	2793.69	2647.115	0.023	0.026	0.028
	S11	101.083	224.040	168.295	254.364	3465.882	3023.082	2863.182	0.073	0.084	0.089
	S4	106.325	224.617	173.710	256.514	2210.94	1996.056	1918.459	0.116	0.129	0.134
	S12	56.226	181.453	110.662	198.321	2731.437	2386.287	2261.6495	0.073	0.083	0.088
3	S10	49.567	78.510	73.119	93.380	3555.1	3104.1	3002.625	0.026	0.030	0.031
	S11	110.287	258.084	187.712	291.170	3850.98	3358.98	3248.28	0.076	0.087	0.090
	S4	107.234	248.844	181.887	281.014	2456.6	2217.84	2164.119	0.114	0.127	0.130
	S12	64.331	208.662	126.929	227.961	3034.93	2651.43	2565.1425	0.075	0.086	0.089
2	S10	55.663	94.202	83.923	110.901	3910.61	3414.51	3358.135	0.028	0.032	0.033
	S11	117.216	286.288	203.103	321.453	4236.078	3694.878	3633.378	0.076	0.087	0.088
	S4	106.860	268.594	187.438	300.651	2702.26	2439.624	2409.779	0.111	0.123	0.125
	S12	71.351	232.080	140.975	253.485	3338.423	2916.573	2868.6355	0.076	0.087	0.088
1	S10	58.992	105.176	90.545	122.873	4266.12	3724.92	3713.645	0.029	0.033	0.033
	S11	121.082	304.929	212.561	341.253	4621.176	4030.776	4018.476	0.074	0.085	0.085
	S4	104.473	282.004	189.074	313.346	2947.92	2661.408	2655.439	0.106	0.118	0.118
	S12	76.111	247.308	150.304	270.141	3641.916	3181.716	3172.1285	0.074	0.085	0.085

Çizelge B.50: 6 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.057	7.609	2.339	7.626	355.51	332.96	287.86	0.021	0.023	0.026
	S11	6.213	6.831	8.262	8.695	385.098	360.498	311.298	0.023	0.024	0.028
	S4	15.727	10.367	18.837	15.085	245.66	233.722	209.846	0.077	0.081	0.090
	S12	2.255	4.580	3.629	5.257	303.493	284.318	245.968	0.017	0.018	0.021
5	S10	0.054	9.060	2.772	9.077	711.02	665.92	598.27	0.013	0.014	0.015
	S11	14.871	21.435	21.301	25.897	770.196	720.996	647.196	0.034	0.036	0.040
	S4	27.606	26.557	35.573	34.839	491.32	467.444	431.63	0.072	0.076	0.082
	S12	7.711	16.145	12.554	18.459	606.986	568.636	511.111	0.030	0.032	0.036
4	S10	0.349	11.021	3.655	11.126	1066.53	998.88	931.23	0.010	0.011	0.012
	S11	23.055	35.880	33.819	42.796	1155.294	1081.494	1007.694	0.037	0.040	0.042
	S4	39.782	42.657	52.579	54.592	736.98	701.166	665.352	0.074	0.078	0.082
	S12	13.031	27.808	21.374	31.718	910.479	852.954	795.429	0.035	0.037	0.040
3	S10	0.454	8.940	3.136	9.076	1422.04	1331.84	1286.74	0.006	0.007	0.007
	S11	30.850	53.011	46.754	62.266	1540.392	1441.992	1392.792	0.040	0.043	0.045
	S4	50.226	58.874	67.888	73.941	982.64	934.888	911.012	0.075	0.079	0.081
	S12	18.798	41.867	31.358	47.506	1213.972	1137.272	1098.922	0.039	0.042	0.043
2	S10	1.898	3.737	3.019	4.307	1777.55	1664.8	1642.25	0.002	0.003	0.003
	S11	37.280	70.604	58.461	81.787	1925.49	1802.49	1777.89	0.042	0.045	0.046
	S4	57.978	73.884	80.143	91.278	1228.3	1168.61	1156.672	0.074	0.078	0.079
	S12	24.258	56.400	41.178	63.677	1517.465	1421.59	1402.415	0.042	0.045	0.045
1	S10	2.578	1.978	3.171	2.751	2133.06	1997.76	1997.76	0.001	0.002	0.002
	S11	41.136	84.702	66.546	97.042	2310.588	2162.988	2162.988	0.042	0.045	0.045
	S4	62.331	85.136	87.872	103.836	1473.96	1402.332	1402.332	0.070	0.074	0.074
	S12	28.408	68.624	48.995	77.146	1820.958	1705.908	1705.908	0.042	0.045	0.045

Çizelge B.51: 9 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.358	12.142	4.000	12.249	355.51	310.41	254.035	0.034	0.039	0.048
	S11	9.645	7.982	12.039	10.875	385.098	335.898	274.398	0.031	0.036	0.044
	S4	23.396	16.001	28.196	23.019	245.66	221.784	191.939	0.115	0.127	0.147
	S12	2.023	5.514	3.677	6.121	303.493	265.143	217.2055	0.020	0.023	0.028
8	S10	0.833	14.326	5.131	14.576	711.02	620.82	519.345	0.021	0.023	0.028
	S11	23.545	28.348	32.050	35.412	770.196	671.796	561.096	0.046	0.053	0.063
	S4	41.045	42.135	53.686	54.448	491.32	443.568	389.847	0.111	0.123	0.140
	S12	9.167	21.795	15.706	24.545	606.986	530.286	443.9985	0.040	0.046	0.055
7	S10	1.083	17.851	6.438	18.176	1066.53	931.23	784.655	0.017	0.020	0.023
	S11	37.215	49.201	51.976	60.366	1155.294	1007.694	847.794	0.052	0.060	0.071
	S4	60.080	68.848	80.734	86.872	736.98	665.352	587.755	0.118	0.131	0.148
	S12	16.317	38.734	27.937	43.629	910.479	795.429	670.7915	0.048	0.055	0.065
6	S10	3.702	14.323	7.999	15.434	1422.04	1241.64	1072.515	0.011	0.012	0.014
	S11	51.541	77.119	74.676	92.581	1540.392	1343.592	1159.092	0.060	0.069	0.080
	S4	77.900	97.938	107.281	121.308	982.64	887.136	797.601	0.123	0.137	0.152
	S12	25.134	61.496	43.583	69.036	1213.972	1060.572	916.7595	0.057	0.065	0.075
5	S10	7.995	5.477	9.639	7.876	1777.55	1552.05	1382.925	0.005	0.006	0.007
	S11	65.776	110.143	98.819	129.876	1925.49	1679.49	1494.99	0.067	0.077	0.087
	S4	94.109	128.740	132.731	156.973	1228.3	1108.92	1019.385	0.128	0.142	0.154
	S12	35.017	88.142	61.460	98.647	1517.465	1325.715	1181.9025	0.065	0.074	0.083
4	S10	13.034	7.182	15.189	11.092	2133.06	1862.46	1715.885	0.007	0.008	0.009
	S11	79.250	145.442	122.883	169.217	2310.588	2015.388	1855.488	0.073	0.084	0.091
	S4	109.789	158.446	157.322	191.383	1473.96	1330.704	1253.107	0.130	0.144	0.153
	S12	45.764	118.759	81.392	132.489	1820.958	1590.858	1466.2205	0.073	0.083	0.090
3	S10	20.717	22.578	27.490	28.793	2488.57	2172.87	2071.395	0.012	0.013	0.014
	S11	91.272	184.229	146.541	211.611	2695.686	2351.286	2240.586	0.078	0.090	0.094
	S4	119.705	186.275	175.587	222.186	1719.62	1552.488	1498.767	0.129	0.143	0.148
	S12	54.061	148.608	98.643	164.827	2124.451	1856.001	1769.7135	0.078	0.089	0.093
2	S10	27.720	36.780	38.754	45.096	2844.08	2483.28	2426.905	0.016	0.018	0.019
	S11	100.463	218.097	165.892	248.235	3080.784	2687.184	2625.684	0.081	0.092	0.095
	S4	124.210	209.986	187.205	247.248	1965.28	1774.272	1744.427	0.126	0.139	0.142
	S12	60.406	173.604	112.487	191.726	2427.944	2121.144	2073.2065	0.079	0.090	0.092
1	S10	31.379	49.820	46.325	59.234	3199.59	2793.69	2782.415	0.019	0.021	0.021
	S11	105.723	241.640	178.215	273.357	3465.882	3023.082	3010.782	0.079	0.090	0.091
	S4	125.221	226.689	193.228	264.255	2210.94	1996.056	1990.087	0.120	0.132	0.133
	S12	66.364	193.477	124.407	213.386	2731.437	2386.287	2376.6995	0.078	0.089	0.090

Çizelge B.52: 12 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.762	15.260	5.340	15.488	355.51	310.41	310.41	0.044	0.050	0.050
	S11	11.761	6.352	13.666	9.880	385.098	335.898	335.898	0.035	0.041	0.041
	S4	28.660	20.796	34.899	29.394	245.66	221.784	221.784	0.142	0.157	0.157
	S12	0.643	4.828	2.091	5.021	303.493	265.143	265.143	0.017	0.019	0.019
11	S10	2.005	17.518	7.260	18.119	711.02	620.82	620.82	0.025	0.029	0.029
	S11	29.099	28.384	37.614	37.114	770.196	671.796	671.796	0.049	0.056	0.056
	S4	49.677	55.049	66.192	69.952	491.32	443.568	443.568	0.142	0.158	0.158
	S12	7.903	23.108	14.835	25.479	606.986	530.286	530.286	0.042	0.048	0.048
10	S10	2.978	21.710	9.491	22.603	1066.53	931.23	931.23	0.021	0.024	0.024
	S11	46.338	51.190	61.695	65.091	1155.294	1007.694	1007.694	0.056	0.065	0.065
	S4	72.852	90.251	99.927	112.107	736.98	665.352	665.352	0.152	0.168	0.168
	S12	15.201	42.390	27.918	46.950	910.479	795.429	795.429	0.052	0.059	0.059
9	S10	7.327	16.486	12.273	18.684	1422.04	1241.64	1185.265	0.013	0.015	0.016
	S11	64.875	84.017	90.080	103.480	1540.392	1343.592	1282.092	0.067	0.077	0.081
	S4	94.963	129.430	133.792	157.919	982.64	887.136	857.291	0.161	0.178	0.184
	S12	24.963	69.831	45.912	77.319	1213.972	1060.572	1012.6345	0.064	0.073	0.076
8	S10	14.187	4.212	15.451	8.468	1777.55	1552.05	1450.575	0.009	0.010	0.011
	S11	84.108	125.121	121.644	150.354	1925.49	1679.49	1568.79	0.078	0.090	0.096
	S4	115.997	172.455	167.734	207.254	1228.3	1108.92	1055.199	0.169	0.187	0.196
	S12	36.628	103.476	67.670	114.464	1517.465	1325.715	1239.4275	0.075	0.086	0.092
7	S10	22.717	14.860	27.175	21.675	2133.06	1862.46	1715.885	0.013	0.015	0.016
	S11	103.717	173.014	155.622	204.130	2310.588	2015.388	1855.488	0.088	0.101	0.110
	S4	138.216	216.763	203.244	258.228	1473.96	1330.704	1253.107	0.175	0.194	0.206
	S12	50.958	146.145	94.801	161.433	1820.958	1590.858	1466.2205	0.089	0.101	0.110
6	S10	37.058	39.227	48.827	50.345	2488.57	2172.87	2003.745	0.020	0.023	0.025
	S11	123.393	233.005	193.294	270.023	2695.686	2351.286	2166.786	0.100	0.115	0.125
	S4	153.301	263.108	232.233	309.098	1719.62	1552.488	1462.953	0.180	0.199	0.211
	S12	62.264	191.425	119.692	210.104	2124.451	1856.001	1712.1885	0.099	0.113	0.123
5	S10	52.470	66.764	72.500	82.505	2844.08	2483.28	2314.155	0.029	0.033	0.036
	S11	142.074	294.473	230.416	337.095	3080.784	2687.184	2502.684	0.109	0.125	0.135
	S4	162.220	309.689	255.126	358.355	1965.28	1774.272	1684.737	0.182	0.202	0.213
	S12	74.103	237.950	145.488	260.181	2427.944	2121.144	1977.3315	0.107	0.123	0.132
4	S10	65.913	96.276	94.796	116.050	3199.59	2793.69	2647.115	0.036	0.042	0.044
	S11	159.021	352.454	264.757	400.160	3465.882	3023.082	2863.182	0.115	0.132	0.140
	S4	167.268	353.362	273.276	403.542	2210.94	1996.056	1918.459	0.183	0.202	0.210
	S12	88.453	285.458	174.090	311.994	2731.437	2386.287	2261.6495	0.114	0.131	0.138
3	S10	77.977	123.510	115.030	146.903	3555.1	3104.1	3002.625	0.041	0.047	0.049
	S11	173.501	406.012	295.305	458.062	3850.98	3358.98	3248.28	0.119	0.136	0.141
	S4	168.698	391.475	286.141	442.085	2456.6	2217.84	2164.119	0.180	0.199	0.204
	S12	101.203	328.262	199.682	358.623	3034.93	2651.43	2565.1425	0.118	0.135	0.140
2	S10	87.567	148.196	132.026	174.466	3910.61	3414.51	3358.135	0.045	0.051	0.052
	S11	184.402	450.381	319.516	505.702	4236.078	3694.878	3633.378	0.119	0.137	0.139
	S4	168.109	422.545	294.872	472.978	2702.26	2439.624	2409.779	0.175	0.194	0.196
	S12	112.248	365.102	221.779	398.776	3338.423	2916.573	2868.6355	0.119	0.137	0.139
1	S10	92.805	165.460	142.443	193.301	4266.12	3724.92	3713.645	0.045	0.052	0.052
	S11	190.483	479.707	334.395	536.852	4621.176	4030.776	4018.476	0.116	0.133	0.134
	S4	164.354	443.642	297.446	492.948	2947.92	2661.408	2655.439	0.167	0.185	0.186
	S12	119.736	389.058	236.454	424.979	3641.916	3181.716	3172.1285	0.117	0.134	0.134

Çizelge B.53: 6 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.078	10.551	3.244	10.575	355.51	332.96	287.86	0.030	0.032	0.037
	S11	8.615	9.473	11.457	12.057	385.098	360.498	311.298	0.031	0.033	0.039
	S4	21.808	14.376	26.121	20.918	245.66	233.722	209.846	0.106	0.112	0.124
	S12	3.128	6.351	5.033	7.289	303.493	284.318	245.968	0.024	0.026	0.030
5	S10	0.075	12.564	3.844	12.586	711.02	665.92	598.27	0.018	0.019	0.021
	S11	20.621	29.724	29.538	35.910	770.196	720.996	647.196	0.047	0.050	0.055
	S4	38.280	36.826	49.328	48.310	491.32	467.444	431.63	0.100	0.106	0.114
	S12	10.692	22.388	17.409	25.596	606.986	568.636	511.111	0.042	0.045	0.050
4	S10	0.484	15.282	5.069	15.428	1066.53	998.88	931.23	0.014	0.015	0.017
	S11	31.970	49.754	46.896	59.344	1155.294	1081.494	1007.694	0.051	0.055	0.059
	S4	55.165	59.151	72.910	75.700	736.98	701.166	665.352	0.103	0.108	0.114
	S12	18.070	38.561	29.638	43.982	910.479	852.954	795.429	0.048	0.052	0.055
3	S10	0.630	12.396	4.348	12.585	1422.04	1331.84	1286.74	0.009	0.009	0.010
	S11	42.779	73.509	64.832	86.343	1540.392	1441.992	1392.792	0.056	0.060	0.062
	S4	69.646	81.638	94.137	102.532	982.64	934.888	911.012	0.104	0.110	0.113
	S12	26.066	58.055	43.483	65.875	1213.972	1137.272	1098.922	0.054	0.058	0.060
2	S10	2.632	5.182	4.187	5.972	1777.55	1664.8	1642.25	0.003	0.004	0.004
	S11	51.695	97.904	81.066	113.412	1925.49	1802.49	1777.89	0.059	0.063	0.064
	S4	80.396	102.453	111.132	126.572	1228.3	1168.61	1156.672	0.103	0.108	0.109
	S12	33.638	78.207	57.101	88.299	1517.465	1421.59	1402.415	0.058	0.062	0.063
1	S10	3.575	2.743	4.398	3.815	2133.06	1997.76	1997.76	0.002	0.002	0.002
	S11	57.041	117.453	92.277	134.565	2310.588	2162.988	2162.988	0.058	0.062	0.062
	S4	86.432	118.056	121.849	143.985	1473.96	1402.332	1402.332	0.098	0.103	0.103
	S12	39.392	95.159	67.939	106.976	1820.958	1705.908	1705.908	0.059	0.063	0.063

Çizelge B.54: 9 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.496	16.837	5.547	16.986	355.51	310.41	254.035	0.048	0.055	0.067
	S11	13.374	11.068	16.694	15.080	385.098	335.898	274.398	0.043	0.050	0.061
	S4	32.443	22.187	39.099	31.920	245.66	221.784	191.939	0.159	0.176	0.204
	S12	2.805	7.646	5.099	8.487	303.493	265.143	217.2055	0.028	0.032	0.039
8	S10	1.156	19.866	7.115	20.213	711.02	620.82	530.62	0.028	0.033	0.038
	S11	32.649	39.310	44.442	49.104	770.196	671.796	573.396	0.064	0.073	0.086
	S4	56.916	58.427	74.444	75.502	491.32	443.568	395.816	0.154	0.170	0.191
	S12	12.712	30.222	21.778	34.035	606.986	530.286	453.586	0.056	0.064	0.075
7	S10	1.502	24.754	8.928	25.204	1066.53	931.23	795.93	0.024	0.027	0.032
	S11	51.605	68.226	72.073	83.707	1155.294	1007.694	860.094	0.072	0.083	0.097
	S4	83.310	95.469	111.951	120.462	736.98	665.352	593.724	0.163	0.181	0.203
	S12	22.626	53.711	38.740	60.498	910.479	795.429	680.379	0.066	0.076	0.089
6	S10	5.134	19.861	11.092	21.401	1422.04	1241.64	1151.44	0.015	0.017	0.019
	S11	71.470	106.938	103.551	128.379	1540.392	1343.592	1245.192	0.083	0.096	0.103
	S4	108.021	135.807	148.763	168.213	982.64	887.136	839.384	0.171	0.190	0.200
	S12	34.853	85.274	60.435	95.730	1213.972	1060.572	983.872	0.079	0.090	0.097
5	S10	11.087	7.595	13.366	10.921	1777.55	1552.05	1552.05	0.008	0.009	0.009
	S11	91.209	152.732	137.029	180.094	1925.49	1679.49	1679.49	0.094	0.107	0.107
	S4	130.498	178.520	184.053	217.669	1228.3	1108.92	1108.92	0.177	0.196	0.196
	S12	48.557	122.224	85.224	136.791	1517.465	1325.715	1325.715	0.090	0.103	0.103
4	S10	18.074	9.959	21.062	15.381	2133.06	1862.46	1997.76	0.010	0.011	0.011
	S11	109.894	201.680	170.398	234.648	2310.588	2015.388	2162.988	0.102	0.116	0.108
	S4	152.240	219.712	218.154	265.384	1473.96	1330.704	1402.332	0.180	0.199	0.189
	S12	63.460	164.680	112.864	183.718	1820.958	1590.858	1705.908	0.101	0.115	0.108
3	S10	28.727	31.308	38.120	39.927	2488.57	2172.87	2488.57	0.016	0.018	0.016
	S11	126.564	255.464	203.203	293.433	2695.686	2351.286	2695.686	0.109	0.125	0.109
	S4	165.991	258.301	243.481	308.098	1719.62	1552.488	1719.62	0.179	0.198	0.179
	S12	74.964	206.070	136.785	228.560	2124.451	1856.001	2124.451	0.108	0.123	0.108
2	S10	38.439	51.002	53.739	62.533	2844.08	2483.28	2844.08	0.022	0.025	0.022
	S11	139.309	302.427	230.037	344.220	3080.784	2687.184	3080.784	0.112	0.128	0.112
	S4	172.237	291.180	259.591	342.851	1965.28	1774.272	1965.28	0.174	0.193	0.174
	S12	83.763	240.731	155.982	265.860	2427.944	2121.144	2427.944	0.110	0.125	0.110
1	S10	43.512	69.084	64.237	82.137	3199.59	2793.69	3199.59	0.026	0.029	0.026
	S11	146.603	335.074	247.125	379.055	3465.882	3023.082	3465.882	0.109	0.125	0.109
	S4	173.640	314.342	267.942	366.434	2210.94	1996.056	2210.94	0.166	0.184	0.166
	S12	92.024	268.288	172.511	295.896	2731.437	2386.287	2731.437	0.108	0.124	0.108

Çizelge B.55: 12 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	1.056	21.160	7.404	21.477	355.51	310.41	310.41	0.060	0.069	0.069
	S11	16.308	8.808	18.951	13.701	385.098	335.898	335.898	0.049	0.056	0.056
	S4	39.742	28.837	48.393	40.759	245.66	221.784	221.784	0.197	0.218	0.218
	S12	0.892	6.695	2.900	6.962	303.493	265.143	265.143	0.023	0.026	0.026
11	S10	2.780	24.291	10.068	25.125	711.02	620.82	620.82	0.035	0.040	0.040
	S11	40.350	39.360	52.158	51.465	770.196	671.796	671.796	0.068	0.078	0.078
	S4	68.886	76.335	91.786	97.000	491.32	443.568	443.568	0.197	0.219	0.219
	S12	10.958	32.043	20.571	35.331	606.986	530.286	530.286	0.058	0.067	0.067
10	S10	4.130	30.105	13.161	31.343	1066.53	931.23	931.23	0.029	0.034	0.034
	S11	64.256	70.983	85.551	90.260	1155.294	1007.694	1007.694	0.078	0.090	0.090
	S4	101.021	125.149	138.565	155.455	736.98	665.352	665.352	0.211	0.234	0.234
	S12	21.078	58.781	38.712	65.104	910.479	795.429	795.429	0.072	0.082	0.082
9	S10	10.160	22.861	17.019	25.909	1422.04	1241.64	1185.265	0.018	0.021	0.022
	S11	89.960	116.504	124.912	143.492	1540.392	1343.592	1282.092	0.093	0.107	0.112
	S4	131.682	179.476	185.525	218.981	982.64	887.136	857.291	0.223	0.247	0.255
	S12	34.615	96.832	63.665	107.216	1213.972	1060.572	1012.6345	0.088	0.101	0.106
8	S10	19.673	5.840	21.425	11.742	1777.55	1552.05	1450.575	0.012	0.014	0.015
	S11	116.629	173.502	168.680	208.491	1925.49	1679.49	1568.79	0.108	0.124	0.133
	S4	160.849	239.138	232.591	287.392	1228.3	1108.92	1055.199	0.234	0.259	0.272
	S12	50.790	143.487	93.836	158.724	1517.465	1325.715	1239.4275	0.105	0.120	0.128
7	S10	31.501	20.606	37.683	30.056	2133.06	1862.46	1715.885	0.018	0.020	0.022
	S11	143.821	239.913	215.795	283.060	2310.588	2015.388	1855.488	0.123	0.140	0.153
	S4	191.659	300.578	281.832	358.076	1473.96	1330.704	1253.107	0.243	0.269	0.286
	S12	70.661	202.655	131.458	223.853	1820.958	1590.858	1466.2205	0.123	0.141	0.153
6	S10	51.388	54.395	67.706	69.812	2488.57	2172.87	2003.745	0.028	0.032	0.035
	S11	171.104	323.101	268.035	374.432	2695.686	2351.286	2166.786	0.139	0.159	0.173
	S4	212.577	364.843	322.030	428.616	1719.62	1552.488	1462.953	0.249	0.276	0.293
	S12	86.340	265.443	165.973	291.345	2124.451	1856.001	1712.1885	0.137	0.157	0.170
5	S10	72.759	92.580	100.533	114.407	2844.08	2483.28	2314.155	0.040	0.046	0.049
	S11	197.009	408.336	319.510	467.439	3080.784	2687.184	2502.684	0.152	0.174	0.187
	S4	224.945	429.435	353.775	496.919	1965.28	1774.272	1684.737	0.253	0.280	0.295
	S12	102.756	329.957	201.743	360.784	2427.944	2121.144	1977.3315	0.149	0.170	0.182
4	S10	91.399	133.503	131.450	160.923	3199.59	2793.69	2647.115	0.050	0.058	0.061
	S11	220.509	488.736	367.130	554.888	3465.882	3023.082	2863.182	0.160	0.184	0.194
	S4	231.945	489.995	378.943	559.578	2210.94	1996.056	1918.459	0.253	0.280	0.292
	S12	122.655	395.835	241.405	432.631	2731.437	2386.287	2261.6495	0.158	0.181	0.191
3	S10	108.128	171.267	159.508	203.705	3555.1	3104.1	3002.625	0.057	0.066	0.068
	S11	240.588	563.003	409.489	635.179	3850.98	3358.98	3248.28	0.165	0.189	0.196
	S4	233.929	542.846	396.782	613.024	2456.6	2217.84	2164.119	0.250	0.276	0.283
	S12	140.335	455.189	276.892	497.290	3034.93	2651.43	2565.1425	0.164	0.188	0.194
2	S10	121.426	205.499	183.076	241.926	3910.61	3414.51	3358.135	0.062	0.071	0.072
	S11	255.704	624.529	443.062	701.240	4236.078	3694.878	3633.378	0.166	0.190	0.193
	S4	233.111	585.929	408.890	655.862	2702.26	2439.624	2409.779	0.243	0.269	0.272
	S12	155.651	506.274	307.533	552.970	3338.423	2916.573	2868.6355	0.166	0.190	0.193
1	S10	128.690	229.437	197.521	268.044	4266.12	3724.92	3713.645	0.063	0.072	0.072
	S11	264.136	665.193	463.694	744.434	4621.176	4030.776	4018.476	0.161	0.185	0.185
	S4	227.904	615.183	412.459	683.554	2947.92	2661.408	2655.439	0.232	0.257	0.257
	S12	166.034	539.494	327.883	589.305	3641.916	3181.716	3172.1285	0.162	0.185	0.186

Çizelge B.56: 6 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.102	13.886	4.268	13.917	355.51	332.96	287.86	0.039	0.042	0.048
	S11	11.245	12.467	14.985	15.841	385.098	360.498	311.298	0.041	0.044	0.051
	S4	28.466	18.921	34.143	27.461	245.66	233.722	209.846	0.139	0.146	0.163
	S12	4.082	8.359	6.590	9.583	303.493	284.318	245.968	0.032	0.034	0.039
5	S10	0.098	16.535	5.059	16.565	711.02	665.92	598.27	0.023	0.025	0.028
	S11	26.917	39.120	38.653	47.195	770.196	720.996	647.196	0.061	0.065	0.073
	S4	49.968	48.468	64.508	63.458	491.32	467.444	431.63	0.131	0.138	0.149
	S12	13.957	29.466	22.797	33.653	606.986	568.636	511.111	0.055	0.059	0.066
4	S10	0.632	20.113	6.666	20.303	1066.53	998.88	931.23	0.019	0.020	0.022
	S11	41.730	65.482	61.375	78.001	1155.294	1081.494	1007.694	0.068	0.072	0.077
	S4	72.008	77.850	95.363	99.452	736.98	701.166	665.352	0.135	0.142	0.149
	S12	23.587	50.751	38.812	57.827	910.479	852.954	795.429	0.064	0.068	0.073
3	S10	0.822	16.315	5.716	16.561	1422.04	1331.84	1286.74	0.012	0.012	0.013
	S11	55.840	96.747	84.864	113.499	1540.392	1441.992	1392.792	0.074	0.079	0.081
	S4	90.910	107.446	123.144	134.719	982.64	934.888	911.012	0.137	0.144	0.148
	S12	34.025	76.408	56.947	86.615	1213.972	1137.272	1098.922	0.071	0.076	0.079
2	S10	3.436	6.820	5.482	7.851	1777.55	1664.8	1642.25	0.004	0.005	0.005
	S11	67.478	128.853	106.134	149.097	1925.49	1802.49	1777.89	0.077	0.083	0.084
	S4	104.942	134.841	145.395	166.323	1228.3	1168.61	1156.672	0.135	0.142	0.144
	S12	43.909	102.931	74.788	116.103	1517.465	1421.59	1402.415	0.077	0.082	0.083
1	S10	4.666	3.610	5.749	5.010	2133.06	1997.76	1997.76	0.003	0.003	0.003
	S11	74.457	154.583	120.832	176.920	2310.588	2162.988	2162.988	0.077	0.082	0.082
	S4	112.822	155.376	159.434	189.222	1473.96	1402.332	1402.332	0.128	0.135	0.135
	S12	51.419	125.241	88.991	140.666	1820.958	1705.908	1705.908	0.077	0.082	0.082

Çizelge B.57: 9 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.715	24.284	8.001	24.498	355.51	310.41	254.035	0.069	0.079	0.096
	S11	19.290	15.963	24.079	21.750	385.098	335.898	274.398	0.063	0.072	0.088
	S4	46.793	32.001	56.393	46.039	245.66	221.784	191.939	0.230	0.254	0.294
	S12	4.046	11.028	7.354	12.241	303.493	265.143	217.2055	0.040	0.046	0.056
8	S10	1.667	28.653	10.263	29.153	711.02	620.82	519.345	0.041	0.047	0.056
	S11	47.090	56.697	64.099	70.824	770.196	671.796	561.096	0.092	0.105	0.126
	S4	82.091	84.269	107.371	108.897	491.32	443.568	389.847	0.222	0.246	0.279
	S12	18.334	43.589	31.411	49.090	606.986	530.286	443.9985	0.081	0.093	0.111
7	S10	2.166	35.703	12.877	36.352	1066.53	931.23	784.655	0.034	0.039	0.046
	S11	74.431	98.403	103.952	120.732	1155.294	1007.694	847.794	0.105	0.120	0.142
	S4	120.159	137.696	161.468	173.743	736.98	665.352	587.755	0.236	0.261	0.296
	S12	32.634	77.467	55.874	87.257	910.479	795.429	670.7915	0.096	0.110	0.130
6	S10	7.405	28.646	15.999	30.867	1422.04	1241.64	1072.515	0.022	0.025	0.029
	S11	103.081	154.237	149.352	185.161	1540.392	1343.592	1159.092	0.120	0.138	0.160
	S4	155.800	195.875	214.563	242.615	982.64	887.136	797.601	0.247	0.273	0.304
	S12	50.269	122.992	87.166	138.072	1213.972	1060.572	916.7595	0.114	0.130	0.151
5	S10	15.991	10.955	19.277	15.752	1777.55	1552.05	1382.925	0.011	0.012	0.014
	S11	131.552	220.286	197.637	259.752	1925.49	1679.49	1494.99	0.135	0.155	0.174
	S4	188.218	257.480	265.462	313.945	1228.3	1108.92	1019.385	0.256	0.283	0.308
	S12	70.034	176.284	122.919	197.295	1517.465	1325.715	1181.9025	0.130	0.149	0.167
4	S10	26.069	14.364	30.378	22.185	2133.06	1862.46	1715.885	0.014	0.016	0.018
	S11	158.500	290.884	245.766	338.434	2310.588	2015.388	1855.488	0.146	0.168	0.182
	S4	219.577	316.892	314.645	382.765	1473.96	1330.704	1253.107	0.260	0.288	0.305
	S12	91.529	237.519	162.784	264.977	1820.958	1590.858	1466.2205	0.146	0.167	0.181
3	S10	41.434	45.156	54.981	57.586	2488.57	2172.87	2071.395	0.023	0.027	0.028
	S11	182.544	368.458	293.081	423.221	2695.686	2351.286	2240.586	0.157	0.180	0.189
	S4	239.410	372.549	351.175	444.372	1719.62	1552.488	1498.767	0.258	0.286	0.296
	S12	108.121	297.217	197.286	329.653	2124.451	1856.001	1769.7135	0.155	0.178	0.186
2	S10	55.440	73.560	77.508	90.192	2844.08	2483.28	2426.905	0.032	0.036	0.037
	S11	200.927	436.193	331.785	496.471	3080.784	2687.184	2625.684	0.161	0.185	0.189
	S4	248.419	419.971	374.410	494.497	1965.28	1774.272	1744.427	0.252	0.279	0.283
	S12	120.811	347.209	224.974	383.452	2427.944	2121.144	2073.2065	0.158	0.181	0.185
1	S10	62.757	99.640	92.649	118.467	3199.59	2793.69	2782.415	0.037	0.042	0.043
	S11	211.446	483.280	356.430	546.714	3465.882	3023.082	3010.782	0.158	0.181	0.182
	S4	250.442	453.377	386.455	528.510	2210.94	1996.056	1990.087	0.239	0.265	0.266
	S12	132.727	386.954	248.814	426.772	2731.437	2386.287	2376.6995	0.156	0.179	0.180

Çizelge B.58: 12 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	1.523	30.519	10.679	30.976	355.51	310.41	310.41	0.087	0.100	0.100
	S11	23.522	12.704	27.333	19.761	385.098	335.898	335.898	0.071	0.081	0.081
	S4	57.320	41.591	69.797	58.787	245.66	221.784	221.784	0.284	0.315	0.315
	S12	1.286	9.656	4.183	10.042	303.493	265.143	265.143	0.033	0.038	0.038
11	S10	4.010	35.035	14.521	36.238	711.02	620.82	620.82	0.051	0.058	0.058
	S11	58.197	56.769	75.228	74.228	770.196	671.796	671.796	0.098	0.112	0.112
	S4	99.355	110.098	132.384	139.904	491.32	443.568	443.568	0.285	0.315	0.315
	S12	15.805	46.216	29.670	50.958	606.986	530.286	530.286	0.084	0.096	0.096
10	S10	5.957	43.420	18.982	45.207	1066.53	931.23	931.23	0.042	0.049	0.049
	S11	92.677	102.380	123.391	130.183	1155.294	1007.694	1007.694	0.113	0.129	0.129
	S4	145.703	180.503	199.854	224.214	736.98	665.352	665.352	0.304	0.337	0.337
	S12	30.401	84.780	55.835	93.900	910.479	795.429	795.429	0.103	0.118	0.118
9	S10	14.655	32.972	24.546	37.369	1422.04	1241.64	1185.265	0.026	0.030	0.032
	S11	129.751	168.035	180.161	206.960	1540.392	1343.592	1282.092	0.134	0.154	0.161
	S4	189.926	258.860	267.584	315.838	982.64	887.136	857.291	0.321	0.356	0.368
	S12	49.926	139.661	91.824	154.639	1213.972	1060.572	1012.6345	0.127	0.146	0.153
8	S10	28.374	8.423	30.901	16.936	1777.55	1552.05	1450.575	0.017	0.020	0.021
	S11	168.216	250.243	243.288	300.707	1925.49	1679.49	1568.79	0.156	0.179	0.192
	S4	231.994	344.910	335.467	414.508	1228.3	1108.92	1055.199	0.337	0.374	0.393
	S12	73.255	206.952	135.341	228.929	1517.465	1325.715	1239.4275	0.151	0.173	0.185
7	S10	45.434	29.721	54.350	43.351	2133.06	1862.46	1715.885	0.025	0.029	0.032
	S11	207.435	346.029	311.243	408.259	2310.588	2015.388	1855.488	0.177	0.203	0.220
	S4	276.431	433.526	406.489	516.455	1473.96	1330.704	1253.107	0.350	0.388	0.412
	S12	101.915	292.291	189.602	322.865	1820.958	1590.858	1466.2205	0.177	0.203	0.220
6	S10	74.117	78.455	97.653	100.690	2488.57	2172.87	2003.745	0.040	0.046	0.050
	S11	246.785	466.011	386.588	540.046	2695.686	2351.286	2166.786	0.200	0.230	0.249
	S4	306.601	526.217	464.466	618.197	1719.62	1552.488	1462.953	0.359	0.398	0.423
	S12	124.529	382.850	239.384	420.209	2124.451	1856.001	1712.1885	0.198	0.226	0.245
5	S10	104.941	133.528	144.999	165.011	2844.08	2483.28	2314.155	0.058	0.066	0.071
	S11	284.148	588.947	460.831	674.191	3080.784	2687.184	2502.684	0.219	0.251	0.269
	S4	324.439	619.378	510.253	716.710	1965.28	1774.272	1684.737	0.365	0.404	0.425
	S12	148.205	475.900	290.975	520.361	2427.944	2121.144	1977.3315	0.214	0.245	0.263
4	S10	131.826	192.552	189.592	232.100	3199.59	2793.69	2647.115	0.073	0.083	0.088
	S11	318.042	704.907	529.514	800.320	3465.882	3023.082	2863.182	0.231	0.265	0.280
	S4	334.536	706.723	546.552	807.084	2210.94	1996.056	1918.459	0.365	0.404	0.421
	S12	176.906	570.915	348.181	623.987	2731.437	2386.287	2261.6495	0.228	0.261	0.276
3	S10	155.954	247.019	230.059	293.805	3555.1	3104.1	3002.625	0.083	0.095	0.098
	S11	347.002	812.024	590.609	916.124	3850.98	3358.98	3248.28	0.238	0.273	0.282
	S4	337.397	782.950	572.282	884.169	2456.6	2217.84	2164.119	0.360	0.399	0.409
	S12	202.407	656.523	399.363	717.245	3034.93	2651.43	2565.1425	0.236	0.271	0.280
2	S10	175.134	296.392	264.052	348.932	3910.61	3414.51	3358.135	0.089	0.102	0.104
	S11	368.803	900.763	639.032	1011.404	4236.078	3694.878	3633.378	0.239	0.274	0.278
	S4	336.218	845.090	589.745	945.955	2702.26	2439.624	2409.779	0.350	0.388	0.393
	S12	224.496	730.204	443.557	797.552	3338.423	2916.573	2868.6355	0.239	0.273	0.278
1	S10	185.610	330.919	284.886	386.602	4266.12	3724.92	3713.645	0.091	0.104	0.104
	S11	380.966	959.413	668.790	1073.703	4621.176	4030.776	4018.476	0.232	0.266	0.267
	S4	328.708	887.283	594.893	985.895	2947.92	2661.408	2655.439	0.334	0.370	0.371
	S12	239.473	778.117	472.908	849.959	3641.916	3181.716	3172.1285	0.233	0.267	0.268

Çizelge B.59: 6 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.014	1.920	0.590	1.924	355.51	332.96	287.86	0.005	0.006	0.007
	S11	1.568	1.724	2.085	2.194	385.098	360.498	311.298	0.006	0.006	0.007
	S4	3.968	2.616	4.753	3.806	245.66	233.722	209.846	0.019	0.020	0.023
	S12	0.569	1.156	0.916	1.326	303.493	284.318	245.968	0.004	0.005	0.005
5	S10	0.014	2.286	0.700	2.290	711.02	665.92	598.27	0.003	0.003	0.004
	S11	3.752	5.408	5.374	6.534	770.196	720.996	647.196	0.008	0.009	0.010
	S4	6.965	6.701	8.975	8.790	491.32	467.444	431.63	0.018	0.019	0.021
	S12	1.946	4.074	3.168	4.657	606.986	568.636	511.111	0.008	0.008	0.009
4	S10	0.088	2.781	0.922	2.807	1066.53	998.88	931.23	0.003	0.003	0.003
	S11	5.817	9.053	8.533	10.798	1155.294	1081.494	1007.694	0.009	0.010	0.011
	S4	10.037	10.763	13.266	13.774	736.98	701.166	665.352	0.019	0.020	0.021
	S12	3.288	7.016	5.393	8.003	910.479	852.954	795.429	0.009	0.009	0.010
3	S10	0.115	2.256	0.791	2.290	1422.04	1331.84	1286.74	0.002	0.002	0.002
	S11	7.784	13.375	11.796	15.710	1540.392	1441.992	1392.792	0.010	0.011	0.011
	S4	12.672	14.854	17.129	18.656	982.64	934.888	911.012	0.019	0.020	0.020
	S12	4.743	10.563	7.912	11.986	1213.972	1137.272	1098.922	0.010	0.011	0.011
2	S10	0.479	0.943	0.762	1.087	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	9.406	17.814	14.750	20.636	1925.49	1802.49	1777.89	0.011	0.011	0.012
	S4	14.628	18.642	20.221	23.030	1228.3	1168.61	1156.672	0.019	0.020	0.020
	S12	6.121	14.230	10.390	16.066	1517.465	1421.59	1402.415	0.011	0.011	0.011
1	S10	0.650	0.499	0.800	0.694	2133.06	1997.76	1997.76	0.000	0.000	0.000
	S11	10.379	21.371	16.790	24.485	2310.588	2162.988	2162.988	0.011	0.011	0.011
	S4	15.727	21.481	22.171	26.198	1473.96	1402.332	1402.332	0.018	0.019	0.019
	S12	7.167	17.314	12.362	19.465	1820.958	1705.908	1705.908	0.011	0.011	0.011

Çizelge B.60: 9 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.090	3.064	1.009	3.091	355.51	310.41	254.035	0.009	0.010	0.012
	S11	2.433	2.014	3.038	2.744	385.098	335.898	274.398	0.008	0.009	0.011
	S4	5.903	4.037	7.114	5.808	245.66	221.784	191.939	0.029	0.032	0.037
	S12	0.510	1.391	0.928	1.544	303.493	265.143	217.2055	0.005	0.006	0.007
8	S10	0.210	3.615	1.295	3.678	711.02	620.82	519.345	0.005	0.006	0.007
	S11	5.941	7.153	8.086	8.935	770.196	671.796	561.096	0.012	0.013	0.016
	S4	10.356	10.631	13.545	13.738	491.32	443.568	389.847	0.028	0.031	0.035
	S12	2.313	5.499	3.963	6.193	606.986	530.286	443.9985	0.010	0.012	0.014
7	S10	0.273	4.504	1.625	4.586	1066.53	931.23	784.655	0.004	0.005	0.006
	S11	9.390	12.414	13.114	15.231	1155.294	1007.694	847.794	0.013	0.015	0.018
	S4	15.159	17.371	20.370	21.918	736.98	665.352	587.755	0.030	0.033	0.037
	S12	4.117	9.773	7.049	11.008	910.479	795.429	670.7915	0.012	0.014	0.016
6	S10	0.934	3.614	2.018	3.894	1422.04	1241.64	1072.515	0.003	0.003	0.004
	S11	13.004	19.458	18.841	23.359	1540.392	1343.592	1159.092	0.015	0.017	0.020
	S4	19.655	24.710	27.068	30.607	982.64	887.136	797.601	0.031	0.035	0.038
	S12	6.342	15.516	10.996	17.418	1213.972	1060.572	916.7595	0.014	0.016	0.019
5	S10	2.017	1.382	2.432	1.987	1777.55	1552.05	1382.925	0.001	0.002	0.002
	S11	16.596	27.790	24.933	32.769	1925.49	1679.49	1494.99	0.017	0.020	0.022
	S4	23.744	32.482	33.489	39.605	1228.3	1108.92	1019.385	0.032	0.036	0.039
	S12	8.835	22.239	15.507	24.890	1517.465	1325.715	1181.9025	0.016	0.019	0.021
4	S10	3.289	1.812	3.832	2.799	2133.06	1862.46	1715.885	0.002	0.002	0.002
	S11	19.995	36.696	31.004	42.695	2310.588	2015.388	1855.488	0.018	0.021	0.023
	S4	27.701	39.977	39.694	48.287	1473.96	1330.704	1253.107	0.033	0.036	0.039
	S12	11.547	29.964	20.536	33.428	1820.958	1590.858	1466.2205	0.018	0.021	0.023
3	S10	5.227	5.697	6.936	7.265	2488.57	2172.87	2071.395	0.003	0.003	0.004
	S11	23.029	46.482	36.973	53.391	2695.686	2351.286	2240.586	0.020	0.023	0.024
	S4	30.203	46.999	44.302	56.059	1719.62	1552.488	1498.767	0.033	0.036	0.037
	S12	13.640	37.495	24.888	41.587	2124.451	1856.001	1769.7135	0.020	0.022	0.023
2	S10	6.994	9.280	9.778	11.378	2844.08	2483.28	2426.905	0.004	0.005	0.005
	S11	25.348	55.027	41.856	62.632	3080.784	2687.184	2625.684	0.020	0.023	0.024
	S4	31.339	52.981	47.233	62.383	1965.28	1774.272	1744.427	0.032	0.035	0.036
	S12	15.241	43.802	28.381	48.374	2427.944	2121.144	2073.2065	0.020	0.023	0.023
1	S10	7.917	12.570	11.688	14.945	3199.59	2793.69	2782.415	0.005	0.005	0.005
	S11	26.675	60.968	44.965	68.970	3465.882	3023.082	3010.782	0.020	0.023	0.023
	S4	31.594	57.195	48.753	66.674	2210.94	1996.056	1990.087	0.030	0.033	0.034
	S12	16.744	48.816	31.389	53.839	2731.437	2386.287	2376.6995	0.020	0.023	0.023

Çizelge B.61: 12 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.192	3.850	1.347	3.908	355.51	310.41	310.41	0.011	0.013	0.013
	S11	2.967	1.603	3.448	2.493	385.098	335.898	335.898	0.009	0.010	0.010
	S4	7.231	5.247	8.805	7.416	245.66	221.784	221.784	0.036	0.040	0.040
	S12	0.162	1.218	0.528	1.267	303.493	265.143	265.143	0.004	0.005	0.005
11	S10	0.506	4.420	1.832	4.572	711.02	620.82	620.82	0.006	0.007	0.007
	S11	7.342	7.162	9.490	9.364	770.196	671.796	671.796	0.012	0.014	0.014
	S4	12.534	13.889	16.701	17.650	491.32	443.568	443.568	0.036	0.040	0.040
	S12	1.994	5.830	3.743	6.429	606.986	530.286	530.286	0.011	0.012	0.012
10	S10	0.751	5.478	2.395	5.703	1066.53	931.23	931.23	0.005	0.006	0.006
	S11	11.692	12.916	15.566	16.423	1155.294	1007.694	1007.694	0.014	0.016	0.016
	S4	18.381	22.771	25.212	28.285	736.98	665.352	665.352	0.038	0.043	0.043
	S12	3.835	10.695	7.044	11.846	910.479	795.429	795.429	0.013	0.015	0.015
9	S10	1.849	4.160	3.097	4.714	1422.04	1241.64	1185.265	0.003	0.004	0.004
	S11	16.369	21.198	22.728	26.109	1540.392	1343.592	1282.092	0.017	0.019	0.020
	S4	23.960	32.656	33.757	39.844	982.64	887.136	857.291	0.041	0.045	0.046
	S12	6.298	17.619	11.584	19.508	1213.972	1060.572	1012.6345	0.016	0.018	0.019
8	S10	3.580	1.063	3.898	2.136	1777.55	1552.05	1450.575	0.002	0.003	0.003
	S11	21.221	31.569	30.692	37.935	1925.49	1679.49	1568.79	0.020	0.023	0.024
	S4	29.267	43.512	42.321	52.292	1228.3	1108.92	1055.199	0.043	0.047	0.050
	S12	9.241	26.108	17.074	28.880	1517.465	1325.715	1239.4275	0.019	0.022	0.023
7	S10	5.732	3.749	6.856	5.469	2133.06	1862.46	1715.885	0.003	0.004	0.004
	S11	26.169	43.653	39.265	51.504	2310.588	2015.388	1855.488	0.022	0.026	0.028
	S4	34.873	54.691	51.280	65.153	1473.96	1330.704	1253.107	0.044	0.049	0.052
	S12	12.857	36.874	23.919	40.731	1820.958	1590.858	1466.2205	0.022	0.026	0.028
6	S10	9.350	9.897	12.319	12.702	2488.57	2172.87	2003.745	0.005	0.006	0.006
	S11	31.133	58.789	48.770	68.129	2695.686	2351.286	2166.786	0.025	0.029	0.031
	S4	38.679	66.384	58.594	77.988	1719.62	1552.488	1462.953	0.045	0.050	0.053
	S12	15.710	48.298	30.199	53.011	2124.451	1856.001	1712.1885	0.025	0.029	0.031
5	S10	13.239	16.845	18.292	20.817	2844.08	2483.28	2314.155	0.007	0.008	0.009
	S11	35.846	74.298	58.136	85.052	3080.784	2687.184	2502.684	0.028	0.032	0.034
	S4	40.929	78.137	64.370	90.416	1965.28	1774.272	1684.737	0.046	0.051	0.054
	S12	18.697	60.037	36.708	65.646	2427.944	2121.144	1977.3315	0.027	0.031	0.033
4	S10	16.630	24.291	23.918	29.280	3199.59	2793.69	2647.115	0.009	0.010	0.011
	S11	40.122	88.927	66.800	100.963	3465.882	3023.082	2863.182	0.029	0.033	0.035
	S4	42.203	89.156	68.950	101.817	2210.94	1996.056	1918.459	0.046	0.051	0.053
	S12	22.317	72.023	43.924	78.718	2731.437	2386.287	2261.6495	0.029	0.033	0.035
3	S10	19.674	31.162	29.023	37.065	3555.1	3104.1	3002.625	0.010	0.012	0.012
	S11	43.776	102.440	74.508	115.573	3850.98	3358.98	3248.28	0.030	0.034	0.036
	S4	42.564	98.772	72.196	111.541	2456.6	2217.84	2164.119	0.045	0.050	0.052
	S12	25.534	82.823	50.381	90.483	3034.93	2651.43	2565.1425	0.030	0.034	0.035
2	S10	22.094	37.391	33.311	44.019	3910.61	3414.51	3358.135	0.011	0.013	0.013
	S11	46.526	113.635	80.616	127.593	4236.078	3694.878	3633.378	0.030	0.035	0.035
	S4	42.415	106.611	74.399	119.336	2702.26	2439.624	2409.779	0.044	0.049	0.050
	S12	28.321	92.118	55.956	100.614	3338.423	2916.573	2868.6355	0.030	0.034	0.035
1	S10	23.415	41.747	35.939	48.771	4266.12	3724.92	3713.645	0.011	0.013	0.013
	S11	48.060	121.034	84.370	135.452	4621.176	4030.776	4018.476	0.029	0.034	0.034
	S4	41.468	111.934	75.048	124.375	2947.92	2661.408	2655.439	0.042	0.047	0.047
	S12	30.210	98.162	59.659	107.226	3641.916	3181.716	3172.1285	0.029	0.034	0.034

Çizelge B.62: 6 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.014	1.920	0.590	1.924	355.51	332.96	287.86	0.005	0.006	0.007
	S11	1.568	1.724	2.085	2.194	385.098	360.498	311.298	0.006	0.006	0.007
	S4	3.968	2.616	4.753	3.806	245.66	233.722	209.846	0.019	0.020	0.023
	S12	0.569	1.156	0.916	1.326	303.493	284.318	245.968	0.004	0.005	0.005
5	S10	0.014	2.286	0.700	2.290	711.02	665.92	598.27	0.003	0.003	0.004
	S11	3.752	5.408	5.374	6.534	770.196	720.996	647.196	0.008	0.009	0.010
	S4	6.965	6.701	8.975	8.790	491.32	467.444	431.63	0.018	0.019	0.021
	S12	1.946	4.074	3.168	4.657	606.986	568.636	511.111	0.008	0.008	0.009
4	S10	0.088	2.781	0.922	2.807	1066.53	998.88	931.23	0.003	0.003	0.003
	S11	5.817	9.053	8.533	10.798	1155.294	1081.494	1007.694	0.009	0.010	0.011
	S4	10.037	10.763	13.266	13.774	736.98	701.166	665.352	0.019	0.020	0.021
	S12	3.288	7.016	5.393	8.003	910.479	852.954	795.429	0.009	0.009	0.010
3	S10	0.115	2.256	0.791	2.290	1422.04	1331.84	1286.74	0.002	0.002	0.002
	S11	7.784	13.375	11.796	15.710	1540.392	1441.992	1392.792	0.010	0.011	0.011
	S4	12.672	14.854	17.129	18.656	982.64	934.888	911.012	0.019	0.020	0.020
	S12	4.743	10.563	7.912	11.986	1213.972	1137.272	1098.922	0.010	0.011	0.011
2	S10	0.479	0.943	0.762	1.087	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	9.406	17.814	14.750	20.636	1925.49	1802.49	1777.89	0.011	0.011	0.012
	S4	14.628	18.642	20.221	23.030	1228.3	1168.61	1156.672	0.019	0.020	0.020
	S12	6.121	14.230	10.390	16.066	1517.465	1421.59	1402.415	0.011	0.011	0.011
1	S10	0.650	0.499	0.800	0.694	2133.06	1997.76	1997.76	0.000	0.000	0.000
	S11	10.379	21.371	16.790	24.485	2310.588	2162.988	2162.988	0.011	0.011	0.011
	S4	15.727	21.481	22.171	26.198	1473.96	1402.332	1402.332	0.018	0.019	0.019
	S12	7.167	17.314	12.362	19.465	1820.958	1705.908	1705.908	0.011	0.011	0.011

Çizelge B.63: 9 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.090	3.064	1.009	3.091	355.51	310.41	254.035	0.009	0.010	0.012
	S11	2.433	2.014	3.038	2.744	385.098	335.898	274.398	0.008	0.009	0.011
	S4	5.903	4.037	7.114	5.808	245.66	221.784	191.939	0.029	0.032	0.037
	S12	0.510	1.391	0.928	1.544	303.493	265.143	217.2055	0.005	0.006	0.007
8	S10	0.210	3.615	1.295	3.678	711.02	620.82	519.345	0.005	0.006	0.007
	S11	5.941	7.153	8.086	8.935	770.196	671.796	561.096	0.012	0.013	0.016
	S4	10.356	10.631	13.545	13.738	491.32	443.568	389.847	0.028	0.031	0.035
	S12	2.313	5.499	3.963	6.193	606.986	530.286	443.9985	0.010	0.012	0.014
7	S10	0.273	4.504	1.625	4.586	1066.53	931.23	784.655	0.004	0.005	0.006
	S11	9.390	12.414	13.114	15.231	1155.294	1007.694	847.794	0.013	0.015	0.018
	S4	15.159	17.371	20.370	21.918	736.98	665.352	587.755	0.030	0.033	0.037
	S12	4.117	9.773	7.049	11.008	910.479	795.429	670.7915	0.012	0.014	0.016
6	S10	0.934	3.614	2.018	3.894	1422.04	1241.64	1072.515	0.003	0.003	0.004
	S11	13.004	19.458	18.841	23.359	1540.392	1343.592	1159.092	0.015	0.017	0.020
	S4	19.655	24.710	27.068	30.607	982.64	887.136	797.601	0.031	0.035	0.038
	S12	6.342	15.516	10.996	17.418	1213.972	1060.572	916.7595	0.014	0.016	0.019
5	S10	2.017	1.382	2.432	1.987	1777.55	1552.05	1382.925	0.001	0.002	0.002
	S11	16.596	27.790	24.933	32.769	1925.49	1679.49	1494.99	0.017	0.020	0.022
	S4	23.744	32.482	33.489	39.605	1228.3	1108.92	1019.385	0.032	0.036	0.039
	S12	8.835	22.239	15.507	24.890	1517.465	1325.715	1181.9025	0.016	0.019	0.021
4	S10	3.289	1.812	3.832	2.799	2133.06	1862.46	1715.885	0.002	0.002	0.002
	S11	19.995	36.696	31.004	42.695	2310.588	2015.388	1855.488	0.018	0.021	0.023
	S4	27.701	39.977	39.694	48.287	1473.96	1330.704	1253.107	0.033	0.036	0.039
	S12	11.547	29.964	20.536	33.428	1820.958	1590.858	1466.2205	0.018	0.021	0.023
3	S10	5.227	5.697	6.936	7.265	2488.57	2172.87	2071.395	0.003	0.003	0.004
	S11	23.029	46.482	36.973	53.391	2695.686	2351.286	2240.586	0.020	0.023	0.024
	S4	30.203	46.999	44.302	56.059	1719.62	1552.488	1498.767	0.033	0.036	0.037
	S12	13.640	37.495	24.888	41.587	2124.451	1856.001	1769.7135	0.020	0.022	0.023
2	S10	6.994	9.280	9.778	11.378	2844.08	2483.28	2426.905	0.004	0.005	0.005
	S11	25.348	55.027	41.856	62.632	3080.784	2687.184	2625.684	0.020	0.023	0.024
	S4	31.339	52.981	47.233	62.383	1965.28	1774.272	1744.427	0.032	0.035	0.036
	S12	15.241	43.802	28.381	48.374	2427.944	2121.144	2073.2065	0.020	0.023	0.023
1	S10	7.917	12.570	11.688	14.945	3199.59	2793.69	2782.415	0.005	0.005	0.005
	S11	26.675	60.968	44.965	68.970	3465.882	3023.082	3010.782	0.020	0.023	0.023
	S4	31.594	57.195	48.753	66.674	2210.94	1996.056	1990.087	0.030	0.033	0.034
	S12	16.744	48.816	31.389	53.839	2731.437	2386.287	2376.6995	0.020	0.023	0.023

Çizelge B.64: 12 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.192	3.850	1.347	3.908	355.51	310.41	310.41	0.011	0.013	0.013
	S11	2.967	1.603	3.448	2.493	385.098	335.898	335.898	0.009	0.010	0.010
	S4	7.231	5.247	8.805	7.416	245.66	221.784	221.784	0.036	0.040	0.040
	S12	0.162	1.218	0.528	1.267	303.493	265.143	265.143	0.004	0.005	0.005
11	S10	0.506	4.420	1.832	4.572	711.02	620.82	620.82	0.006	0.007	0.007
	S11	7.342	7.162	9.490	9.364	770.196	671.796	671.796	0.012	0.014	0.014
	S4	12.534	13.889	16.701	17.650	491.32	443.568	443.568	0.036	0.040	0.040
	S12	1.994	5.830	3.743	6.429	606.986	530.286	530.286	0.011	0.012	0.012
10	S10	0.751	5.478	2.395	5.703	1066.53	931.23	931.23	0.005	0.006	0.006
	S11	11.692	12.916	15.566	16.423	1155.294	1007.694	1007.694	0.014	0.016	0.016
	S4	18.381	22.771	25.212	28.285	736.98	665.352	665.352	0.038	0.043	0.043
	S12	3.835	10.695	7.044	11.846	910.479	795.429	795.429	0.013	0.015	0.015
9	S10	1.849	4.160	3.097	4.714	1422.04	1241.64	1185.265	0.003	0.004	0.004
	S11	16.369	21.198	22.728	26.109	1540.392	1343.592	1282.092	0.017	0.019	0.020
	S4	23.960	32.656	33.757	39.844	982.64	887.136	857.291	0.041	0.045	0.046
	S12	6.298	17.619	11.584	19.508	1213.972	1060.572	1012.6345	0.016	0.018	0.019
8	S10	3.580	1.063	3.898	2.136	1777.55	1552.05	1450.575	0.002	0.003	0.003
	S11	21.221	31.569	30.692	37.935	1925.49	1679.49	1568.79	0.020	0.023	0.024
	S4	29.267	43.512	42.321	52.292	1228.3	1108.92	1055.199	0.043	0.047	0.050
	S12	9.241	26.108	17.074	28.880	1517.465	1325.715	1239.4275	0.019	0.022	0.023
7	S10	5.732	3.749	6.856	5.469	2133.06	1862.46	1715.885	0.003	0.004	0.004
	S11	26.169	43.653	39.265	51.504	2310.588	2015.388	1855.488	0.022	0.026	0.028
	S4	34.873	54.691	51.280	65.153	1473.96	1330.704	1253.107	0.044	0.049	0.052
	S12	12.857	36.874	23.919	40.731	1820.958	1590.858	1466.2205	0.022	0.026	0.028
6	S10	9.350	9.897	12.319	12.702	2488.57	2172.87	2003.745	0.005	0.006	0.006
	S11	31.133	58.789	48.770	68.129	2695.686	2351.286	2166.786	0.025	0.029	0.031
	S4	38.679	66.384	58.594	77.988	1719.62	1552.488	1462.953	0.045	0.050	0.053
	S12	15.710	48.298	30.199	53.011	2124.451	1856.001	1712.1885	0.025	0.029	0.031
5	S10	13.239	16.845	18.292	20.817	2844.08	2483.28	2314.155	0.007	0.008	0.009
	S11	35.846	74.298	58.136	85.052	3080.784	2687.184	2502.684	0.028	0.032	0.034
	S4	40.929	78.137	64.370	90.416	1965.28	1774.272	1684.737	0.046	0.051	0.054
	S12	18.697	60.037	36.708	65.646	2427.944	2121.144	1977.3315	0.027	0.031	0.033
4	S10	16.630	24.291	23.918	29.280	3199.59	2793.69	2647.115	0.009	0.010	0.011
	S11	40.122	88.927	66.800	100.963	3465.882	3023.082	2863.182	0.029	0.033	0.035
	S4	42.203	89.156	68.950	101.817	2210.94	1996.056	1918.459	0.046	0.051	0.053
	S12	22.317	72.023	43.924	78.718	2731.437	2386.287	2261.6495	0.029	0.033	0.035
3	S10	19.674	31.162	29.023	37.065	3555.1	3104.1	3002.625	0.010	0.012	0.012
	S11	43.776	102.440	74.508	115.573	3850.98	3358.98	3248.28	0.030	0.034	0.036
	S4	42.564	98.772	72.196	111.541	2456.6	2217.84	2164.119	0.045	0.050	0.052
	S12	25.534	82.823	50.381	90.483	3034.93	2651.43	2565.1425	0.030	0.034	0.035
2	S10	22.094	37.391	33.311	44.019	3910.61	3414.51	3358.135	0.011	0.013	0.013
	S11	46.526	113.635	80.616	127.593	4236.078	3694.878	3633.378	0.030	0.035	0.035
	S4	42.415	106.611	74.399	119.336	2702.26	2439.624	2409.779	0.044	0.049	0.050
	S12	28.321	92.118	55.956	100.614	3338.423	2916.573	2868.6355	0.030	0.034	0.035
1	S10	23.415	41.747	35.939	48.771	4266.12	3724.92	3713.645	0.011	0.013	0.013
	S11	48.060	121.034	84.370	135.452	4621.176	4030.776	4018.476	0.029	0.034	0.034
	S4	41.468	111.934	75.048	124.375	2947.92	2661.408	2655.439	0.042	0.047	0.047
	S12	30.210	98.162	59.659	107.226	3641.916	3181.716	3172.1285	0.029	0.034	0.034

Çizelge B.65: 6 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.027	3.600	1.107	3.608	355.51	332.96	287.86	0.010	0.011	0.013
	S11	2.939	3.232	3.909	4.113	385.098	360.498	311.298	0.011	0.011	0.013
	S4	7.440	4.905	8.911	7.137	245.66	233.722	209.846	0.036	0.038	0.042
	S12	1.067	2.167	1.717	2.487	303.493	284.318	245.968	0.008	0.009	0.010
5	S10	0.026	4.286	1.311	4.294	711.02	665.92	598.27	0.006	0.006	0.007
	S11	7.035	10.141	10.077	12.251	770.196	720.996	647.196	0.016	0.017	0.019
	S4	13.060	12.564	16.829	16.482	491.32	467.444	431.63	0.034	0.036	0.039
	S12	3.648	7.638	5.939	8.732	606.986	568.636	511.111	0.014	0.015	0.017
4	S10	0.165	5.214	1.729	5.263	1066.53	998.88	931.23	0.005	0.005	0.006
	S11	10.907	16.974	15.999	20.246	1155.294	1081.494	1007.694	0.018	0.019	0.020
	S4	18.820	20.180	24.874	25.826	736.98	701.166	665.352	0.035	0.037	0.039
	S12	6.165	13.156	10.111	15.005	910.479	852.954	795.429	0.016	0.018	0.019
3	S10	0.215	4.229	1.484	4.293	1422.04	1331.84	1286.74	0.003	0.003	0.003
	S11	14.595	25.078	22.118	29.457	1540.392	1441.992	1392.792	0.019	0.020	0.021
	S4	23.761	27.852	32.116	34.980	982.64	934.888	911.012	0.036	0.037	0.038
	S12	8.893	19.806	14.835	22.474	1213.972	1137.272	1098.922	0.019	0.020	0.020
2	S10	0.898	1.768	1.428	2.037	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	17.636	33.401	27.656	38.692	1925.49	1802.49	1777.89	0.020	0.021	0.022
	S4	27.428	34.953	37.914	43.181	1228.3	1168.61	1156.672	0.035	0.037	0.037
	S12	11.476	26.681	19.480	30.124	1517.465	1421.59	1402.415	0.020	0.021	0.021
1	S10	1.220	0.936	1.500	1.302	2133.06	1997.76	1997.76	0.001	0.001	0.001
	S11	19.460	40.070	31.481	45.908	2310.588	2162.988	2162.988	0.020	0.021	0.021
	S4	29.487	40.276	41.570	49.122	1473.96	1402.332	1402.332	0.033	0.035	0.035
	S12	13.439	32.464	23.178	36.496	1820.958	1705.908	1705.908	0.020	0.021	0.021

Çizelge B.66: 9 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.169	5.744	1.892	5.795	355.51	310.41	254.035	0.016	0.019	0.023
	S11	4.563	3.776	5.696	5.145	385.098	335.898	274.398	0.015	0.017	0.021
	S4	11.068	7.570	13.339	10.890	245.66	221.784	191.939	0.054	0.060	0.069
	S12	0.957	2.608	1.740	2.896	303.493	265.143	217.2055	0.010	0.011	0.013
8	S10	0.394	6.778	2.428	6.896	711.02	620.82	519.345	0.010	0.011	0.013
	S11	11.139	13.411	15.162	16.753	770.196	671.796	561.096	0.022	0.025	0.030
	S4	19.418	19.933	25.397	25.758	491.32	443.568	389.847	0.052	0.058	0.066
	S12	4.337	10.311	7.430	11.612	606.986	530.286	443.9985	0.019	0.022	0.026
7	S10	0.512	8.445	3.046	8.599	1066.53	931.23	784.655	0.008	0.009	0.011
	S11	17.606	23.276	24.589	28.558	1155.294	1007.694	847.794	0.025	0.028	0.034
	S4	28.422	32.570	38.193	41.097	736.98	665.352	587.755	0.056	0.062	0.070
	S12	7.719	18.324	13.216	20.640	910.479	795.429	670.7915	0.023	0.026	0.031
6	S10	1.752	6.776	3.784	7.301	1422.04	1241.64	1072.515	0.005	0.006	0.007
	S11	24.383	36.483	35.328	43.798	1540.392	1343.592	1159.092	0.028	0.033	0.038
	S4	36.853	46.332	50.752	57.388	982.64	887.136	797.601	0.058	0.065	0.072
	S12	11.891	29.092	20.618	32.659	1213.972	1060.572	916.7595	0.027	0.031	0.036
5	S10	3.782	2.591	4.560	3.726	1777.55	1552.05	1382.925	0.003	0.003	0.003
	S11	31.117	52.106	46.749	61.441	1925.49	1679.49	1494.99	0.032	0.037	0.041
	S4	44.521	60.904	62.792	74.260	1228.3	1108.92	1019.385	0.060	0.067	0.073
	S12	16.566	41.698	29.075	46.668	1517.465	1325.715	1181.9025	0.031	0.035	0.039
4	S10	6.166	3.398	7.186	5.247	2133.06	1862.46	1715.885	0.003	0.004	0.004
	S11	37.491	68.805	58.133	80.053	2310.588	2015.388	1855.488	0.035	0.040	0.043
	S4	51.939	74.957	74.426	90.539	1473.96	1330.704	1253.107	0.061	0.068	0.072
	S12	21.650	56.182	38.505	62.677	1820.958	1590.858	1466.2205	0.034	0.039	0.043
3	S10	9.801	10.681	13.005	13.621	2488.57	2172.87	2071.395	0.005	0.006	0.007
	S11	43.179	87.155	69.325	100.108	2695.686	2351.286	2240.586	0.037	0.043	0.045
	S4	56.630	88.122	83.066	105.111	1719.62	1552.488	1498.767	0.061	0.068	0.070
	S12	25.575	70.303	46.666	77.976	2124.451	1856.001	1769.7135	0.037	0.042	0.044
2	S10	13.114	17.400	18.334	21.334	2844.08	2483.28	2426.905	0.008	0.009	0.009
	S11	47.527	103.176	78.480	117.434	3080.784	2687.184	2625.684	0.038	0.044	0.045
	S4	58.761	99.339	88.562	116.967	1965.28	1774.272	1744.427	0.060	0.066	0.067
	S12	28.577	82.128	53.215	90.701	2427.944	2121.144	2073.2065	0.037	0.043	0.044
1	S10	14.844	23.569	21.915	28.022	3199.59	2793.69	2782.415	0.009	0.010	0.010
	S11	50.015	114.314	84.309	129.319	3465.882	3023.082	3010.782	0.037	0.043	0.043
	S4	59.239	107.241	91.412	125.013	2210.94	1996.056	1990.087	0.057	0.063	0.063
	S12	31.395	91.530	58.854	100.948	2731.437	2386.287	2376.6995	0.037	0.042	0.042

Çizelge B.67: 12 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.360	7.219	2.526	7.327	355.51	310.41	310.41	0.021	0.024	0.024
	S11	5.564	3.005	6.465	4.674	385.098	335.898	335.898	0.017	0.019	0.019
	S4	13.558	9.838	16.510	13.905	245.66	221.784	221.784	0.067	0.074	0.074
	S12	0.304	2.284	0.989	2.375	303.493	265.143	265.143	0.008	0.009	0.009
11	S10	0.949	8.287	3.435	8.572	711.02	620.82	620.82	0.012	0.014	0.014
	S11	13.766	13.428	17.794	17.558	770.196	671.796	671.796	0.023	0.026	0.026
	S4	23.501	26.042	31.314	33.093	491.32	443.568	443.568	0.067	0.075	0.075
	S12	3.739	10.932	7.018	12.053	606.986	530.286	530.286	0.020	0.023	0.023
10	S10	1.409	10.271	4.490	10.693	1066.53	931.23	931.23	0.010	0.011	0.011
	S11	21.922	24.217	29.187	30.793	1155.294	1007.694	1007.694	0.027	0.031	0.031
	S4	34.464	42.696	47.273	53.035	736.98	665.352	665.352	0.072	0.080	0.080
	S12	7.191	20.054	13.207	22.211	910.479	795.429	795.429	0.024	0.028	0.028
9	S10	3.466	7.799	5.806	8.839	1422.04	1241.64	1185.265	0.006	0.007	0.007
	S11	30.691	39.747	42.615	48.954	1540.392	1343.592	1282.092	0.032	0.036	0.038
	S4	44.925	61.230	63.294	74.708	982.64	887.136	857.291	0.076	0.084	0.087
	S12	11.809	33.035	21.720	36.578	1213.972	1060.572	1012.6345	0.030	0.034	0.036
8	S10	6.712	1.992	7.309	4.006	1777.55	1552.05	1450.575	0.004	0.005	0.005
	S11	39.789	59.192	57.547	71.129	1925.49	1679.49	1568.79	0.037	0.042	0.045
	S4	54.876	81.585	79.351	98.047	1228.3	1108.92	1055.199	0.080	0.088	0.093
	S12	17.328	48.952	32.013	54.150	1517.465	1325.715	1239.4275	0.036	0.041	0.044
7	S10	10.747	7.030	12.856	10.254	2133.06	1862.46	1715.885	0.006	0.007	0.007
	S11	49.066	81.849	73.621	96.569	2310.588	2015.388	1855.488	0.042	0.048	0.052
	S4	65.387	102.546	96.150	122.161	1473.96	1330.704	1253.107	0.083	0.092	0.097
	S12	24.107	69.138	44.848	76.370	1820.958	1590.858	1466.2205	0.042	0.048	0.052
6	S10	17.531	18.558	23.099	23.817	2488.57	2172.87	2003.745	0.010	0.011	0.012
	S11	58.374	110.230	91.443	127.742	2695.686	2351.286	2166.786	0.047	0.054	0.059
	S4	72.523	124.470	109.864	146.227	1719.62	1552.488	1462.953	0.085	0.094	0.100
	S12	29.456	90.559	56.623	99.396	2124.451	1856.001	1712.1885	0.047	0.054	0.058
5	S10	24.823	31.585	34.298	39.031	2844.08	2483.28	2314.155	0.014	0.016	0.017
	S11	67.212	139.309	109.004	159.472	3080.784	2687.184	2502.684	0.052	0.059	0.064
	S4	76.742	146.507	120.694	169.529	1965.28	1774.272	1684.737	0.086	0.096	0.101
	S12	35.056	112.569	68.827	123.085	2427.944	2121.144	1977.3315	0.051	0.058	0.062
4	S10	31.182	45.546	44.846	54.901	3199.59	2793.69	2647.115	0.017	0.020	0.021
	S11	75.229	166.738	125.250	189.306	3465.882	3023.082	2863.182	0.055	0.063	0.066
	S4	79.131	167.167	129.281	190.906	2210.94	1996.056	1918.459	0.086	0.096	0.100
	S12	41.845	135.043	82.358	147.597	2731.437	2386.287	2261.6495	0.054	0.062	0.065
3	S10	36.889	58.430	54.418	69.496	3555.1	3104.1	3002.625	0.020	0.022	0.023
	S11	82.079	192.075	139.702	216.699	3850.98	3358.98	3248.28	0.056	0.065	0.067
	S4	79.807	185.198	135.367	209.140	2456.6	2217.84	2164.119	0.085	0.094	0.097
	S12	47.877	155.293	94.465	169.656	3034.93	2651.43	2565.1425	0.056	0.064	0.066
2	S10	41.426	70.108	62.458	82.536	3910.61	3414.51	3358.135	0.021	0.024	0.025
	S11	87.236	213.065	151.156	239.236	4236.078	3694.878	3633.378	0.056	0.065	0.066
	S4	79.529	199.896	139.497	223.755	2702.26	2439.624	2409.779	0.083	0.092	0.093
	S12	53.102	172.721	104.918	188.652	3338.423	2916.573	2868.6355	0.057	0.065	0.066
1	S10	43.904	78.275	67.386	91.446	4266.12	3724.92	3713.645	0.021	0.025	0.025
	S11	90.113	226.938	158.195	253.972	4621.176	4030.776	4018.476	0.055	0.063	0.063
	S4	77.752	209.877	140.715	233.202	2947.92	2661.408	2655.439	0.079	0.088	0.088
	S12	56.645	184.055	111.861	201.048	3641.916	3181.716	3172.1285	0.055	0.063	0.063

Çizelge B.68: 6 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.042	5.649	1.737	5.662	355.51	332.96	287.86	0.016	0.017	0.020
	S11	4.612	5.072	6.134	6.455	385.098	360.498	311.298	0.017	0.018	0.021
	S4	11.676	7.697	13.985	11.200	245.66	233.722	209.846	0.057	0.060	0.067
	S12	1.675	3.400	2.695	3.903	303.493	284.318	245.968	0.013	0.014	0.016
5	S10	0.040	6.727	2.058	6.739	711.02	665.92	598.27	0.009	0.010	0.011
	S11	11.040	15.914	15.814	19.226	770.196	720.996	647.196	0.025	0.027	0.030
	S4	20.495	19.717	26.410	25.865	491.32	467.444	431.63	0.054	0.056	0.061
	S12	5.725	11.987	9.321	13.704	606.986	568.636	511.111	0.023	0.024	0.027
4	S10	0.259	8.182	2.714	8.260	1066.53	998.88	931.23	0.008	0.008	0.009
	S11	17.116	26.638	25.108	31.773	1155.294	1081.494	1007.694	0.028	0.029	0.032
	S4	29.535	31.669	39.036	40.530	736.98	701.166	665.352	0.055	0.058	0.061
	S12	9.675	20.645	15.868	23.548	910.479	852.954	795.429	0.026	0.028	0.030
3	S10	0.337	6.637	2.328	6.738	1422.04	1331.84	1286.74	0.005	0.005	0.005
	S11	22.904	39.356	34.711	46.227	1540.392	1441.992	1392.792	0.030	0.032	0.033
	S4	37.288	43.709	50.401	54.895	982.64	934.888	911.012	0.056	0.059	0.060
	S12	13.956	31.083	23.280	35.269	1213.972	1137.272	1098.922	0.029	0.031	0.032
2	S10	1.409	2.775	2.242	3.197	1777.55	1664.8	1642.25	0.002	0.002	0.002
	S11	27.677	52.417	43.402	60.720	1925.49	1802.49	1777.89	0.032	0.034	0.034
	S4	43.044	54.853	59.499	67.766	1228.3	1168.61	1156.672	0.055	0.058	0.059
	S12	18.010	41.872	30.571	47.275	1517.465	1421.59	1402.415	0.031	0.033	0.034
1	S10	1.914	1.469	2.354	2.043	2133.06	1997.76	1997.76	0.001	0.001	0.001
	S11	30.540	62.884	49.405	72.046	2310.588	2162.988	2162.988	0.031	0.033	0.033
	S4	46.276	63.206	65.237	77.089	1473.96	1402.332	1402.332	0.052	0.055	0.055
	S12	21.090	50.948	36.374	57.275	1820.958	1705.908	1705.908	0.031	0.034	0.034

Çizelge B.69: 9 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.266	9.014	2.970	9.094	355.51	310.41	254.035	0.026	0.029	0.036
	S11	7.160	5.926	8.938	8.074	385.098	335.898	274.398	0.023	0.027	0.033
	S4	17.370	11.879	20.934	17.090	245.66	221.784	191.939	0.085	0.094	0.109
	S12	1.502	4.094	2.730	4.544	303.493	265.143	217.2055	0.015	0.017	0.021
8	S10	0.619	10.636	3.810	10.822	711.02	620.82	519.345	0.015	0.017	0.021
	S11	17.480	21.046	23.794	26.290	770.196	671.796	561.096	0.034	0.039	0.047
	S4	30.473	31.281	39.857	40.423	491.32	443.568	389.847	0.082	0.091	0.104
	S12	6.806	16.181	11.660	18.222	606.986	530.286	443.9985	0.030	0.034	0.041
7	S10	0.804	13.253	4.780	13.494	1066.53	931.23	784.655	0.013	0.014	0.017
	S11	27.629	36.528	38.588	44.817	1155.294	1007.694	847.794	0.039	0.044	0.053
	S4	44.604	51.114	59.938	64.495	736.98	665.352	587.755	0.088	0.097	0.110
	S12	12.114	28.756	20.741	32.391	910.479	795.429	670.7915	0.036	0.041	0.048
6	S10	2.749	10.633	5.939	11.458	1422.04	1241.64	1072.515	0.008	0.009	0.011
	S11	38.265	57.254	55.441	68.733	1540.392	1343.592	1159.092	0.045	0.051	0.059
	S4	57.834	72.710	79.647	90.061	982.64	887.136	797.601	0.092	0.102	0.113
	S12	18.660	45.656	32.357	51.254	1213.972	1060.572	916.7595	0.042	0.048	0.056
5	S10	5.936	4.066	7.156	5.847	1777.55	1552.05	1382.925	0.004	0.005	0.005
	S11	48.833	81.772	73.365	96.422	1925.49	1679.49	1494.99	0.050	0.057	0.064
	S4	69.868	95.579	98.541	116.539	1228.3	1108.92	1019.385	0.095	0.105	0.114
	S12	25.997	65.438	45.629	73.237	1517.465	1325.715	1181.9025	0.048	0.055	0.062
4	S10	9.677	5.332	11.277	8.235	2133.06	1862.46	1715.885	0.005	0.006	0.007
	S11	58.837	107.979	91.230	125.629	2310.588	2015.388	1855.488	0.054	0.062	0.068
	S4	81.509	117.633	116.799	142.085	1473.96	1330.704	1253.107	0.096	0.107	0.113
	S12	33.976	88.169	60.427	98.362	1820.958	1590.858	1466.2205	0.054	0.062	0.067
3	S10	15.381	16.762	20.409	21.376	2488.57	2172.87	2071.395	0.009	0.010	0.010
	S11	67.762	136.774	108.794	157.103	2695.686	2351.286	2240.586	0.058	0.067	0.070
	S4	88.871	138.293	130.359	164.954	1719.62	1552.488	1498.767	0.096	0.106	0.110
	S12	40.135	110.329	73.234	122.370	2124.451	1856.001	1769.7135	0.058	0.066	0.069
2	S10	20.580	27.306	28.772	33.480	2844.08	2483.28	2426.905	0.012	0.013	0.014
	S11	74.586	161.918	123.161	184.294	3080.784	2687.184	2625.684	0.060	0.069	0.070
	S4	92.215	155.897	138.984	183.561	1965.28	1774.272	1744.427	0.093	0.103	0.105
	S12	44.846	128.887	83.512	142.340	2427.944	2121.144	2073.2065	0.059	0.067	0.069
1	S10	23.296	36.987	34.392	43.976	3199.59	2793.69	2782.415	0.014	0.016	0.016
	S11	78.490	179.397	132.310	202.944	3465.882	3023.082	3010.782	0.059	0.067	0.067
	S4	92.966	168.297	143.455	196.187	2210.94	1996.056	1990.087	0.089	0.098	0.099
	S12	49.269	143.640	92.362	158.421	2731.437	2386.287	2376.6995	0.058	0.066	0.067

Çizelge B.70: 12 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.566	11.329	3.964	11.499	355.51	310.41	310.41	0.032	0.037	0.037
	S11	8.731	4.716	10.146	7.335	385.098	335.898	335.898	0.026	0.030	0.030
	S4	21.278	15.439	25.909	21.822	245.66	221.784	221.784	0.105	0.117	0.117
	S12	0.477	3.585	1.553	3.728	303.493	265.143	265.143	0.012	0.014	0.014
11	S10	1.489	13.005	5.390	13.452	711.02	620.82	620.82	0.019	0.022	0.022
	S11	21.603	21.073	27.925	27.554	770.196	671.796	671.796	0.036	0.042	0.042
	S4	36.881	40.869	49.142	51.933	491.32	443.568	443.568	0.106	0.117	0.117
	S12	5.867	17.156	11.014	18.916	606.986	530.286	530.286	0.031	0.036	0.036
10	S10	2.211	16.118	7.046	16.781	1066.53	931.23	931.23	0.016	0.018	0.018
	S11	34.402	38.004	45.804	48.325	1155.294	1007.694	1007.694	0.042	0.048	0.048
	S4	54.086	67.004	74.187	83.230	736.98	665.352	665.352	0.113	0.125	0.125
	S12	11.285	31.471	20.726	34.856	910.479	795.429	795.429	0.038	0.044	0.044
9	S10	5.440	12.240	9.112	13.872	1422.04	1241.64	1185.265	0.010	0.011	0.012
	S11	48.164	62.376	66.877	76.825	1540.392	1343.592	1282.092	0.050	0.057	0.060
	S4	70.502	96.091	99.329	117.241	982.64	887.136	857.291	0.119	0.132	0.137
	S12	18.533	51.843	34.086	57.403	1213.972	1060.572	1012.6345	0.047	0.054	0.057
8	S10	10.533	3.127	11.471	6.287	1777.55	1552.05	1450.575	0.006	0.007	0.008
	S11	62.443	92.892	90.311	111.625	1925.49	1679.49	1568.79	0.058	0.066	0.071
	S4	86.118	128.033	124.528	153.869	1228.3	1108.92	1055.199	0.125	0.139	0.146
	S12	27.193	76.822	50.239	84.980	1517.465	1325.715	1239.4275	0.056	0.064	0.069
7	S10	16.865	11.033	20.175	16.092	2133.06	1862.46	1715.885	0.009	0.011	0.012
	S11	77.001	128.449	115.536	151.549	2310.588	2015.388	1855.488	0.066	0.075	0.082
	S4	102.613	160.928	150.892	191.712	1473.96	1330.704	1253.107	0.130	0.144	0.153
	S12	37.832	108.501	70.382	119.850	1820.958	1590.858	1466.2205	0.066	0.075	0.082
6	S10	27.513	29.123	36.250	37.377	2488.57	2172.87	2003.745	0.015	0.017	0.019
	S11	91.609	172.987	143.505	200.469	2695.686	2351.286	2166.786	0.074	0.085	0.093
	S4	113.813	195.336	172.413	229.479	1719.62	1552.488	1462.953	0.133	0.148	0.157
	S12	46.226	142.117	88.861	155.985	2124.451	1856.001	1712.1885	0.073	0.084	0.091
5	S10	38.955	49.567	53.825	61.253	2844.08	2483.28	2314.155	0.022	0.025	0.026
	S11	105.478	218.622	171.064	250.265	3080.784	2687.184	2502.684	0.081	0.093	0.100
	S4	120.434	229.918	189.410	266.048	1965.28	1774.272	1684.737	0.135	0.150	0.158
	S12	55.015	176.658	108.012	193.162	2427.944	2121.144	1977.3315	0.080	0.091	0.098
4	S10	48.935	71.477	70.378	86.157	3199.59	2793.69	2647.115	0.027	0.031	0.033
	S11	118.060	261.667	196.560	297.085	3465.882	3023.082	2863.182	0.086	0.098	0.104
	S4	124.182	262.341	202.885	299.596	2210.94	1996.056	1918.459	0.136	0.150	0.156
	S12	65.669	211.928	129.247	231.629	2731.437	2386.287	2261.6495	0.085	0.097	0.102
3	S10	57.891	91.695	85.400	109.063	3555.1	3104.1	3002.625	0.031	0.035	0.036
	S11	128.810	301.429	219.239	340.072	3850.98	3358.98	3248.28	0.088	0.101	0.105
	S4	125.244	290.637	212.435	328.210	2456.6	2217.84	2164.119	0.134	0.148	0.152
	S12	75.135	243.707	148.247	266.247	3034.93	2651.43	2565.1425	0.088	0.100	0.104
2	S10	65.011	110.023	98.018	129.526	3910.61	3414.51	3358.135	0.033	0.038	0.039
	S11	136.903	334.370	237.214	375.441	4236.078	3694.878	3633.378	0.089	0.102	0.103
	S4	124.807	313.704	218.918	351.146	2702.26	2439.624	2409.779	0.130	0.144	0.146
	S12	83.335	271.057	164.652	296.057	3338.423	2916.573	2868.6355	0.089	0.102	0.103
1	S10	68.900	122.840	105.752	143.510	4266.12	3724.92	3713.645	0.034	0.039	0.039
	S11	141.418	356.142	248.260	398.567	4621.176	4030.776	4018.476	0.086	0.099	0.099
	S4	122.019	329.366	220.829	365.972	2947.92	2661.408	2655.439	0.124	0.138	0.138
	S12	88.894	288.843	175.547	315.511	3641.916	3181.716	3172.1285	0.087	0.099	0.099

Çizelge B.71: 6 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.068	9.211	2.831	9.231	355.51	332.96	287.86	0.026	0.028	0.032
	S11	7.462	8.270	9.942	10.508	385.098	360.498	311.298	0.027	0.029	0.034
	S4	18.889	12.550	22.654	18.217	245.66	233.722	209.846	0.092	0.097	0.108
	S12	2.709	5.545	4.372	6.357	303.493	284.318	245.968	0.021	0.022	0.026
5	S10	0.065	10.968	3.356	10.988	711.02	665.92	598.27	0.015	0.017	0.018
	S11	17.860	25.949	25.645	31.307	770.196	720.996	647.196	0.041	0.043	0.048
	S4	33.156	32.150	42.800	42.096	491.32	467.444	431.63	0.087	0.092	0.099
	S12	9.261	19.545	15.124	22.324	606.986	568.636	511.111	0.037	0.039	0.044
4	S10	0.419	13.342	4.422	13.467	1066.53	998.88	931.23	0.013	0.013	0.014
	S11	27.690	43.436	40.720	51.742	1155.294	1081.494	1007.694	0.045	0.048	0.051
	S4	47.780	51.640	63.271	65.973	736.98	701.166	665.352	0.090	0.094	0.099
	S12	15.651	33.664	25.750	38.359	910.479	852.954	795.429	0.042	0.045	0.048
3	S10	0.545	10.822	3.792	10.985	1422.04	1331.84	1286.74	0.008	0.008	0.009
	S11	37.052	64.174	56.304	75.290	1540.392	1441.992	1392.792	0.049	0.052	0.054
	S4	60.322	71.271	81.703	89.368	982.64	934.888	911.012	0.091	0.096	0.098
	S12	22.577	50.683	37.781	57.456	1213.972	1137.272	1098.922	0.047	0.051	0.052
2	S10	2.280	4.524	3.637	5.208	1777.55	1664.8	1642.25	0.003	0.003	0.003
	S11	44.774	85.471	70.415	98.903	1925.49	1802.49	1777.89	0.051	0.055	0.056
	S4	69.633	89.443	96.466	110.333	1228.3	1168.61	1156.672	0.090	0.094	0.095
	S12	29.135	68.276	49.618	77.017	1517.465	1421.59	1402.415	0.051	0.054	0.055
1	S10	3.096	2.395	3.814	3.323	2133.06	1997.76	1997.76	0.002	0.002	0.002
	S11	49.405	102.538	80.166	117.359	2310.588	2162.988	2162.988	0.051	0.054	0.054
	S4	74.861	103.064	105.780	125.522	1473.96	1402.332	1402.332	0.085	0.090	0.090
	S12	34.118	83.075	59.041	93.310	1820.958	1705.908	1705.908	0.051	0.055	0.055

Çizelge B.72: 9 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.451	15.291	5.038	15.426	355.51	310.41	254.035	0.043	0.050	0.061
	S11	12.146	10.052	15.161	13.695	385.098	335.898	274.398	0.039	0.045	0.055
	S4	29.464	20.150	35.509	28.989	245.66	221.784	191.939	0.145	0.160	0.185
	S12	2.548	6.944	4.631	7.708	303.493	265.143	217.2055	0.025	0.029	0.035
8	S10	1.050	18.042	6.462	18.356	711.02	620.82	519.345	0.026	0.030	0.035
	S11	29.651	35.700	40.361	44.595	770.196	671.796	561.096	0.058	0.066	0.079
	S4	51.690	53.062	67.608	68.568	491.32	443.568	389.847	0.140	0.155	0.176
	S12	11.544	27.447	19.778	30.910	606.986	530.286	443.9985	0.051	0.058	0.070
7	S10	1.364	22.481	8.108	22.890	1066.53	931.23	784.655	0.021	0.025	0.029
	S11	46.866	61.961	65.455	76.021	1155.294	1007.694	847.794	0.066	0.075	0.090
	S4	75.660	86.702	101.671	109.400	736.98	665.352	587.755	0.148	0.164	0.186
	S12	20.549	48.778	35.182	54.943	910.479	795.429	670.7915	0.060	0.069	0.082
6	S10	4.663	18.037	10.074	19.436	1422.04	1241.64	1072.515	0.014	0.016	0.018
	S11	64.907	97.118	94.042	116.590	1540.392	1343.592	1159.092	0.076	0.087	0.101
	S4	98.102	123.336	135.103	152.766	982.64	887.136	797.601	0.155	0.172	0.192
	S12	31.653	77.444	54.886	86.939	1213.972	1060.572	916.7595	0.072	0.082	0.095
5	S10	10.069	6.898	12.138	9.918	1777.55	1552.05	1382.925	0.007	0.008	0.009
	S11	82.834	138.707	124.445	163.557	1925.49	1679.49	1494.99	0.085	0.097	0.109
	S4	118.514	162.126	167.152	197.681	1228.3	1108.92	1019.385	0.161	0.178	0.194
	S12	44.098	111.000	77.398	124.230	1517.465	1325.715	1181.9025	0.082	0.094	0.105
4	S10	16.415	9.045	19.128	13.969	2133.06	1862.46	1715.885	0.009	0.010	0.011
	S11	99.802	183.160	154.750	213.100	2310.588	2015.388	1855.488	0.092	0.106	0.115
	S4	138.260	199.536	198.121	241.014	1473.96	1330.704	1253.107	0.164	0.181	0.192
	S12	57.632	149.557	102.500	166.847	1820.958	1590.858	1466.2205	0.092	0.105	0.114
3	S10	26.089	28.433	34.619	36.260	2488.57	2172.87	2071.395	0.015	0.017	0.018
	S11	114.942	232.005	184.543	266.488	2695.686	2351.286	2240.586	0.099	0.113	0.119
	S4	150.748	234.581	221.122	279.806	1719.62	1552.488	1498.767	0.163	0.180	0.187
	S12	68.080	187.147	124.224	207.571	2124.451	1856.001	1769.7135	0.098	0.112	0.117
2	S10	34.909	46.318	48.804	56.791	2844.08	2483.28	2426.905	0.020	0.023	0.023
	S11	126.517	274.656	208.913	312.611	3080.784	2687.184	2625.684	0.101	0.116	0.119
	S4	156.421	264.441	235.753	311.367	1965.28	1774.272	1744.427	0.158	0.175	0.178
	S12	76.071	218.625	141.658	241.446	2427.944	2121.144	2073.2065	0.099	0.114	0.116
1	S10	39.516	62.740	58.338	74.595	3199.59	2793.69	2782.415	0.023	0.027	0.027
	S11	133.140	304.305	224.432	344.247	3465.882	3023.082	3010.782	0.099	0.114	0.114
	S4	157.695	285.476	243.338	332.784	2210.94	1996.056	1990.087	0.151	0.167	0.167
	S12	83.574	243.652	156.669	268.724	2731.437	2386.287	2376.6995	0.098	0.113	0.113

Çizelge B.73: 12 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.959	19.217	6.724	19.505	355.51	310.41	310.41	0.055	0.063	0.063
	S11	14.811	8.000	17.211	12.443	385.098	335.898	335.898	0.045	0.051	0.051
	S4	36.092	26.189	43.949	37.016	245.66	221.784	221.784	0.179	0.198	0.198
	S12	0.810	6.080	2.634	6.323	303.493	265.143	265.143	0.021	0.024	0.024
11	S10	2.525	22.060	9.143	22.818	711.02	620.82	620.82	0.032	0.037	0.037
	S11	36.645	35.745	47.368	46.739	770.196	671.796	671.796	0.062	0.071	0.071
	S4	62.560	69.325	83.358	88.093	491.32	443.568	443.568	0.179	0.199	0.199
	S12	9.952	29.101	18.682	32.086	606.986	530.286	530.286	0.053	0.061	0.061
10	S10	3.751	27.340	11.953	28.465	1066.53	931.23	931.23	0.027	0.031	0.031
	S11	58.355	64.465	77.695	81.972	1155.294	1007.694	1007.694	0.071	0.081	0.081
	S4	91.744	113.656	125.841	141.180	736.98	665.352	665.352	0.192	0.212	0.212
	S12	19.143	53.383	35.158	59.126	910.479	795.429	795.429	0.065	0.074	0.074
9	S10	9.227	20.762	15.456	23.530	1422.04	1241.64	1185.265	0.017	0.019	0.020
	S11	81.699	105.806	113.441	130.315	1540.392	1343.592	1282.092	0.085	0.097	0.102
	S4	119.590	162.995	168.488	198.872	982.64	887.136	857.291	0.202	0.224	0.232
	S12	31.437	87.940	57.819	97.371	1213.972	1060.572	1012.6345	0.080	0.092	0.096
8	S10	17.866	5.304	19.457	10.664	1777.55	1552.05	1450.575	0.011	0.013	0.013
	S11	105.920	157.569	153.190	189.345	1925.49	1679.49	1568.79	0.098	0.113	0.121
	S4	146.079	217.178	211.232	261.002	1228.3	1108.92	1055.199	0.212	0.235	0.247
	S12	46.126	130.311	85.219	144.148	1517.465	1325.715	1239.4275	0.095	0.109	0.116
7	S10	28.608	18.714	34.222	27.296	2133.06	1862.46	1715.885	0.016	0.018	0.020
	S11	130.614	217.882	195.979	257.067	2310.588	2015.388	1855.488	0.111	0.128	0.139
	S4	174.059	272.976	255.952	325.194	1473.96	1330.704	1253.107	0.221	0.244	0.260
	S12	64.172	184.045	119.386	203.297	1820.958	1590.858	1466.2205	0.112	0.128	0.139
6	S10	46.669	49.400	61.489	63.401	2488.57	2172.87	2003.745	0.025	0.029	0.032
	S11	155.392	293.431	243.421	340.049	2695.686	2351.286	2166.786	0.126	0.145	0.157
	S4	193.056	331.340	292.458	389.257	1719.62	1552.488	1462.953	0.226	0.251	0.266
	S12	78.411	241.068	150.732	264.591	2124.451	1856.001	1712.1885	0.125	0.143	0.155
5	S10	66.078	84.078	91.301	103.901	2844.08	2483.28	2314.155	0.037	0.042	0.045
	S11	178.918	370.839	290.170	424.515	3080.784	2687.184	2502.684	0.138	0.158	0.170
	S4	204.288	390.001	321.288	451.287	1965.28	1774.272	1684.737	0.230	0.254	0.268
	S12	93.320	299.657	183.217	327.653	2427.944	2121.144	1977.3315	0.135	0.154	0.166
4	S10	83.006	121.244	119.379	146.145	3199.59	2793.69	2647.115	0.046	0.052	0.055
	S11	200.260	443.856	333.417	503.934	3465.882	3023.082	2863.182	0.145	0.167	0.176
	S4	210.645	444.999	344.145	508.193	2210.94	1996.056	1918.459	0.230	0.255	0.265
	S12	111.392	359.486	219.237	392.903	2731.437	2386.287	2261.6495	0.144	0.165	0.174
3	S10	98.199	155.539	144.860	184.999	3555.1	3104.1	3002.625	0.052	0.060	0.062
	S11	218.495	511.303	371.886	576.852	3850.98	3358.98	3248.28	0.150	0.172	0.178
	S4	212.447	492.997	360.346	556.731	2456.6	2217.84	2164.119	0.227	0.251	0.257
	S12	127.448	413.390	251.465	451.624	3034.93	2651.43	2565.1425	0.149	0.170	0.176
2	S10	110.276	186.628	166.264	219.711	3910.61	3414.51	3358.135	0.056	0.064	0.065
	S11	232.223	567.179	402.376	636.846	4236.078	3694.878	3633.378	0.150	0.172	0.175
	S4	211.705	532.124	371.342	595.635	2702.26	2439.624	2409.779	0.220	0.244	0.247
	S12	141.357	459.784	279.292	502.191	3338.423	2916.573	2868.6355	0.150	0.172	0.175
1	S10	116.872	208.368	179.383	243.430	4266.12	3724.92	3713.645	0.057	0.065	0.066
	S11	239.881	604.109	421.114	676.074	4621.176	4030.776	4018.476	0.146	0.168	0.168
	S4	206.976	558.692	374.583	620.784	2947.92	2661.408	2655.439	0.211	0.233	0.234
	S12	150.788	489.953	297.774	535.189	3641.916	3181.716	3172.1285	0.147	0.168	0.169

Çizelge B.74: 6 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.030	4.027	1.238	4.036	355.51	332.96	287.86	0.011	0.012	0.014
	S11	3.288	3.615	4.372	4.602	385.098	360.498	311.298	0.012	0.013	0.015
	S4	8.323	5.487	9.969	7.984	245.66	233.722	209.846	0.041	0.043	0.048
	S12	1.194	2.424	1.921	2.782	303.493	284.318	245.968	0.009	0.010	0.011
5	S10	0.029	4.795	1.467	4.804	711.02	665.92	598.27	0.007	0.007	0.008
	S11	7.870	11.344	11.273	13.705	770.196	720.996	647.196	0.018	0.019	0.021
	S4	14.610	14.055	18.826	18.438	491.32	467.444	431.63	0.038	0.040	0.044
	S12	4.081	8.545	6.644	9.769	606.986	568.636	511.111	0.016	0.017	0.019
4	S10	0.185	5.833	1.935	5.888	1066.53	998.88	931.23	0.006	0.006	0.006
	S11	12.201	18.989	17.898	22.649	1155.294	1081.494	1007.694	0.020	0.021	0.022
	S4	21.054	22.575	27.827	28.892	736.98	701.166	665.352	0.039	0.041	0.043
	S12	6.897	14.717	11.312	16.786	910.479	852.954	795.429	0.018	0.020	0.021
3	S10	0.240	4.731	1.660	4.803	1422.04	1331.84	1286.74	0.003	0.004	0.004
	S11	16.327	28.055	24.743	32.953	1540.392	1441.992	1392.792	0.021	0.023	0.024
	S4	26.581	31.158	35.928	39.132	982.64	934.888	911.012	0.040	0.042	0.043
	S12	9.948	22.157	16.595	25.142	1213.972	1137.272	1098.922	0.021	0.022	0.023
2	S10	1.005	1.978	1.598	2.279	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	19.730	37.366	30.939	43.284	1925.49	1802.49	1777.89	0.022	0.024	0.024
	S4	30.684	39.102	42.414	48.307	1228.3	1168.61	1156.672	0.039	0.041	0.042
	S12	12.838	29.848	21.793	33.700	1517.465	1421.59	1402.415	0.022	0.024	0.024
1	S10	1.364	1.047	1.678	1.456	2133.06	1997.76	1997.76	0.001	0.001	0.001
	S11	21.770	44.827	35.218	51.358	2310.588	2162.988	2162.988	0.022	0.024	0.024
	S4	32.988	45.057	46.505	54.953	1473.96	1402.332	1402.332	0.037	0.039	0.039
	S12	15.034	36.318	25.930	40.828	1820.958	1705.908	1705.908	0.022	0.024	0.024

Çizelge B.75: 9 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.189	6.426	2.117	6.483	355.51	310.41	254.035	0.018	0.021	0.026
	S11	5.104	4.224	6.372	5.755	385.098	335.898	274.398	0.017	0.019	0.023
	S4	12.382	8.468	14.922	12.183	245.66	221.784	191.939	0.061	0.067	0.078
	S12	1.071	2.918	1.946	3.239	303.493	265.143	217.2055	0.011	0.012	0.015
8	S10	0.441	7.582	2.716	7.714	711.02	620.82	519.345	0.011	0.012	0.015
	S11	12.461	15.003	16.962	18.741	770.196	671.796	561.096	0.024	0.028	0.033
	S4	21.723	22.299	28.412	28.816	491.32	443.568	389.847	0.059	0.065	0.074
	S12	4.852	11.534	8.312	12.990	606.986	530.286	443.9985	0.021	0.024	0.029
7	S10	0.573	9.447	3.407	9.619	1066.53	931.23	784.655	0.009	0.010	0.012
	S11	19.696	26.039	27.507	31.948	1155.294	1007.694	847.794	0.028	0.032	0.038
	S4	31.796	36.436	42.727	45.975	736.98	665.352	587.755	0.062	0.069	0.078
	S12	8.636	20.499	14.785	23.090	910.479	795.429	670.7915	0.025	0.029	0.034
6	S10	1.959	7.580	4.233	8.168	1422.04	1241.64	1072.515	0.006	0.007	0.008
	S11	27.277	40.814	39.521	48.997	1540.392	1343.592	1159.092	0.032	0.036	0.042
	S4	41.227	51.832	56.777	64.200	982.64	887.136	797.601	0.065	0.072	0.080
	S12	13.302	32.546	23.066	36.536	1213.972	1060.572	916.7595	0.030	0.034	0.040
5	S10	4.231	2.899	5.101	4.168	1777.55	1552.05	1382.925	0.003	0.003	0.004
	S11	34.811	58.291	52.298	68.734	1925.49	1679.49	1494.99	0.036	0.041	0.046
	S4	49.805	68.133	70.245	83.075	1228.3	1108.92	1019.385	0.068	0.075	0.081
	S12	18.532	46.648	32.526	52.207	1517.465	1325.715	1181.9025	0.034	0.039	0.044
4	S10	6.898	3.801	8.038	5.870	2133.06	1862.46	1715.885	0.004	0.004	0.005
	S11	41.942	76.973	65.033	89.555	2310.588	2015.388	1855.488	0.039	0.044	0.048
	S4	58.104	83.855	83.260	101.286	1473.96	1330.704	1253.107	0.069	0.076	0.081
	S12	24.220	62.851	43.075	70.117	1820.958	1590.858	1466.2205	0.039	0.044	0.048
3	S10	10.964	11.949	14.549	15.238	2488.57	2172.87	2071.395	0.006	0.007	0.007
	S11	48.304	97.500	77.554	111.991	2695.686	2351.286	2240.586	0.042	0.048	0.050
	S4	63.352	98.582	92.926	117.588	1719.62	1552.488	1498.767	0.068	0.076	0.078
	S12	28.611	78.648	52.205	87.231	2124.451	1856.001	1769.7135	0.041	0.047	0.049
2	S10	14.670	19.465	20.510	23.866	2844.08	2483.28	2426.905	0.008	0.010	0.010
	S11	53.168	115.423	87.795	131.374	3080.784	2687.184	2625.684	0.043	0.049	0.050
	S4	65.736	111.131	99.075	130.851	1965.28	1774.272	1744.427	0.067	0.074	0.075
	S12	31.969	91.877	59.532	101.467	2427.944	2121.144	2073.2065	0.042	0.048	0.049
1	S10	16.607	26.366	24.516	31.348	3199.59	2793.69	2782.415	0.010	0.011	0.011
	S11	55.952	127.883	94.317	144.669	3465.882	3023.082	3010.782	0.042	0.048	0.048
	S4	66.271	119.971	102.262	139.852	2210.94	1996.056	1990.087	0.063	0.070	0.070
	S12	35.122	102.394	65.840	112.931	2731.437	2386.287	2376.6995	0.041	0.047	0.048

Çizelge B.76: 12 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.489	9.805	3.431	9.952	355.51	310.41	310.41	0.028	0.032	0.032
	S11	7.557	4.082	8.781	6.349	385.098	335.898	335.898	0.023	0.026	0.026
	S4	18.415	13.362	22.424	18.887	245.66	221.784	221.784	0.091	0.101	0.101
	S12	0.413	3.102	1.344	3.226	303.493	265.143	265.143	0.011	0.012	0.012
11	S10	1.288	11.256	4.665	11.642	711.02	620.82	620.82	0.016	0.019	0.019
	S11	18.697	18.238	24.169	23.847	770.196	671.796	671.796	0.031	0.036	0.036
	S4	31.920	35.371	42.531	44.947	491.32	443.568	443.568	0.091	0.101	0.101
	S12	5.078	14.848	9.532	16.371	606.986	530.286	530.286	0.027	0.031	0.031
10	S10	1.914	13.950	6.099	14.524	1066.53	931.23	931.23	0.014	0.016	0.016
	S11	29.775	32.892	39.642	41.824	1155.294	1007.694	1007.694	0.036	0.042	0.042
	S4	46.810	57.991	64.208	72.034	736.98	665.352	665.352	0.098	0.108	0.108
	S12	9.767	27.237	17.938	30.168	910.479	795.429	795.429	0.033	0.038	0.038
9	S10	4.708	10.593	7.886	12.006	1422.04	1241.64	1185.265	0.008	0.010	0.010
	S11	41.685	53.985	57.881	66.491	1540.392	1343.592	1282.092	0.043	0.049	0.052
	S4	61.018	83.165	85.967	101.470	982.64	887.136	857.291	0.103	0.114	0.118
	S12	16.040	44.869	29.501	49.681	1213.972	1060.572	1012.6345	0.041	0.047	0.049
8	S10	9.116	2.706	9.928	5.441	1777.55	1552.05	1450.575	0.006	0.006	0.007
	S11	54.043	80.396	78.162	96.609	1925.49	1679.49	1568.79	0.050	0.058	0.062
	S4	74.534	110.810	107.777	133.170	1228.3	1108.92	1055.199	0.108	0.120	0.126
	S12	23.535	66.488	43.481	73.549	1517.465	1325.715	1239.4275	0.048	0.055	0.059
7	S10	14.597	9.548	17.461	13.927	2133.06	1862.46	1715.885	0.008	0.009	0.010
	S11	66.643	111.170	99.994	131.163	2310.588	2015.388	1855.488	0.057	0.065	0.071
	S4	88.810	139.280	130.594	165.923	1473.96	1330.704	1253.107	0.113	0.125	0.132
	S12	32.743	93.905	60.914	103.728	1820.958	1590.858	1466.2205	0.057	0.065	0.071
6	S10	23.812	25.205	31.373	32.349	2488.57	2172.87	2003.745	0.013	0.015	0.016
	S11	79.285	149.717	124.200	173.502	2695.686	2351.286	2166.786	0.064	0.074	0.080
	S4	98.503	169.059	149.220	198.610	1719.62	1552.488	1462.953	0.115	0.128	0.136
	S12	40.008	123.000	76.907	135.002	2124.451	1856.001	1712.1885	0.064	0.073	0.079
5	S10	33.715	42.899	46.584	53.013	2844.08	2483.28	2314.155	0.019	0.021	0.023
	S11	91.289	189.213	148.053	216.599	3080.784	2687.184	2502.684	0.070	0.081	0.087
	S4	104.234	198.989	163.930	230.259	1965.28	1774.272	1684.737	0.117	0.130	0.137
	S12	47.614	152.894	93.482	167.178	2427.944	2121.144	1977.3315	0.069	0.079	0.085
4	S10	42.352	61.862	60.911	74.567	3199.59	2793.69	2647.115	0.023	0.027	0.028
	S11	102.178	226.468	170.118	257.121	3465.882	3023.082	2863.182	0.074	0.085	0.090
	S4	107.477	227.051	175.593	259.294	2210.94	1996.056	1918.459	0.117	0.130	0.135
	S12	56.835	183.420	111.861	200.470	2731.437	2386.287	2261.6495	0.073	0.084	0.089
3	S10	50.104	79.361	73.912	94.392	3555.1	3104.1	3002.625	0.027	0.030	0.031
	S11	111.482	260.881	189.747	294.326	3850.98	3358.98	3248.28	0.076	0.088	0.091
	S4	108.396	251.541	183.859	284.060	2456.6	2217.84	2164.119	0.116	0.128	0.131
	S12	65.028	210.923	128.305	230.431	3034.93	2651.43	2565.1425	0.076	0.087	0.090
2	S10	56.266	95.223	84.833	112.102	3910.61	3414.51	3358.135	0.029	0.033	0.033
	S11	118.487	289.391	205.304	324.937	4236.078	3694.878	3633.378	0.077	0.088	0.089
	S4	108.018	271.504	189.469	303.910	2702.26	2439.624	2409.779	0.112	0.125	0.126
	S12	72.125	234.595	142.503	256.232	3338.423	2916.573	2868.6355	0.077	0.088	0.089
1	S10	59.632	106.315	91.526	124.205	4266.12	3724.92	3713.645	0.029	0.033	0.033
	S11	122.394	308.234	214.864	344.952	4621.176	4030.776	4018.476	0.075	0.086	0.086
	S4	105.605	285.060	191.123	316.741	2947.92	2661.408	2655.439	0.107	0.119	0.119
	S12	76.936	249.988	151.932	273.069	3641.916	3181.716	3172.1285	0.075	0.086	0.086

Çizelge B.77: 6 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.030	4.027	1.238	4.036	355.51	332.96	287.86	0.011	0.012	0.014
	S11	3.288	3.615	4.372	4.602	385.098	360.498	311.298	0.012	0.013	0.015
	S4	8.323	5.487	9.969	7.984	245.66	233.722	209.846	0.041	0.043	0.048
	S12	1.194	2.424	1.921	2.782	303.493	284.318	245.968	0.009	0.010	0.011
5	S10	0.029	4.795	1.467	4.804	711.02	665.92	598.27	0.007	0.007	0.008
	S11	7.870	11.344	11.273	13.705	770.196	720.996	647.196	0.018	0.019	0.021
	S4	14.610	14.055	18.826	18.438	491.32	467.444	431.63	0.038	0.040	0.044
	S12	4.081	8.545	6.644	9.769	606.986	568.636	511.111	0.016	0.017	0.019
4	S10	0.185	5.833	1.935	5.888	1066.53	998.88	931.23	0.006	0.006	0.006
	S11	12.201	18.989	17.898	22.649	1155.294	1081.494	1007.694	0.020	0.021	0.022
	S4	21.054	22.575	27.827	28.892	736.98	701.166	665.352	0.039	0.041	0.043
	S12	6.897	14.717	11.312	16.786	910.479	852.954	795.429	0.018	0.020	0.021
3	S10	0.240	4.731	1.660	4.803	1422.04	1331.84	1286.74	0.003	0.004	0.004
	S11	16.327	28.055	24.743	32.953	1540.392	1441.992	1392.792	0.021	0.023	0.024
	S4	26.581	31.158	35.928	39.132	982.64	934.888	911.012	0.040	0.042	0.043
	S12	9.948	22.157	16.595	25.142	1213.972	1137.272	1098.922	0.021	0.022	0.023
2	S10	1.005	1.978	1.598	2.279	1777.55	1664.8	1642.25	0.001	0.001	0.001
	S11	19.730	37.366	30.939	43.284	1925.49	1802.49	1777.89	0.022	0.024	0.024
	S4	30.684	39.102	42.414	48.307	1228.3	1168.61	1156.672	0.039	0.041	0.042
	S12	12.838	29.848	21.793	33.700	1517.465	1421.59	1402.415	0.022	0.024	0.024
1	S10	1.364	1.047	1.678	1.456	2133.06	1997.76	1997.76	0.001	0.001	0.001
	S11	21.770	44.827	35.218	51.358	2310.588	2162.988	2162.988	0.022	0.024	0.024
	S4	32.988	45.057	46.505	54.953	1473.96	1402.332	1402.332	0.037	0.039	0.039
	S12	15.034	36.318	25.930	40.828	1820.958	1705.908	1705.908	0.022	0.024	0.024

Çizelge B.78: 9 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.208	7.074	2.330	7.136	355.51	310.41	254.035	0.020	0.023	0.028
	S11	5.619	4.650	7.014	6.336	385.098	335.898	274.398	0.018	0.021	0.026
	S4	13.630	9.322	16.427	13.411	245.66	221.784	191.939	0.067	0.074	0.086
	S12	1.179	3.212	2.142	3.566	303.493	265.143	217.2055	0.012	0.013	0.016
8	S10	0.486	8.346	2.989	8.492	711.02	620.82	519.345	0.012	0.014	0.016
	S11	13.717	16.515	18.671	20.630	770.196	671.796	561.096	0.027	0.031	0.037
	S4	23.912	24.547	31.276	31.720	491.32	443.568	389.847	0.065	0.072	0.081
	S12	5.341	12.697	9.150	14.299	606.986	530.286	443.9985	0.024	0.027	0.032
7	S10	0.631	10.400	3.751	10.589	1066.53	931.23	784.655	0.010	0.011	0.013
	S11	21.681	28.664	30.280	35.168	1155.294	1007.694	847.794	0.030	0.035	0.041
	S4	35.001	40.109	47.034	50.609	736.98	665.352	587.755	0.069	0.076	0.086
	S12	9.506	22.565	16.276	25.417	910.479	795.429	670.7915	0.028	0.032	0.038
6	S10	2.157	8.344	4.660	8.991	1422.04	1241.64	1072.515	0.006	0.007	0.008
	S11	30.026	44.927	43.505	53.935	1540.392	1343.592	1159.092	0.035	0.040	0.047
	S4	45.383	57.056	62.500	70.671	982.64	887.136	797.601	0.072	0.080	0.089
	S12	14.643	35.826	25.391	40.219	1213.972	1060.572	916.7595	0.033	0.038	0.044
5	S10	4.658	3.191	5.615	4.588	1777.55	1552.05	1382.925	0.003	0.004	0.004
	S11	38.319	64.167	57.569	75.663	1925.49	1679.49	1494.99	0.039	0.045	0.051
	S4	54.826	75.001	77.326	91.448	1228.3	1108.92	1019.385	0.074	0.082	0.090
	S12	20.400	51.350	35.805	57.470	1517.465	1325.715	1181.9025	0.038	0.043	0.049
4	S10	7.594	4.184	8.849	6.462	2133.06	1862.46	1715.885	0.004	0.005	0.005
	S11	46.169	84.731	71.589	98.582	2310.588	2015.388	1855.488	0.043	0.049	0.053
	S4	63.960	92.307	91.652	111.495	1473.96	1330.704	1253.107	0.076	0.084	0.089
	S12	26.661	69.186	47.417	77.185	1820.958	1590.858	1466.2205	0.042	0.049	0.053
3	S10	12.069	13.154	16.015	16.774	2488.57	2172.87	2071.395	0.007	0.008	0.008
	S11	53.173	107.327	85.371	123.279	2695.686	2351.286	2240.586	0.046	0.052	0.055
	S4	69.737	108.519	102.293	129.440	1719.62	1552.488	1498.767	0.075	0.083	0.086
	S12	31.494	86.576	57.467	96.024	2124.451	1856.001	1769.7135	0.045	0.052	0.054
2	S10	16.149	21.427	22.577	26.272	2844.08	2483.28	2426.905	0.009	0.011	0.011
	S11	58.528	127.058	96.645	144.616	3080.784	2687.184	2625.684	0.047	0.054	0.055
	S4	72.362	122.333	109.061	144.041	1965.28	1774.272	1744.427	0.073	0.081	0.083
	S12	35.191	101.138	65.532	111.695	2427.944	2121.144	2073.2065	0.046	0.053	0.054
1	S10	18.280	29.024	26.988	34.508	3199.59	2793.69	2782.415	0.011	0.012	0.012
	S11	61.592	140.774	103.824	159.251	3465.882	3023.082	3010.782	0.046	0.053	0.053
	S4	72.951	132.063	112.570	153.949	2210.94	1996.056	1990.087	0.070	0.077	0.077
	S12	38.662	112.715	72.476	124.314	2731.437	2386.287	2376.6995	0.046	0.052	0.052

Çizelge B.79: 12 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.551	11.031	3.860	11.196	355.51	310.41	310.41	0.031	0.036	0.036
	S11	8.502	4.592	9.879	7.142	385.098	335.898	335.898	0.026	0.029	0.029
	S4	20.717	15.032	25.227	21.248	245.66	221.784	221.784	0.103	0.114	0.114
	S12	0.465	3.490	1.512	3.630	303.493	265.143	265.143	0.012	0.014	0.014
11	S10	1.449	12.663	5.248	13.098	711.02	620.82	620.82	0.018	0.021	0.021
	S11	21.034	20.518	27.190	26.828	770.196	671.796	671.796	0.035	0.040	0.040
	S4	35.910	39.793	47.848	50.566	491.32	443.568	443.568	0.103	0.114	0.114
	S12	5.713	16.704	10.724	18.418	606.986	530.286	530.286	0.030	0.035	0.035
10	S10	2.153	15.693	6.861	16.339	1066.53	931.23	931.23	0.015	0.018	0.018
	S11	33.496	37.003	44.597	47.052	1155.294	1007.694	1007.694	0.041	0.047	0.047
	S4	52.662	65.239	72.234	81.038	736.98	665.352	665.352	0.110	0.122	0.122
	S12	10.988	30.642	20.181	33.939	910.479	795.429	795.429	0.037	0.043	0.043
9	S10	5.297	11.917	8.872	13.506	1422.04	1241.64	1185.265	0.009	0.011	0.011
	S11	46.896	60.733	65.116	74.802	1540.392	1343.592	1282.092	0.049	0.056	0.058
	S4	68.645	93.560	96.713	114.154	982.64	887.136	857.291	0.116	0.129	0.133
	S12	18.045	50.478	33.188	55.891	1213.972	1060.572	1012.6345	0.046	0.053	0.055
8	S10	10.255	3.044	11.169	6.121	1777.55	1552.05	1450.575	0.006	0.007	0.008
	S11	60.799	90.446	87.932	108.685	1925.49	1679.49	1568.79	0.056	0.065	0.069
	S4	83.850	124.662	121.249	149.817	1228.3	1108.92	1055.199	0.122	0.135	0.142
	S12	26.477	74.799	48.916	82.742	1517.465	1325.715	1239.4275	0.055	0.062	0.067
7	S10	16.421	10.742	19.644	15.668	2133.06	1862.46	1715.885	0.009	0.011	0.011
	S11	74.974	125.066	112.493	147.558	2310.588	2015.388	1855.488	0.064	0.073	0.080
	S4	99.911	156.690	146.918	186.663	1473.96	1330.704	1253.107	0.127	0.140	0.149
	S12	36.835	105.643	68.528	116.694	1820.958	1590.858	1466.2205	0.064	0.073	0.080
6	S10	26.788	28.356	35.295	36.393	2488.57	2172.87	2003.745	0.015	0.017	0.018
	S11	89.196	168.431	139.725	195.190	2695.686	2351.286	2166.786	0.072	0.083	0.090
	S4	110.816	190.192	167.873	223.436	1719.62	1552.488	1462.953	0.130	0.144	0.153
	S12	45.009	138.374	86.521	151.877	2124.451	1856.001	1712.1885	0.071	0.082	0.089
5	S10	37.929	48.261	52.407	59.640	2844.08	2483.28	2314.155	0.021	0.024	0.026
	S11	102.700	212.864	166.559	243.674	3080.784	2687.184	2502.684	0.079	0.091	0.097
	S4	117.263	223.863	184.422	259.042	1965.28	1774.272	1684.737	0.132	0.146	0.154
	S12	53.566	172.005	105.168	188.075	2427.944	2121.144	1977.3315	0.077	0.089	0.095
4	S10	47.646	69.595	68.524	83.888	3199.59	2793.69	2647.115	0.026	0.030	0.032
	S11	114.951	254.776	191.383	289.261	3465.882	3023.082	2863.182	0.083	0.096	0.101
	S4	120.912	255.432	197.541	291.706	2210.94	1996.056	1918.459	0.132	0.146	0.152
	S12	63.940	206.347	125.844	225.529	2731.437	2386.287	2261.6495	0.083	0.095	0.100
3	S10	56.367	89.281	83.151	106.191	3555.1	3104.1	3002.625	0.030	0.034	0.035
	S11	125.418	293.491	213.465	331.117	3850.98	3358.98	3248.28	0.086	0.099	0.102
	S4	121.946	282.983	206.841	319.567	2456.6	2217.84	2164.119	0.130	0.144	0.148
	S12	73.156	237.289	144.343	259.235	3034.93	2651.43	2565.1425	0.085	0.098	0.101
2	S10	63.299	107.126	95.437	126.115	3910.61	3414.51	3358.135	0.032	0.037	0.038
	S11	133.297	325.565	230.967	365.554	4236.078	3694.878	3633.378	0.086	0.099	0.101
	S4	121.520	305.442	213.153	341.898	2702.26	2439.624	2409.779	0.127	0.140	0.142
	S12	81.140	263.919	160.316	288.261	3338.423	2916.573	2868.6355	0.086	0.099	0.100
1	S10	67.085	119.605	102.967	139.730	4266.12	3724.92	3713.645	0.033	0.038	0.038
	S11	137.693	346.763	241.722	388.071	4621.176	4030.776	4018.476	0.084	0.096	0.097
	S4	118.806	320.693	215.013	356.334	2947.92	2661.408	2655.439	0.121	0.134	0.134
	S12	86.553	281.236	170.924	307.202	3641.916	3181.716	3172.1285	0.084	0.097	0.097

Çizelge B.80: 6 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.056	7.550	2.321	7.567	355.51	332.96	287.86	0.021	0.023	0.026
	S11	6.165	6.779	8.199	8.628	385.098	360.498	311.298	0.022	0.024	0.028
	S4	15.606	10.288	18.692	14.969	245.66	233.722	209.846	0.076	0.080	0.089
	S12	2.238	4.545	3.602	5.216	303.493	284.318	245.968	0.017	0.018	0.021
5	S10	0.054	8.991	2.751	9.007	711.02	665.92	598.27	0.013	0.014	0.015
	S11	14.757	21.270	21.138	25.697	770.196	720.996	647.196	0.033	0.036	0.040
	S4	27.394	26.353	35.300	34.571	491.32	467.444	431.63	0.072	0.076	0.082
	S12	7.651	16.021	12.458	18.317	606.986	568.636	511.111	0.030	0.032	0.036
4	S10	0.347	10.936	3.627	11.040	1066.53	998.88	931.23	0.010	0.011	0.012
	S11	22.878	35.604	33.559	42.467	1155.294	1081.494	1007.694	0.037	0.039	0.042
	S4	39.476	42.329	52.175	54.172	736.98	701.166	665.352	0.074	0.077	0.081
	S12	12.931	27.595	21.209	31.474	910.479	852.954	795.429	0.035	0.037	0.040
3	S10	0.451	8.871	3.112	9.006	1422.04	1331.84	1286.74	0.006	0.007	0.007
	S11	30.613	52.603	46.394	61.787	1540.392	1441.992	1392.792	0.040	0.043	0.044
	S4	49.839	58.421	67.365	73.373	982.64	934.888	911.012	0.075	0.078	0.081
	S12	18.653	41.545	31.116	47.141	1213.972	1137.272	1098.922	0.039	0.041	0.043
2	S10	1.884	3.708	2.996	4.273	1777.55	1664.8	1642.25	0.002	0.003	0.003
	S11	36.993	70.060	58.011	81.158	1925.49	1802.49	1777.89	0.042	0.045	0.046
	S4	57.532	73.316	79.527	90.575	1228.3	1168.61	1156.672	0.074	0.078	0.078
	S12	24.072	55.966	40.862	63.187	1517.465	1421.59	1402.415	0.042	0.044	0.045
1	S10	2.558	1.963	3.147	2.730	2133.06	1997.76	1997.76	0.001	0.002	0.002
	S11	40.819	84.050	66.034	96.296	2310.588	2162.988	2162.988	0.042	0.045	0.045
	S4	61.852	84.481	87.196	103.037	1473.96	1402.332	1402.332	0.070	0.073	0.073
	S12	28.189	68.096	48.618	76.553	1820.958	1705.908	1705.908	0.042	0.045	0.045

Çizelge B.81: 9 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.355	12.049	3.969	12.155	355.51	310.41	254.035	0.034	0.039	0.048
	S11	9.571	7.920	11.947	10.791	385.098	335.898	274.398	0.031	0.036	0.044
	S4	23.216	15.878	27.980	22.842	245.66	221.784	191.939	0.114	0.126	0.146
	S12	2.008	5.471	3.649	6.074	303.493	265.143	217.2055	0.020	0.023	0.028
8	S10	0.827	14.216	5.092	14.464	711.02	620.82	519.345	0.020	0.023	0.028
	S11	23.364	28.130	31.803	35.139	770.196	671.796	561.096	0.046	0.052	0.063
	S4	40.730	41.811	53.273	54.029	491.32	443.568	389.847	0.110	0.122	0.139
	S12	9.097	21.627	15.585	24.356	606.986	530.286	443.9985	0.040	0.046	0.055
7	S10	1.075	17.714	6.389	18.036	1066.53	931.23	784.655	0.017	0.019	0.023
	S11	36.929	48.823	51.576	59.902	1155.294	1007.694	847.794	0.052	0.059	0.071
	S4	59.617	68.318	80.113	86.203	736.98	665.352	587.755	0.117	0.130	0.147
	S12	16.192	38.436	27.722	43.293	910.479	795.429	670.7915	0.048	0.054	0.065
6	S10	3.674	14.213	7.938	15.315	1422.04	1241.64	1072.515	0.011	0.012	0.014
	S11	51.144	76.525	74.102	91.869	1540.392	1343.592	1159.092	0.060	0.068	0.079
	S4	77.301	97.184	106.456	120.375	982.64	887.136	797.601	0.123	0.136	0.151
	S12	24.941	61.023	43.248	68.505	1213.972	1060.572	916.7595	0.056	0.065	0.075
5	S10	7.934	5.435	9.564	7.815	1777.55	1552.05	1382.925	0.005	0.006	0.007
	S11	65.270	109.296	98.059	128.877	1925.49	1679.49	1494.99	0.067	0.077	0.086
	S4	93.385	127.750	131.710	155.765	1228.3	1108.92	1019.385	0.127	0.140	0.153
	S12	34.748	87.464	60.987	97.888	1517.465	1325.715	1181.9025	0.065	0.074	0.083
4	S10	12.934	7.127	15.072	11.007	2133.06	1862.46	1715.885	0.007	0.008	0.009
	S11	78.641	144.323	121.938	167.916	2310.588	2015.388	1855.488	0.073	0.083	0.090
	S4	108.944	157.227	156.112	189.911	1473.96	1330.704	1253.107	0.129	0.143	0.152
	S12	45.412	117.846	80.766	131.469	1820.958	1590.858	1466.2205	0.072	0.083	0.090
3	S10	20.558	22.404	27.279	28.572	2488.57	2172.87	2071.395	0.011	0.013	0.014
	S11	90.570	182.812	145.413	209.983	2695.686	2351.286	2240.586	0.078	0.089	0.094
	S4	118.784	184.842	174.237	220.477	1719.62	1552.488	1498.767	0.128	0.142	0.147
	S12	53.645	147.465	97.884	163.559	2124.451	1856.001	1769.7135	0.077	0.088	0.092
2	S10	27.507	36.497	38.456	44.749	2844.08	2483.28	2426.905	0.016	0.018	0.018
	S11	99.691	216.419	164.616	246.326	3080.784	2687.184	2625.684	0.080	0.092	0.094
	S4	123.254	208.370	185.765	245.346	1965.28	1774.272	1744.427	0.125	0.138	0.141
	S12	59.941	172.269	111.622	190.251	2427.944	2121.144	2073.2065	0.078	0.090	0.092
1	S10	31.137	49.437	45.968	58.778	3199.59	2793.69	2782.415	0.018	0.021	0.021
	S11	104.910	239.781	176.844	271.254	3465.882	3023.082	3010.782	0.078	0.090	0.090
	S4	124.258	224.945	191.741	262.222	2210.94	1996.056	1990.087	0.119	0.131	0.132
	S12	65.853	191.989	123.450	211.745	2731.437	2386.287	2376.6995	0.078	0.089	0.089

Çizelge B.82: 12 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	0.756	15.142	5.298	15.369	355.51	310.41	310.41	0.043	0.050	0.050
	S11	11.670	6.303	13.561	9.804	385.098	335.898	335.898	0.035	0.040	0.040
	S4	28.440	20.636	34.630	29.168	245.66	221.784	221.784	0.141	0.156	0.156
	S12	0.638	4.791	2.075	4.982	303.493	265.143	265.143	0.016	0.019	0.019
11	S10	1.990	17.383	7.205	17.980	711.02	620.82	620.82	0.025	0.029	0.029
	S11	28.875	28.166	37.325	36.829	770.196	671.796	671.796	0.048	0.056	0.056
	S4	49.295	54.625	65.683	69.414	491.32	443.568	443.568	0.141	0.156	0.156
	S12	7.842	22.930	14.721	25.283	606.986	530.286	530.286	0.042	0.048	0.048
10	S10	2.955	21.543	9.418	22.430	1066.53	931.23	931.23	0.021	0.024	0.024
	S11	45.982	50.796	61.221	64.591	1155.294	1007.694	1007.694	0.056	0.064	0.064
	S4	72.291	89.557	99.158	111.244	736.98	665.352	665.352	0.151	0.167	0.167
	S12	15.084	42.064	27.703	46.589	910.479	795.429	795.429	0.051	0.059	0.059
9	S10	7.271	16.359	12.179	18.541	1422.04	1241.64	1185.265	0.013	0.015	0.016
	S11	64.376	83.371	89.388	102.684	1540.392	1343.592	1282.092	0.067	0.076	0.080
	S4	94.233	128.434	132.763	156.704	982.64	887.136	857.291	0.159	0.177	0.183
	S12	24.771	69.293	45.559	76.725	1213.972	1060.572	1012.6345	0.063	0.072	0.076
8	S10	14.078	4.179	15.332	8.403	1777.55	1552.05	1450.575	0.009	0.010	0.011
	S11	83.461	124.159	120.708	149.197	1925.49	1679.49	1568.79	0.077	0.089	0.095
	S4	115.105	171.128	166.443	205.660	1228.3	1108.92	1055.199	0.167	0.185	0.195
	S12	36.346	102.680	67.150	113.584	1517.465	1325.715	1239.4275	0.075	0.086	0.092
7	S10	22.542	14.746	26.966	21.509	2133.06	1862.46	1715.885	0.013	0.014	0.016
	S11	102.919	171.684	154.424	202.559	2310.588	2015.388	1855.488	0.088	0.101	0.109
	S4	137.152	215.096	201.681	256.241	1473.96	1330.704	1253.107	0.174	0.193	0.204
	S12	50.566	145.021	94.072	160.191	1820.958	1590.858	1466.2205	0.088	0.101	0.109
6	S10	36.773	38.926	48.451	49.958	2488.57	2172.87	2003.745	0.020	0.023	0.025
	S11	122.443	231.213	191.807	267.946	2695.686	2351.286	2166.786	0.099	0.114	0.124
	S4	152.121	261.084	230.447	306.721	1719.62	1552.488	1462.953	0.178	0.198	0.210
	S12	61.785	189.953	118.771	208.488	2124.451	1856.001	1712.1885	0.098	0.112	0.122
5	S10	52.067	66.251	71.942	81.871	2844.08	2483.28	2314.155	0.029	0.033	0.035
	S11	140.981	292.208	228.643	334.502	3080.784	2687.184	2502.684	0.109	0.124	0.134
	S4	160.972	307.307	253.164	355.598	1965.28	1774.272	1684.737	0.181	0.200	0.211
	S12	73.533	236.119	144.369	258.179	2427.944	2121.144	1977.3315	0.106	0.122	0.131
4	S10	65.406	95.536	94.067	115.157	3199.59	2793.69	2647.115	0.036	0.041	0.044
	S11	157.798	349.742	262.720	397.082	3465.882	3023.082	2863.182	0.115	0.131	0.139
	S4	165.981	350.643	271.174	400.438	2210.94	1996.056	1918.459	0.181	0.201	0.209
	S12	87.773	283.262	172.751	309.594	2731.437	2386.287	2261.6495	0.113	0.130	0.137
3	S10	77.377	122.560	114.145	145.773	3555.1	3104.1	3002.625	0.041	0.047	0.049
	S11	172.167	402.889	293.033	454.539	3850.98	3358.98	3248.28	0.118	0.135	0.140
	S4	167.401	388.464	283.940	438.684	2456.6	2217.84	2164.119	0.179	0.198	0.203
	S12	100.425	325.737	198.146	355.864	3034.93	2651.43	2565.1425	0.117	0.134	0.139
2	S10	86.893	147.056	131.010	173.124	3910.61	3414.51	3358.135	0.044	0.051	0.052
	S11	182.983	446.917	317.058	501.812	4236.078	3694.878	3633.378	0.118	0.136	0.138
	S4	166.816	419.294	292.604	469.339	2702.26	2439.624	2409.779	0.174	0.192	0.195
	S12	111.385	362.293	220.072	395.709	3338.423	2916.573	2868.6355	0.119	0.136	0.138
1	S10	92.091	164.187	141.347	191.814	4266.12	3724.92	3713.645	0.045	0.051	0.052
	S11	189.018	476.017	331.823	532.722	4621.176	4030.776	4018.476	0.115	0.132	0.133
	S4	163.090	440.229	295.158	489.156	2947.92	2661.408	2655.439	0.166	0.184	0.184
	S12	118.815	386.066	234.635	421.710	3641.916	3181.716	3172.1285	0.116	0.133	0.133

Çizelge B.83: 6 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.078	10.490	3.225	10.513	355.51	332.96	287.86	0.030	0.032	0.037
	S11	8.565	9.418	11.390	11.987	385.098	360.498	311.298	0.031	0.033	0.039
	S4	21.682	14.293	25.970	20.797	245.66	233.722	209.846	0.106	0.111	0.124
	S12	3.110	6.314	5.004	7.247	303.493	284.318	245.968	0.024	0.025	0.029
5	S10	0.075	12.491	3.822	12.513	711.02	665.92	598.27	0.018	0.019	0.021
	S11	20.502	29.552	29.367	35.702	770.196	720.996	647.196	0.046	0.050	0.055
	S4	38.059	36.613	49.043	48.031	491.32	467.444	431.63	0.100	0.105	0.114
	S12	10.630	22.259	17.308	25.448	606.986	568.636	511.111	0.042	0.045	0.050
4	S10	0.481	15.194	5.039	15.338	1066.53	998.88	931.23	0.014	0.015	0.016
	S11	31.785	49.466	46.624	59.001	1155.294	1081.494	1007.694	0.051	0.055	0.059
	S4	54.846	58.809	72.488	75.263	736.98	701.166	665.352	0.102	0.107	0.113
	S12	17.965	38.338	29.467	43.728	910.479	852.954	795.429	0.048	0.051	0.055
3	S10	0.626	12.324	4.323	12.512	1422.04	1331.84	1286.74	0.009	0.009	0.010
	S11	42.532	73.084	64.457	85.843	1540.392	1441.992	1392.792	0.056	0.060	0.062
	S4	69.243	81.166	93.593	101.939	982.64	934.888	911.012	0.104	0.109	0.112
	S12	25.915	57.719	43.231	65.494	1213.972	1137.272	1098.922	0.054	0.058	0.060
2	S10	2.617	5.152	4.163	5.937	1777.55	1664.8	1642.25	0.003	0.004	0.004
	S11	51.396	97.337	80.597	112.756	1925.49	1802.49	1777.89	0.059	0.063	0.063
	S4	79.931	101.860	110.489	125.840	1228.3	1168.61	1156.672	0.102	0.108	0.109
	S12	33.444	77.755	56.770	87.788	1517.465	1421.59	1402.415	0.058	0.062	0.063
1	S10	3.554	2.727	4.372	3.793	2133.06	1997.76	1997.76	0.002	0.002	0.002
	S11	56.711	116.774	91.743	133.787	2310.588	2162.988	2162.988	0.058	0.062	0.062
	S4	85.932	117.373	121.144	143.152	1473.96	1402.332	1402.332	0.097	0.102	0.102
	S12	39.164	94.608	67.546	106.357	1820.958	1705.908	1705.908	0.058	0.062	0.062

Çizelge B.84: 9 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.493	16.739	5.515	16.887	355.51	310.41	254.035	0.048	0.054	0.066
	S11	13.297	11.004	16.598	14.993	385.098	335.898	274.398	0.043	0.049	0.060
	S4	32.255	22.059	38.873	31.736	245.66	221.784	191.939	0.158	0.175	0.203
	S12	2.789	7.602	5.070	8.438	303.493	265.143	217.2055	0.028	0.032	0.039
8	S10	1.149	19.751	7.074	20.096	711.02	620.82	519.345	0.028	0.032	0.039
	S11	32.460	39.082	44.185	48.820	770.196	671.796	561.096	0.063	0.073	0.087
	S4	56.587	58.089	74.014	75.065	491.32	443.568	389.847	0.153	0.169	0.193
	S12	12.638	30.047	21.652	33.839	606.986	530.286	443.9985	0.056	0.064	0.076
7	S10	1.493	24.611	8.876	25.059	1066.53	931.23	784.655	0.023	0.027	0.032
	S11	51.307	67.831	71.656	83.223	1155.294	1007.694	847.794	0.072	0.083	0.098
	S4	82.828	94.917	111.303	119.765	736.98	665.352	587.755	0.163	0.180	0.204
	S12	22.496	53.400	38.515	60.148	910.479	795.429	670.7915	0.066	0.076	0.090
6	S10	5.104	19.746	11.028	21.277	1422.04	1241.64	1072.515	0.015	0.017	0.020
	S11	71.056	106.319	102.952	127.636	1540.392	1343.592	1159.092	0.083	0.095	0.110
	S4	107.397	135.021	147.903	167.240	982.64	887.136	797.601	0.170	0.189	0.210
	S12	34.652	84.781	60.086	95.177	1213.972	1060.572	916.7595	0.078	0.090	0.104
5	S10	11.023	7.551	13.288	10.858	1777.55	1552.05	1382.925	0.007	0.009	0.010
	S11	90.682	151.848	136.236	179.053	1925.49	1679.49	1494.99	0.093	0.107	0.120
	S4	129.743	177.487	182.989	216.410	1228.3	1108.92	1019.385	0.176	0.195	0.212
	S12	48.276	121.517	84.731	136.000	1517.465	1325.715	1181.9025	0.090	0.103	0.115
4	S10	17.970	9.901	20.940	15.292	2133.06	1862.46	1715.885	0.010	0.011	0.012
	S11	109.258	200.513	169.412	233.291	2310.588	2015.388	1855.488	0.101	0.116	0.126
	S4	151.360	218.441	216.892	263.849	1473.96	1330.704	1253.107	0.179	0.198	0.211
	S12	63.093	163.727	112.211	182.655	1820.958	1590.858	1466.2205	0.100	0.115	0.125
3	S10	28.561	31.127	37.899	39.696	2488.57	2172.87	2071.395	0.016	0.018	0.019
	S11	125.832	253.987	202.028	291.736	2695.686	2351.286	2240.586	0.108	0.124	0.130
	S4	165.031	256.807	242.073	306.316	1719.62	1552.488	1498.767	0.178	0.197	0.204
	S12	74.530	204.878	135.994	227.238	2124.451	1856.001	1769.7135	0.107	0.122	0.128
2	S10	38.216	50.707	53.428	62.172	2844.08	2483.28	2426.905	0.022	0.025	0.026
	S11	138.503	300.678	228.707	342.229	3080.784	2687.184	2625.684	0.111	0.127	0.130
	S4	171.241	289.496	258.090	340.868	1965.28	1774.272	1744.427	0.173	0.192	0.195
	S12	83.278	239.339	155.080	264.322	2427.944	2121.144	2073.2065	0.109	0.125	0.127
1	S10	43.260	68.684	63.865	81.662	3199.59	2793.69	2782.415	0.026	0.029	0.029
	S11	145.755	333.136	245.695	376.862	3465.882	3023.082	3010.782	0.109	0.125	0.125
	S4	172.636	312.524	266.393	364.314	2210.94	1996.056	1990.087	0.165	0.183	0.183
	S12	91.492	266.737	171.513	294.184	2731.437	2386.287	2376.6995	0.108	0.123	0.124

Çizelge B.85: 12 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	1.050	21.038	7.361	21.353	355.51	310.41	310.41	0.060	0.069	0.069
	S11	16.214	8.757	18.841	13.622	385.098	335.898	335.898	0.049	0.056	0.056
	S4	39.512	28.670	48.113	40.523	245.66	221.784	221.784	0.196	0.217	0.217
	S12	0.887	6.656	2.883	6.922	303.493	265.143	265.143	0.023	0.026	0.026
11	S10	2.764	24.151	10.009	24.980	711.02	620.82	620.82	0.035	0.040	0.040
	S11	40.117	39.132	51.856	51.167	770.196	671.796	671.796	0.067	0.077	0.077
	S4	68.487	75.893	91.255	96.439	491.32	443.568	443.568	0.196	0.217	0.217
	S12	10.895	31.858	20.452	35.126	606.986	530.286	530.286	0.058	0.066	0.066
10	S10	4.106	29.930	13.085	31.162	1066.53	931.23	931.23	0.029	0.033	0.033
	S11	63.884	70.573	85.056	89.738	1155.294	1007.694	1007.694	0.078	0.089	0.089
	S4	100.436	124.425	137.764	154.556	736.98	665.352	665.352	0.210	0.232	0.232
	S12	20.956	58.441	38.488	64.727	910.479	795.429	795.429	0.071	0.081	0.081
9	S10	10.102	22.729	16.920	25.759	1422.04	1241.64	1185.265	0.018	0.021	0.022
	S11	89.440	115.830	124.189	142.662	1540.392	1343.592	1282.092	0.093	0.106	0.111
	S4	130.920	178.438	184.452	217.714	982.64	887.136	857.291	0.222	0.245	0.254
	S12	34.415	96.272	63.297	106.596	1213.972	1060.572	1012.6345	0.088	0.101	0.105
8	S10	19.559	5.806	21.301	11.674	1777.55	1552.05	1450.575	0.012	0.014	0.015
	S11	115.955	172.498	167.704	207.285	1925.49	1679.49	1568.79	0.108	0.123	0.132
	S4	159.919	237.754	231.245	285.730	1228.3	1108.92	1055.199	0.233	0.258	0.271
	S12	50.496	142.657	93.293	157.806	1517.465	1325.715	1239.4275	0.104	0.119	0.127
7	S10	31.319	20.487	37.465	29.883	2133.06	1862.46	1715.885	0.018	0.020	0.022
	S11	142.989	238.526	214.547	281.422	2310.588	2015.388	1855.488	0.122	0.140	0.152
	S4	190.550	298.839	280.202	356.004	1473.96	1330.704	1253.107	0.242	0.268	0.284
	S12	70.252	201.483	130.697	222.558	1820.958	1590.858	1466.2205	0.122	0.140	0.152
6	S10	51.090	54.081	67.315	69.408	2488.57	2172.87	2003.745	0.028	0.032	0.035
	S11	170.115	321.232	266.484	372.266	2695.686	2351.286	2166.786	0.138	0.158	0.172
	S4	211.347	362.733	320.167	426.137	1719.62	1552.488	1462.953	0.248	0.274	0.291
	S12	85.840	263.908	165.013	289.660	2124.451	1856.001	1712.1885	0.136	0.156	0.169
5	S10	72.338	92.044	99.951	113.746	2844.08	2483.28	2314.155	0.040	0.046	0.049
	S11	195.869	405.975	317.662	464.735	3080.784	2687.184	2502.684	0.151	0.173	0.186
	S4	223.643	426.952	351.729	494.045	1965.28	1774.272	1684.737	0.251	0.278	0.293
	S12	102.161	328.049	200.576	358.697	2427.944	2121.144	1977.3315	0.148	0.169	0.181
4	S10	90.871	132.731	130.690	159.992	3199.59	2793.69	2647.115	0.050	0.057	0.060
	S11	219.234	485.909	365.006	551.679	3465.882	3023.082	2863.182	0.159	0.182	0.193
	S4	230.603	487.161	376.751	556.342	2210.94	1996.056	1918.459	0.252	0.279	0.290
	S12	121.946	393.545	240.009	430.129	2731.437	2386.287	2261.6495	0.157	0.180	0.190
3	S10	107.502	170.276	158.585	202.527	3555.1	3104.1	3002.625	0.057	0.065	0.067
	S11	239.197	559.747	407.121	631.505	3850.98	3358.98	3248.28	0.164	0.188	0.194
	S4	232.575	539.706	394.487	609.478	2456.6	2217.84	2164.119	0.248	0.275	0.282
	S12	139.524	452.557	275.290	494.414	3034.93	2651.43	2565.1425	0.163	0.186	0.193
2	S10	120.724	204.310	182.017	240.527	3910.61	3414.51	3358.135	0.062	0.070	0.072
	S11	254.225	620.917	440.500	697.184	4236.078	3694.878	3633.378	0.165	0.189	0.192
	S4	231.763	582.540	406.525	652.069	2702.26	2439.624	2409.779	0.241	0.267	0.271
	S12	154.750	503.346	305.754	549.771	3338.423	2916.573	2868.6355	0.165	0.188	0.192
1	S10	127.945	228.110	196.378	266.494	4266.12	3724.92	3713.645	0.062	0.072	0.072
	S11	262.609	661.346	461.012	740.128	4621.176	4030.776	4018.476	0.160	0.184	0.184
	S4	226.586	611.625	410.073	679.600	2947.92	2661.408	2655.439	0.231	0.255	0.256
	S12	165.074	536.374	325.986	585.896	3641.916	3181.716	3172.1285	0.161	0.184	0.185

Çizelge B.86: 6 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	0.104	14.145	4.348	14.176	355.51	332.96	287.86	0.040	0.043	0.049
	S11	11.456	12.700	15.266	16.136	385.098	360.498	311.298	0.042	0.045	0.052
	S4	29.001	19.273	34.783	27.974	245.66	233.722	209.846	0.142	0.149	0.166
	S12	4.159	8.515	6.713	9.762	303.493	284.318	245.968	0.032	0.034	0.040
5	S10	0.100	16.843	5.153	16.873	711.02	665.92	598.27	0.024	0.025	0.028
	S11	27.422	39.849	39.377	48.076	770.196	720.996	647.196	0.062	0.067	0.074
	S4	50.906	49.371	65.718	64.643	491.32	467.444	431.63	0.134	0.141	0.152
	S12	14.219	30.015	23.223	34.281	606.986	568.636	511.111	0.056	0.060	0.067
4	S10	0.644	20.488	6.790	20.681	1066.53	998.88	931.23	0.019	0.021	0.022
	S11	42.514	66.702	62.525	79.456	1155.294	1081.494	1007.694	0.069	0.073	0.079
	S4	73.360	79.301	97.150	101.309	736.98	701.166	665.352	0.137	0.144	0.152
	S12	24.030	51.697	39.539	58.906	910.479	852.954	795.429	0.065	0.069	0.074
3	S10	0.837	16.619	5.823	16.870	1422.04	1331.84	1286.74	0.012	0.013	0.013
	S11	56.889	98.550	86.454	115.616	1540.392	1441.992	1392.792	0.075	0.080	0.083
	S4	92.617	109.449	125.452	137.234	982.64	934.888	911.012	0.140	0.147	0.151
	S12	34.664	77.832	58.013	88.231	1213.972	1137.272	1098.922	0.073	0.078	0.080
2	S10	3.500	6.948	5.585	7.998	1777.55	1664.8	1642.25	0.004	0.005	0.005
	S11	68.745	131.255	108.121	151.878	1925.49	1802.49	1777.89	0.079	0.084	0.085
	S4	106.913	137.354	148.119	169.427	1228.3	1168.61	1156.672	0.138	0.145	0.146
	S12	44.733	104.849	76.188	118.269	1517.465	1421.59	1402.415	0.078	0.083	0.084
1	S10	4.754	3.677	5.857	5.103	2133.06	1997.76	1997.76	0.003	0.003	0.003
	S11	75.855	157.464	123.094	180.220	2310.588	2162.988	2162.988	0.078	0.083	0.083
	S4	114.940	158.271	162.422	192.753	1473.96	1402.332	1402.332	0.131	0.137	0.137
	S12	52.384	127.574	90.657	143.290	1820.958	1705.908	1705.908	0.079	0.084	0.084

Çizelge B.87: 9 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	0.712	24.177	7.965	24.391	355.51	310.41	254.035	0.069	0.079	0.096
	S11	19.205	15.893	23.973	21.655	385.098	335.898	274.398	0.062	0.071	0.087
	S4	46.587	31.861	56.146	45.837	245.66	221.784	191.939	0.229	0.253	0.293
	S12	4.028	10.979	7.322	12.188	303.493	265.143	217.2055	0.040	0.046	0.056
8	S10	1.659	28.527	10.218	29.025	711.02	620.82	519.345	0.041	0.047	0.056
	S11	46.884	56.448	63.818	70.513	770.196	671.796	561.096	0.092	0.105	0.126
	S4	81.731	83.900	106.901	108.419	491.32	443.568	389.847	0.221	0.244	0.278
	S12	18.254	43.398	31.273	48.874	606.986	530.286	443.9985	0.081	0.092	0.110
7	S10	2.157	35.546	12.820	36.193	1066.53	931.23	784.655	0.034	0.039	0.046
	S11	74.104	97.971	103.496	120.203	1155.294	1007.694	847.794	0.104	0.119	0.142
	S4	119.632	137.092	160.760	172.981	736.98	665.352	587.755	0.235	0.260	0.294
	S12	32.491	77.127	55.629	86.875	910.479	795.429	670.7915	0.095	0.109	0.130
6	S10	7.372	28.520	15.928	30.732	1422.04	1241.64	1072.515	0.022	0.025	0.029
	S11	102.629	153.561	148.698	184.350	1540.392	1343.592	1159.092	0.120	0.137	0.159
	S4	155.117	195.017	213.622	241.552	982.64	887.136	797.601	0.246	0.272	0.303
	S12	50.049	122.453	86.784	137.467	1213.972	1060.572	916.7595	0.113	0.130	0.150
5	S10	15.921	10.907	19.193	15.683	1777.55	1552.05	1382.925	0.011	0.012	0.014
	S11	130.975	219.320	196.771	258.613	1925.49	1679.49	1494.99	0.134	0.154	0.173
	S4	187.392	256.351	264.298	312.569	1228.3	1108.92	1019.385	0.254	0.282	0.307
	S12	69.727	175.511	122.380	196.429	1517.465	1325.715	1181.9025	0.129	0.148	0.166
4	S10	25.955	14.301	30.245	22.087	2133.06	1862.46	1715.885	0.014	0.016	0.018
	S11	157.805	289.609	244.688	336.951	2310.588	2015.388	1855.488	0.146	0.167	0.182
	S4	218.615	315.503	313.265	381.087	1473.96	1330.704	1253.107	0.259	0.286	0.304
	S12	91.127	236.477	162.071	263.816	1820.958	1590.858	1466.2205	0.145	0.166	0.180
3	S10	41.252	44.958	54.739	57.334	2488.57	2172.87	2071.395	0.023	0.026	0.028
	S11	181.743	366.842	291.796	421.365	2695.686	2351.286	2240.586	0.156	0.179	0.188
	S4	238.360	370.916	349.635	442.424	1719.62	1552.488	1498.767	0.257	0.285	0.295
	S12	107.647	295.914	196.421	328.208	2124.451	1856.001	1769.7135	0.154	0.177	0.185
2	S10	55.197	73.238	77.169	89.797	2844.08	2483.28	2426.905	0.032	0.036	0.037
	S11	200.046	434.280	330.330	494.294	3080.784	2687.184	2625.684	0.160	0.184	0.188
	S4	247.330	418.130	372.769	492.329	1965.28	1774.272	1744.427	0.251	0.277	0.282
	S12	120.282	345.686	223.988	381.771	2427.944	2121.144	2073.2065	0.157	0.180	0.184
1	S10	62.482	99.203	92.243	117.948	3199.59	2793.69	2782.415	0.037	0.042	0.042
	S11	210.519	481.161	354.867	544.316	3465.882	3023.082	3010.782	0.157	0.180	0.181
	S4	249.344	451.390	384.761	526.193	2210.94	1996.056	1990.087	0.238	0.264	0.264
	S12	132.145	385.258	247.723	424.901	2731.437	2386.287	2376.6995	0.156	0.178	0.179

Çizelge B.88: 12 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	1.517	30.385	10.632	30.840	355.51	310.41	310.41	0.087	0.099	0.099
	S11	23.419	12.649	27.213	19.674	385.098	335.898	335.898	0.071	0.081	0.081
	S4	57.069	41.409	69.491	58.529	245.66	221.784	221.784	0.283	0.313	0.313
	S12	1.280	9.614	4.165	9.998	303.493	265.143	265.143	0.033	0.038	0.038
11	S10	3.993	34.882	14.457	36.079	711.02	620.82	620.82	0.051	0.058	0.058
	S11	57.942	56.520	74.898	73.903	770.196	671.796	671.796	0.097	0.111	0.111
	S4	98.919	109.615	131.803	139.291	491.32	443.568	443.568	0.284	0.314	0.314
	S12	15.736	46.014	29.540	50.734	606.986	530.286	530.286	0.084	0.096	0.096
10	S10	5.930	43.230	18.899	45.009	1066.53	931.23	931.23	0.042	0.048	0.048
	S11	92.271	101.931	122.850	129.612	1155.294	1007.694	1007.694	0.112	0.129	0.129
	S4	145.064	179.711	198.977	223.230	736.98	665.352	665.352	0.303	0.336	0.336
	S12	30.268	84.408	55.590	93.488	910.479	795.429	795.429	0.103	0.118	0.118
9	S10	14.590	32.828	24.439	37.205	1422.04	1241.64	1185.265	0.026	0.030	0.031
	S11	129.182	167.298	179.371	206.052	1540.392	1343.592	1282.092	0.134	0.153	0.161
	S4	189.093	257.725	266.411	314.453	982.64	887.136	857.291	0.320	0.354	0.367
	S12	49.707	139.049	91.422	153.961	1213.972	1060.572	1012.6345	0.127	0.145	0.152
8	S10	28.250	8.386	30.766	16.861	1777.55	1552.05	1450.575	0.017	0.020	0.021
	S11	167.478	249.146	242.222	299.389	1925.49	1679.49	1568.79	0.155	0.178	0.191
	S4	230.977	343.398	333.996	412.691	1228.3	1108.92	1055.199	0.336	0.372	0.391
	S12	72.934	206.045	134.747	227.925	1517.465	1325.715	1239.4275	0.150	0.172	0.184
7	S10	45.235	29.590	54.112	43.161	2133.06	1862.46	1715.885	0.025	0.029	0.032
	S11	206.525	344.512	309.878	406.469	2310.588	2015.388	1855.488	0.176	0.202	0.219
	S4	275.219	431.625	404.707	514.191	1473.96	1330.704	1253.107	0.349	0.386	0.410
	S12	101.468	291.009	188.771	321.449	1820.958	1590.858	1466.2205	0.177	0.202	0.219
6	S10	73.792	78.111	97.225	100.248	2488.57	2172.87	2003.745	0.040	0.046	0.050
	S11	245.703	463.968	384.893	537.678	2695.686	2351.286	2166.786	0.199	0.229	0.248
	S4	305.257	523.909	462.430	615.486	1719.62	1552.488	1462.953	0.358	0.396	0.421
	S12	123.983	381.172	238.334	418.367	2124.451	1856.001	1712.1885	0.197	0.225	0.244
5	S10	104.481	132.943	144.363	164.287	2844.08	2483.28	2314.155	0.058	0.066	0.071
	S11	282.902	586.364	458.811	671.235	3080.784	2687.184	2502.684	0.218	0.250	0.268
	S4	323.017	616.662	508.015	713.567	1965.28	1774.272	1684.737	0.363	0.402	0.424
	S12	147.556	473.813	289.699	518.080	2427.944	2121.144	1977.3315	0.213	0.244	0.262
4	S10	131.248	191.708	188.760	231.082	3199.59	2793.69	2647.115	0.072	0.083	0.087
	S11	316.647	701.817	527.192	796.811	3465.882	3023.082	2863.182	0.230	0.264	0.278
	S4	333.069	703.624	544.156	803.545	2210.94	1996.056	1918.459	0.363	0.403	0.419
	S12	176.131	568.412	346.654	621.251	2731.437	2386.287	2261.6495	0.227	0.260	0.275
3	S10	155.270	245.936	229.051	292.517	3555.1	3104.1	3002.625	0.082	0.094	0.097
	S11	345.481	808.463	588.020	912.107	3850.98	3358.98	3248.28	0.237	0.272	0.281
	S4	335.918	779.517	569.773	880.293	2456.6	2217.84	2164.119	0.358	0.397	0.407
	S12	201.519	653.645	397.612	714.100	3034.93	2651.43	2565.1425	0.235	0.269	0.278
2	S10	174.366	295.093	262.894	347.402	3910.61	3414.51	3358.135	0.089	0.102	0.103
	S11	367.186	896.813	636.230	1006.969	4236.078	3694.878	3633.378	0.238	0.273	0.277
	S4	334.744	841.384	587.159	941.807	2702.26	2439.624	2409.779	0.349	0.386	0.391
	S12	223.512	727.002	441.612	794.055	3338.423	2916.573	2868.6355	0.238	0.272	0.277
1	S10	184.796	329.468	283.637	384.907	4266.12	3724.92	3713.645	0.090	0.103	0.104
	S11	379.296	955.207	665.858	1068.995	4621.176	4030.776	4018.476	0.231	0.265	0.266
	S4	327.267	883.393	592.284	981.573	2947.92	2661.408	2655.439	0.333	0.369	0.370
	S12	238.423	774.705	470.834	846.232	3641.916	3181.716	3172.1285	0.232	0.266	0.267

Model 3

Çizelge B.89: 6 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	3.903	2.032	4.513	3.203	355.51	332.96	287.86	0.013	0.014	0.016
	S3	7.943	5.939	9.725	8.322	263.11	250.51	225.31	0.037	0.039	0.043
	S11	0.486	3.674	1.588	3.820	385.098	360.498	311.298	0.010	0.011	0.012
	S4	2.257	3.679	3.361	4.356	245.66	233.722	209.846	0.018	0.019	0.021
	S12	2.197	1.729	2.715	2.388	303.493	284.318	245.968	0.009	0.010	0.011
5	S10	9.645	2.152	10.290	5.045	711.02	665.92	598.27	0.014	0.015	0.017
	S3	15.539	13.796	19.678	18.458	526.22	501.02	463.22	0.037	0.039	0.042
	S11	1.045	10.139	4.087	10.453	770.196	720.996	647.196	0.014	0.014	0.016
	S4	4.537	10.341	7.639	11.702	491.32	467.444	431.63	0.024	0.025	0.027
	S12	5.643	6.419	7.569	8.112	606.986	568.636	511.111	0.013	0.014	0.016
4	S10	15.399	2.443	16.132	7.063	1066.53	998.88	931.23	0.015	0.016	0.017
	S3	23.052	21.577	29.525	28.493	789.33	751.53	713.73	0.037	0.039	0.041
	S11	1.497	16.670	6.498	17.119	1155.294	1081.494	1007.694	0.015	0.016	0.017
	S4	6.991	17.034	12.101	19.132	736.98	701.166	665.352	0.026	0.027	0.029
	S12	9.034	11.220	12.400	13.930	910.479	852.954	795.429	0.015	0.016	0.018
3	S10	20.469	1.117	20.804	7.258	1422.04	1331.84	1286.74	0.015	0.016	0.016
	S3	29.844	29.081	38.568	38.034	1052.44	1002.04	976.84	0.037	0.038	0.039
	S11	1.899	24.448	9.233	25.018	1540.392	1441.992	1392.792	0.016	0.017	0.018
	S4	9.585	23.979	16.779	26.855	982.64	934.888	911.012	0.027	0.029	0.029
	S12	12.519	17.212	17.683	20.968	1213.972	1137.272	1098.922	0.017	0.018	0.019
2	S10	24.484	1.455	24.920	8.800	1777.55	1664.8	1642.25	0.014	0.015	0.015
	S3	35.273	35.710	45.986	46.292	1315.55	1252.55	1239.95	0.035	0.037	0.037
	S11	2.193	32.529	11.952	33.186	1925.49	1802.49	1777.89	0.017	0.018	0.019
	S4	12.125	30.629	21.314	34.267	1228.3	1168.61	1156.672	0.028	0.029	0.030
	S12	15.760	23.610	22.843	28.338	1517.465	1421.59	1402.415	0.019	0.020	0.020
1	S10	27.082	4.574	28.454	12.698	2133.06	1997.76	1997.76	0.013	0.014	0.014
	S3	38.587	40.748	50.811	52.324	1578.66	1503.06	1503.06	0.033	0.035	0.035
	S11	2.330	39.224	14.097	39.923	2310.588	2162.988	2162.988	0.017	0.018	0.018
	S4	13.551	35.797	24.290	39.862	1473.96	1402.332	1402.332	0.027	0.028	0.028
	S12	18.244	29.173	26.996	34.646	1820.958	1705.908	1705.908	0.019	0.020	0.020

Çizelge B.90: 9 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	5.467	2.496	6.216	4.136	355.51	310.41	254.035	0.017	0.020	0.024
	S3	11.760	7.825	14.107	11.353	263.11	237.91	206.41	0.054	0.059	0.068
	S11	1.094	4.020	2.300	4.348	385.098	335.898	274.398	0.011	0.013	0.016
	S4	2.676	4.648	4.070	5.450	245.66	221.784	191.939	0.022	0.025	0.028
	S12	3.037	1.583	3.512	2.494	303.493	265.143	217.2055	0.012	0.013	0.016
8	S10	13.601	2.489	14.348	6.569	711.02	620.82	519.345	0.020	0.023	0.028
	S3	23.770	18.749	29.395	25.880	526.22	475.82	419.12	0.056	0.062	0.070
	S11	2.452	11.374	5.864	12.110	770.196	671.796	561.096	0.016	0.018	0.022
	S4	5.535	12.890	9.402	14.551	491.32	443.568	389.847	0.030	0.033	0.037
	S12	8.068	6.621	10.054	9.041	606.986	530.286	443.9985	0.017	0.019	0.023
7	S10	21.986	2.847	22.840	9.442	1066.53	931.23	987.605	0.021	0.025	0.023
	S3	36.042	29.740	44.964	40.552	789.33	713.73	745.23	0.057	0.063	0.060
	S11	3.657	18.892	9.325	19.990	1155.294	1007.694	1069.194	0.017	0.020	0.019
	S4	8.760	21.210	15.123	23.838	736.98	665.352	695.197	0.032	0.036	0.034
	S12	13.140	11.809	16.682	15.750	910.479	795.429	843.3665	0.018	0.021	0.020
6	S10	29.661	1.142	30.003	10.040	1422.04	1241.64	1275.465	0.021	0.024	0.024
	S3	48.056	40.993	60.354	55.410	1052.44	951.64	970.54	0.057	0.063	0.062
	S11	4.811	28.524	13.368	29.967	1540.392	1343.592	1380.492	0.019	0.022	0.022
	S4	12.575	30.293	21.663	34.065	982.64	887.136	905.043	0.035	0.038	0.038
	S12	18.738	18.869	24.399	24.491	1213.972	1060.572	1089.3345	0.020	0.023	0.022
5	S10	36.624	2.136	37.265	13.123	1777.55	1552.05	1585.875	0.021	0.024	0.023
	S3	59.491	52.239	75.163	70.087	1315.55	1189.55	1208.45	0.057	0.063	0.062
	S11	5.811	39.710	17.724	41.453	1925.49	1679.49	1716.39	0.022	0.025	0.024
	S4	17.065	39.951	29.050	45.071	1228.3	1108.92	1126.827	0.037	0.041	0.040
	S12	24.642	27.231	32.811	34.624	1517.465	1325.715	1354.4775	0.023	0.026	0.026
4	S10	42.894	6.591	44.871	19.459	2133.06	1862.46	1918.835	0.021	0.024	0.023
	S3	70.162	63.118	89.097	84.167	1578.66	1427.46	1458.96	0.056	0.062	0.061
	S11	6.616	51.565	22.085	53.549	2310.588	2015.388	2076.888	0.023	0.027	0.026
	S4	20.295	49.397	35.114	55.485	1473.96	1330.704	1360.549	0.038	0.042	0.041
	S12	30.643	37.039	41.755	46.232	1820.958	1590.858	1638.7955	0.025	0.029	0.028
3	S10	46.977	11.790	50.514	25.883	2488.57	2172.87	2274.345	0.020	0.023	0.022
	S3	78.671	73.679	100.775	97.280	1841.77	1665.37	1722.07	0.055	0.061	0.059
	S11	7.250	63.919	26.425	66.094	2695.686	2351.286	2461.986	0.025	0.028	0.027
	S4	23.620	58.419	41.145	65.505	1719.62	1552.488	1606.209	0.038	0.042	0.041
	S12	35.114	46.712	49.127	57.246	2124.451	1856.001	1942.2885	0.027	0.031	0.029
2	S10	49.831	16.668	54.831	31.617	2844.08	2483.28	2629.855	0.019	0.022	0.021
	S3	84.613	82.815	109.457	108.199	2104.88	1903.28	1985.18	0.052	0.058	0.055
	S11	7.647	74.482	29.991	76.776	3080.784	2687.184	2847.084	0.025	0.029	0.027
	S4	26.957	66.301	46.848	74.388	1965.28	1774.272	1851.869	0.038	0.042	0.040
	S12	38.543	55.051	55.058	66.614	2427.944	2121.144	2245.7815	0.027	0.031	0.030
1	S10	51.686	21.459	58.124	36.965	3199.59	2793.69	2985.365	0.018	0.021	0.019
	S3	87.755	89.171	114.506	115.498	2367.99	2141.19	2248.29	0.049	0.054	0.051
	S11	7.846	81.862	32.405	84.215	3465.882	3023.082	3232.182	0.024	0.028	0.026
	S4	29.123	72.008	50.725	80.744	2210.94	1996.056	2097.529	0.037	0.040	0.038
	S12	41.651	61.762	60.180	74.257	2731.437	2386.287	2549.2745	0.027	0.031	0.029

Çizelge B.91: 12 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	7.417	3.529	8.476	5.754	355.51	310.41	310.41	0.024	0.027	0.027
	S3	16.449	11.724	19.966	16.659	263.11	237.91	237.91	0.076	0.084	0.084
	S11	1.941	5.008	3.444	5.590	385.098	335.898	335.898	0.015	0.017	0.017
	S4	2.810	7.187	4.965	8.029	245.66	221.784	221.784	0.033	0.036	0.036
	S12	3.884	1.612	4.367	2.777	303.493	265.143	265.143	0.014	0.016	0.016
11	S10	18.598	3.280	19.582	8.859	711.02	620.82	620.82	0.028	0.032	0.032
	S3	33.533	28.450	42.068	38.510	526.22	475.82	475.82	0.080	0.088	0.088
	S11	4.390	14.790	8.827	16.107	770.196	671.796	671.796	0.021	0.024	0.024
	S4	5.976	19.683	11.881	21.476	491.32	443.568	443.568	0.044	0.048	0.048
	S12	10.745	8.157	13.192	11.380	606.986	530.286	530.286	0.022	0.025	0.025
10	S10	30.260	3.634	31.350	12.712	1066.53	931.23	931.23	0.029	0.034	0.034
	S3	51.185	45.352	64.790	60.707	789.33	713.73	713.73	0.082	0.091	0.091
	S11	6.619	24.823	14.066	26.809	1155.294	1007.694	1007.694	0.023	0.027	0.027
	S4	9.708	32.289	19.394	35.201	736.98	665.352	665.352	0.048	0.053	0.053
	S12	17.725	14.913	22.199	20.230	910.479	795.429	795.429	0.024	0.028	0.028
9	S10	40.930	0.912	41.203	13.191	1422.04	1241.64	1185.265	0.029	0.033	0.035
	S3	68.827	62.956	87.713	83.604	1052.44	951.64	920.14	0.083	0.092	0.095
	S11	8.796	38.131	20.235	40.769	1540.392	1343.592	1282.092	0.026	0.030	0.032
	S4	14.470	46.198	28.329	50.539	982.64	887.136	857.291	0.051	0.057	0.059
	S12	25.639	24.528	32.998	32.220	1213.972	1060.572	1012.6345	0.027	0.031	0.033
8	S10	50.804	4.155	52.050	19.396	1777.55	1552.05	1450.575	0.029	0.034	0.036
	S3	86.310	81.138	110.651	107.031	1315.55	1189.55	1132.85	0.084	0.093	0.098
	S11	10.768	54.113	27.002	57.343	1925.49	1679.49	1568.79	0.030	0.034	0.037
	S4	20.572	61.302	38.963	67.474	1228.3	1108.92	1055.199	0.055	0.061	0.064
	S12	34.292	36.298	45.181	46.585	1517.465	1325.715	1239.4275	0.031	0.035	0.038
7	S10	60.063	11.426	63.491	29.445	2133.06	1862.46	1715.885	0.030	0.034	0.037
	S3	103.796	99.782	133.730	130.921	1578.66	1427.46	1345.56	0.085	0.094	0.099
	S11	12.495	72.060	34.113	75.809	2310.588	2015.388	1855.488	0.033	0.038	0.041
	S4	24.882	76.759	47.910	84.224	1473.96	1330.704	1253.107	0.057	0.063	0.067
	S12	43.810	51.158	59.157	64.301	1820.958	1590.858	1466.2205	0.035	0.040	0.044
6	S10	66.041	20.217	72.106	40.029	2488.57	2172.87	2003.745	0.029	0.033	0.036
	S3	119.208	119.715	155.122	155.477	1841.77	1665.37	1570.87	0.084	0.093	0.099
	S11	14.022	92.574	41.794	96.781	2695.686	2351.286	2166.786	0.036	0.041	0.045
	S4	30.259	92.822	58.105	101.900	1719.62	1552.488	1462.953	0.059	0.066	0.070
	S12	51.107	66.780	71.141	82.112	2124.451	1856.001	1712.1885	0.039	0.044	0.048
5	S10	70.971	29.919	79.947	51.210	2844.08	2483.28	2314.155	0.028	0.032	0.035
	S3	132.522	139.667	174.422	179.423	2104.88	1903.28	1808.78	0.085	0.094	0.099
	S11	15.273	112.656	49.070	117.238	3080.784	2687.184	2502.684	0.038	0.044	0.047
	S4	36.394	108.946	69.078	119.865	1965.28	1774.272	1684.737	0.061	0.068	0.071
	S12	58.241	82.796	83.080	100.268	2427.944	2121.144	1977.3315	0.041	0.047	0.051
4	S10	75.984	40.197	88.043	62.992	3199.59	2793.69	2647.115	0.028	0.032	0.033
	S3	143.865	158.427	191.393	201.586	2367.99	2141.19	2059.29	0.085	0.094	0.098
	S11	16.261	131.041	55.573	135.919	3465.882	3023.082	2863.182	0.039	0.045	0.047
	S4	42.427	124.123	79.664	136.851	2210.94	1996.056	1918.459	0.062	0.069	0.071
	S12	66.335	99.205	96.097	119.106	2731.437	2386.287	2261.6495	0.044	0.050	0.053
3	S10	80.163	49.734	95.083	73.783	3555.1	3104.1	3002.625	0.027	0.031	0.032
	S3	152.792	175.185	205.347	221.022	2631.1	2379.1	2322.4	0.084	0.093	0.095
	S11	16.977	147.818	61.323	152.911	3850.98	3358.98	3248.28	0.040	0.046	0.047
	S4	48.317	137.514	89.571	152.009	2456.6	2217.84	2164.119	0.062	0.069	0.070
	S12	73.349	114.192	107.607	136.197	3034.93	2651.43	2565.1425	0.045	0.051	0.053
2	S10	83.302	58.493	100.850	83.484	3910.61	3414.51	3358.135	0.026	0.030	0.030
	S3	159.129	188.666	215.729	236.404	2894.21	2617.01	2585.51	0.082	0.090	0.091
	S11	17.427	161.801	65.967	167.029	4236.078	3694.878	3633.378	0.039	0.045	0.046

1	S4	53.255	148.606	97.837	164.583	2702.26	2439.624	2409.779	0.061	0.067	0.068
	S12	79.346	127.313	117.540	151.117	3338.423	2916.573	2868.6355	0.045	0.052	0.053
	S10	85.180	65.181	104.734	90.735	4266.12	3724.92	3713.645	0.025	0.028	0.028
	S3	161.939	197.622	221.226	246.204	3157.32	2854.92	2848.62	0.078	0.086	0.086
	S11	17.616	170.959	68.904	176.244	4621.176	4030.776	4018.476	0.038	0.044	0.044
	S4	57.280	156.267	104.160	173.451	2947.92	2661.408	2655.439	0.059	0.065	0.065
	S12	83.523	135.874	124.285	160.930	3641.916	3181.716	3172.1285	0.044	0.051	0.051

Çizelge B.92: 6 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	3.903	2.032	4.513	3.203	355.51	332.96	287.86	0.013	0.014	0.016
	S3	7.943	5.939	9.725	8.322	263.11	250.51	225.31	0.037	0.039	0.043
	S11	0.486	3.674	1.588	3.820	385.098	360.498	311.298	0.010	0.011	0.012
	S4	2.257	3.679	3.361	4.356	245.66	233.722	209.846	0.018	0.019	0.021
	S12	2.197	1.729	2.715	2.388	303.493	284.318	245.968	0.009	0.010	0.011
5	S10	9.645	2.152	10.290	5.045	711.02	665.92	598.27	0.014	0.015	0.017
	S3	15.539	13.796	19.678	18.458	526.22	501.02	463.22	0.037	0.039	0.042
	S11	1.045	10.139	4.087	10.453	770.196	720.996	647.196	0.014	0.014	0.016
	S4	4.537	10.341	7.639	11.702	491.32	467.444	431.63	0.024	0.025	0.027
	S12	5.643	6.419	7.569	8.112	606.986	568.636	511.111	0.013	0.014	0.016
4	S10	15.399	2.443	16.132	7.063	1066.53	998.88	931.23	0.015	0.016	0.017
	S3	23.052	21.577	29.525	28.493	789.33	751.53	713.73	0.037	0.039	0.041
	S11	1.497	16.670	6.498	17.119	1155.294	1081.494	1007.694	0.015	0.016	0.017
	S4	6.991	17.034	12.101	19.132	736.98	701.166	665.352	0.026	0.027	0.029
	S12	9.034	11.220	12.400	13.930	910.479	852.954	795.429	0.015	0.016	0.018
3	S10	20.469	1.117	20.804	7.258	1422.04	1331.84	1286.74	0.015	0.016	0.016
	S3	29.844	29.081	38.568	38.034	1052.44	1002.04	976.84	0.037	0.038	0.039
	S11	1.899	24.448	9.233	25.018	1540.392	1441.992	1392.792	0.016	0.017	0.018
	S4	9.585	23.979	16.779	26.855	982.64	934.888	911.012	0.027	0.029	0.029
	S12	12.519	17.212	17.683	20.968	1213.972	1137.272	1098.922	0.017	0.018	0.019
2	S10	24.484	1.455	24.920	8.800	1777.55	1664.8	1642.25	0.014	0.015	0.015
	S3	35.273	35.710	45.986	46.292	1315.55	1252.55	1239.95	0.035	0.037	0.037
	S11	2.193	32.529	11.952	33.186	1925.49	1802.49	1777.89	0.017	0.018	0.019
	S4	12.125	30.629	21.314	34.267	1228.3	1168.61	1156.672	0.028	0.029	0.030
	S12	15.760	23.610	22.843	28.338	1517.465	1421.59	1402.415	0.019	0.020	0.020
1	S10	27.082	4.574	28.454	12.698	2133.06	1997.76	1997.76	0.013	0.014	0.014
	S3	38.587	40.748	50.811	52.324	1578.66	1503.06	1503.06	0.033	0.035	0.035
	S11	2.330	39.224	14.097	39.923	2310.588	2162.988	2162.988	0.017	0.018	0.018
	S4	13.551	35.797	24.290	39.862	1473.96	1402.332	1402.332	0.027	0.028	0.028
	S12	18.244	29.173	26.996	34.646	1820.958	1705.908	1705.908	0.019	0.020	0.020

Çizelge B.93: 9 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	5.467	2.496	6.216	4.136	355.51	310.41	254.035	0.017	0.020	0.024
	S3	11.760	7.825	14.107	11.353	263.11	237.91	206.41	0.054	0.059	0.068
	S11	1.094	4.020	2.300	4.348	385.098	335.898	274.398	0.011	0.013	0.016
	S4	2.676	4.648	4.070	5.450	245.66	221.784	191.939	0.022	0.025	0.028
	S12	3.037	1.583	3.512	2.494	303.493	265.143	217.2055	0.012	0.013	0.016
8	S10	13.601	2.489	14.348	6.569	711.02	620.82	519.345	0.020	0.023	0.028
	S3	23.770	18.749	29.395	25.880	526.22	475.82	419.12	0.056	0.062	0.070
	S11	2.452	11.374	5.864	12.110	770.196	671.796	561.096	0.016	0.018	0.022
	S4	5.535	12.890	9.402	14.551	491.32	443.568	389.847	0.030	0.033	0.037
	S12	8.068	6.621	10.054	9.041	606.986	530.286	443.9985	0.017	0.019	0.023
7	S10	21.986	2.847	22.840	9.442	1066.53	931.23	987.605	0.021	0.025	0.023
	S3	36.042	29.740	44.964	40.552	789.33	713.73	745.23	0.057	0.063	0.060
	S11	3.657	18.892	9.325	19.990	1155.294	1007.694	1069.194	0.017	0.020	0.019
	S4	8.760	21.210	15.123	23.838	736.98	665.352	695.197	0.032	0.036	0.034
	S12	13.140	11.809	16.682	15.750	910.479	795.429	843.3665	0.018	0.021	0.020
6	S10	29.661	1.142	30.003	10.040	1422.04	1241.64	1275.465	0.021	0.024	0.024
	S3	48.056	40.993	60.354	55.410	1052.44	951.64	970.54	0.057	0.063	0.062
	S11	4.811	28.524	13.368	29.967	1540.392	1343.592	1380.492	0.019	0.022	0.022
	S4	12.575	30.293	21.663	34.065	982.64	887.136	905.043	0.035	0.038	0.038
	S12	18.738	18.869	24.399	24.491	1213.972	1060.572	1089.3345	0.020	0.023	0.022
5	S10	36.624	2.136	37.265	13.123	1777.55	1552.05	1585.875	0.021	0.024	0.023
	S3	59.491	52.239	75.163	70.087	1315.55	1189.55	1208.45	0.057	0.063	0.062
	S11	5.811	39.710	17.724	41.453	1925.49	1679.49	1716.39	0.022	0.025	0.024
	S4	17.065	39.951	29.050	45.071	1228.3	1108.92	1126.827	0.037	0.041	0.040
	S12	24.642	27.231	32.811	34.624	1517.465	1325.715	1354.4775	0.023	0.026	0.026
4	S10	42.894	6.591	44.871	19.459	2133.06	1862.46	1918.835	0.021	0.024	0.023
	S3	70.162	63.118	89.097	84.167	1578.66	1427.46	1458.96	0.056	0.062	0.061
	S11	6.616	51.565	22.085	53.549	2310.588	2015.388	2076.888	0.023	0.027	0.026
	S4	20.295	49.397	35.114	55.485	1473.96	1330.704	1360.549	0.038	0.042	0.041
	S12	30.643	37.039	41.755	46.232	1820.958	1590.858	1638.7955	0.025	0.029	0.028
3	S10	46.977	11.790	50.514	25.883	2488.57	2172.87	2274.345	0.020	0.023	0.022
	S3	78.671	73.679	100.775	97.280	1841.77	1665.37	1722.07	0.055	0.061	0.059
	S11	7.250	63.919	26.425	66.094	2695.686	2351.286	2461.986	0.025	0.028	0.027
	S4	23.620	58.419	41.145	65.505	1719.62	1552.488	1606.209	0.038	0.042	0.041
	S12	35.114	46.712	49.127	57.246	2124.451	1856.001	1942.2885	0.027	0.031	0.029
2	S10	49.831	16.668	54.831	31.617	2844.08	2483.28	2629.855	0.019	0.022	0.021
	S3	84.613	82.815	109.457	108.199	2104.88	1903.28	1985.18	0.052	0.058	0.055
	S11	7.647	74.482	29.991	76.776	3080.784	2687.184	2847.084	0.025	0.029	0.027
	S4	26.957	66.301	46.848	74.388	1965.28	1774.272	1851.869	0.038	0.042	0.040
	S12	38.543	55.051	55.058	66.614	2427.944	2121.144	2245.7815	0.027	0.031	0.030
1	S10	51.686	21.459	58.124	36.965	3199.59	2793.69	2985.365	0.018	0.021	0.019
	S3	87.755	89.171	114.506	115.498	2367.99	2141.19	2248.29	0.049	0.054	0.051
	S11	7.846	81.862	32.405	84.215	3465.882	3023.082	3232.182	0.024	0.028	0.026
	S4	29.123	72.008	50.725	80.744	2210.94	1996.056	2097.529	0.037	0.040	0.038
	S12	41.651	61.762	60.180	74.257	2731.437	2386.287	2549.2745	0.027	0.031	0.029

Çizelge B.94: 12 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	8.344	3.970	9.535	6.473	355.51	310.41	310.41	0.027	0.031	0.031
	S3	18.505	13.190	22.462	18.741	263.11	237.91	237.91	0.085	0.094	0.094
	S11	2.184	5.634	3.874	6.289	385.098	335.898	335.898	0.016	0.019	0.019
	S4	3.161	8.085	5.586	9.033	245.66	221.784	221.784	0.037	0.041	0.041
	S12	4.369	1.813	4.913	3.124	303.493	265.143	265.143	0.016	0.019	0.019
11	S10	20.923	3.690	22.030	9.966	711.02	620.82	620.82	0.031	0.035	0.035
	S3	37.725	32.006	47.327	43.324	526.22	475.82	475.82	0.090	0.099	0.099
	S11	4.938	16.639	9.930	18.120	770.196	671.796	671.796	0.024	0.027	0.027
	S4	6.723	22.143	13.366	24.160	491.32	443.568	443.568	0.049	0.054	0.054
	S12	12.088	9.177	14.841	12.803	606.986	530.286	530.286	0.024	0.028	0.028
10	S10	34.042	4.088	35.269	14.301	1066.53	931.23	931.23	0.033	0.038	0.038
	S3	57.583	51.021	72.889	68.295	789.33	713.73	713.73	0.092	0.102	0.102
	S11	7.447	27.926	15.825	30.160	1155.294	1007.694	1007.694	0.026	0.030	0.030
	S4	10.921	36.325	21.819	39.601	736.98	665.352	665.352	0.054	0.060	0.060
	S12	19.941	16.777	24.974	22.759	910.479	795.429	795.429	0.027	0.031	0.031
9	S10	46.046	1.026	46.354	14.839	1422.04	1241.64	1185.265	0.033	0.037	0.039
	S3	77.430	70.825	98.677	94.054	1052.44	951.64	920.14	0.094	0.104	0.107
	S11	9.895	42.897	22.764	45.866	1540.392	1343.592	1282.092	0.030	0.034	0.036
	S4	16.278	51.973	31.870	56.856	982.64	887.136	857.291	0.058	0.064	0.066
	S12	28.844	27.594	37.122	36.247	1213.972	1060.572	1012.6345	0.031	0.035	0.037
8	S10	57.154	4.674	58.556	21.820	1777.55	1552.05	1450.575	0.033	0.038	0.040
	S3	97.098	91.280	124.482	120.409	1315.55	1189.55	1132.85	0.095	0.105	0.110
	S11	12.114	60.877	30.377	64.511	1925.49	1679.49	1568.79	0.034	0.038	0.041
	S4	23.144	68.965	43.833	75.908	1228.3	1108.92	1055.199	0.062	0.068	0.072
	S12	38.578	40.835	50.828	52.408	1517.465	1325.715	1239.4275	0.035	0.040	0.042
7	S10	67.571	12.854	71.427	33.126	2133.06	1862.46	1715.885	0.033	0.038	0.042
	S3	116.770	112.255	150.447	147.286	1578.66	1427.46	1345.56	0.095	0.105	0.112
	S11	14.057	81.068	38.377	85.285	2310.588	2015.388	1855.488	0.037	0.042	0.046
	S4	27.993	86.354	53.899	94.752	1473.96	1330.704	1253.107	0.064	0.071	0.076
	S12	49.286	57.552	66.552	72.338	1820.958	1590.858	1466.2205	0.040	0.045	0.049
6	S10	74.296	22.744	81.119	45.033	2488.57	2172.87	2003.745	0.033	0.037	0.040
	S3	134.108	134.679	174.512	174.912	1841.77	1665.37	1570.87	0.095	0.105	0.111
	S11	15.775	104.146	47.019	108.879	2695.686	2351.286	2166.786	0.040	0.046	0.050
	S4	34.041	104.425	65.369	114.637	1719.62	1552.488	1462.953	0.067	0.074	0.078
	S12	57.495	75.127	80.033	92.376	2124.451	1856.001	1712.1885	0.043	0.050	0.054
5	S10	79.843	33.658	89.940	57.611	2844.08	2483.28	2314.155	0.032	0.036	0.039
	S3	149.087	157.125	196.225	201.851	2104.88	1903.28	1808.78	0.096	0.106	0.112
	S11	17.182	126.739	55.204	131.893	3080.784	2687.184	2502.684	0.043	0.049	0.053
	S4	40.944	122.565	77.713	134.848	1965.28	1774.272	1684.737	0.069	0.076	0.080
	S12	65.522	93.145	93.465	112.802	2427.944	2121.144	1977.3315	0.046	0.053	0.057
4	S10	85.482	45.221	99.049	70.866	3199.59	2793.69	2647.115	0.031	0.035	0.037
	S3	161.848	178.231	215.317	226.785	2367.99	2141.19	2059.29	0.096	0.106	0.110
	S11	18.293	147.422	62.520	152.909	3465.882	3023.082	2863.182	0.044	0.051	0.053
	S4	47.730	139.638	89.622	153.957	2210.94	1996.056	1918.459	0.070	0.077	0.080
	S12	74.627	111.606	108.109	133.994	2731.437	2386.287	2261.6495	0.049	0.056	0.059
3	S10	90.184	55.951	106.969	83.006	3555.1	3104.1	3002.625	0.030	0.034	0.036
	S3	171.891	197.083	231.016	248.650	2631.1	2379.1	2322.4	0.095	0.105	0.107
	S11	19.099	166.295	68.988	172.025	3850.98	3358.98	3248.28	0.045	0.051	0.053
	S4	54.357	154.703	100.767	171.010	2456.6	2217.84	2164.119	0.070	0.077	0.079
	S12	82.518	128.466	121.058	153.221	3034.93	2651.43	2565.1425	0.050	0.058	0.060
2	S10	93.714	65.805	113.456	93.919	3910.61	3414.51	3358.135	0.029	0.033	0.034
	S3	179.021	212.249	242.695	265.955	2894.21	2617.01	2585.51	0.092	0.102	0.103
	S11	19.605	182.027	74.213	187.908	4236.078	3694.878	3633.378	0.044	0.051	0.052

1	S4	59.912	167.182	110.066	185.156	2702.26	2439.624	2409.779	0.069	0.076	0.077
	S12	89.264	143.227	132.232	170.006	3338.423	2916.573	2868.6355	0.051	0.058	0.059
	S10	95.827	73.329	117.826	102.077	4266.12	3724.92	3713.645	0.028	0.032	0.032
	S3	182.182	222.325	248.879	276.980	3157.32	2854.92	2848.62	0.088	0.097	0.097
	S11	19.818	192.329	77.516	198.274	4621.176	4030.776	4018.476	0.043	0.049	0.049
	S4	64.440	175.800	117.180	195.132	2947.92	2661.408	2655.439	0.066	0.073	0.073
	S12	93.964	152.858	139.821	181.047	3641.916	3181.716	3172.1285	0.050	0.057	0.057

Çizelge B.95: 6 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	7.319	3.810	8.462	6.006	355.51	332.96	287.86	0.024	0.025	0.029
	S3	14.894	11.135	18.234	15.603	263.11	250.51	225.31	0.069	0.073	0.081
	S11	0.911	6.889	2.977	7.162	385.098	360.498	311.298	0.019	0.020	0.023
	S4	4.232	6.898	6.301	8.168	245.66	233.722	209.846	0.033	0.035	0.039
	S12	4.119	3.242	5.091	4.477	303.493	284.318	245.968	0.017	0.018	0.021
5	S10	18.084	4.035	19.294	9.460	711.02	665.92	598.27	0.027	0.029	0.032
	S3	29.135	25.867	36.895	34.608	526.22	501.02	463.22	0.070	0.074	0.080
	S11	1.959	19.011	7.663	19.599	770.196	720.996	647.196	0.025	0.027	0.030
	S4	8.506	19.389	14.323	21.941	491.32	467.444	431.63	0.045	0.047	0.051
	S12	10.581	12.035	14.192	15.210	606.986	568.636	511.111	0.025	0.027	0.030
4	S10	28.873	4.581	30.247	13.243	1066.53	998.88	931.23	0.028	0.030	0.032
	S3	43.223	40.457	55.360	53.424	789.33	751.53	713.73	0.070	0.074	0.078
	S11	2.807	31.257	12.184	32.099	1155.294	1081.494	1007.694	0.028	0.030	0.032
	S4	13.108	31.940	22.689	35.872	736.98	701.166	665.352	0.049	0.051	0.054
	S12	16.939	21.037	23.250	26.119	910.479	852.954	795.429	0.029	0.031	0.033
3	S10	38.380	2.095	39.008	13.608	1422.04	1331.84	1286.74	0.027	0.029	0.030
	S3	55.957	54.527	72.315	71.314	1052.44	1002.04	976.84	0.069	0.072	0.074
	S11	3.561	45.840	17.313	46.908	1540.392	1441.992	1392.792	0.030	0.033	0.034
	S4	17.972	44.961	31.461	50.353	982.64	934.888	911.012	0.051	0.054	0.055
	S12	23.474	32.273	33.156	39.315	1213.972	1137.272	1098.922	0.032	0.035	0.036
2	S10	45.907	2.728	46.725	16.500	1777.55	1664.8	1642.25	0.026	0.028	0.028
	S3	66.137	66.956	86.224	86.797	1315.55	1252.55	1239.95	0.066	0.069	0.070
	S11	4.112	60.991	22.409	62.225	1925.49	1802.49	1777.89	0.032	0.035	0.035
	S4	22.735	57.430	39.964	64.250	1228.3	1168.61	1156.672	0.052	0.055	0.056
	S12	29.549	44.269	42.830	53.134	1517.465	1421.59	1402.415	0.035	0.037	0.038
1	S10	50.779	8.575	53.351	23.809	2133.06	1997.76	1997.76	0.025	0.027	0.027
	S3	72.350	76.403	95.271	98.108	1578.66	1503.06	1503.06	0.062	0.065	0.065
	S11	4.369	73.545	26.433	74.856	2310.588	2162.988	2162.988	0.032	0.035	0.035
	S4	25.407	67.119	45.543	74.741	1473.96	1402.332	1402.332	0.051	0.053	0.053
	S12	34.207	54.699	50.617	64.961	1820.958	1705.908	1705.908	0.036	0.038	0.038

Çizelge B.96: 9 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	10.250	4.681	11.654	7.756	355.51	310.41	254.035	0.033	0.038	0.046
	S3	22.049	14.672	26.451	21.287	263.11	237.91	206.41	0.101	0.111	0.128
	S11	2.051	7.538	4.312	8.153	385.098	335.898	274.398	0.021	0.024	0.030
	S4	5.017	8.714	7.632	10.219	245.66	221.784	191.939	0.042	0.046	0.053
	S12	5.694	2.969	6.584	4.677	303.493	265.143	217.2055	0.022	0.025	0.030
8	S10	25.502	4.667	26.902	12.317	711.02	620.82	519.345	0.038	0.043	0.052
	S3	44.569	35.155	55.115	48.525	526.22	475.82	419.12	0.105	0.116	0.132
	S11	4.597	21.327	10.995	22.706	770.196	671.796	561.096	0.029	0.034	0.040
	S4	10.379	24.169	17.629	27.283	491.32	443.568	389.847	0.056	0.062	0.070
	S12	15.127	12.414	18.851	16.952	606.986	530.286	443.9985	0.031	0.036	0.042
7	S10	41.223	5.337	42.824	17.704	1066.53	931.23	987.605	0.040	0.046	0.043
	S3	67.579	55.762	84.307	76.036	789.33	713.73	745.23	0.107	0.118	0.113
	S11	6.857	35.423	17.484	37.480	1155.294	1007.694	1069.194	0.032	0.037	0.035
	S4	16.424	39.769	28.355	44.696	736.98	665.352	695.197	0.061	0.067	0.064
	S12	24.637	22.141	31.280	29.532	910.479	795.429	843.3665	0.034	0.039	0.037
6	S10	55.614	2.141	56.256	18.825	1422.04	1241.64	1275.465	0.040	0.045	0.044
	S3	90.105	76.862	113.163	103.894	1052.44	951.64	970.54	0.108	0.119	0.117
	S11	9.020	53.483	25.065	56.189	1540.392	1343.592	1380.492	0.036	0.042	0.041
	S4	23.579	56.799	40.618	63.872	982.64	887.136	905.043	0.065	0.072	0.071
	S12	35.134	35.380	45.748	45.920	1213.972	1060.572	1089.3345	0.038	0.043	0.042
5	S10	68.670	4.004	69.872	24.605	1777.55	1552.05	1585.875	0.039	0.045	0.044
	S3	111.546	97.949	140.930	131.412	1315.55	1189.55	1208.45	0.107	0.118	0.117
	S11	10.896	74.456	33.233	77.725	1925.49	1679.49	1716.39	0.040	0.046	0.045
	S4	31.997	74.908	54.469	84.507	1228.3	1108.92	1126.827	0.069	0.076	0.075
	S12	46.204	51.058	61.521	64.919	1517.465	1325.715	1354.4775	0.043	0.049	0.048
4	S10	80.426	12.358	84.133	36.486	2133.06	1862.46	1918.835	0.039	0.045	0.044
	S3	131.554	118.347	167.058	157.813	1578.66	1427.46	1458.96	0.106	0.117	0.115
	S11	12.405	96.683	41.410	100.405	2310.588	2015.388	2076.888	0.043	0.050	0.048
	S4	38.053	92.619	65.839	104.035	1473.96	1330.704	1360.549	0.071	0.078	0.076
	S12	57.456	69.448	78.291	86.685	1820.958	1590.858	1638.7955	0.048	0.054	0.053
3	S10	88.082	22.106	94.713	48.530	2488.57	2172.87	2274.345	0.038	0.044	0.042
	S3	147.509	138.148	188.953	182.401	1841.77	1665.37	1722.07	0.103	0.113	0.110
	S11	13.593	119.848	49.548	123.926	2695.686	2351.286	2461.986	0.046	0.053	0.050
	S4	44.287	109.535	77.147	122.821	1719.62	1552.488	1606.209	0.071	0.079	0.076
	S12	65.838	87.584	92.114	107.336	2124.451	1856.001	1942.2885	0.051	0.058	0.055
2	S10	93.433	31.252	102.809	59.282	2844.08	2483.28	2629.855	0.036	0.041	0.039
	S3	158.649	155.278	205.232	202.873	2104.88	1903.28	1985.18	0.098	0.108	0.103
	S11	14.338	139.653	56.234	143.954	3080.784	2687.184	2847.084	0.047	0.054	0.051
	S4	50.545	124.314	87.839	139.478	1965.28	1774.272	1851.869	0.071	0.079	0.075
	S12	72.268	103.221	103.235	124.901	2427.944	2121.144	2245.7815	0.051	0.059	0.056
1	S10	96.911	40.236	108.982	69.310	3199.59	2793.69	2985.365	0.034	0.039	0.037
	S3	164.541	167.196	214.700	216.558	2367.99	2141.19	2248.29	0.091	0.101	0.096
	S11	14.712	153.490	60.759	157.904	3465.882	3023.082	3232.182	0.046	0.052	0.049
	S4	54.606	135.014	95.110	151.396	2210.94	1996.056	2097.529	0.068	0.076	0.072
	S12	78.097	115.804	112.838	139.233	2731.437	2386.287	2549.2745	0.051	0.058	0.055

Çizelge B.97: 12 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	13.127	6.245	15.000	10.183	355.51	310.41	310.41	0.042	0.048	0.048
	S3	29.112	20.750	35.337	29.483	263.11	237.91	237.91	0.134	0.149	0.149
	S11	3.436	8.863	6.095	9.894	385.098	335.898	335.898	0.026	0.029	0.029
	S4	4.972	12.719	8.788	14.211	245.66	221.784	221.784	0.058	0.064	0.064
	S12	6.874	2.853	7.729	4.915	303.493	265.143	265.143	0.025	0.029	0.029
11	S10	32.916	5.804	34.657	15.679	711.02	620.82	620.82	0.049	0.056	0.056
	S3	59.348	50.352	74.453	68.156	526.22	475.82	475.82	0.141	0.156	0.156
	S11	7.769	26.176	15.621	28.506	770.196	671.796	671.796	0.037	0.042	0.042
	S4	10.577	34.835	21.027	38.008	491.32	443.568	443.568	0.077	0.086	0.086
	S12	19.016	14.436	23.347	20.141	606.986	530.286	530.286	0.038	0.044	0.044
10	S10	53.554	6.432	55.484	22.498	1066.53	931.23	931.23	0.052	0.060	0.060
	S3	90.587	80.265	114.667	107.441	789.33	713.73	713.73	0.145	0.161	0.161
	S11	11.715	43.932	24.895	47.447	1155.294	1007.694	1007.694	0.041	0.047	0.047
	S4	17.181	57.145	34.325	62.300	736.98	665.352	665.352	0.085	0.094	0.094
	S12	31.370	26.393	39.288	35.804	910.479	795.429	795.429	0.043	0.049	0.049
9	S10	72.438	1.613	72.922	23.345	1422.04	1241.64	1185.265	0.051	0.059	0.062
	S3	121.811	111.421	155.237	147.964	1052.44	951.64	920.14	0.148	0.163	0.169
	S11	15.567	67.484	35.812	72.154	1540.392	1343.592	1282.092	0.047	0.054	0.056
	S4	25.609	81.763	50.137	89.445	982.64	887.136	857.291	0.091	0.101	0.104
	S12	45.377	43.411	58.400	57.024	1213.972	1060.572	1012.6345	0.048	0.055	0.058
8	S10	89.914	7.353	92.119	34.327	1777.55	1552.05	1450.575	0.052	0.059	0.064
	S3	152.753	143.600	195.833	189.425	1315.55	1189.55	1132.85	0.149	0.165	0.173
	S11	19.057	95.769	47.788	101.487	1925.49	1679.49	1568.79	0.053	0.060	0.065
	S4	36.409	108.494	68.957	119.417	1228.3	1108.92	1055.199	0.097	0.108	0.113
	S12	60.690	64.240	79.962	82.447	1517.465	1325.715	1239.4275	0.054	0.062	0.067
7	S10	106.300	20.222	112.367	52.112	2133.06	1862.46	1715.885	0.053	0.060	0.065
	S3	183.700	176.596	236.679	231.706	1578.66	1427.46	1345.56	0.150	0.166	0.176
	S11	22.114	127.534	60.374	134.168	2310.588	2015.388	1855.488	0.058	0.067	0.072
	S4	44.037	135.851	84.792	149.062	1473.96	1330.704	1253.107	0.101	0.112	0.119
	S12	77.536	90.540	104.698	113.800	1820.958	1590.858	1466.2205	0.062	0.072	0.078
6	S10	116.881	35.781	127.615	70.845	2488.57	2172.87	2003.745	0.051	0.059	0.064
	S3	210.976	211.874	274.538	275.167	1841.77	1665.37	1570.87	0.149	0.165	0.175
	S11	24.816	163.840	73.968	171.285	2695.686	2351.286	2166.786	0.064	0.073	0.079
	S4	53.553	164.279	102.836	180.345	1719.62	1552.488	1462.953	0.105	0.116	0.123
	S12	90.450	118.188	125.906	145.323	2124.451	1856.001	1712.1885	0.068	0.078	0.085
5	S10	125.607	52.951	141.492	90.633	2844.08	2483.28	2314.155	0.050	0.057	0.061
	S3	234.541	247.185	308.696	317.547	2104.88	1903.28	1808.78	0.151	0.167	0.176
	S11	27.030	199.382	86.845	207.491	3080.784	2687.184	2502.684	0.067	0.077	0.083
	S4	64.412	192.816	122.256	212.139	1965.28	1774.272	1684.737	0.108	0.120	0.126
	S12	103.077	146.534	147.037	177.457	2427.944	2121.144	1977.3315	0.073	0.084	0.090
4	S10	134.479	71.141	155.821	111.485	3199.59	2793.69	2647.115	0.049	0.056	0.059
	S3	254.615	280.388	338.731	356.772	2367.99	2141.19	2059.29	0.151	0.167	0.173
	S11	28.778	231.920	98.354	240.553	3465.882	3023.082	2863.182	0.069	0.080	0.084
	S4	75.088	219.676	140.991	242.202	2210.94	1996.056	1918.459	0.110	0.121	0.126
	S12	117.402	175.576	170.075	210.796	2731.437	2386.287	2261.6495	0.077	0.088	0.093
3	S10	141.875	88.020	168.281	130.583	3555.1	3104.1	3002.625	0.047	0.054	0.056
	S3	270.414	310.046	363.428	391.171	2631.1	2379.1	2322.4	0.149	0.164	0.168
	S11	30.047	261.611	108.530	270.625	3850.98	3358.98	3248.28	0.070	0.081	0.083
	S4	85.512	243.375	158.525	269.029	2456.6	2217.84	2164.119	0.110	0.121	0.124
	S12	129.815	202.100	190.445	241.044	3034.93	2651.43	2565.1425	0.079	0.091	0.094
2	S10	147.429	103.523	178.486	147.751	3910.61	3414.51	3358.135	0.046	0.052	0.053
	S3	281.631	333.905	381.802	418.394	2894.21	2617.01	2585.51	0.145	0.160	0.162
	S11	30.842	286.360	116.750	295.612	4236.078	3694.878	3633.378	0.070	0.080	0.081

1	S4	94.252	263.007	173.154	291.282	2702.26	2439.624	2409.779	0.108	0.119	0.121
	S12	140.428	225.322	208.024	267.450	3338.423	2916.573	2868.6355	0.080	0.092	0.093
	S10	150.753	115.359	185.361	160.585	4266.12	3724.92	3713.645	0.043	0.050	0.050
	S3	286.604	349.756	391.531	435.737	3157.32	2854.92	2848.62	0.138	0.153	0.153
	S11	31.177	302.567	121.947	311.920	4621.176	4030.776	4018.476	0.067	0.077	0.078
	S4	101.376	276.564	184.345	306.977	2947.92	2661.408	2655.439	0.104	0.115	0.116
	S12	147.821	240.472	219.963	284.818	3641.916	3181.716	3172.1285	0.078	0.090	0.090

Çizelge B.98: 6 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	10.149	5.126	11.687	8.171	355.51	332.96	287.86	0.033	0.035	0.041
	S3	20.653	14.980	25.147	21.176	263.11	250.51	225.31	0.096	0.100	0.112
	S11	1.263	9.268	4.043	9.647	385.098	360.498	311.298	0.025	0.027	0.031
	S4	5.868	9.281	8.653	11.041	245.66	233.722	209.846	0.045	0.047	0.053
	S12	5.711	4.361	7.020	6.075	303.493	284.318	245.968	0.023	0.025	0.029
5	S10	25.076	5.428	26.705	12.951	711.02	665.92	598.27	0.038	0.040	0.045
	S3	40.401	34.801	50.841	46.921	526.22	501.02	463.22	0.097	0.101	0.110
	S11	2.717	25.577	10.390	26.392	770.196	720.996	647.196	0.034	0.037	0.041
	S4	11.795	26.085	19.621	29.624	491.32	467.444	431.63	0.060	0.063	0.069
	S12	14.673	16.192	19.530	20.594	606.986	568.636	511.111	0.034	0.036	0.040
4	S10	40.038	6.163	41.886	18.174	1066.53	998.88	931.23	0.039	0.042	0.045
	S3	59.936	54.430	76.264	72.410	789.33	751.53	713.73	0.097	0.101	0.107
	S11	3.893	42.052	16.509	43.220	1155.294	1081.494	1007.694	0.037	0.040	0.043
	S4	18.176	42.971	31.067	48.423	736.98	701.166	665.352	0.066	0.069	0.073
	S12	23.489	28.303	31.980	35.350	910.479	852.954	795.429	0.039	0.041	0.044
3	S10	53.220	2.818	54.065	18.784	1422.04	1331.84	1286.74	0.038	0.041	0.042
	S3	77.594	73.358	99.601	96.637	1052.44	1002.04	976.84	0.095	0.099	0.102
	S11	4.938	61.671	23.439	63.153	1540.392	1441.992	1392.792	0.041	0.044	0.045
	S4	24.922	60.489	43.068	67.966	982.64	934.888	911.012	0.069	0.073	0.075
	S12	32.550	43.419	45.576	53.184	1213.972	1137.272	1098.922	0.044	0.047	0.048
2	S10	63.657	3.670	64.758	22.767	1777.55	1664.8	1642.25	0.036	0.039	0.039
	S3	91.710	90.081	118.735	117.594	1315.55	1252.55	1239.95	0.090	0.095	0.096
	S11	5.702	82.055	30.319	83.766	1925.49	1802.49	1777.89	0.044	0.046	0.047
	S4	31.526	77.265	54.705	86.722	1228.3	1168.61	1156.672	0.071	0.074	0.075
	S12	40.975	59.558	58.842	71.851	1517.465	1421.59	1402.415	0.047	0.051	0.051
1	S10	70.413	11.537	73.874	32.661	2133.06	1997.76	1997.76	0.035	0.037	0.037
	S3	100.326	102.790	131.163	132.888	1578.66	1503.06	1503.06	0.084	0.088	0.088
	S11	6.058	98.946	35.742	100.763	2310.588	2162.988	2162.988	0.044	0.047	0.047
	S4	35.231	90.300	62.321	100.869	1473.96	1402.332	1402.332	0.068	0.072	0.072
	S12	47.434	73.590	69.511	87.820	1820.958	1705.908	1705.908	0.048	0.051	0.051

Çizelge B.99: 9 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	14.214	6.490	16.161	10.754	355.51	310.41	254.035	0.045	0.052	0.064
	S3	30.575	20.346	36.679	29.518	263.11	237.91	206.41	0.139	0.154	0.178
	S11	2.844	10.452	5.980	11.305	385.098	335.898	274.398	0.029	0.034	0.041
	S4	6.957	12.084	10.583	14.171	245.66	221.784	191.939	0.058	0.064	0.074
	S12	7.895	4.117	9.130	6.485	303.493	265.143	217.2055	0.030	0.034	0.042
8	S10	35.363	6.471	37.304	17.080	711.02	620.82	519.345	0.052	0.060	0.072
	S3	61.802	48.748	76.426	67.288	526.22	475.82	419.12	0.145	0.161	0.182
	S11	6.374	29.573	15.246	31.485	770.196	671.796	561.096	0.041	0.047	0.056
	S4	14.392	33.515	24.446	37.832	491.32	443.568	389.847	0.077	0.085	0.097
	S12	20.976	17.214	26.140	23.507	606.986	530.286	443.9985	0.043	0.049	0.059
7	S10	57.163	7.401	59.383	24.550	1066.53	931.23	987.605	0.056	0.064	0.060
	S3	93.709	77.324	116.906	105.436	789.33	713.73	745.23	0.148	0.164	0.157
	S11	9.509	49.120	24.245	51.973	1155.294	1007.694	1069.194	0.045	0.052	0.049
	S4	22.775	55.146	39.319	61.979	736.98	665.352	695.197	0.084	0.093	0.089
	S12	34.164	30.702	43.374	40.951	910.479	795.429	843.3665	0.048	0.055	0.051
6	S10	77.117	2.969	78.008	26.104	1422.04	1241.64	1275.465	0.055	0.063	0.061
	S3	124.945	106.583	156.920	144.066	1052.44	951.64	970.54	0.149	0.165	0.162
	S11	12.507	74.163	34.756	77.915	1540.392	1343.592	1380.492	0.051	0.058	0.056
	S4	32.696	78.761	56.324	88.570	982.64	887.136	905.043	0.090	0.100	0.098
	S12	48.719	49.060	63.436	63.675	1213.972	1060.572	1089.3345	0.052	0.060	0.058
5	S10	95.223	5.553	96.889	34.120	1777.55	1552.05	1585.875	0.055	0.062	0.061
	S3	154.677	135.822	195.424	182.225	1315.55	1189.55	1208.45	0.149	0.164	0.162
	S11	15.109	103.246	46.083	107.779	1925.49	1679.49	1716.39	0.056	0.064	0.063
	S4	44.369	103.873	75.530	117.184	1228.3	1108.92	1126.827	0.095	0.106	0.104
	S12	64.069	70.801	85.309	90.022	1517.465	1325.715	1354.4775	0.059	0.068	0.066
4	S10	111.523	17.136	116.664	50.593	2133.06	1862.46	1918.835	0.055	0.063	0.061
	S3	182.421	164.108	231.653	218.834	1578.66	1427.46	1458.96	0.147	0.162	0.159
	S11	17.202	134.068	57.422	139.228	2310.588	2015.388	2076.888	0.060	0.069	0.067
	S4	52.767	128.432	91.296	144.262	1473.96	1330.704	1360.549	0.098	0.108	0.106
	S12	79.673	96.301	108.563	120.203	1820.958	1590.858	1638.7955	0.066	0.076	0.073
3	S10	122.140	30.653	131.336	67.295	2488.57	2172.87	2274.345	0.053	0.060	0.058
	S3	204.545	191.566	262.015	252.929	1841.77	1665.37	1722.07	0.142	0.157	0.152
	S11	18.850	166.189	68.706	171.844	2695.686	2351.286	2461.986	0.064	0.073	0.070
	S4	61.411	151.889	106.978	170.312	1719.62	1552.488	1606.209	0.099	0.110	0.106
	S12	91.296	121.450	127.731	148.839	2124.451	1856.001	1942.2885	0.070	0.080	0.077
2	S10	129.560	43.336	142.561	82.205	2844.08	2483.28	2629.855	0.050	0.057	0.054
	S3	219.993	215.319	284.589	281.317	2104.88	1903.28	1985.18	0.135	0.150	0.143
	S11	19.882	193.652	77.977	199.616	3080.784	2687.184	2847.084	0.065	0.074	0.070
	S4	70.089	172.382	121.804	193.409	1965.28	1774.272	1851.869	0.098	0.109	0.104
	S12	100.212	143.133	143.152	173.196	2427.944	2121.144	2245.7815	0.071	0.082	0.077
1	S10	134.384	55.795	151.122	96.110	3199.59	2793.69	2985.365	0.047	0.054	0.051
	S3	228.163	231.845	297.717	300.294	2367.99	2141.19	2248.29	0.127	0.140	0.134
	S11	20.400	212.840	84.252	218.960	3465.882	3023.082	3232.182	0.063	0.072	0.068
	S4	75.720	187.220	131.886	209.935	2210.94	1996.056	2097.529	0.095	0.105	0.100
	S12	108.294	160.581	156.468	193.069	2731.437	2386.287	2549.2745	0.071	0.081	0.076

Çizelge B.100: 12 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	18.203	8.660	20.801	14.121	355.51	310.41	310.41	0.059	0.067	0.067
	S3	40.369	28.773	49.000	40.883	263.11	237.91	237.91	0.186	0.206	0.206
	S11	4.764	12.290	8.451	13.719	385.098	335.898	335.898	0.036	0.041	0.041
	S4	6.895	17.637	12.186	19.706	245.66	221.784	221.784	0.080	0.089	0.089
	S12	9.531	3.956	10.718	6.815	303.493	265.143	265.143	0.035	0.040	0.040
11	S10	45.643	8.049	48.058	21.742	711.02	620.82	620.82	0.068	0.077	0.077
	S3	82.295	69.821	103.242	94.510	526.22	475.82	475.82	0.196	0.217	0.217
	S11	10.773	36.297	21.662	39.529	770.196	671.796	671.796	0.051	0.059	0.059
	S4	14.666	48.305	29.157	52.705	491.32	443.568	443.568	0.107	0.119	0.119
	S12	26.369	20.018	32.374	27.929	606.986	530.286	530.286	0.053	0.061	0.061
10	S10	74.262	8.919	76.937	31.197	1066.53	931.23	931.23	0.072	0.083	0.083
	S3	125.615	111.300	159.005	148.985	789.33	713.73	713.73	0.201	0.223	0.223
	S11	16.245	60.920	34.521	65.793	1155.294	1007.694	1007.694	0.057	0.065	0.065
	S4	23.824	79.242	47.597	86.389	736.98	665.352	665.352	0.117	0.130	0.130
	S12	43.500	36.598	54.479	49.648	910.479	795.429	795.429	0.060	0.068	0.068
9	S10	100.448	2.237	101.119	32.372	1422.04	1241.64	1185.265	0.071	0.081	0.085
	S3	168.911	154.503	215.262	205.177	1052.44	951.64	920.14	0.205	0.226	0.234
	S11	21.586	93.578	49.659	100.054	1540.392	1343.592	1282.092	0.065	0.074	0.078
	S4	35.511	113.377	69.524	124.030	982.64	887.136	857.291	0.126	0.140	0.145
	S12	62.923	60.196	80.981	79.073	1213.972	1060.572	1012.6345	0.067	0.076	0.080
8	S10	124.680	10.196	127.739	47.600	1777.55	1552.05	1450.575	0.072	0.082	0.088
	S3	211.817	199.125	271.554	262.670	1315.55	1189.55	1132.85	0.206	0.228	0.240
	S11	26.426	132.800	66.266	140.728	1925.49	1679.49	1568.79	0.073	0.084	0.090
	S4	50.487	150.445	95.621	165.591	1228.3	1108.92	1055.199	0.135	0.149	0.157
	S12	84.157	89.080	110.881	114.327	1517.465	1325.715	1239.4275	0.075	0.086	0.092
7	S10	147.403	28.042	155.816	72.262	2133.06	1862.46	1715.885	0.073	0.084	0.091
	S3	254.731	244.880	328.195	321.299	1578.66	1427.46	1345.56	0.208	0.230	0.244
	S11	30.665	176.847	83.719	186.046	2310.588	2015.388	1855.488	0.081	0.092	0.100
	S4	61.065	188.379	117.579	206.699	1473.96	1330.704	1253.107	0.140	0.155	0.165
	S12	107.517	125.548	145.181	157.803	1820.958	1590.858	1466.2205	0.087	0.099	0.108
6	S10	162.075	49.616	176.959	98.238	2488.57	2172.87	2003.745	0.071	0.081	0.088
	S3	292.554	293.799	380.693	381.565	1841.77	1665.37	1570.87	0.207	0.229	0.243
	S11	34.412	227.192	102.570	237.515	2695.686	2351.286	2166.786	0.088	0.101	0.110
	S4	74.259	227.800	142.599	250.078	1719.62	1552.488	1462.953	0.145	0.161	0.171
	S12	125.424	163.888	174.590	201.515	2124.451	1856.001	1712.1885	0.095	0.109	0.118
5	S10	174.174	73.425	196.202	125.677	2844.08	2483.28	2314.155	0.069	0.079	0.085
	S3	325.230	342.763	428.058	440.332	2104.88	1903.28	1808.78	0.209	0.231	0.243
	S11	37.482	276.476	120.425	287.721	3080.784	2687.184	2502.684	0.093	0.107	0.115
	S4	89.317	267.371	169.529	294.166	1965.28	1774.272	1684.737	0.150	0.166	0.175
	S12	142.933	203.193	203.891	246.073	2427.944	2121.144	1977.3315	0.101	0.116	0.124
4	S10	186.477	98.649	216.072	154.592	3199.59	2793.69	2647.115	0.068	0.077	0.082
	S3	353.066	388.804	469.707	494.724	2367.99	2141.19	2059.29	0.209	0.231	0.240
	S11	39.906	321.596	136.385	333.567	3465.882	3023.082	2863.182	0.096	0.110	0.117
	S4	104.123	304.617	195.508	335.854	2210.94	1996.056	1918.459	0.152	0.168	0.175
	S12	162.797	243.465	235.837	292.304	2731.437	2386.287	2261.6495	0.107	0.122	0.129
3	S10	196.733	122.055	233.349	181.075	3555.1	3104.1	3002.625	0.066	0.075	0.078
	S3	374.975	429.931	503.954	542.423	2631.1	2379.1	2322.4	0.206	0.228	0.234
	S11	41.665	362.767	150.495	375.267	3850.98	3358.98	3248.28	0.097	0.112	0.116
	S4	118.577	337.480	219.821	373.053	2456.6	2217.84	2164.119	0.152	0.168	0.172
	S12	180.010	280.245	264.083	334.248	3034.93	2651.43	2565.1425	0.110	0.126	0.130
2	S10	204.435	143.551	247.500	204.882	3910.61	3414.51	3358.135	0.063	0.072	0.074
	S3	390.528	463.015	529.432	580.173	2894.21	2617.01	2585.51	0.200	0.222	0.224
	S11	42.768	397.086	161.893	409.916	4236.078	3694.878	3633.378	0.097	0.111	0.113

1	S4	130.696	364.703	240.106	403.911	2702.26	2439.624	2409.779	0.149	0.166	0.168
	S12	194.726	312.446	288.460	370.864	3338.423	2916.573	2868.6355	0.111	0.127	0.129
	S10	209.044	159.965	257.034	222.678	4266.12	3724.92	3713.645	0.060	0.069	0.069
	S3	397.424	484.995	542.923	604.223	3157.32	2854.92	2848.62	0.191	0.212	0.212
	S11	43.232	419.560	169.100	432.529	4621.176	4030.776	4018.476	0.094	0.107	0.108
	S4	140.575	383.502	255.625	425.674	2947.92	2661.408	2655.439	0.144	0.160	0.160
	S12	204.979	333.455	305.015	394.948	3641.916	3181.716	3172.1285	0.108	0.124	0.125

Çizelge B.101: 6 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	12.662	6.037	14.473	9.836	355.51	332.96	287.86	0.041	0.043	0.050
	S3	25.768	17.643	31.061	25.373	263.11	250.51	225.31	0.118	0.124	0.138
	S11	1.575	10.915	4.850	11.388	385.098	360.498	311.298	0.030	0.032	0.037
	S4	7.322	10.930	10.601	13.127	245.66	233.722	209.846	0.053	0.056	0.063
	S12	7.126	5.136	8.667	7.274	303.493	284.318	245.968	0.029	0.030	0.035
5	S10	31.287	6.393	33.205	15.779	711.02	665.92	598.27	0.047	0.050	0.056
	S3	50.407	40.986	62.703	56.108	526.22	501.02	463.22	0.119	0.125	0.135
	S11	3.390	30.123	12.427	31.140	770.196	720.996	647.196	0.040	0.043	0.048
	S4	14.717	30.722	23.933	35.137	491.32	467.444	431.63	0.072	0.075	0.081
	S12	18.307	19.070	24.027	24.562	606.986	568.636	511.111	0.040	0.043	0.048
4	S10	49.954	7.258	52.131	22.244	1066.53	998.88	931.23	0.049	0.052	0.056
	S3	74.780	64.104	94.011	86.538	789.33	751.53	713.73	0.119	0.125	0.132
	S11	4.857	49.526	19.715	50.983	1155.294	1081.494	1007.694	0.044	0.047	0.051
	S4	22.678	50.608	37.860	57.411	736.98	701.166	665.352	0.078	0.082	0.086
	S12	29.307	33.333	39.306	42.125	910.479	852.954	795.429	0.046	0.049	0.053
3	S10	66.401	3.319	67.397	23.239	1422.04	1331.84	1286.74	0.047	0.051	0.052
	S3	96.812	86.396	122.731	115.440	1052.44	1002.04	976.84	0.117	0.122	0.126
	S11	6.161	72.632	27.950	74.480	1540.392	1441.992	1392.792	0.048	0.052	0.053
	S4	31.094	71.240	52.466	80.568	982.64	934.888	911.012	0.082	0.086	0.088
	S12	40.612	51.136	55.953	63.320	1213.972	1137.272	1098.922	0.052	0.056	0.058
2	S10	79.424	4.322	80.720	28.149	1777.55	1664.8	1642.25	0.045	0.048	0.049
	S3	114.425	106.090	146.252	140.418	1315.55	1252.55	1239.95	0.111	0.117	0.118
	S11	7.114	96.639	36.106	98.773	1925.49	1802.49	1777.89	0.051	0.055	0.056
	S4	39.334	90.997	66.633	102.797	1228.3	1168.61	1156.672	0.084	0.088	0.089
	S12	51.123	70.143	72.166	85.480	1517.465	1421.59	1402.415	0.056	0.060	0.061
1	S10	87.853	13.588	91.929	39.943	2133.06	1997.76	1997.76	0.043	0.046	0.046
	S3	125.174	121.059	161.492	158.611	1578.66	1503.06	1503.06	0.102	0.107	0.107
	S11	7.559	116.531	42.518	118.798	2310.588	2162.988	2162.988	0.051	0.055	0.055
	S4	43.957	106.349	75.862	119.536	1473.96	1402.332	1402.332	0.081	0.085	0.085
	S12	59.182	86.669	85.183	104.424	1820.958	1705.908	1705.908	0.057	0.061	0.061

Çizelge B.102: 9 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	20.500	9.361	23.309	15.511	355.51	310.41	254.035	0.066	0.075	0.092
	S3	44.099	29.345	52.902	42.574	263.11	237.91	206.41	0.201	0.222	0.256
	S11	4.102	15.075	8.625	16.306	385.098	335.898	274.398	0.042	0.049	0.059
	S4	10.035	17.428	15.263	20.439	245.66	221.784	191.939	0.083	0.092	0.106
	S12	11.387	5.937	13.169	9.354	303.493	265.143	217.2055	0.043	0.050	0.061
8	S10	51.005	9.333	53.804	24.634	711.02	620.82	519.345	0.076	0.087	0.104
	S3	89.137	70.309	110.230	97.050	526.22	475.82	419.12	0.209	0.232	0.263
	S11	9.194	42.654	21.990	45.412	770.196	671.796	561.096	0.059	0.068	0.081
	S4	20.757	48.338	35.259	54.565	491.32	443.568	389.847	0.111	0.123	0.140
	S12	30.253	24.828	37.702	33.904	606.986	530.286	443.9985	0.062	0.071	0.085
7	S10	82.446	10.674	85.648	35.408	1066.53	931.23	987.605	0.080	0.092	0.087
	S3	135.158	111.524	168.615	152.072	789.33	713.73	745.23	0.214	0.236	0.226
	S11	13.714	70.847	34.968	74.961	1155.294	1007.694	1069.194	0.065	0.074	0.070
	S4	32.849	79.538	56.710	89.393	736.98	665.352	695.197	0.121	0.134	0.129
	S12	49.274	44.282	62.559	59.064	910.479	795.429	843.3665	0.069	0.079	0.074
6	S10	111.227	4.283	112.512	37.651	1422.04	1241.64	1275.465	0.079	0.091	0.088
	S3	180.209	153.725	226.327	207.788	1052.44	951.64	970.54	0.215	0.238	0.233
	S11	18.039	106.966	50.129	112.378	1540.392	1343.592	1380.492	0.073	0.084	0.081
	S4	47.158	113.597	81.237	127.744	982.64	887.136	905.043	0.130	0.144	0.141
	S12	70.267	70.759	91.495	91.840	1213.972	1060.572	1089.3345	0.076	0.087	0.084
5	S10	137.341	8.009	139.743	49.211	1777.55	1552.05	1585.875	0.079	0.090	0.088
	S3	223.092	195.897	281.861	262.825	1315.55	1189.55	1208.45	0.214	0.237	0.233
	S11	21.792	148.913	66.466	155.450	1925.49	1679.49	1716.39	0.081	0.093	0.091
	S4	63.993	149.817	108.938	169.015	1228.3	1108.92	1126.827	0.138	0.152	0.150
	S12	92.407	102.117	123.042	129.839	1517.465	1325.715	1354.4775	0.086	0.098	0.096
4	S10	160.851	24.716	168.266	72.971	2133.06	1862.46	1918.835	0.079	0.090	0.088
	S3	263.107	236.694	334.115	315.626	1578.66	1427.46	1458.96	0.212	0.234	0.229
	S11	24.810	193.367	82.820	200.810	2310.588	2015.388	2076.888	0.087	0.100	0.097
	S4	76.106	185.238	131.677	208.070	1473.96	1330.704	1360.549	0.141	0.156	0.153
	S12	114.913	138.896	156.582	173.370	1820.958	1590.858	1638.7955	0.095	0.109	0.106
3	S10	176.163	44.212	189.426	97.060	2488.57	2172.87	2274.345	0.076	0.087	0.083
	S3	295.017	276.297	377.906	364.802	1841.77	1665.37	1722.07	0.205	0.227	0.219
	S11	27.187	239.696	99.096	247.852	2695.686	2351.286	2461.986	0.092	0.105	0.101
	S4	88.574	219.070	154.295	245.642	1719.62	1552.488	1606.209	0.143	0.158	0.153
	S12	131.677	175.168	184.227	214.671	2124.451	1856.001	1942.2885	0.101	0.116	0.111
2	S10	186.866	62.504	205.617	118.564	2844.08	2483.28	2629.855	0.072	0.083	0.078
	S3	317.298	310.556	410.465	405.745	2104.88	1903.28	1985.18	0.195	0.216	0.207
	S11	28.675	279.306	112.467	287.908	3080.784	2687.184	2847.084	0.093	0.107	0.101
	S4	101.090	248.628	175.679	278.956	1965.28	1774.272	1851.869	0.142	0.157	0.151
	S12	144.537	206.442	206.469	249.802	2427.944	2121.144	2245.7815	0.103	0.118	0.111
1	S10	193.822	80.473	217.964	138.620	3199.59	2793.69	2985.365	0.068	0.078	0.073
	S3	329.081	334.392	429.399	433.117	2367.99	2141.19	2248.29	0.183	0.202	0.193
	S11	29.424	306.981	121.518	315.808	3465.882	3023.082	3232.182	0.091	0.104	0.098
	S4	109.211	270.028	190.219	302.791	2210.94	1996.056	2097.529	0.137	0.152	0.144
	S12	156.193	231.607	225.675	278.465	2731.437	2386.287	2549.2745	0.102	0.117	0.109

Çizelge B.103: 12 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	26.254	12.490	30.001	20.367	355.51	310.41	310.41	0.084	0.097	0.097
	S3	58.224	41.499	70.674	58.966	263.11	237.91	237.91	0.269	0.297	0.297
	S11	6.872	17.726	12.189	19.787	385.098	335.898	335.898	0.051	0.059	0.059
	S4	9.945	25.438	17.576	28.422	245.66	221.784	221.784	0.116	0.128	0.128
	S12	13.747	5.705	15.459	9.829	303.493	265.143	265.143	0.051	0.058	0.058
11	S10	65.832	11.609	69.314	31.358	711.02	620.82	620.82	0.097	0.112	0.112
	S3	118.695	100.703	148.906	136.312	526.22	475.82	475.82	0.283	0.313	0.313
	S11	15.537	52.351	31.243	57.012	770.196	671.796	671.796	0.074	0.085	0.085
	S4	21.153	69.670	42.054	76.016	491.32	443.568	443.568	0.155	0.171	0.171
	S12	38.032	28.872	46.693	40.282	606.986	530.286	530.286	0.077	0.088	0.088
10	S10	107.108	12.863	110.967	44.996	1066.53	931.23	931.23	0.104	0.119	0.119
	S3	181.175	160.529	229.334	214.882	789.33	713.73	713.73	0.291	0.321	0.321
	S11	23.430	87.865	49.790	94.894	1155.294	1007.694	1007.694	0.082	0.094	0.094
	S4	34.362	114.291	68.649	124.600	736.98	665.352	665.352	0.169	0.187	0.187
	S12	62.740	52.785	78.576	71.607	910.479	795.429	795.429	0.086	0.099	0.099
9	S10	144.877	3.227	145.845	46.690	1422.04	1241.64	1185.265	0.103	0.117	0.123
	S3	243.622	222.841	310.474	295.928	1052.44	951.64	920.14	0.295	0.326	0.337
	S11	31.133	134.969	71.624	144.309	1540.392	1343.592	1282.092	0.094	0.107	0.113
	S4	51.217	163.525	100.275	178.890	982.64	887.136	857.291	0.182	0.202	0.209
	S12	90.754	86.821	116.800	114.047	1213.972	1060.572	1012.6345	0.096	0.110	0.115
8	S10	179.827	14.705	184.239	68.653	1777.55	1552.05	1450.575	0.104	0.119	0.127
	S3	305.505	287.199	391.665	378.851	1315.55	1189.55	1132.85	0.298	0.329	0.346
	S11	38.114	191.539	95.576	202.973	1925.49	1679.49	1568.79	0.105	0.121	0.129
	S4	72.818	216.988	137.915	238.834	1228.3	1108.92	1055.199	0.194	0.215	0.226
	S12	121.380	128.481	159.924	164.894	1517.465	1325.715	1239.4275	0.109	0.124	0.133
7	S10	212.601	40.445	224.734	104.225	2133.06	1862.46	1715.885	0.105	0.121	0.131
	S3	367.400	353.192	473.358	463.412	1578.66	1427.46	1345.56	0.300	0.332	0.352
	S11	44.228	255.068	120.748	268.336	2310.588	2015.388	1855.488	0.116	0.133	0.145
	S4	88.074	271.701	169.585	298.123	1473.96	1330.704	1253.107	0.202	0.224	0.238
	S12	155.072	181.079	209.396	227.601	1820.958	1590.858	1466.2205	0.125	0.143	0.155
6	S10	233.761	71.561	255.230	141.689	2488.57	2172.87	2003.745	0.103	0.117	0.127
	S3	421.952	423.748	549.077	550.334	1841.77	1665.37	1570.87	0.299	0.330	0.350
	S11	49.633	327.680	147.937	342.570	2695.686	2351.286	2166.786	0.127	0.146	0.158
	S4	107.105	328.558	205.672	360.689	1719.62	1552.488	1462.953	0.210	0.232	0.247
	S12	180.899	236.377	251.812	290.647	2124.451	1856.001	1712.1885	0.137	0.157	0.170
5	S10	251.213	105.901	282.983	181.265	2844.08	2483.28	2314.155	0.099	0.114	0.122
	S3	469.081	494.370	617.392	635.094	2104.88	1903.28	1808.78	0.302	0.334	0.351
	S11	54.061	398.764	173.690	414.982	3080.784	2687.184	2502.684	0.135	0.154	0.166
	S4	128.823	385.631	244.513	424.278	1965.28	1774.272	1684.737	0.216	0.239	0.252
	S12	206.154	293.067	294.074	354.913	2427.944	2121.144	1977.3315	0.146	0.167	0.179
4	S10	268.957	142.282	311.642	222.970	3199.59	2793.69	2647.115	0.097	0.112	0.118
	S3	509.229	560.776	677.462	713.544	2367.99	2141.19	2059.29	0.301	0.333	0.347
	S11	57.557	463.840	196.709	481.107	3465.882	3023.082	2863.182	0.139	0.159	0.168
	S4	150.177	439.351	281.982	484.404	2210.94	1996.056	1918.459	0.219	0.243	0.252
	S12	234.804	351.151	340.149	421.593	2731.437	2386.287	2261.6495	0.154	0.177	0.186
3	S10	283.749	176.041	336.562	261.166	3555.1	3104.1	3002.625	0.095	0.108	0.112
	S3	540.829	620.092	726.857	782.341	2631.1	2379.1	2322.4	0.297	0.329	0.337
	S11	60.093	523.222	217.060	541.250	3850.98	3358.98	3248.28	0.141	0.161	0.167
	S4	171.025	486.750	317.050	538.058	2456.6	2217.84	2164.119	0.219	0.243	0.249
	S12	259.630	404.199	380.889	482.088	3034.93	2651.43	2565.1425	0.159	0.182	0.188
2	S10	294.858	207.045	356.971	295.503	3910.61	3414.51	3358.135	0.091	0.105	0.106
	S3	563.261	667.810	763.604	836.788	2894.21	2617.01	2585.51	0.289	0.320	0.324
	S11	61.684	572.720	233.500	591.225	4236.078	3694.878	3633.378	0.140	0.160	0.163

1	S4	188.503	526.013	346.307	582.564	2702.26	2439.624	2409.779	0.216	0.239	0.242
	S12	280.855	450.643	416.048	534.900	3338.423	2916.573	2868.6355	0.160	0.183	0.186
	S10	301.506	230.719	370.721	321.171	4266.12	3724.92	3713.645	0.087	0.100	0.100
	S3	573.208	699.513	783.061	871.475	3157.32	2854.92	2848.62	0.276	0.305	0.306
	S11	62.354	605.134	243.894	623.840	4621.176	4030.776	4018.476	0.135	0.155	0.155
	S4	202.752	553.128	368.690	613.953	2947.92	2661.408	2655.439	0.208	0.231	0.231
	S12	295.643	480.944	439.926	569.637	3641.916	3181.716	3172.1285	0.156	0.179	0.180

Çizelge B.104: 6 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	1.847	0.961	2.135	1.515	355.51	332.96	287.86	0.006	0.006	0.007
	S3	3.758	2.809	4.601	3.937	263.11	250.51	225.31	0.017	0.018	0.020
	S11	0.230	1.738	0.751	1.807	385.098	360.498	311.298	0.005	0.005	0.006
	S4	1.068	1.741	1.590	2.061	245.66	233.722	209.846	0.008	0.009	0.010
	S12	1.039	0.818	1.285	1.130	303.493	284.318	245.968	0.004	0.005	0.005
5	S10	4.563	1.018	4.868	2.387	711.02	665.92	598.27	0.007	0.007	0.008
	S3	7.351	6.527	9.309	8.732	526.22	501.02	463.22	0.018	0.019	0.020
	S11	0.494	4.797	1.933	4.945	770.196	720.996	647.196	0.006	0.007	0.008
	S4	2.146	4.892	3.614	5.536	491.32	467.444	431.63	0.011	0.012	0.013
	S12	2.670	3.037	3.581	3.838	606.986	568.636	511.111	0.006	0.007	0.008
4	S10	7.285	1.156	7.632	3.341	1066.53	998.88	931.23	0.007	0.008	0.008
	S3	10.905	10.208	13.968	13.479	789.33	751.53	713.73	0.018	0.019	0.020
	S11	0.708	7.886	3.074	8.099	1155.294	1081.494	1007.694	0.007	0.007	0.008
	S4	3.307	8.059	5.725	9.051	736.98	701.166	665.352	0.012	0.013	0.014
	S12	4.274	5.308	5.866	6.590	910.479	852.954	795.429	0.007	0.008	0.008
3	S10	9.684	0.529	9.842	3.434	1422.04	1331.84	1286.74	0.007	0.007	0.008
	S3	14.118	13.757	18.246	17.993	1052.44	1002.04	976.84	0.017	0.018	0.019
	S11	0.898	11.566	4.368	11.835	1540.392	1441.992	1392.792	0.008	0.008	0.008
	S4	4.535	11.344	7.938	12.704	982.64	934.888	911.012	0.013	0.014	0.014
	S12	5.923	8.143	8.365	9.919	1213.972	1137.272	1098.922	0.008	0.009	0.009
2	S10	11.583	0.688	11.789	4.163	1777.55	1664.8	1642.25	0.007	0.007	0.007
	S3	16.687	16.894	21.755	21.900	1315.55	1252.55	1239.95	0.017	0.017	0.018
	S11	1.038	15.389	5.654	15.700	1925.49	1802.49	1777.89	0.008	0.009	0.009
	S4	5.736	14.490	10.083	16.211	1228.3	1168.61	1156.672	0.013	0.014	0.014
	S12	7.455	11.169	10.806	13.406	1517.465	1421.59	1402.415	0.009	0.009	0.010
1	S10	12.812	2.164	13.461	6.007	2133.06	1997.76	1997.76	0.006	0.007	0.007
	S3	18.255	19.277	24.038	24.753	1578.66	1503.06	1503.06	0.016	0.016	0.016
	S11	1.102	18.556	6.669	18.887	2310.588	2162.988	2162.988	0.008	0.009	0.009
	S4	6.410	16.935	11.491	18.858	1473.96	1402.332	1402.332	0.013	0.013	0.013
	S12	8.631	13.801	12.771	16.390	1820.958	1705.908	1705.908	0.009	0.010	0.010

Çizelge B.105: 9 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	2.586	1.181	2.940	1.957	355.51	310.41	254.035	0.008	0.009	0.012
	S3	5.563	3.702	6.674	5.371	263.11	237.91	206.41	0.025	0.028	0.032
	S11	0.518	1.902	1.088	2.057	385.098	335.898	274.398	0.005	0.006	0.007
	S4	1.266	2.199	1.926	2.578	245.66	221.784	191.939	0.010	0.012	0.013
	S12	1.437	0.749	1.661	1.180	303.493	265.143	217.2055	0.005	0.006	0.008
8	S10	6.434	1.177	6.788	3.108	711.02	620.82	519.345	0.010	0.011	0.013
	S3	11.245	8.870	13.906	12.243	526.22	475.82	419.12	0.026	0.029	0.033
	S11	1.160	5.381	2.774	5.729	770.196	671.796	561.096	0.007	0.009	0.010
	S4	2.619	6.098	4.448	6.884	491.32	443.568	389.847	0.014	0.016	0.018
	S12	3.817	3.132	4.756	4.277	606.986	530.286	443.9985	0.008	0.009	0.011
7	S10	10.401	1.347	10.805	4.467	1066.53	931.23	987.605	0.010	0.012	0.011
	S3	17.051	14.069	21.271	19.184	789.33	713.73	745.23	0.027	0.030	0.029
	S11	1.730	8.938	4.411	9.457	1155.294	1007.694	1069.194	0.008	0.009	0.009
	S4	4.144	10.034	7.154	11.277	736.98	665.352	695.197	0.015	0.017	0.016
	S12	6.216	5.586	7.892	7.451	910.479	795.429	843.3665	0.009	0.010	0.009
6	S10	14.032	0.540	14.194	4.750	1422.04	1241.64	1275.465	0.010	0.011	0.011
	S3	22.734	19.393	28.552	26.213	1052.44	951.64	970.54	0.027	0.030	0.029
	S11	2.276	13.494	6.324	14.177	1540.392	1343.592	1380.492	0.009	0.011	0.010
	S4	5.949	14.331	10.248	16.115	982.64	887.136	905.043	0.016	0.018	0.018
	S12	8.865	8.927	11.542	11.586	1213.972	1060.572	1089.3345	0.010	0.011	0.011
5	S10	17.326	1.010	17.629	6.208	1777.55	1552.05	1585.875	0.010	0.011	0.011
	S3	28.144	24.713	35.558	33.156	1315.55	1189.55	1208.45	0.027	0.030	0.029
	S11	2.749	18.786	8.385	19.611	1925.49	1679.49	1716.39	0.010	0.012	0.011
	S4	8.073	18.900	13.743	21.322	1228.3	1108.92	1126.827	0.017	0.019	0.019
	S12	11.658	12.882	15.522	16.380	1517.465	1325.715	1354.4775	0.011	0.012	0.012
4	S10	20.292	3.118	21.227	9.206	2133.06	1862.46	1918.835	0.010	0.011	0.011
	S3	33.192	29.860	42.150	39.817	1578.66	1427.46	1458.96	0.027	0.030	0.029
	S11	3.130	24.394	10.448	25.333	2310.588	2015.388	2076.888	0.011	0.013	0.012
	S4	9.601	23.369	16.612	26.249	1473.96	1330.704	1360.549	0.018	0.020	0.019
	S12	14.497	17.522	19.753	21.871	1820.958	1590.858	1638.7955	0.012	0.014	0.013
3	S10	22.224	5.578	23.897	12.245	2488.57	2172.87	2274.345	0.010	0.011	0.011
	S3	37.218	34.856	47.674	46.021	1841.77	1665.37	1722.07	0.026	0.029	0.028
	S11	3.430	30.239	12.501	31.267	2695.686	2351.286	2461.986	0.012	0.013	0.013
	S4	11.174	27.637	19.465	30.989	1719.62	1552.488	1606.209	0.018	0.020	0.019
	S12	16.612	22.098	23.241	27.082	2124.451	1856.001	1942.2885	0.013	0.015	0.014
2	S10	23.574	7.885	25.939	14.957	2844.08	2483.28	2629.855	0.009	0.010	0.010
	S3	40.028	39.178	51.782	51.186	2104.88	1903.28	1985.18	0.025	0.027	0.026
	S11	3.618	35.236	14.188	36.321	3080.784	2687.184	2847.084	0.012	0.014	0.013
	S4	12.753	31.365	22.163	35.191	1965.28	1774.272	1851.869	0.018	0.020	0.019
	S12	18.234	26.043	26.047	31.514	2427.944	2121.144	2245.7815	0.013	0.015	0.014
1	S10	24.451	10.152	27.497	17.487	3199.59	2793.69	2985.365	0.009	0.010	0.009
	S3	41.515	42.185	54.170	54.639	2367.99	2141.19	2248.29	0.023	0.026	0.024
	S11	3.712	38.727	15.330	39.840	3465.882	3023.082	3232.182	0.011	0.013	0.012
	S4	13.777	34.065	23.997	38.198	2210.94	1996.056	2097.529	0.017	0.019	0.018
	S12	19.704	29.218	28.470	35.129	2731.437	2386.287	2549.2745	0.013	0.015	0.014

Çizelge B.106: 12 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	3.312	1.576	3.785	2.569	355.51	310.41	310.41	0.011	0.012	0.012
	S3	7.345	5.235	8.916	7.439	263.11	237.91	237.91	0.034	0.037	0.037
	S11	0.867	2.236	1.538	2.496	385.098	335.898	335.898	0.006	0.007	0.007
	S4	1.255	3.209	2.217	3.585	245.66	221.784	221.784	0.015	0.016	0.016
	S12	1.734	0.720	1.950	1.240	303.493	265.143	265.143	0.006	0.007	0.007
11	S10	8.305	1.465	8.744	3.956	711.02	620.82	620.82	0.012	0.014	0.014
	S3	14.974	12.704	18.785	17.196	526.22	475.82	475.82	0.036	0.039	0.039
	S11	1.960	6.604	3.941	7.192	770.196	671.796	671.796	0.009	0.011	0.011
	S4	2.669	8.789	5.305	9.590	491.32	443.568	443.568	0.020	0.022	0.022
	S12	4.798	3.642	5.891	5.082	606.986	530.286	530.286	0.010	0.011	0.011
10	S10	13.512	1.623	13.999	5.676	1066.53	931.23	931.23	0.013	0.015	0.015
	S3	22.856	20.251	28.931	27.108	789.33	713.73	713.73	0.037	0.041	0.041
	S11	2.956	11.085	6.281	11.971	1155.294	1007.694	1007.694	0.010	0.012	0.012
	S4	4.335	14.418	8.660	15.719	736.98	665.352	665.352	0.021	0.024	0.024
	S12	7.915	6.659	9.913	9.033	910.479	795.429	795.429	0.011	0.012	0.012
9	S10	18.277	0.407	18.399	5.890	1422.04	1241.64	1185.265	0.013	0.015	0.016
	S3	30.734	28.112	39.167	37.332	1052.44	951.64	920.14	0.037	0.041	0.043
	S11	3.928	17.027	9.036	18.205	1540.392	1343.592	1282.092	0.012	0.014	0.014
	S4	6.461	20.629	12.650	22.568	982.64	887.136	857.291	0.023	0.025	0.026
	S12	11.449	10.953	14.735	14.387	1213.972	1060.572	1012.6345	0.012	0.014	0.015
8	S10	22.686	1.855	23.242	8.661	1777.55	1552.05	1450.575	0.013	0.015	0.016
	S3	38.541	36.231	49.410	47.794	1315.55	1189.55	1132.85	0.038	0.042	0.044
	S11	4.808	24.163	12.057	25.606	1925.49	1679.49	1568.79	0.013	0.015	0.016
	S4	9.186	27.374	17.398	30.130	1228.3	1108.92	1055.199	0.025	0.027	0.029
	S12	15.313	16.208	20.175	20.802	1517.465	1325.715	1239.4275	0.014	0.016	0.017
7	S10	26.820	5.102	28.351	13.148	2133.06	1862.46	1715.885	0.013	0.015	0.017
	S3	46.349	44.557	59.716	58.461	1578.66	1427.46	1345.56	0.038	0.042	0.044
	S11	5.580	32.178	15.233	33.852	2310.588	2015.388	1855.488	0.015	0.017	0.018
	S4	11.111	34.276	21.394	37.609	1473.96	1330.704	1253.107	0.026	0.028	0.030
	S12	19.563	22.844	26.416	28.713	1820.958	1590.858	1466.2205	0.016	0.018	0.020
6	S10	29.490	9.028	32.198	17.875	2488.57	2172.87	2003.745	0.013	0.015	0.016
	S3	53.231	53.458	69.268	69.427	1841.77	1665.37	1570.87	0.038	0.042	0.044
	S11	6.261	41.338	18.663	43.217	2695.686	2351.286	2166.786	0.016	0.018	0.020
	S4	13.512	41.449	25.946	45.502	1719.62	1552.488	1462.953	0.026	0.029	0.031
	S12	22.821	29.820	31.767	36.666	2124.451	1856.001	1712.1885	0.017	0.020	0.021
5	S10	31.692	13.360	35.699	22.867	2844.08	2483.28	2314.155	0.013	0.014	0.015
	S3	59.176	62.367	77.886	80.120	2104.88	1903.28	1808.78	0.038	0.042	0.044
	S11	6.820	50.306	21.912	52.352	3080.784	2687.184	2502.684	0.017	0.019	0.021
	S4	16.252	48.649	30.846	53.524	1965.28	1774.272	1684.737	0.027	0.030	0.032
	S12	26.007	36.972	37.099	44.774	2427.944	2121.144	1977.3315	0.018	0.021	0.023
4	S10	33.930	17.950	39.315	28.129	3199.59	2793.69	2647.115	0.012	0.014	0.015
	S3	64.241	70.744	85.464	90.016	2367.99	2141.19	2059.29	0.038	0.042	0.044
	S11	7.261	58.515	24.816	60.694	3465.882	3023.082	2863.182	0.018	0.020	0.021
	S4	18.945	55.426	35.573	61.109	2210.94	1996.056	1918.459	0.028	0.031	0.032
	S12	29.621	44.299	42.911	53.186	2731.437	2386.287	2261.6495	0.019	0.022	0.024
3	S10	35.796	22.208	42.459	32.947	3555.1	3104.1	3002.625	0.012	0.014	0.014
	S3	68.228	78.227	91.696	98.695	2631.1	2379.1	2322.4	0.038	0.041	0.042
	S11	7.581	66.007	27.383	68.281	3850.98	3358.98	3248.28	0.018	0.020	0.021
	S4	21.575	61.405	39.997	67.878	2456.6	2217.84	2164.119	0.028	0.031	0.031
	S12	32.753	50.991	48.051	60.817	3034.93	2651.43	2565.1425	0.020	0.023	0.024
2	S10	37.198	26.120	45.033	37.279	3910.61	3414.51	3358.135	0.012	0.013	0.013
	S3	71.058	84.247	96.332	105.564	2894.21	2617.01	2585.51	0.036	0.040	0.041
	S11	7.782	72.251	29.457	74.585	4236.078	3694.878	3633.378	0.018	0.020	0.021

1	S4	23.780	66.359	43.688	73.493	2702.26	2439.624	2409.779	0.027	0.030	0.030
	S12	35.431	56.850	52.486	67.480	3338.423	2916.573	2868.6355	0.020	0.023	0.024
	S10	38.036	29.106	46.768	40.517	4266.12	3724.92	3713.645	0.011	0.013	0.013
	S3	72.312	88.246	98.786	109.940	3157.32	2854.92	2848.62	0.035	0.039	0.039
	S11	7.866	76.340	30.768	78.700	4621.176	4030.776	4018.476	0.017	0.020	0.020
	S4	25.578	69.779	46.512	77.453	2947.92	2661.408	2655.439	0.026	0.029	0.029
	S12	37.297	60.673	55.498	71.862	3641.916	3181.716	3172.1285	0.020	0.023	0.023

Çizelge B.107: 6 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	1.847	0.961	2.135	1.515	355.51	332.96	287.86	0.006	0.006	0.007
	S3	3.758	2.809	4.601	3.937	263.11	250.51	225.31	0.017	0.018	0.020
	S11	0.230	1.738	0.751	1.807	385.098	360.498	311.298	0.005	0.005	0.006
	S4	1.068	1.741	1.590	2.061	245.66	233.722	209.846	0.008	0.009	0.010
	S12	1.039	0.818	1.285	1.130	303.493	284.318	245.968	0.004	0.005	0.005
5	S10	4.563	1.018	4.868	2.387	711.02	665.92	598.27	0.007	0.007	0.008
	S3	7.351	6.527	9.309	8.732	526.22	501.02	463.22	0.018	0.019	0.020
	S11	0.494	4.797	1.933	4.945	770.196	720.996	647.196	0.006	0.007	0.008
	S4	2.146	4.892	3.614	5.536	491.32	467.444	431.63	0.011	0.012	0.013
	S12	2.670	3.037	3.581	3.838	606.986	568.636	511.111	0.006	0.007	0.008
4	S10	7.285	1.156	7.632	3.341	1066.53	998.88	931.23	0.007	0.008	0.008
	S3	10.905	10.208	13.968	13.479	789.33	751.53	713.73	0.018	0.019	0.020
	S11	0.708	7.886	3.074	8.099	1155.294	1081.494	1007.694	0.007	0.007	0.008
	S4	3.307	8.059	5.725	9.051	736.98	701.166	665.352	0.012	0.013	0.014
	S12	4.274	5.308	5.866	6.590	910.479	852.954	795.429	0.007	0.008	0.008
3	S10	9.684	0.529	9.842	3.434	1422.04	1331.84	1286.74	0.007	0.007	0.008
	S3	14.118	13.757	18.246	17.993	1052.44	1002.04	976.84	0.017	0.018	0.019
	S11	0.898	11.566	4.368	11.835	1540.392	1441.992	1392.792	0.008	0.008	0.008
	S4	4.535	11.344	7.938	12.704	982.64	934.888	911.012	0.013	0.014	0.014
	S12	5.923	8.143	8.365	9.919	1213.972	1137.272	1098.922	0.008	0.009	0.009
2	S10	11.583	0.688	11.789	4.163	1777.55	1664.8	1642.25	0.007	0.007	0.007
	S3	16.687	16.894	21.755	21.900	1315.55	1252.55	1239.95	0.017	0.017	0.018
	S11	1.038	15.389	5.654	15.700	1925.49	1802.49	1777.89	0.008	0.009	0.009
	S4	5.736	14.490	10.083	16.211	1228.3	1168.61	1156.672	0.013	0.014	0.014
	S12	7.455	11.169	10.806	13.406	1517.465	1421.59	1402.415	0.009	0.009	0.010
1	S10	12.812	2.164	13.461	6.007	2133.06	1997.76	1997.76	0.006	0.007	0.007
	S3	18.255	19.277	24.038	24.753	1578.66	1503.06	1503.06	0.016	0.016	0.016
	S11	1.102	18.556	6.669	18.887	2310.588	2162.988	2162.988	0.008	0.009	0.009
	S4	6.410	16.935	11.491	18.858	1473.96	1402.332	1402.332	0.013	0.013	0.013
	S12	8.631	13.801	12.771	16.390	1820.958	1705.908	1705.908	0.009	0.010	0.010

Çizelge B.108: 9 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	2.586	1.181	2.940	1.957	355.51	310.41	254.035	0.008	0.009	0.012
	S3	5.563	3.702	6.674	5.371	263.11	237.91	206.41	0.025	0.028	0.032
	S11	0.518	1.902	1.088	2.057	385.098	335.898	274.398	0.005	0.006	0.007
	S4	1.266	2.199	1.926	2.578	245.66	221.784	191.939	0.010	0.012	0.013
	S12	1.437	0.749	1.661	1.180	303.493	265.143	217.2055	0.005	0.006	0.008
8	S10	6.434	1.177	6.788	3.108	711.02	620.82	519.345	0.010	0.011	0.013
	S3	11.245	8.870	13.906	12.243	526.22	475.82	419.12	0.026	0.029	0.033
	S11	1.160	5.381	2.774	5.729	770.196	671.796	561.096	0.007	0.009	0.010
	S4	2.619	6.098	4.448	6.884	491.32	443.568	389.847	0.014	0.016	0.018
	S12	3.817	3.132	4.756	4.277	606.986	530.286	443.9985	0.008	0.009	0.011
7	S10	10.401	1.347	10.805	4.467	1066.53	931.23	987.605	0.010	0.012	0.011
	S3	17.051	14.069	21.271	19.184	789.33	713.73	745.23	0.027	0.030	0.029
	S11	1.730	8.938	4.411	9.457	1155.294	1007.694	1069.194	0.008	0.009	0.009
	S4	4.144	10.034	7.154	11.277	736.98	665.352	695.197	0.015	0.017	0.016
	S12	6.216	5.586	7.892	7.451	910.479	795.429	843.3665	0.009	0.010	0.009
6	S10	14.032	0.540	14.194	4.750	1422.04	1241.64	1275.465	0.010	0.011	0.011
	S3	22.734	19.393	28.552	26.213	1052.44	951.64	970.54	0.027	0.030	0.029
	S11	2.276	13.494	6.324	14.177	1540.392	1343.592	1380.492	0.009	0.011	0.010
	S4	5.949	14.331	10.248	16.115	982.64	887.136	905.043	0.016	0.018	0.018
	S12	8.865	8.927	11.542	11.586	1213.972	1060.572	1089.3345	0.010	0.011	0.011
5	S10	17.326	1.010	17.629	6.208	1777.55	1552.05	1585.875	0.010	0.011	0.011
	S3	28.144	24.713	35.558	33.156	1315.55	1189.55	1208.45	0.027	0.030	0.029
	S11	2.749	18.786	8.385	19.611	1925.49	1679.49	1716.39	0.010	0.012	0.011
	S4	8.073	18.900	13.743	21.322	1228.3	1108.92	1126.827	0.017	0.019	0.019
	S12	11.658	12.882	15.522	16.380	1517.465	1325.715	1354.4775	0.011	0.012	0.012
4	S10	20.292	3.118	21.227	9.206	2133.06	1862.46	1918.835	0.010	0.011	0.011
	S3	33.192	29.860	42.150	39.817	1578.66	1427.46	1458.96	0.027	0.030	0.029
	S11	3.130	24.394	10.448	25.333	2310.588	2015.388	2076.888	0.011	0.013	0.012
	S4	9.601	23.369	16.612	26.249	1473.96	1330.704	1360.549	0.018	0.020	0.019
	S12	14.497	17.522	19.753	21.871	1820.958	1590.858	1638.7955	0.012	0.014	0.013
3	S10	22.224	5.578	23.897	12.245	2488.57	2172.87	2274.345	0.010	0.011	0.011
	S3	37.218	34.856	47.674	46.021	1841.77	1665.37	1722.07	0.026	0.029	0.028
	S11	3.430	30.239	12.501	31.267	2695.686	2351.286	2461.986	0.012	0.013	0.013
	S4	11.174	27.637	19.465	30.989	1719.62	1552.488	1606.209	0.018	0.020	0.019
	S12	16.612	22.098	23.241	27.082	2124.451	1856.001	1942.2885	0.013	0.015	0.014
2	S10	23.574	7.885	25.939	14.957	2844.08	2483.28	2629.855	0.009	0.010	0.010
	S3	40.028	39.178	51.782	51.186	2104.88	1903.28	1985.18	0.025	0.027	0.026
	S11	3.618	35.236	14.188	36.321	3080.784	2687.184	2847.084	0.012	0.014	0.013
	S4	12.753	31.365	22.163	35.191	1965.28	1774.272	1851.869	0.018	0.020	0.019
	S12	18.234	26.043	26.047	31.514	2427.944	2121.144	2245.7815	0.013	0.015	0.014
1	S10	24.451	10.152	27.497	17.487	3199.59	2793.69	2985.365	0.009	0.010	0.009
	S3	41.515	42.185	54.170	54.639	2367.99	2141.19	2248.29	0.023	0.026	0.024
	S11	3.712	38.727	15.330	39.840	3465.882	3023.082	3232.182	0.011	0.013	0.012
	S4	13.777	34.065	23.997	38.198	2210.94	1996.056	2097.529	0.017	0.019	0.018
	S12	19.704	29.218	28.470	35.129	2731.437	2386.287	2549.2745	0.013	0.015	0.014

Çizelge B.109: 12 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	3.312	1.576	3.785	2.569	355.51	310.41	310.41	0.011	0.012	0.012
	S3	7.345	5.235	8.916	7.439	263.11	237.91	237.91	0.034	0.037	0.037
	S11	0.867	2.236	1.538	2.496	385.098	335.898	335.898	0.006	0.007	0.007
	S4	1.255	3.209	2.217	3.585	245.66	221.784	221.784	0.015	0.016	0.016
	S12	1.734	0.720	1.950	1.240	303.493	265.143	265.143	0.006	0.007	0.007
11	S10	8.305	1.465	8.744	3.956	711.02	620.82	620.82	0.012	0.014	0.014
	S3	14.974	12.704	18.785	17.196	526.22	475.82	475.82	0.036	0.039	0.039
	S11	1.960	6.604	3.941	7.192	770.196	671.796	671.796	0.009	0.011	0.011
	S4	2.669	8.789	5.305	9.590	491.32	443.568	443.568	0.020	0.022	0.022
	S12	4.798	3.642	5.891	5.082	606.986	530.286	530.286	0.010	0.011	0.011
10	S10	13.512	1.623	13.999	5.676	1066.53	931.23	931.23	0.013	0.015	0.015
	S3	22.856	20.251	28.931	27.108	789.33	713.73	713.73	0.037	0.041	0.041
	S11	2.956	11.085	6.281	11.971	1155.294	1007.694	1007.694	0.010	0.012	0.012
	S4	4.335	14.418	8.660	15.719	736.98	665.352	665.352	0.021	0.024	0.024
	S12	7.915	6.659	9.913	9.033	910.479	795.429	795.429	0.011	0.012	0.012
9	S10	18.277	0.407	18.399	5.890	1422.04	1241.64	1185.265	0.013	0.015	0.016
	S3	30.734	28.112	39.167	37.332	1052.44	951.64	920.14	0.037	0.041	0.043
	S11	3.928	17.027	9.036	18.205	1540.392	1343.592	1282.092	0.012	0.014	0.014
	S4	6.461	20.629	12.650	22.568	982.64	887.136	857.291	0.023	0.025	0.026
	S12	11.449	10.953	14.735	14.387	1213.972	1060.572	1012.6345	0.012	0.014	0.015
8	S10	22.686	1.855	23.242	8.661	1777.55	1552.05	1450.575	0.013	0.015	0.016
	S3	38.541	36.231	49.410	47.794	1315.55	1189.55	1132.85	0.038	0.042	0.044
	S11	4.808	24.163	12.057	25.606	1925.49	1679.49	1568.79	0.013	0.015	0.016
	S4	9.186	27.374	17.398	30.130	1228.3	1108.92	1055.199	0.025	0.027	0.029
	S12	15.313	16.208	20.175	20.802	1517.465	1325.715	1239.4275	0.014	0.016	0.017
7	S10	26.820	5.102	28.351	13.148	2133.06	1862.46	1715.885	0.013	0.015	0.017
	S3	46.349	44.557	59.716	58.461	1578.66	1427.46	1345.56	0.038	0.042	0.044
	S11	5.580	32.178	15.233	33.852	2310.588	2015.388	1855.488	0.015	0.017	0.018
	S4	11.111	34.276	21.394	37.609	1473.96	1330.704	1253.107	0.026	0.028	0.030
	S12	19.563	22.844	26.416	28.713	1820.958	1590.858	1466.2205	0.016	0.018	0.020
6	S10	29.490	9.028	32.198	17.875	2488.57	2172.87	2003.745	0.013	0.015	0.016
	S3	53.231	53.458	69.268	69.427	1841.77	1665.37	1570.87	0.038	0.042	0.044
	S11	6.261	41.338	18.663	43.217	2695.686	2351.286	2166.786	0.016	0.018	0.020
	S4	13.512	41.449	25.946	45.502	1719.62	1552.488	1462.953	0.026	0.029	0.031
	S12	22.821	29.820	31.767	36.666	2124.451	1856.001	1712.1885	0.017	0.020	0.021
5	S10	31.692	13.360	35.699	22.867	2844.08	2483.28	2314.155	0.013	0.014	0.015
	S3	59.176	62.367	77.886	80.120	2104.88	1903.28	1808.78	0.038	0.042	0.044
	S11	6.820	50.306	21.912	52.352	3080.784	2687.184	2502.684	0.017	0.019	0.021
	S4	16.252	48.649	30.846	53.524	1965.28	1774.272	1684.737	0.027	0.030	0.032
	S12	26.007	36.972	37.099	44.774	2427.944	2121.144	1977.3315	0.018	0.021	0.023
4	S10	33.930	17.950	39.315	28.129	3199.59	2793.69	2647.115	0.012	0.014	0.015
	S3	64.241	70.744	85.464	90.016	2367.99	2141.19	2059.29	0.038	0.042	0.044
	S11	7.261	58.515	24.816	60.694	3465.882	3023.082	2863.182	0.018	0.020	0.021
	S4	18.945	55.426	35.573	61.109	2210.94	1996.056	1918.459	0.028	0.031	0.032
	S12	29.621	44.299	42.911	53.186	2731.437	2386.287	2261.6495	0.019	0.022	0.024
3	S10	35.796	22.208	42.459	32.947	3555.1	3104.1	3002.625	0.012	0.014	0.014
	S3	68.228	78.227	91.696	98.695	2631.1	2379.1	2322.4	0.038	0.041	0.042
	S11	7.581	66.007	27.383	68.281	3850.98	3358.98	3248.28	0.018	0.020	0.021
	S4	21.575	61.405	39.997	67.878	2456.6	2217.84	2164.119	0.028	0.031	0.031
	S12	32.753	50.991	48.051	60.817	3034.93	2651.43	2565.1425	0.020	0.023	0.024
2	S10	37.198	26.120	45.033	37.279	3910.61	3414.51	3358.135	0.012	0.013	0.013
	S3	71.058	84.247	96.332	105.564	2894.21	2617.01	2585.51	0.036	0.040	0.041
	S11	7.782	72.251	29.457	74.585	4236.078	3694.878	3633.378	0.018	0.020	0.021

1	S4	23.780	66.359	43.688	73.493	2702.26	2439.624	2409.779	0.027	0.030	0.030
	S12	35.431	56.850	52.486	67.480	3338.423	2916.573	2868.6355	0.020	0.023	0.024
	S10	38.036	29.106	46.768	40.517	4266.12	3724.92	3713.645	0.011	0.013	0.013
	S3	72.312	88.246	98.786	109.940	3157.32	2854.92	2848.62	0.035	0.039	0.039
	S11	7.866	76.340	30.768	78.700	4621.176	4030.776	4018.476	0.017	0.020	0.020
	S4	25.578	69.779	46.512	77.453	2947.92	2661.408	2655.439	0.026	0.029	0.029
	S12	37.297	60.673	55.498	71.862	3641.916	3181.716	3172.1285	0.020	0.023	0.023

Çizelge B.110: 6 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	3.462	1.803	4.003	2.841	355.51	332.96	287.86	0.011	0.012	0.014
	S3	7.046	5.268	8.626	7.381	263.11	250.51	225.31	0.033	0.034	0.038
	S11	0.431	3.259	1.408	3.388	385.098	360.498	311.298	0.009	0.009	0.011
	S4	2.002	3.263	2.981	3.864	245.66	233.722	209.846	0.016	0.017	0.018
	S12	1.949	1.534	2.409	2.118	303.493	284.318	245.968	0.008	0.008	0.010
5	S10	8.555	1.909	9.128	4.475	711.02	665.92	598.27	0.013	0.014	0.015
	S3	13.783	12.237	17.454	16.372	526.22	501.02	463.22	0.033	0.035	0.038
	S11	0.927	8.994	3.625	9.272	770.196	720.996	647.196	0.012	0.013	0.014
	S4	4.024	9.173	6.776	10.380	491.32	467.444	431.63	0.021	0.022	0.024
	S12	5.006	5.694	6.714	7.195	606.986	568.636	511.111	0.012	0.013	0.014
4	S10	13.659	2.167	14.309	6.265	1066.53	998.88	931.23	0.013	0.014	0.015
	S3	20.448	19.139	26.189	25.274	789.33	751.53	713.73	0.033	0.035	0.037
	S11	1.328	14.787	5.764	15.185	1155.294	1081.494	1007.694	0.013	0.014	0.015
	S4	6.201	15.110	10.734	16.970	736.98	701.166	665.352	0.023	0.024	0.026
	S12	8.014	9.952	10.999	12.356	910.479	852.954	795.429	0.014	0.014	0.016
3	S10	18.157	0.991	18.454	6.438	1422.04	1331.84	1286.74	0.013	0.014	0.014
	S3	26.472	25.795	34.211	33.737	1052.44	1002.04	976.84	0.033	0.034	0.035
	S11	1.685	21.686	8.190	22.191	1540.392	1441.992	1392.792	0.014	0.015	0.016
	S4	8.502	21.270	14.883	23.821	982.64	934.888	911.012	0.024	0.025	0.026
	S12	11.105	15.268	15.685	18.599	1213.972	1137.272	1098.922	0.015	0.016	0.017
2	S10	21.717	1.290	22.104	7.806	1777.55	1664.8	1642.25	0.012	0.013	0.013
	S3	31.288	31.675	40.791	41.062	1315.55	1252.55	1239.95	0.031	0.033	0.033
	S11	1.945	28.853	10.601	29.437	1925.49	1802.49	1777.89	0.015	0.016	0.017
	S4	10.755	27.169	18.906	30.395	1228.3	1168.61	1156.672	0.025	0.026	0.026
	S12	13.979	20.943	20.262	25.136	1517.465	1421.59	1402.415	0.017	0.018	0.018
1	S10	24.022	4.057	25.239	11.263	2133.06	1997.76	1997.76	0.012	0.013	0.013
	S3	34.227	36.144	45.071	46.413	1578.66	1503.06	1503.06	0.029	0.031	0.031
	S11	2.067	34.793	12.505	35.413	2310.588	2162.988	2162.988	0.015	0.016	0.016
	S4	12.020	31.752	21.545	35.358	1473.96	1402.332	1402.332	0.024	0.025	0.025
	S12	16.183	25.877	23.946	30.732	1820.958	1705.908	1705.908	0.017	0.018	0.018

Çizelge B.111: 9 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	4.849	2.214	5.513	3.669	355.51	310.41	254.035	0.016	0.018	0.022
	S3	10.431	6.941	12.513	10.070	263.11	237.91	206.41	0.048	0.053	0.061
	S11	0.970	3.566	2.040	3.857	385.098	335.898	274.398	0.010	0.011	0.014
	S4	2.374	4.123	3.610	4.835	245.66	221.784	191.939	0.020	0.022	0.025
	S12	2.694	1.404	3.115	2.212	303.493	265.143	217.2055	0.010	0.012	0.014
8	S10	12.065	2.208	12.727	5.827	711.02	620.82	519.345	0.018	0.020	0.025
	S3	21.084	16.631	26.074	22.956	526.22	475.82	419.12	0.050	0.055	0.062
	S11	2.175	10.089	5.201	10.742	770.196	671.796	561.096	0.014	0.016	0.019
	S4	4.910	11.434	8.340	12.907	491.32	443.568	389.847	0.026	0.029	0.033
	S12	7.156	5.873	8.918	8.020	606.986	530.286	443.9985	0.015	0.017	0.020
7	S10	19.502	2.525	20.259	8.375	1066.53	931.23	987.605	0.019	0.022	0.021
	S3	31.970	26.380	39.884	35.971	789.33	713.73	745.23	0.051	0.056	0.054
	S11	3.244	16.758	8.271	17.731	1155.294	1007.694	1069.194	0.015	0.018	0.017
	S4	7.770	18.814	13.414	21.145	736.98	665.352	695.197	0.029	0.032	0.030
	S12	11.655	10.474	14.798	13.971	910.479	795.429	843.3665	0.016	0.019	0.018
6	S10	26.310	1.013	26.613	8.906	1422.04	1241.64	1275.465	0.019	0.021	0.021
	S3	42.626	36.362	53.535	49.150	1052.44	951.64	970.54	0.051	0.056	0.055
	S11	4.267	25.302	11.857	26.582	1540.392	1343.592	1380.492	0.017	0.020	0.019
	S4	11.155	26.870	19.216	30.216	982.64	887.136	905.043	0.031	0.034	0.033
	S12	16.621	16.737	21.642	21.724	1213.972	1060.572	1089.3345	0.018	0.020	0.020
5	S10	32.486	1.894	33.055	11.640	1777.55	1552.05	1585.875	0.019	0.021	0.021
	S3	52.770	46.337	66.671	62.168	1315.55	1189.55	1208.45	0.051	0.056	0.055
	S11	5.155	35.224	15.722	36.770	1925.49	1679.49	1716.39	0.019	0.022	0.021
	S4	15.137	35.437	25.768	39.978	1228.3	1108.92	1126.827	0.033	0.036	0.035
	S12	21.858	24.155	29.104	30.712	1517.465	1325.715	1354.4775	0.020	0.023	0.023
4	S10	38.047	5.846	39.801	17.261	2133.06	1862.46	1918.835	0.019	0.021	0.021
	S3	62.235	55.987	79.031	74.658	1578.66	1427.46	1458.96	0.050	0.055	0.054
	S11	5.869	45.739	19.590	47.499	2310.588	2015.388	2076.888	0.021	0.024	0.023
	S4	18.002	43.816	31.147	49.217	1473.96	1330.704	1360.549	0.033	0.037	0.036
	S12	27.181	32.854	37.038	41.009	1820.958	1590.858	1638.7955	0.023	0.026	0.025
3	S10	41.669	10.458	44.807	22.958	2488.57	2172.87	2274.345	0.018	0.021	0.020
	S3	69.783	65.355	89.389	86.290	1841.77	1665.37	1722.07	0.049	0.054	0.052
	S11	6.431	56.697	23.440	58.627	2695.686	2351.286	2461.986	0.022	0.025	0.024
	S4	20.951	51.819	36.497	58.104	1719.62	1552.488	1606.209	0.034	0.037	0.036
	S12	31.147	41.434	43.577	50.778	2124.451	1856.001	1942.2885	0.024	0.027	0.026
2	S10	44.201	14.785	48.636	28.045	2844.08	2483.28	2629.855	0.017	0.020	0.018
	S3	75.053	73.458	97.091	95.974	2104.88	1903.28	1985.18	0.046	0.051	0.049
	S11	6.783	66.067	26.603	68.101	3080.784	2687.184	2847.084	0.022	0.025	0.024
	S4	23.912	58.810	41.555	65.984	1965.28	1774.272	1851.869	0.034	0.037	0.036
	S12	34.189	48.831	48.838	59.088	2427.944	2121.144	2245.7815	0.024	0.028	0.026
1	S10	45.846	19.035	51.557	32.789	3199.59	2793.69	2985.365	0.016	0.018	0.017
	S3	77.840	79.097	101.569	102.449	2367.99	2141.19	2248.29	0.043	0.048	0.046
	S11	6.960	72.613	28.744	74.701	3465.882	3023.082	3232.182	0.022	0.025	0.023
	S4	25.833	63.872	44.994	71.622	2210.94	1996.056	2097.529	0.032	0.036	0.034
	S12	36.946	54.784	53.381	65.868	2731.437	2386.287	2549.2745	0.024	0.028	0.026

Çizelge B.112: 12 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	6.210	2.954	7.096	4.817	355.51	310.41	310.41	0.020	0.023	0.023
	S3	13.772	9.816	16.717	13.948	263.11	237.91	237.91	0.064	0.070	0.070
	S11	1.625	4.193	2.883	4.680	385.098	335.898	335.898	0.012	0.014	0.014
	S4	2.352	6.017	4.157	6.723	245.66	221.784	221.784	0.027	0.030	0.030
	S12	3.252	1.349	3.657	2.325	303.493	265.143	265.143	0.012	0.014	0.014
11	S10	15.572	2.746	16.395	7.417	711.02	620.82	620.82	0.023	0.026	0.026
	S3	28.076	23.820	35.222	32.243	526.22	475.82	475.82	0.067	0.074	0.074
	S11	3.675	12.383	7.390	13.486	770.196	671.796	671.796	0.018	0.020	0.020
	S4	5.004	16.480	9.947	17.981	491.32	443.568	443.568	0.037	0.041	0.041
	S12	8.996	6.829	11.045	9.528	606.986	530.286	530.286	0.018	0.021	0.021
10	S10	25.335	3.043	26.248	10.643	1066.53	931.23	931.23	0.025	0.028	0.028
	S3	42.855	37.971	54.246	50.828	789.33	713.73	713.73	0.069	0.076	0.076
	S11	5.542	20.783	11.777	22.446	1155.294	1007.694	1007.694	0.019	0.022	0.022
	S4	8.128	27.034	16.238	29.473	736.98	665.352	665.352	0.040	0.044	0.044
	S12	14.841	12.486	18.586	16.938	910.479	795.429	795.429	0.020	0.023	0.023
9	S10	34.269	0.763	34.498	11.044	1422.04	1241.64	1185.265	0.024	0.028	0.029
	S3	57.626	52.711	73.439	69.998	1052.44	951.64	920.14	0.070	0.077	0.080
	S11	7.364	31.925	16.942	34.135	1540.392	1343.592	1282.092	0.022	0.025	0.027
	S4	12.115	38.680	23.719	42.314	982.64	887.136	857.291	0.043	0.048	0.049
	S12	21.467	20.537	27.628	26.977	1213.972	1060.572	1012.6345	0.023	0.026	0.027
8	S10	42.536	3.478	43.580	16.239	1777.55	1552.05	1450.575	0.025	0.028	0.030
	S3	72.264	67.934	92.644	89.613	1315.55	1189.55	1132.85	0.070	0.078	0.082
	S11	9.016	45.306	22.607	48.011	1925.49	1679.49	1568.79	0.025	0.029	0.031
	S4	17.224	51.326	32.622	56.493	1228.3	1108.92	1055.199	0.046	0.051	0.054
	S12	28.711	30.391	37.828	39.004	1517.465	1325.715	1239.4275	0.026	0.029	0.031
7	S10	50.288	9.567	53.158	24.653	2133.06	1862.46	1715.885	0.025	0.029	0.031
	S3	86.904	83.544	111.967	109.615	1578.66	1427.46	1345.56	0.071	0.078	0.083
	S11	10.462	60.333	28.562	63.472	2310.588	2015.388	1855.488	0.027	0.031	0.034
	S4	20.833	64.268	40.113	70.518	1473.96	1330.704	1253.107	0.048	0.053	0.056
	S12	36.681	42.832	49.530	53.836	1820.958	1590.858	1466.2205	0.030	0.034	0.037
6	S10	55.294	16.927	60.372	33.515	2488.57	2172.87	2003.745	0.024	0.028	0.030
	S3	99.808	100.233	129.878	130.175	1841.77	1665.37	1570.87	0.071	0.078	0.083
	S11	11.740	77.509	34.993	81.031	2695.686	2351.286	2166.786	0.030	0.034	0.037
	S4	25.334	77.717	48.649	85.317	1719.62	1552.488	1462.953	0.050	0.055	0.058
	S12	42.790	55.912	59.563	68.749	2124.451	1856.001	1712.1885	0.032	0.037	0.040
5	S10	59.422	25.050	66.936	42.876	2844.08	2483.28	2314.155	0.024	0.027	0.029
	S3	110.956	116.938	146.037	150.224	2104.88	1903.28	1808.78	0.071	0.079	0.083
	S11	12.788	94.323	41.084	98.159	3080.784	2687.184	2502.684	0.032	0.037	0.039
	S4	30.472	91.217	57.837	100.358	1965.28	1774.272	1684.737	0.051	0.057	0.060
	S12	48.763	69.322	69.560	83.951	2427.944	2121.144	1977.3315	0.035	0.040	0.042
4	S10	63.619	33.655	73.715	52.741	3199.59	2793.69	2647.115	0.023	0.026	0.028
	S3	120.452	132.645	160.246	168.781	2367.99	2141.19	2059.29	0.071	0.079	0.082
	S11	13.614	109.716	46.529	113.800	3465.882	3023.082	2863.182	0.033	0.038	0.040
	S4	35.523	103.924	66.700	114.580	2210.94	1996.056	1918.459	0.052	0.057	0.060
	S12	55.540	83.061	80.458	99.723	2731.437	2386.287	2261.6495	0.037	0.042	0.044
3	S10	67.118	41.640	79.610	61.776	3555.1	3104.1	3002.625	0.022	0.026	0.027
	S3	127.927	146.676	171.930	185.054	2631.1	2379.1	2322.4	0.070	0.078	0.080
	S11	14.214	123.762	51.343	128.026	3850.98	3358.98	3248.28	0.033	0.038	0.039
	S4	40.454	115.135	74.994	127.271	2456.6	2217.84	2164.119	0.052	0.057	0.059
	S12	61.412	95.609	90.095	114.032	3034.93	2651.43	2565.1425	0.038	0.043	0.044
2	S10	69.745	48.974	84.437	69.898	3910.61	3414.51	3358.135	0.022	0.025	0.025
	S3	133.233	157.963	180.622	197.933	2894.21	2617.01	2585.51	0.068	0.076	0.077
	S11	14.591	135.470	55.232	139.847	4236.078	3694.878	3633.378	0.033	0.038	0.038

1	S4	44.588	124.422	81.915	137.799	2702.26	2439.624	2409.779	0.051	0.056	0.057
	S12	66.433	106.595	98.411	126.524	3338.423	2916.573	2868.6355	0.038	0.043	0.044
	S10	71.318	54.574	87.690	75.969	4266.12	3724.92	3713.645	0.021	0.024	0.024
	S3	135.586	165.462	185.224	206.137	3157.32	2854.92	2848.62	0.065	0.072	0.072
	S11	14.749	143.138	57.690	147.562	4621.176	4030.776	4018.476	0.032	0.037	0.037
	S4	47.959	130.836	87.210	145.224	2947.92	2661.408	2655.439	0.049	0.055	0.055
	S12	69.931	113.762	104.059	134.741	3641.916	3181.716	3172.1285	0.037	0.042	0.042

Çizelge B.113: 6 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	5.434	2.663	6.233	4.293	355.51	332.96	287.86	0.018	0.019	0.022
	S3	11.057	7.783	13.392	11.100	263.11	250.51	225.31	0.051	0.053	0.059
	S11	0.676	4.815	2.121	5.018	385.098	360.498	311.298	0.013	0.014	0.016
	S4	3.142	4.822	4.588	5.764	245.66	233.722	209.846	0.023	0.025	0.027
	S12	3.058	2.266	3.738	3.183	303.493	284.318	245.968	0.012	0.013	0.015
5	S10	13.426	2.820	14.272	6.848	711.02	665.92	598.27	0.020	0.021	0.024
	S3	21.631	18.080	27.055	24.569	526.22	501.02	463.22	0.051	0.054	0.058
	S11	1.455	13.288	5.441	13.725	770.196	720.996	647.196	0.018	0.019	0.021
	S4	6.315	13.552	10.381	15.447	491.32	467.444	431.63	0.031	0.033	0.036
	S12	7.856	8.412	10.379	10.769	606.986	568.636	511.111	0.018	0.019	0.021
4	S10	21.436	3.202	22.396	9.633	1066.53	998.88	931.23	0.021	0.022	0.024
	S3	32.089	28.278	40.573	37.905	789.33	751.53	713.73	0.051	0.054	0.057
	S11	2.084	21.848	8.638	22.473	1155.294	1081.494	1007.694	0.019	0.021	0.022
	S4	9.731	22.325	16.429	25.244	736.98	701.166	665.352	0.034	0.036	0.038
	S12	12.576	14.704	16.987	18.477	910.479	852.954	795.429	0.020	0.022	0.023
3	S10	28.494	1.464	28.933	10.012	1422.04	1331.84	1286.74	0.020	0.022	0.022
	S3	41.543	38.112	52.977	50.575	1052.44	1002.04	976.84	0.050	0.053	0.054
	S11	2.644	32.040	12.256	32.833	1540.392	1441.992	1392.792	0.021	0.023	0.024
	S4	13.343	31.426	22.771	35.429	982.64	934.888	911.012	0.036	0.038	0.039
	S12	17.427	22.558	24.195	27.786	1213.972	1137.272	1098.922	0.023	0.024	0.025
2	S10	34.082	1.906	34.654	12.131	1777.55	1664.8	1642.25	0.019	0.021	0.021
	S3	49.101	46.800	63.141	61.530	1315.55	1252.55	1239.95	0.048	0.050	0.051
	S11	3.053	42.631	15.842	43.546	1925.49	1802.49	1777.89	0.023	0.024	0.024
	S4	16.879	40.142	28.921	45.205	1228.3	1168.61	1156.672	0.037	0.039	0.039
	S12	21.938	30.943	31.220	37.524	1517.465	1421.59	1402.415	0.025	0.026	0.027
1	S10	37.699	5.994	39.497	17.304	2133.06	1997.76	1997.76	0.019	0.020	0.020
	S3	53.714	53.403	69.735	69.517	1578.66	1503.06	1503.06	0.044	0.046	0.046
	S11	3.244	51.406	18.665	52.379	2310.588	2162.988	2162.988	0.023	0.024	0.024
	S4	18.863	46.914	32.937	52.573	1473.96	1402.332	1402.332	0.036	0.037	0.037
	S12	25.396	38.233	36.866	45.851	1820.958	1705.908	1705.908	0.025	0.027	0.027

Çizelge B.114: 9 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	7.610	3.475	8.652	5.758	355.51	310.41	254.035	0.024	0.028	0.034
	S3	16.370	10.893	19.638	15.804	263.11	237.91	206.41	0.075	0.083	0.095
	S11	1.523	5.596	3.202	6.053	385.098	335.898	274.398	0.016	0.018	0.022
	S4	3.725	6.470	5.666	7.587	245.66	221.784	191.939	0.031	0.034	0.040
	S12	4.227	2.204	4.888	3.472	303.493	265.143	217.2055	0.016	0.018	0.023
8	S10	18.933	3.465	19.973	9.144	711.02	620.82	519.345	0.028	0.032	0.038
	S3	33.088	26.099	40.918	36.026	526.22	475.82	419.12	0.078	0.086	0.098
	S11	3.413	15.833	8.163	16.857	770.196	671.796	561.096	0.022	0.025	0.030
	S4	7.705	17.944	13.088	20.255	491.32	443.568	389.847	0.041	0.046	0.052
	S12	11.230	9.216	13.995	12.585	606.986	530.286	443.9985	0.023	0.026	0.032
7	S10	30.605	3.962	31.793	13.144	1066.53	931.23	987.605	0.030	0.034	0.032
	S3	50.172	41.399	62.591	56.450	789.33	713.73	745.23	0.079	0.088	0.084
	S11	5.091	26.299	12.980	27.826	1155.294	1007.694	1069.194	0.024	0.028	0.026
	S4	12.194	29.525	21.051	33.183	736.98	665.352	695.197	0.045	0.050	0.048
	S12	18.291	16.438	23.222	21.925	910.479	795.429	843.3665	0.026	0.029	0.028
6	S10	41.288	1.590	41.765	13.976	1422.04	1241.64	1275.465	0.029	0.034	0.033
	S3	66.895	57.064	84.014	77.132	1052.44	951.64	970.54	0.080	0.088	0.087
	S11	6.696	39.707	18.608	41.716	1540.392	1343.592	1380.492	0.027	0.031	0.030
	S4	17.505	42.168	30.156	47.420	982.64	887.136	905.043	0.048	0.053	0.052
	S12	26.084	26.266	33.964	34.092	1213.972	1060.572	1089.3345	0.028	0.032	0.031
5	S10	50.982	2.973	51.874	18.267	1777.55	1552.05	1585.875	0.029	0.033	0.033
	S3	82.813	72.719	104.629	97.563	1315.55	1189.55	1208.45	0.080	0.088	0.087
	S11	8.089	55.278	24.673	57.704	1925.49	1679.49	1716.39	0.030	0.034	0.034
	S4	23.755	55.613	40.439	62.740	1228.3	1108.92	1126.827	0.051	0.057	0.056
	S12	34.302	37.906	45.674	48.197	1517.465	1325.715	1354.4775	0.032	0.036	0.036
4	S10	59.709	9.175	62.462	27.088	2133.06	1862.46	1918.835	0.029	0.034	0.033
	S3	97.667	87.863	124.026	117.163	1578.66	1427.46	1458.96	0.079	0.087	0.085
	S11	9.210	71.779	30.743	74.542	2310.588	2015.388	2076.888	0.032	0.037	0.036
	S4	28.251	68.762	48.880	77.237	1473.96	1330.704	1360.549	0.052	0.058	0.057
	S12	42.657	51.559	58.124	64.356	1820.958	1590.858	1638.7955	0.035	0.040	0.039
3	S10	65.393	16.412	70.317	36.030	2488.57	2172.87	2274.345	0.028	0.032	0.031
	S3	109.513	102.564	140.282	135.417	1841.77	1665.37	1722.07	0.076	0.084	0.081
	S11	10.092	88.977	36.785	92.005	2695.686	2351.286	2461.986	0.034	0.039	0.037
	S4	32.879	81.321	57.275	91.184	1719.62	1552.488	1606.209	0.053	0.059	0.057
	S12	48.880	65.024	68.387	79.688	2124.451	1856.001	1942.2885	0.038	0.043	0.041
2	S10	69.366	23.202	76.327	44.012	2844.08	2483.28	2629.855	0.027	0.031	0.029
	S3	117.784	115.281	152.368	150.616	2104.88	1903.28	1985.18	0.072	0.080	0.077
	S11	10.645	103.680	41.749	106.874	3080.784	2687.184	2847.084	0.035	0.040	0.038
	S4	37.526	92.293	65.213	103.550	1965.28	1774.272	1851.869	0.053	0.058	0.056
	S12	53.653	76.633	76.643	92.729	2427.944	2121.144	2245.7815	0.038	0.044	0.041
1	S10	71.948	29.872	80.910	51.457	3199.59	2793.69	2985.365	0.025	0.029	0.027
	S3	122.158	124.129	159.396	160.776	2367.99	2141.19	2248.29	0.068	0.075	0.072
	S11	10.922	113.954	45.108	117.230	3465.882	3023.082	3232.182	0.034	0.039	0.036
	S4	40.540	100.237	70.611	112.399	2210.94	1996.056	2097.529	0.051	0.056	0.054
	S12	57.980	85.974	83.772	103.368	2731.437	2386.287	2549.2745	0.038	0.043	0.041

Çizelge B.115: 12 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	9.746	4.637	11.137	7.560	355.51	310.41	310.41	0.031	0.036	0.036
	S3	21.613	15.405	26.235	21.889	263.11	237.91	237.91	0.100	0.110	0.110
	S11	2.551	6.580	4.525	7.345	385.098	335.898	335.898	0.019	0.022	0.022
	S4	3.692	9.443	6.524	10.550	245.66	221.784	221.784	0.043	0.048	0.048
	S12	5.103	2.118	5.738	3.649	303.493	265.143	265.143	0.019	0.022	0.022
11	S10	24.437	4.309	25.730	11.640	711.02	620.82	620.82	0.036	0.041	0.041
	S3	44.061	37.382	55.275	50.600	526.22	475.82	475.82	0.105	0.116	0.116
	S11	5.768	19.433	11.598	21.163	770.196	671.796	671.796	0.027	0.032	0.032
	S4	7.852	25.862	15.611	28.218	491.32	443.568	443.568	0.057	0.064	0.064
	S12	14.118	10.718	17.333	14.953	606.986	530.286	530.286	0.029	0.033	0.033
10	S10	39.759	4.775	41.192	16.703	1066.53	931.23	931.23	0.039	0.044	0.044
	S3	67.254	59.590	85.130	79.766	789.33	713.73	713.73	0.108	0.119	0.119
	S11	8.698	32.616	18.482	35.225	1155.294	1007.694	1007.694	0.030	0.035	0.035
	S4	12.755	42.426	25.483	46.252	736.98	665.352	665.352	0.063	0.070	0.070
	S12	23.290	19.594	29.168	26.581	910.479	795.429	795.429	0.032	0.037	0.037
9	S10	53.779	1.198	54.139	17.332	1422.04	1241.64	1185.265	0.038	0.044	0.046
	S3	90.434	82.720	115.250	109.851	1052.44	951.64	920.14	0.110	0.121	0.125
	S11	11.557	50.102	26.587	53.569	1540.392	1343.592	1282.092	0.035	0.040	0.042
	S4	19.012	60.702	37.223	66.405	982.64	887.136	857.291	0.068	0.075	0.077
	S12	33.688	32.229	43.357	42.335	1213.972	1060.572	1012.6345	0.036	0.041	0.043
8	S10	66.753	5.459	68.391	25.485	1777.55	1552.05	1450.575	0.038	0.044	0.047
	S3	113.406	106.611	145.389	140.632	1315.55	1189.55	1132.85	0.111	0.122	0.128
	S11	14.148	71.101	35.479	75.345	1925.49	1679.49	1568.79	0.039	0.045	0.048
	S4	27.031	80.548	51.195	88.657	1228.3	1108.92	1055.199	0.072	0.080	0.084
	S12	45.057	47.693	59.365	61.210	1517.465	1325.715	1239.4275	0.040	0.046	0.049
7	S10	78.919	15.013	83.423	38.689	2133.06	1862.46	1715.885	0.039	0.045	0.049
	S3	136.382	131.108	175.714	172.022	1578.66	1427.46	1345.56	0.111	0.123	0.131
	S11	16.418	94.683	44.823	99.608	2310.588	2015.388	1855.488	0.043	0.049	0.054
	S4	32.694	100.858	62.951	110.666	1473.96	1330.704	1253.107	0.075	0.083	0.088
	S12	57.564	67.218	77.729	84.487	1820.958	1590.858	1466.2205	0.046	0.053	0.058
6	S10	86.774	26.564	94.743	52.596	2488.57	2172.87	2003.745	0.038	0.044	0.047
	S3	156.632	157.299	203.822	204.288	1841.77	1665.37	1570.87	0.111	0.123	0.130
	S11	18.424	121.638	54.915	127.165	2695.686	2351.286	2166.786	0.047	0.054	0.059
	S4	39.758	121.963	76.347	133.891	1719.62	1552.488	1462.953	0.078	0.086	0.092
	S12	67.151	87.745	93.475	107.890	2124.451	1856.001	1712.1885	0.051	0.058	0.063
5	S10	93.252	39.311	105.046	67.287	2844.08	2483.28	2314.155	0.037	0.042	0.045
	S3	174.127	183.514	229.181	235.752	2104.88	1903.28	1808.78	0.112	0.124	0.130
	S11	20.068	148.024	64.475	154.044	3080.784	2687.184	2502.684	0.050	0.057	0.062
	S4	47.820	143.149	90.765	157.495	1965.28	1774.272	1684.737	0.080	0.089	0.093
	S12	76.526	108.789	109.162	131.747	2427.944	2121.144	1977.3315	0.054	0.062	0.067
4	S10	99.839	52.816	115.684	82.768	3199.59	2793.69	2647.115	0.036	0.041	0.044
	S3	189.030	208.164	251.479	264.873	2367.99	2141.19	2059.29	0.112	0.124	0.129
	S11	21.366	172.181	73.020	178.591	3465.882	3023.082	2863.182	0.052	0.059	0.062
	S4	55.747	163.091	104.674	179.815	2210.94	1996.056	1918.459	0.081	0.090	0.094
	S12	87.161	130.350	126.266	156.498	2731.437	2386.287	2261.6495	0.057	0.066	0.069
3	S10	105.330	65.348	124.934	96.947	3555.1	3104.1	3002.625	0.035	0.040	0.042
	S3	200.760	230.183	269.815	290.411	2631.1	2379.1	2322.4	0.110	0.122	0.125
	S11	22.307	194.224	80.574	200.916	3850.98	3358.98	3248.28	0.052	0.060	0.062
	S4	63.486	180.686	117.691	199.731	2456.6	2217.84	2164.119	0.081	0.090	0.092
	S12	96.377	150.042	141.389	178.955	3034.93	2651.43	2565.1425	0.059	0.067	0.070
2	S10	109.454	76.857	132.511	109.693	3910.61	3414.51	3358.135	0.034	0.039	0.039
	S3	209.087	247.896	283.456	310.622	2894.21	2617.01	2585.51	0.107	0.119	0.120
	S11	22.898	212.598	86.677	219.467	4236.078	3694.878	3633.378	0.052	0.059	0.060

1	S4	69.974	195.260	128.552	216.252	2702.26	2439.624	2409.779	0.080	0.089	0.090
	S12	104.256	167.282	154.440	198.559	3338.423	2916.573	2868.6355	0.059	0.068	0.069
	S10	111.921	85.645	137.615	119.221	4266.12	3724.92	3713.645	0.032	0.037	0.037
	S3	212.779	259.664	290.678	323.498	3157.32	2854.92	2848.62	0.102	0.113	0.114
	S11	23.146	224.631	90.535	231.574	4621.176	4030.776	4018.476	0.050	0.057	0.058
	S4	75.263	205.325	136.861	227.904	2947.92	2661.408	2655.439	0.077	0.086	0.086
	S12	109.745	178.530	163.304	211.454	3641.916	3181.716	3172.1285	0.058	0.066	0.067

Çizelge B.116: 6 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	8.416	4.025	9.624	6.550	355.51	332.96	287.86	0.027	0.029	0.033
	S3	17.128	11.764	20.657	16.902	263.11	250.51	225.31	0.079	0.082	0.092
	S11	1.047	7.278	3.230	7.592	385.098	360.498	311.298	0.020	0.021	0.024
	S4	4.867	7.288	7.053	8.748	245.66	233.722	209.846	0.036	0.037	0.042
	S12	4.736	3.425	5.764	4.846	303.493	284.318	245.968	0.019	0.020	0.023
5	S10	20.796	4.263	22.075	10.501	711.02	665.92	598.27	0.031	0.033	0.037
	S3	33.505	27.329	41.703	37.380	526.22	501.02	463.22	0.079	0.083	0.090
	S11	2.253	20.085	8.279	20.761	770.196	720.996	647.196	0.027	0.029	0.032
	S4	9.782	20.484	15.927	23.419	491.32	467.444	431.63	0.048	0.050	0.054
	S12	12.168	12.715	15.982	16.366	606.986	568.636	511.111	0.027	0.029	0.032
4	S10	33.203	4.840	34.655	14.801	1066.53	998.88	931.23	0.032	0.035	0.037
	S3	49.705	42.743	62.527	57.654	789.33	751.53	713.73	0.079	0.083	0.088
	S11	3.228	33.023	13.135	33.991	1155.294	1081.494	1007.694	0.029	0.031	0.034
	S4	15.073	33.744	25.196	38.266	736.98	701.166	665.352	0.052	0.055	0.058
	S12	19.479	22.226	26.147	28.070	910.479	852.954	795.429	0.031	0.033	0.035
3	S10	44.135	2.213	44.799	15.453	1422.04	1331.84	1286.74	0.032	0.034	0.035
	S3	64.349	57.607	81.631	76.911	1052.44	1002.04	976.84	0.078	0.081	0.084
	S11	4.095	48.429	18.624	49.658	1540.392	1441.992	1392.792	0.032	0.034	0.036
	S4	20.668	47.501	34.918	53.701	982.64	934.888	911.012	0.055	0.057	0.059
	S12	26.994	34.096	37.223	42.194	1213.972	1137.272	1098.922	0.035	0.037	0.038
2	S10	52.791	2.882	53.656	18.719	1777.55	1664.8	1642.25	0.030	0.032	0.033
	S3	76.056	70.738	97.277	93.555	1315.55	1252.55	1239.95	0.074	0.078	0.078
	S11	4.729	64.436	24.060	65.855	1925.49	1802.49	1777.89	0.034	0.037	0.037
	S4	26.145	60.674	44.347	68.517	1228.3	1168.61	1156.672	0.056	0.059	0.059
	S12	33.980	46.770	48.011	56.964	1517.465	1421.59	1402.415	0.038	0.040	0.041
1	S10	58.394	9.060	61.112	26.578	2133.06	1997.76	1997.76	0.029	0.031	0.031
	S3	83.201	80.719	107.416	105.679	1578.66	1503.06	1503.06	0.068	0.071	0.071
	S11	5.024	77.700	28.334	79.207	2310.588	2162.988	2162.988	0.034	0.037	0.037
	S4	29.218	70.911	50.491	79.676	1473.96	1402.332	1402.332	0.054	0.057	0.057
	S12	39.337	57.789	56.674	69.590	1820.958	1705.908	1705.908	0.038	0.041	0.041

Çizelge B.117: 9 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	12.908	5.894	14.677	9.767	355.51	310.41	254.035	0.041	0.047	0.058
	S3	27.767	18.477	33.311	26.808	263.11	237.91	206.41	0.127	0.140	0.161
	S11	2.583	9.492	5.431	10.267	385.098	335.898	274.398	0.027	0.031	0.037
	S4	6.319	10.974	9.611	12.870	245.66	221.784	191.939	0.052	0.058	0.067
	S12	7.170	3.739	8.292	5.890	303.493	265.143	217.2055	0.027	0.031	0.038
8	S10	32.116	5.877	33.879	15.511	711.02	620.82	519.345	0.048	0.055	0.065
	S3	56.127	44.271	69.408	61.109	526.22	475.82	419.12	0.132	0.146	0.166
	S11	5.789	26.858	13.846	28.594	770.196	671.796	561.096	0.037	0.043	0.051
	S4	13.070	30.437	22.201	34.358	491.32	443.568	389.847	0.070	0.077	0.088
	S12	19.049	15.633	23.739	21.348	606.986	530.286	443.9985	0.039	0.045	0.053
7	S10	51.913	6.721	53.930	22.295	1066.53	931.23	987.605	0.051	0.058	0.055
	S3	85.104	70.223	106.171	95.754	789.33	713.73	745.23	0.135	0.149	0.142
	S11	8.635	44.610	22.018	47.200	1155.294	1007.694	1069.194	0.041	0.047	0.044
	S4	20.684	50.082	35.708	56.288	736.98	665.352	695.197	0.076	0.085	0.081
	S12	31.026	27.883	39.391	37.191	910.479	795.429	843.3665	0.043	0.050	0.047
6	S10	70.036	2.697	70.845	23.707	1422.04	1241.64	1275.465	0.050	0.057	0.056
	S3	113.471	96.795	142.510	130.837	1052.44	951.64	970.54	0.135	0.150	0.147
	S11	11.359	67.353	31.565	70.760	1540.392	1343.592	1380.492	0.046	0.053	0.051
	S4	29.694	71.528	51.152	80.436	982.64	887.136	905.043	0.082	0.091	0.089
	S12	44.245	44.555	57.611	57.828	1213.972	1060.572	1089.3345	0.048	0.055	0.053
5	S10	86.479	5.043	87.991	30.986	1777.55	1552.05	1585.875	0.050	0.057	0.055
	S3	140.473	123.350	177.478	165.491	1315.55	1189.55	1208.45	0.135	0.149	0.147
	S11	13.722	93.765	41.851	97.882	1925.49	1679.49	1716.39	0.051	0.058	0.057
	S4	40.294	94.335	68.595	106.423	1228.3	1108.92	1126.827	0.087	0.096	0.094
	S12	58.186	64.299	77.475	81.755	1517.465	1325.715	1354.4775	0.054	0.062	0.060
4	S10	101.282	15.563	105.951	45.947	2133.06	1862.46	1918.835	0.050	0.057	0.055
	S3	165.669	149.038	210.381	198.739	1578.66	1427.46	1458.96	0.133	0.147	0.144
	S11	15.622	121.756	52.149	126.443	2310.588	2015.388	2076.888	0.055	0.063	0.061
	S4	47.921	116.638	82.913	131.015	1473.96	1330.704	1360.549	0.089	0.098	0.096
	S12	72.357	87.458	98.594	109.165	1820.958	1590.858	1638.7955	0.060	0.069	0.067
3	S10	110.924	27.839	119.275	61.116	2488.57	2172.87	2274.345	0.048	0.055	0.052
	S3	185.762	173.975	237.955	229.703	1841.77	1665.37	1722.07	0.129	0.143	0.138
	S11	17.119	150.928	62.397	156.064	2695.686	2351.286	2461.986	0.058	0.066	0.063
	S4	55.772	137.941	97.154	154.673	1719.62	1552.488	1606.209	0.090	0.100	0.096
	S12	82.912	110.297	116.002	135.171	2124.451	1856.001	1942.2885	0.064	0.073	0.070
2	S10	117.663	39.357	129.470	74.656	2844.08	2483.28	2629.855	0.046	0.052	0.049
	S3	199.792	195.546	258.456	255.484	2104.88	1903.28	1985.18	0.123	0.136	0.130
	S11	18.056	175.869	70.817	181.286	3080.784	2687.184	2847.084	0.059	0.067	0.064
	S4	63.653	156.553	110.619	175.649	1965.28	1774.272	1851.869	0.089	0.099	0.095
	S12	91.010	129.989	130.006	157.292	2427.944	2121.144	2245.7815	0.065	0.074	0.070
1	S10	122.043	50.671	137.245	87.284	3199.59	2793.69	2985.365	0.043	0.049	0.046
	S3	207.211	210.555	270.378	272.718	2367.99	2141.19	2248.29	0.115	0.127	0.121
	S11	18.527	193.295	76.516	198.853	3465.882	3023.082	3232.182	0.057	0.066	0.062
	S4	68.766	170.027	119.775	190.657	2210.94	1996.056	2097.529	0.086	0.096	0.091
	S12	98.349	145.835	142.100	175.340	2731.437	2386.287	2549.2745	0.064	0.073	0.069

Çizelge B.118: 12 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	16.531	7.865	18.891	12.824	355.51	310.41	310.41	0.053	0.061	0.061
	S3	36.662	26.131	44.501	37.129	263.11	237.91	237.91	0.169	0.187	0.187
	S11	4.327	11.161	7.675	12.459	385.098	335.898	335.898	0.032	0.037	0.037
	S4	6.262	16.018	11.067	17.896	245.66	221.784	221.784	0.073	0.081	0.081
	S12	8.656	3.592	9.734	6.189	303.493	265.143	265.143	0.032	0.037	0.037
11	S10	41.452	7.310	43.645	19.745	711.02	620.82	620.82	0.061	0.070	0.070
	S3	74.738	63.409	93.761	85.831	526.22	475.82	475.82	0.178	0.197	0.197
	S11	9.783	32.964	19.672	35.899	770.196	671.796	671.796	0.047	0.053	0.053
	S4	13.319	43.869	26.480	47.865	491.32	443.568	443.568	0.097	0.108	0.108
	S12	23.947	18.180	29.401	25.364	606.986	530.286	530.286	0.048	0.055	0.055
10	S10	67.442	8.100	69.872	28.332	1066.53	931.23	931.23	0.066	0.075	0.075
	S3	114.080	101.080	144.403	135.303	789.33	713.73	713.73	0.183	0.202	0.202
	S11	14.753	55.325	31.351	59.751	1155.294	1007.694	1007.694	0.052	0.059	0.059
	S4	21.637	71.965	43.226	78.456	736.98	665.352	665.352	0.106	0.118	0.118
	S12	39.505	33.237	49.476	45.088	910.479	795.429	795.429	0.054	0.062	0.062
9	S10	91.224	2.032	91.833	29.399	1422.04	1241.64	1185.265	0.065	0.074	0.077
	S3	153.400	140.315	195.495	186.335	1052.44	951.64	920.14	0.186	0.205	0.212
	S11	19.603	84.985	45.099	90.866	1540.392	1343.592	1282.092	0.059	0.068	0.071
	S4	32.250	102.966	63.140	112.641	982.64	887.136	857.291	0.115	0.127	0.131
	S12	57.144	54.668	73.545	71.812	1213.972	1060.572	1012.6345	0.061	0.069	0.073
8	S10	113.231	9.259	116.009	43.229	1777.55	1552.05	1450.575	0.065	0.075	0.080
	S3	192.366	180.839	246.618	238.549	1315.55	1189.55	1132.85	0.187	0.207	0.218
	S11	23.999	120.605	60.181	127.805	1925.49	1679.49	1568.79	0.066	0.076	0.081
	S4	45.851	136.630	86.840	150.385	1228.3	1108.92	1055.199	0.122	0.136	0.143
	S12	76.429	80.900	100.699	103.828	1517.465	1325.715	1239.4275	0.068	0.078	0.084
7	S10	133.867	25.467	141.507	65.627	2133.06	1862.46	1715.885	0.066	0.076	0.082
	S3	231.339	222.393	298.057	291.795	1578.66	1427.46	1345.56	0.189	0.209	0.222
	S11	27.849	160.607	76.031	168.962	2310.588	2015.388	1855.488	0.073	0.084	0.091
	S4	55.457	171.081	106.782	187.718	1473.96	1330.704	1253.107	0.127	0.141	0.150
	S12	97.644	114.019	131.849	143.312	1820.958	1590.858	1466.2205	0.079	0.090	0.098
6	S10	147.191	45.060	160.709	89.217	2488.57	2172.87	2003.745	0.065	0.074	0.080
	S3	265.689	266.820	345.735	346.526	1841.77	1665.37	1570.87	0.188	0.208	0.221
	S11	31.252	206.329	93.151	215.705	2695.686	2351.286	2166.786	0.080	0.092	0.100
	S4	67.440	206.882	129.505	227.114	1719.62	1552.488	1462.953	0.132	0.146	0.155
	S12	113.906	148.838	158.557	183.010	2124.451	1856.001	1712.1885	0.086	0.099	0.107
5	S10	158.180	66.682	178.185	114.136	2844.08	2483.28	2314.155	0.063	0.072	0.077
	S3	295.364	311.288	388.750	399.897	2104.88	1903.28	1808.78	0.190	0.210	0.221
	S11	34.040	251.088	109.367	261.300	3080.784	2687.184	2502.684	0.085	0.097	0.104
	S4	81.116	242.819	153.961	267.153	1965.28	1774.272	1684.737	0.136	0.151	0.159
	S12	129.808	184.534	185.168	223.477	2427.944	2121.144	1977.3315	0.092	0.105	0.113
4	S10	169.353	89.590	196.230	140.396	3199.59	2793.69	2647.115	0.061	0.070	0.074
	S3	320.644	353.101	426.574	449.294	2367.99	2141.19	2059.29	0.190	0.210	0.218
	S11	36.242	292.064	123.861	302.936	3465.882	3023.082	2863.182	0.087	0.100	0.106
	S4	94.561	276.644	177.554	305.013	2210.94	1996.056	1918.459	0.138	0.153	0.159
	S12	147.848	221.108	214.180	265.462	2731.437	2386.287	2261.6495	0.097	0.111	0.117
3	S10	178.667	110.847	211.921	164.447	3555.1	3104.1	3002.625	0.060	0.068	0.071
	S3	340.541	390.451	457.676	492.613	2631.1	2379.1	2322.4	0.187	0.207	0.212
	S11	37.839	329.455	136.675	340.806	3850.98	3358.98	3248.28	0.088	0.101	0.105
	S4	107.688	306.490	199.635	338.796	2456.6	2217.84	2164.119	0.138	0.153	0.157
	S12	163.480	254.510	239.833	303.554	3034.93	2651.43	2565.1425	0.100	0.114	0.118
2	S10	185.662	130.369	224.773	186.068	3910.61	3414.51	3358.135	0.057	0.066	0.067
	S3	354.666	420.497	480.815	526.896	2894.21	2617.01	2585.51	0.182	0.201	0.204
	S11	38.840	360.622	147.027	372.274	4236.078	3694.878	3633.378	0.088	0.101	0.102

1	S4	118.694	331.212	218.058	366.821	2702.26	2439.624	2409.779	0.136	0.150	0.152
	S12	176.845	283.755	261.971	336.808	3338.423	2916.573	2868.6355	0.101	0.115	0.117
	S10	189.848	145.276	233.430	202.230	4266.12	3724.92	3713.645	0.055	0.063	0.063
	S3	360.929	440.459	493.067	548.738	3157.32	2854.92	2848.62	0.174	0.192	0.193
	S11	39.262	381.032	153.572	392.811	4621.176	4030.776	4018.476	0.085	0.097	0.098
	S4	127.666	348.285	232.152	386.585	2947.92	2661.408	2655.439	0.131	0.145	0.146
	S12	186.156	302.834	277.006	358.681	3641.916	3181.716	3172.1285	0.098	0.113	0.113

Çizelge B.119: 6 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	3.8733	2.0164	4.478	3.178	355.51	332.96	287.86	0.013	0.013	0.016
	S3	7.8823	5.8928	9.650	8.257	263.11	250.51	225.31	0.037	0.039	0.043
	S11	0.4819	3.6457	1.576	3.790	385.098	360.498	311.298	0.010	0.011	0.012
	S4	2.2397	3.6508	3.335	4.323	245.66	233.722	209.846	0.018	0.018	0.021
	S12	2.1797	1.7156	2.694	2.370	303.493	284.318	245.968	0.009	0.009	0.011
5	S10	9.5705	2.1353	10.211	5.006	711.02	665.92	598.27	0.014	0.015	0.017
	S3	15.4193	13.6897	19.526	18.315	526.22	501.02	463.22	0.037	0.039	0.042
	S11	1.037	10.0613	4.055	10.372	770.196	720.996	647.196	0.013	0.014	0.016
	S4	4.5018	10.2613	7.580	11.612	491.32	467.444	431.63	0.024	0.025	0.027
	S12	5.5999	6.3695	7.511	8.049	606.986	568.636	511.111	0.013	0.014	0.016
4	S10	15.2806	2.4243	16.008	7.008	1066.53	998.88	931.23	0.015	0.016	0.017
	S3	22.8748	21.4111	29.298	28.274	789.33	751.53	713.73	0.037	0.039	0.041
	S11	1.4857	16.5421	6.448	16.988	1155.294	1081.494	1007.694	0.015	0.016	0.017
	S4	6.9369	16.9034	12.008	18.984	736.98	701.166	665.352	0.026	0.027	0.029
	S12	8.9647	11.1336	12.305	13.823	910.479	852.954	795.429	0.015	0.016	0.017
3	S10	20.3116	1.1085	20.644	7.202	1422.04	1331.84	1286.74	0.015	0.016	0.016
	S3	29.6142	28.8571	38.271	37.741	1052.44	1002.04	976.84	0.036	0.038	0.039
	S11	1.8845	24.2598	9.162	24.825	1540.392	1441.992	1392.792	0.016	0.017	0.018
	S4	9.5115	23.7946	16.650	26.648	982.64	934.888	911.012	0.027	0.029	0.029
	S12	12.423	17.0798	17.547	20.807	1213.972	1137.272	1098.922	0.017	0.018	0.019
2	S10	24.2953	1.4435	24.728	8.732	1777.55	1664.8	1642.25	0.014	0.015	0.015
	S3	35.0019	35.4351	45.632	45.936	1315.55	1252.55	1239.95	0.035	0.037	0.037
	S11	2.1763	32.2783	11.860	32.931	1925.49	1802.49	1777.89	0.017	0.018	0.019
	S4	12.0321	30.3936	21.150	34.003	1228.3	1168.61	1156.672	0.028	0.029	0.029
	S12	15.6382	23.4285	22.667	28.120	1517.465	1421.59	1402.415	0.019	0.020	0.020
1	S10	26.8736	4.5384	28.235	12.600	2133.06	1997.76	1997.76	0.013	0.014	0.014
	S3	38.29	40.4347	50.420	51.922	1578.66	1503.06	1503.06	0.033	0.035	0.035
	S11	2.3122	38.9223	13.989	39.616	2310.588	2162.988	2162.988	0.017	0.018	0.018
	S4	13.4463	35.5214	24.103	39.555	1473.96	1402.332	1402.332	0.027	0.028	0.028
	S12	18.1035	28.9483	26.788	34.379	1820.958	1705.908	1705.908	0.019	0.020	0.020

Çizelge B.120: 9 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	5.425	2.477	6.168	4.105	355.51	310.41	254.035	0.017	0.020	0.024
	S3	11.669	7.765	13.999	11.266	263.11	237.91	206.41	0.053	0.059	0.068
	S11	1.086	3.989	2.282	4.315	385.098	335.898	274.398	0.011	0.013	0.016
	S4	2.655	4.612	4.039	5.408	245.66	221.784	191.939	0.022	0.024	0.028
	S12	3.013	1.571	3.485	2.475	303.493	265.143	217.2055	0.011	0.013	0.016
8	S10	13.497	2.470	14.238	6.519	711.02	620.82	519.345	0.020	0.023	0.027
	S3	23.587	18.605	29.169	25.681	526.22	475.82	419.12	0.055	0.061	0.070
	S11	2.433	11.287	5.819	12.017	770.196	671.796	561.096	0.016	0.018	0.021
	S4	5.493	12.791	9.330	14.439	491.32	443.568	389.847	0.029	0.033	0.037
	S12	8.006	6.570	9.976	8.972	606.986	530.286	443.9985	0.016	0.019	0.022
7	S10	21.816	2.825	22.664	9.370	1066.53	931.23	987.605	0.021	0.024	0.023
	S3	35.765	29.511	44.618	40.241	789.33	713.73	745.23	0.057	0.063	0.060
	S11	3.629	18.747	9.253	19.836	1155.294	1007.694	1069.194	0.017	0.020	0.019
	S4	8.692	21.047	15.006	23.655	736.98	665.352	695.197	0.032	0.036	0.034
	S12	13.039	11.718	16.554	15.629	910.479	795.429	843.3665	0.018	0.021	0.020
6	S10	29.432	1.133	29.772	9.963	1422.04	1241.64	1275.465	0.021	0.024	0.023
	S3	47.686	40.678	59.889	54.984	1052.44	951.64	970.54	0.057	0.063	0.062
	S11	4.774	28.305	13.265	29.737	1540.392	1343.592	1380.492	0.019	0.022	0.022
	S4	12.479	30.060	21.497	33.803	982.64	887.136	905.043	0.034	0.038	0.037
	S12	18.594	18.724	24.211	24.302	1213.972	1060.572	1089.3345	0.020	0.023	0.022
5	S10	36.342	2.119	36.978	13.022	1777.55	1552.05	1585.875	0.021	0.024	0.023
	S3	59.034	51.837	74.585	69.547	1315.55	1189.55	1208.45	0.057	0.063	0.062
	S11	5.767	39.405	17.588	41.135	1925.49	1679.49	1716.39	0.021	0.024	0.024
	S4	16.934	39.644	28.827	44.724	1228.3	1108.92	1126.827	0.036	0.040	0.040
	S12	24.452	27.022	32.559	34.357	1517.465	1325.715	1354.4775	0.023	0.026	0.025
4	S10	42.564	6.540	44.526	19.309	2133.06	1862.46	1918.835	0.021	0.024	0.023
	S3	69.622	62.633	88.412	83.519	1578.66	1427.46	1458.96	0.056	0.062	0.061
	S11	6.565	51.168	21.915	53.137	2310.588	2015.388	2076.888	0.023	0.026	0.026
	S4	20.139	49.017	34.844	55.059	1473.96	1330.704	1360.549	0.037	0.041	0.040
	S12	30.408	36.754	41.434	45.876	1820.958	1590.858	1638.7955	0.025	0.029	0.028
3	S10	46.615	11.699	50.125	25.684	2488.57	2172.87	2274.345	0.020	0.023	0.022
	S3	78.066	73.112	100.000	96.532	1841.77	1665.37	1722.07	0.054	0.060	0.058
	S11	7.194	63.427	26.222	65.585	2695.686	2351.286	2461.986	0.024	0.028	0.027
	S4	23.438	57.969	40.829	65.001	1719.62	1552.488	1606.209	0.038	0.042	0.040
	S12	34.844	46.352	48.749	56.805	2124.451	1856.001	1942.2885	0.027	0.031	0.029
2	S10	49.448	16.540	54.409	31.374	2844.08	2483.28	2629.855	0.019	0.022	0.021
	S3	83.962	82.178	108.615	107.366	2104.88	1903.28	1985.18	0.052	0.057	0.055
	S11	7.588	73.909	29.761	76.185	3080.784	2687.184	2847.084	0.025	0.028	0.027
	S4	26.750	65.791	46.487	73.816	1965.28	1774.272	1851.869	0.038	0.042	0.040
	S12	38.247	54.628	54.635	66.102	2427.944	2121.144	2245.7815	0.027	0.031	0.029
1	S10	51.288	21.294	57.677	36.681	3199.59	2793.69	2985.365	0.018	0.021	0.019
	S3	87.080	88.485	113.626	114.609	2367.99	2141.19	2248.29	0.048	0.054	0.051
	S11	7.786	81.232	32.155	83.568	3465.882	3023.082	3232.182	0.024	0.028	0.026
	S4	28.899	71.454	50.335	80.123	2210.94	1996.056	2097.529	0.036	0.040	0.038
	S12	41.331	61.287	59.717	73.686	2731.437	2386.287	2549.2745	0.027	0.031	0.029

Çizelge B.121: 12 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	8.435	4.013	9.639	6.543	355.51	310.41	310.41	0.027	0.031	0.031
	S3	18.706	13.333	22.706	18.944	263.11	237.91	237.91	0.086	0.095	0.095
	S11	2.208	5.695	3.916	6.357	385.098	335.898	335.898	0.017	0.019	0.019
	S4	3.195	8.173	5.647	9.131	245.66	221.784	221.784	0.037	0.041	0.041
	S12	4.417	1.833	4.966	3.158	303.493	265.143	265.143	0.016	0.019	0.019
11	S10	21.150	3.730	22.269	10.075	711.02	620.82	620.82	0.031	0.036	0.036
	S3	38.134	32.353	47.839	43.793	526.22	475.82	475.82	0.091	0.101	0.101
	S11	4.992	16.819	10.037	18.317	770.196	671.796	671.796	0.024	0.027	0.027
	S4	6.796	22.383	13.511	24.422	491.32	443.568	443.568	0.050	0.055	0.055
	S12	12.219	9.276	15.001	12.941	606.986	530.286	530.286	0.025	0.028	0.028
10	S10	34.411	4.133	35.651	14.456	1066.53	931.23	931.23	0.033	0.038	0.038
	S3	58.207	51.574	73.679	69.036	789.33	713.73	713.73	0.093	0.103	0.103
	S11	7.528	28.229	15.996	30.487	1155.294	1007.694	1007.694	0.026	0.030	0.030
	S4	11.040	36.719	22.055	40.030	736.98	665.352	665.352	0.054	0.060	0.060
	S12	20.157	16.958	25.244	23.005	910.479	795.429	795.429	0.028	0.032	0.032
9	S10	46.545	1.037	46.856	15.000	1422.04	1241.64	1185.265	0.033	0.038	0.040
	S3	78.269	71.593	99.747	95.074	1052.44	951.64	920.14	0.095	0.105	0.108
	S11	10.002	43.362	23.011	46.362	1540.392	1343.592	1282.092	0.030	0.035	0.036
	S4	16.455	52.536	32.216	57.473	982.64	887.136	857.291	0.058	0.065	0.067
	S12	29.157	27.893	37.525	36.640	1213.972	1060.572	1012.6345	0.031	0.035	0.037
8	S10	57.774	4.724	59.191	22.056	1777.55	1552.05	1450.575	0.033	0.038	0.041
	S3	98.151	92.269	125.831	121.714	1315.55	1189.55	1132.85	0.096	0.106	0.111
	S11	12.245	61.536	30.706	65.210	1925.49	1679.49	1568.79	0.034	0.039	0.042
	S4	23.395	69.713	44.308	76.731	1228.3	1108.92	1055.199	0.062	0.069	0.073
	S12	38.996	41.277	51.379	52.976	1517.465	1325.715	1239.4275	0.035	0.040	0.043
7	S10	68.303	12.994	72.201	33.485	2133.06	1862.46	1715.885	0.034	0.039	0.042
	S3	118.036	113.471	152.077	148.882	1578.66	1427.46	1345.56	0.096	0.107	0.113
	S11	14.209	81.946	38.793	86.209	2310.588	2015.388	1855.488	0.037	0.043	0.046
	S4	28.296	87.290	54.483	95.779	1473.96	1330.704	1253.107	0.065	0.072	0.076
	S12	49.821	58.176	67.273	73.122	1820.958	1590.858	1466.2205	0.040	0.046	0.050
6	S10	75.101	22.991	81.998	45.521	2488.57	2172.87	2003.745	0.033	0.038	0.041
	S3	135.562	136.139	176.403	176.807	1841.77	1665.37	1570.87	0.096	0.106	0.113
	S11	15.946	105.275	47.528	110.059	2695.686	2351.286	2166.786	0.041	0.047	0.051
	S4	34.410	105.557	66.077	115.880	1719.62	1552.488	1462.953	0.067	0.075	0.079
	S12	58.118	75.941	80.900	93.377	2124.451	1856.001	1712.1885	0.044	0.050	0.055
5	S10	80.708	34.023	90.915	58.236	2844.08	2483.28	2314.155	0.032	0.037	0.039
	S3	150.703	158.828	198.351	204.039	2104.88	1903.28	1808.78	0.097	0.107	0.113
	S11	17.368	128.112	55.802	133.322	3080.784	2687.184	2502.684	0.043	0.050	0.053
	S4	41.387	123.893	78.555	136.309	1965.28	1774.272	1684.737	0.069	0.077	0.081
	S12	66.232	94.155	94.478	114.024	2427.944	2121.144	1977.3315	0.047	0.054	0.058
4	S10	86.409	45.712	100.122	71.634	3199.59	2793.69	2647.115	0.031	0.036	0.038
	S3	163.602	180.162	217.650	229.242	2367.99	2141.19	2059.29	0.097	0.107	0.111
	S11	18.491	149.019	63.197	154.567	3465.882	3023.082	2863.182	0.045	0.051	0.054
	S4	48.248	141.152	90.593	155.626	2210.94	1996.056	1918.459	0.070	0.078	0.081
	S12	75.436	112.815	109.281	135.446	2731.437	2386.287	2261.6495	0.050	0.057	0.060
3	S10	91.161	56.557	108.128	83.905	3555.1	3104.1	3002.625	0.030	0.035	0.036
	S3	173.754	199.219	233.519	251.345	2631.1	2379.1	2322.4	0.096	0.106	0.108
	S11	19.306	168.097	69.735	173.889	3850.98	3358.98	3248.28	0.045	0.052	0.054
	S4	54.946	156.380	101.860	172.863	2456.6	2217.84	2164.119	0.070	0.078	0.080
	S12	83.412	129.858	122.369	154.882	3034.93	2651.43	2565.1425	0.051	0.058	0.060
2	S10	94.730	66.518	114.685	94.937	3910.61	3414.51	3358.135	0.029	0.034	0.034
	S3	180.961	214.549	245.325	268.837	2894.21	2617.01	2585.51	0.093	0.103	0.104
	S11	19.818	183.999	75.017	189.944	4236.078	3694.878	3633.378	0.045	0.051	0.052

1	S4	60.561	168.994	111.259	187.162	2702.26	2439.624	2409.779	0.069	0.077	0.078
	S12	90.231	144.780	133.665	171.849	3338.423	2916.573	2868.6355	0.051	0.059	0.060
	S10	96.866	74.124	119.103	103.183	4266.12	3724.92	3713.645	0.028	0.032	0.032
	S3	184.156	224.734	251.576	279.981	3157.32	2854.92	2848.62	0.089	0.098	0.098
	S11	20.033	194.413	78.356	200.423	4621.176	4030.776	4018.476	0.043	0.050	0.050
	S4	65.139	177.705	118.450	197.247	2947.92	2661.408	2655.439	0.067	0.074	0.074
	S12	94.982	154.514	141.336	183.009	3641.916	3181.716	3172.1285	0.050	0.058	0.058

Çizelge B.122: 6 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	3.8733	2.0164	4.478	3.178	355.51	332.96	287.86	0.013	0.013	0.016
	S3	7.8823	5.8928	9.650	8.257	263.11	250.51	225.31	0.037	0.039	0.043
	S11	0.4819	3.6457	1.576	3.790	385.098	360.498	311.298	0.010	0.011	0.012
	S4	2.2397	3.6508	3.335	4.323	245.66	233.722	209.846	0.018	0.018	0.021
	S12	2.1797	1.7156	2.694	2.370	303.493	284.318	245.968	0.009	0.009	0.011
5	S10	9.5705	2.1353	10.211	5.006	711.02	665.92	598.27	0.014	0.015	0.017
	S3	15.4193	13.6897	19.526	18.315	526.22	501.02	463.22	0.037	0.039	0.042
	S11	1.037	10.0613	4.055	10.372	770.196	720.996	647.196	0.013	0.014	0.016
	S4	4.5018	10.2613	7.580	11.612	491.32	467.444	431.63	0.024	0.025	0.027
	S12	5.5999	6.3695	7.511	8.049	606.986	568.636	511.111	0.013	0.014	0.016
4	S10	15.2806	2.4243	16.008	7.008	1066.53	998.88	931.23	0.015	0.016	0.017
	S3	22.8748	21.4111	29.298	28.274	789.33	751.53	713.73	0.037	0.039	0.041
	S11	1.4857	16.5421	6.448	16.988	1155.294	1081.494	1007.694	0.015	0.016	0.017
	S4	6.9369	16.9034	12.008	18.984	736.98	701.166	665.352	0.026	0.027	0.029
	S12	8.9647	11.1336	12.305	13.823	910.479	852.954	795.429	0.015	0.016	0.017
3	S10	20.3116	1.1085	20.644	7.202	1422.04	1331.84	1286.74	0.015	0.016	0.016
	S3	29.6142	28.8571	38.271	37.741	1052.44	1002.04	976.84	0.036	0.038	0.039
	S11	1.8845	24.2598	9.162	24.825	1540.392	1441.992	1392.792	0.016	0.017	0.018
	S4	9.5115	23.7946	16.650	26.648	982.64	934.888	911.012	0.027	0.029	0.029
	S12	12.423	17.0798	17.547	20.807	1213.972	1137.272	1098.922	0.017	0.018	0.019
2	S10	24.2953	1.4435	24.728	8.732	1777.55	1664.8	1642.25	0.014	0.015	0.015
	S3	35.0019	35.4351	45.632	45.936	1315.55	1252.55	1239.95	0.035	0.037	0.037
	S11	2.1763	32.2783	11.860	32.931	1925.49	1802.49	1777.89	0.017	0.018	0.019
	S4	12.0321	30.3936	21.150	34.003	1228.3	1168.61	1156.672	0.028	0.029	0.029
	S12	15.6382	23.4285	22.667	28.120	1517.465	1421.59	1402.415	0.019	0.020	0.020
1	S10	26.8736	4.5384	28.235	12.600	2133.06	1997.76	1997.76	0.013	0.014	0.014
	S3	38.29	40.4347	50.420	51.922	1578.66	1503.06	1503.06	0.033	0.035	0.035
	S11	2.3122	38.9223	13.989	39.616	2310.588	2162.988	2162.988	0.017	0.018	0.018
	S4	13.4463	35.5214	24.103	39.555	1473.96	1402.332	1402.332	0.027	0.028	0.028
	S12	18.1035	28.9483	26.788	34.379	1820.958	1705.908	1705.908	0.019	0.020	0.020

Çizelge B.123: 9 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	5.972	2.727	6.790	4.518	355.51	310.41	254.035	0.019	0.022	0.027
	S3	12.845	8.548	15.410	12.401	263.11	237.91	206.41	0.059	0.065	0.075
	S11	1.195	4.391	2.512	4.750	385.098	335.898	274.398	0.012	0.014	0.017
	S4	2.923	5.077	4.446	5.954	245.66	221.784	191.939	0.024	0.027	0.031
	S12	3.317	1.730	3.836	2.725	303.493	265.143	217.2055	0.013	0.014	0.018
8	S10	14.857	2.719	15.673	7.176	711.02	620.82	519.345	0.022	0.025	0.030
	S3	25.965	20.480	32.109	28.269	526.22	475.82	419.12	0.061	0.067	0.077
	S11	2.678	12.425	6.405	13.228	770.196	671.796	561.096	0.017	0.020	0.024
	S4	6.046	14.080	10.270	15.894	491.32	443.568	389.847	0.032	0.036	0.041
	S12	8.812	7.232	10.982	9.876	606.986	530.286	443.9985	0.018	0.021	0.025
7	S10	24.016	3.109	24.948	10.314	1066.53	931.23	987.605	0.023	0.027	0.025
	S3	39.370	32.486	49.116	44.297	789.33	713.73	745.23	0.062	0.069	0.066
	S11	3.995	20.637	10.186	21.835	1155.294	1007.694	1069.194	0.019	0.022	0.020
	S4	9.569	23.169	16.519	26.039	736.98	665.352	695.197	0.035	0.039	0.037
	S12	14.353	12.899	18.223	17.205	910.479	795.429	843.3665	0.020	0.023	0.022
6	S10	32.399	1.247	32.773	10.967	1422.04	1241.64	1275.465	0.023	0.026	0.026
	S3	52.493	44.778	65.926	60.526	1052.44	951.64	970.54	0.063	0.069	0.068
	S11	5.255	31.158	14.602	32.734	1540.392	1343.592	1380.492	0.021	0.024	0.024
	S4	13.737	33.090	23.663	37.210	982.64	887.136	905.043	0.038	0.042	0.041
	S12	20.468	20.611	26.651	26.752	1213.972	1060.572	1089.3345	0.022	0.025	0.025
5	S10	40.006	2.333	40.705	14.335	1777.55	1552.05	1585.875	0.023	0.026	0.026
	S3	64.984	57.062	82.103	76.558	1315.55	1189.55	1208.45	0.062	0.069	0.068
	S11	6.348	43.376	19.361	45.281	1925.49	1679.49	1716.39	0.024	0.027	0.026
	S4	18.640	43.640	31.732	49.232	1228.3	1108.92	1126.827	0.040	0.044	0.044
	S12	26.917	29.745	35.841	37.820	1517.465	1325.715	1354.4775	0.025	0.029	0.028
4	S10	46.854	7.200	49.014	21.256	2133.06	1862.46	1918.835	0.023	0.026	0.026
	S3	76.640	68.946	97.324	91.938	1578.66	1427.46	1458.96	0.062	0.068	0.067
	S11	7.227	56.325	24.124	58.493	2310.588	2015.388	2076.888	0.025	0.029	0.028
	S4	22.169	53.958	38.356	60.608	1473.96	1330.704	1360.549	0.041	0.046	0.045
	S12	33.473	40.459	45.610	50.501	1820.958	1590.858	1638.7955	0.028	0.032	0.031
3	S10	51.314	12.878	55.178	28.273	2488.57	2172.87	2274.345	0.022	0.025	0.024
	S3	85.935	80.482	110.080	106.262	1841.77	1665.37	1722.07	0.060	0.066	0.064
	S11	7.919	69.821	28.865	72.196	2695.686	2351.286	2461.986	0.027	0.031	0.029
	S4	25.800	63.813	44.944	71.553	1719.62	1552.488	1606.209	0.042	0.046	0.045
	S12	38.356	51.024	53.663	62.531	2124.451	1856.001	1942.2885	0.029	0.034	0.032
2	S10	54.432	18.207	59.894	34.536	2844.08	2483.28	2629.855	0.021	0.024	0.023
	S3	92.425	90.461	119.564	118.189	2104.88	1903.28	1985.18	0.057	0.063	0.060
	S11	8.353	81.358	32.760	83.864	3080.784	2687.184	2847.084	0.027	0.031	0.029
	S4	29.446	72.423	51.173	81.256	1965.28	1774.272	1851.869	0.041	0.046	0.044
	S12	42.102	60.134	60.142	72.764	2427.944	2121.144	2245.7815	0.030	0.034	0.032
1	S10	56.458	23.441	63.490	40.378	3199.59	2793.69	2985.365	0.020	0.023	0.021
	S3	95.857	97.404	125.079	126.162	2367.99	2141.19	2248.29	0.053	0.059	0.056
	S11	8.571	89.420	35.397	91.991	3465.882	3023.082	3232.182	0.027	0.030	0.028
	S4	31.812	78.656	55.409	88.199	2210.94	1996.056	2097.529	0.040	0.044	0.042
	S12	45.497	67.464	65.736	81.114	2731.437	2386.287	2549.2745	0.030	0.034	0.032

Çizelge B.124: 12 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	9.489	4.514	10.843	7.361	355.51	310.41	310.41	0.031	0.035	0.035
	S3	21.044	14.999	25.544	21.312	263.11	237.91	237.91	0.097	0.107	0.107
	S11	2.484	6.407	4.406	7.152	385.098	335.898	335.898	0.019	0.021	0.021
	S4	3.594	9.194	6.353	10.272	245.66	221.784	221.784	0.042	0.046	0.046
	S12	4.969	2.062	5.587	3.553	303.493	265.143	265.143	0.018	0.021	0.021
11	S10	23.794	4.196	25.052	11.334	711.02	620.82	620.82	0.035	0.040	0.040
	S3	42.900	36.397	53.819	49.267	526.22	475.82	475.82	0.102	0.113	0.113
	S11	5.616	18.921	11.292	20.606	770.196	671.796	671.796	0.027	0.031	0.031
	S4	7.645	25.181	15.200	27.475	491.32	443.568	443.568	0.056	0.062	0.062
	S12	13.746	10.435	16.877	14.559	606.986	530.286	530.286	0.028	0.032	0.032
10	S10	38.712	4.649	40.107	16.263	1066.53	931.23	931.23	0.038	0.043	0.043
	S3	65.482	58.020	82.889	77.665	789.33	713.73	713.73	0.105	0.116	0.116
	S11	8.469	31.757	17.996	34.298	1155.294	1007.694	1007.694	0.030	0.034	0.034
	S4	12.420	41.308	24.812	45.034	736.98	665.352	665.352	0.061	0.068	0.068
	S12	22.676	19.078	28.400	25.881	910.479	795.429	795.429	0.031	0.036	0.036
9	S10	52.363	1.166	52.713	16.875	1422.04	1241.64	1185.265	0.037	0.042	0.044
	S3	88.053	80.542	112.215	106.958	1052.44	951.64	920.14	0.107	0.118	0.122
	S11	11.253	48.782	25.887	52.158	1540.392	1343.592	1282.092	0.034	0.039	0.041
	S4	18.512	59.103	36.242	64.657	982.64	887.136	857.291	0.066	0.073	0.075
	S12	32.801	31.380	42.215	41.220	1213.972	1060.572	1012.6345	0.035	0.040	0.042
8	S10	64.995	5.315	66.590	24.814	1777.55	1552.05	1450.575	0.037	0.043	0.046
	S3	110.419	103.803	141.560	136.929	1315.55	1189.55	1132.85	0.108	0.119	0.125
	S11	13.776	69.228	34.544	73.361	1925.49	1679.49	1568.79	0.038	0.044	0.047
	S4	26.319	78.427	49.847	86.322	1228.3	1108.92	1055.199	0.070	0.078	0.082
	S12	43.871	46.437	57.802	59.598	1517.465	1325.715	1239.4275	0.039	0.045	0.048
7	S10	76.841	14.618	81.226	37.670	2133.06	1862.46	1715.885	0.038	0.044	0.047
	S3	132.790	127.655	171.087	167.492	1578.66	1427.46	1345.56	0.108	0.120	0.127
	S11	15.985	92.190	43.642	96.985	2310.588	2015.388	1855.488	0.042	0.048	0.052
	S4	31.833	98.202	61.293	107.751	1473.96	1330.704	1253.107	0.073	0.081	0.086
	S12	56.048	65.448	75.682	82.262	1820.958	1590.858	1466.2205	0.045	0.052	0.056
6	S10	84.489	25.865	92.248	51.211	2488.57	2172.87	2003.745	0.037	0.042	0.046
	S3	152.507	153.156	198.454	198.908	1841.77	1665.37	1570.87	0.108	0.119	0.127
	S11	17.939	118.434	53.469	123.816	2695.686	2351.286	2166.786	0.046	0.053	0.057
	S4	38.711	118.751	74.337	130.365	1719.62	1552.488	1462.953	0.076	0.084	0.089
	S12	65.383	85.434	91.013	105.049	2124.451	1856.001	1712.1885	0.049	0.057	0.061
5	S10	90.796	38.276	102.279	65.515	2844.08	2483.28	2314.155	0.036	0.041	0.044
	S3	169.541	178.681	223.145	229.543	2104.88	1903.28	1808.78	0.109	0.121	0.127
	S11	19.539	144.126	62.777	149.988	3080.784	2687.184	2502.684	0.049	0.056	0.060
	S4	46.561	139.380	88.375	153.348	1965.28	1774.272	1684.737	0.078	0.086	0.091
	S12	74.511	105.924	106.288	128.277	2427.944	2121.144	1977.3315	0.053	0.060	0.065
4	S10	97.210	51.425	112.637	80.588	3199.59	2793.69	2647.115	0.035	0.040	0.043
	S3	184.052	202.682	244.856	257.898	2367.99	2141.19	2059.29	0.109	0.120	0.125
	S11	20.803	167.647	71.097	173.887	3465.882	3023.082	2863.182	0.050	0.058	0.061
	S4	54.279	158.796	101.917	175.079	2210.94	1996.056	1918.459	0.079	0.088	0.091
	S12	84.866	126.917	122.941	152.377	2731.437	2386.287	2261.6495	0.056	0.064	0.067
3	S10	102.556	63.627	121.644	94.394	3555.1	3104.1	3002.625	0.034	0.039	0.041
	S3	195.473	224.121	262.709	282.763	2631.1	2379.1	2322.4	0.107	0.119	0.122
	S11	21.720	189.109	78.452	195.625	3850.98	3358.98	3248.28	0.051	0.058	0.060
	S4	61.814	175.927	114.592	194.471	2456.6	2217.84	2164.119	0.079	0.088	0.090
	S12	93.838	146.091	137.666	174.242	3034.93	2651.43	2565.1425	0.057	0.066	0.068
2	S10	106.571	74.833	129.021	106.804	3910.61	3414.51	3358.135	0.033	0.038	0.038
	S3	203.581	241.368	275.991	302.442	2894.21	2617.01	2585.51	0.104	0.116	0.117
	S11	22.295	206.999	84.394	213.687	4236.078	3694.878	3633.378	0.050	0.058	0.059

1	S4	68.131	190.118	125.167	210.557	2702.26	2439.624	2409.779	0.078	0.086	0.087
	S12	101.510	162.877	150.373	193.330	3338.423	2916.573	2868.6355	0.058	0.066	0.067
	S10	108.974	83.389	133.991	116.081	4266.12	3724.92	3713.645	0.031	0.036	0.036
	S3	207.176	252.826	283.023	314.979	3157.32	2854.92	2848.62	0.100	0.110	0.111
	S11	22.537	218.715	88.151	225.476	4621.176	4030.776	4018.476	0.049	0.056	0.056
	S4	73.281	199.918	133.257	221.902	2947.92	2661.408	2655.439	0.075	0.083	0.084
	S12	106.855	173.829	159.003	205.885	3641.916	3181.716	3172.1285	0.057	0.065	0.065

Çizelge B.125: 6 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	7.2625	3.7808	8.397	5.960	355.51	332.96	287.86	0.024	0.025	0.029
	S3	14.7793	11.049	18.094	15.483	263.11	250.51	225.31	0.069	0.072	0.080
	S11	0.9035	6.8357	2.954	7.107	385.098	360.498	311.298	0.018	0.020	0.023
	S4	4.1995	6.8453	6.253	8.105	245.66	233.722	209.846	0.033	0.035	0.039
	S12	4.087	3.2167	5.052	4.443	303.493	284.318	245.968	0.017	0.018	0.021
5	S10	17.9447	4.0036	19.146	9.387	711.02	665.92	598.27	0.027	0.029	0.032
	S3	28.9112	25.6683	36.612	34.342	526.22	501.02	463.22	0.070	0.073	0.079
	S11	1.9444	18.8649	7.604	19.448	770.196	720.996	647.196	0.025	0.027	0.030
	S4	8.4408	19.2399	14.213	21.772	491.32	467.444	431.63	0.044	0.047	0.050
	S12	10.4997	11.9428	14.083	15.093	606.986	568.636	511.111	0.025	0.027	0.030
4	S10	28.6511	4.5456	30.015	13.141	1066.53	998.88	931.23	0.028	0.030	0.032
	S3	42.8902	40.1459	54.934	53.013	789.33	751.53	713.73	0.070	0.073	0.077
	S11	2.7858	31.0164	12.091	31.852	1155.294	1081.494	1007.694	0.028	0.029	0.032
	S4	13.0068	31.6939	22.515	35.596	736.98	701.166	665.352	0.048	0.051	0.053
	S12	16.8088	20.8755	23.071	25.918	910.479	852.954	795.429	0.028	0.030	0.033
3	S10	38.0843	2.0784	38.708	13.504	1422.04	1331.84	1286.74	0.027	0.029	0.030
	S3	55.5267	54.107	71.759	70.765	1052.44	1002.04	976.84	0.068	0.072	0.073
	S11	3.5334	45.487	17.180	46.547	1540.392	1441.992	1392.792	0.030	0.032	0.033
	S4	17.8341	44.6149	31.219	49.965	982.64	934.888	911.012	0.051	0.053	0.055
	S12	23.2931	32.0247	32.901	39.013	1213.972	1137.272	1098.922	0.032	0.034	0.036
2	S10	45.5537	2.7065	46.366	16.373	1777.55	1664.8	1642.25	0.026	0.028	0.028
	S3	65.6285	66.4409	85.561	86.129	1315.55	1252.55	1239.95	0.065	0.069	0.069
	S11	4.0805	60.5217	22.237	61.746	1925.49	1802.49	1777.89	0.032	0.034	0.035
	S4	22.5602	56.9881	39.657	63.756	1228.3	1168.61	1156.672	0.052	0.055	0.055
	S12	29.3217	43.9284	42.500	52.725	1517.465	1421.59	1402.415	0.035	0.037	0.038
1	S10	50.3881	8.5094	52.941	23.626	2133.06	1997.76	1997.76	0.025	0.027	0.027
	S3	71.7938	75.815	94.538	97.353	1578.66	1503.06	1503.06	0.062	0.065	0.065
	S11	4.3354	72.9793	26.229	74.280	2310.588	2162.988	2162.988	0.032	0.034	0.034
	S4	25.2118	66.6025	45.193	74.166	1473.96	1402.332	1402.332	0.050	0.053	0.053
	S12	33.9441	54.278	50.228	64.461	1820.958	1705.908	1705.908	0.035	0.038	0.038

Çizelge B.126: 9 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	10.171	4.645	11.565	7.696	355.51	310.41	254.035	0.033	0.037	0.046
	S3	21.880	14.559	26.248	21.123	263.11	237.91	206.41	0.100	0.110	0.127
	S11	2.035	7.480	4.279	8.090	385.098	335.898	274.398	0.021	0.024	0.029
	S4	4.979	8.647	7.573	10.141	245.66	221.784	191.939	0.041	0.046	0.053
	S12	5.650	2.946	6.534	4.641	303.493	265.143	217.2055	0.022	0.025	0.030
8	S10	25.306	4.631	26.695	12.222	711.02	620.82	519.345	0.038	0.043	0.051
	S3	44.226	34.884	54.691	48.152	526.22	475.82	419.12	0.104	0.115	0.130
	S11	4.562	21.163	10.910	22.531	770.196	671.796	561.096	0.029	0.034	0.040
	S4	10.299	23.983	17.494	27.073	491.32	443.568	389.847	0.055	0.061	0.069
	S12	15.010	12.319	18.706	16.822	606.986	530.286	443.9985	0.031	0.035	0.042
7	S10	40.906	5.296	42.495	17.568	1066.53	931.23	987.605	0.040	0.046	0.043
	S3	67.059	55.333	83.659	75.451	789.33	713.73	745.23	0.106	0.117	0.112
	S11	6.804	35.151	17.350	37.192	1155.294	1007.694	1069.194	0.032	0.037	0.035
	S4	16.298	39.463	28.137	44.353	736.98	665.352	695.197	0.060	0.067	0.064
	S12	24.448	21.971	31.039	29.305	910.479	795.429	843.3665	0.034	0.039	0.037
6	S10	55.186	2.125	55.823	18.681	1422.04	1241.64	1275.465	0.039	0.045	0.044
	S3	89.411	76.271	112.293	103.095	1052.44	951.64	970.54	0.107	0.118	0.116
	S11	8.950	53.072	24.872	55.757	1540.392	1343.592	1380.492	0.036	0.041	0.040
	S4	23.398	56.362	40.306	63.381	982.64	887.136	905.043	0.065	0.071	0.070
	S12	34.863	35.108	45.396	45.567	1213.972	1060.572	1089.3345	0.038	0.043	0.042
5	S10	68.142	3.974	69.334	24.416	1777.55	1552.05	1585.875	0.039	0.045	0.044
	S3	110.688	97.195	139.846	130.401	1315.55	1189.55	1208.45	0.106	0.118	0.116
	S11	10.812	73.884	32.977	77.127	1925.49	1679.49	1716.39	0.040	0.046	0.045
	S4	31.750	74.332	54.050	83.857	1228.3	1108.92	1126.827	0.068	0.076	0.074
	S12	45.848	50.666	61.048	64.420	1517.465	1325.715	1354.4775	0.042	0.049	0.048
4	S10	79.807	12.263	83.486	36.205	2133.06	1862.46	1918.835	0.039	0.045	0.044
	S3	130.542	117.437	165.773	156.599	1578.66	1427.46	1458.96	0.105	0.116	0.114
	S11	12.310	95.940	41.091	99.633	2310.588	2015.388	2076.888	0.043	0.049	0.048
	S4	37.760	91.907	65.332	103.235	1473.96	1330.704	1360.549	0.070	0.078	0.076
	S12	57.014	68.914	77.689	86.018	1820.958	1590.858	1638.7955	0.047	0.054	0.052
3	S10	87.404	21.936	93.985	48.157	2488.57	2172.87	2274.345	0.038	0.043	0.041
	S3	146.374	137.086	187.500	180.998	1841.77	1665.37	1722.07	0.102	0.113	0.109
	S11	13.489	118.926	49.167	122.973	2695.686	2351.286	2461.986	0.046	0.052	0.050
	S4	43.946	108.693	76.554	121.876	1719.62	1552.488	1606.209	0.071	0.079	0.076
	S12	65.332	86.910	91.405	106.510	2124.451	1856.001	1942.2885	0.050	0.057	0.055
2	S10	92.714	31.012	102.018	58.826	2844.08	2483.28	2629.855	0.036	0.041	0.039
	S3	157.429	154.083	203.654	201.312	2104.88	1903.28	1985.18	0.097	0.107	0.103
	S11	14.227	138.579	55.801	142.847	3080.784	2687.184	2847.084	0.046	0.053	0.050
	S4	50.156	123.358	87.164	138.405	1965.28	1774.272	1851.869	0.070	0.078	0.075
	S12	71.712	102.427	102.440	123.941	2427.944	2121.144	2245.7815	0.051	0.058	0.055
1	S10	96.166	39.927	108.144	68.777	3199.59	2793.69	2985.365	0.034	0.039	0.036
	S3	163.275	165.910	213.048	214.892	2367.99	2141.19	2248.29	0.091	0.100	0.096
	S11	14.599	152.310	60.292	156.689	3465.882	3023.082	3232.182	0.045	0.052	0.048
	S4	54.186	133.976	94.378	150.231	2210.94	1996.056	2097.529	0.068	0.075	0.072
	S12	77.496	114.913	111.970	138.162	2731.437	2386.287	2549.2745	0.051	0.058	0.054

Çizelge B.127: 12 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	13.026	6.197	14.885	10.105	355.51	310.41	310.41	0.042	0.048	0.048
	S3	28.888	20.590	35.065	29.256	263.11	237.91	237.91	0.133	0.147	0.147
	S11	3.409	8.795	6.048	9.817	385.098	335.898	335.898	0.025	0.029	0.029
	S4	4.934	12.621	8.720	14.101	245.66	221.784	221.784	0.057	0.064	0.064
	S12	6.821	2.831	7.670	4.877	303.493	265.143	265.143	0.025	0.029	0.029
11	S10	32.663	5.760	34.391	15.559	711.02	620.82	620.82	0.048	0.055	0.055
	S3	58.891	49.964	73.880	67.632	526.22	475.82	475.82	0.140	0.155	0.155
	S11	7.709	25.974	15.501	28.287	770.196	671.796	671.796	0.037	0.042	0.042
	S4	10.495	34.567	20.865	37.716	491.32	443.568	443.568	0.077	0.085	0.085
	S12	18.870	14.325	23.167	19.986	606.986	530.286	530.286	0.038	0.044	0.044
10	S10	53.142	6.382	55.057	22.325	1066.53	931.23	931.23	0.052	0.059	0.059
	S3	89.891	79.647	113.785	106.614	789.33	713.73	713.73	0.144	0.159	0.159
	S11	11.625	43.594	24.703	47.082	1155.294	1007.694	1007.694	0.041	0.047	0.047
	S4	17.049	56.706	34.061	61.821	736.98	665.352	665.352	0.084	0.093	0.093
	S12	31.129	26.189	38.986	35.528	910.479	795.429	795.429	0.043	0.049	0.049
9	S10	71.881	1.601	72.361	23.165	1422.04	1241.64	1185.265	0.051	0.058	0.061
	S3	120.874	110.564	154.043	146.826	1052.44	951.64	920.14	0.146	0.162	0.167
	S11	15.447	66.965	35.536	71.599	1540.392	1343.592	1282.092	0.046	0.053	0.056
	S4	25.412	81.134	49.752	88.757	982.64	887.136	857.291	0.090	0.100	0.104
	S12	45.028	43.077	57.951	56.585	1213.972	1060.572	1012.6345	0.048	0.055	0.057
8	S10	89.222	7.296	91.411	34.063	1777.55	1552.05	1450.575	0.051	0.059	0.063
	S3	151.578	142.495	194.326	187.968	1315.55	1189.55	1132.85	0.148	0.163	0.172
	S11	18.911	95.033	47.420	100.706	1925.49	1679.49	1568.79	0.052	0.060	0.064
	S4	36.129	107.660	68.427	118.498	1228.3	1108.92	1055.199	0.096	0.107	0.112
	S12	60.223	63.746	79.347	81.813	1517.465	1325.715	1239.4275	0.054	0.062	0.066
7	S10	105.483	20.067	111.503	51.711	2133.06	1862.46	1715.885	0.052	0.060	0.065
	S3	182.287	175.238	234.858	229.924	1578.66	1427.46	1345.56	0.149	0.165	0.175
	S11	21.944	126.553	59.910	133.136	2310.588	2015.388	1855.488	0.058	0.066	0.072
	S4	43.699	134.806	84.140	147.915	1473.96	1330.704	1253.107	0.100	0.111	0.118
	S12	76.940	89.843	103.893	112.925	1820.958	1590.858	1466.2205	0.062	0.071	0.077
6	S10	115.982	35.505	126.633	70.300	2488.57	2172.87	2003.745	0.051	0.058	0.063
	S3	209.353	210.244	272.427	273.050	1841.77	1665.37	1570.87	0.148	0.164	0.174
	S11	24.626	162.580	73.399	169.968	2695.686	2351.286	2166.786	0.063	0.072	0.078
	S4	53.141	163.015	102.045	178.957	1719.62	1552.488	1462.953	0.104	0.115	0.122
	S12	89.754	117.279	124.938	144.205	2124.451	1856.001	1712.1885	0.068	0.078	0.084
5	S10	124.640	52.543	140.403	89.935	2844.08	2483.28	2314.155	0.049	0.057	0.061
	S3	232.736	245.284	306.321	315.104	2104.88	1903.28	1808.78	0.150	0.166	0.174
	S11	26.823	197.848	86.177	205.895	3080.784	2687.184	2502.684	0.067	0.077	0.082
	S4	63.916	191.333	121.316	210.507	1965.28	1774.272	1684.737	0.107	0.119	0.125
	S12	102.284	145.406	145.906	176.092	2427.944	2121.144	1977.3315	0.073	0.083	0.089
4	S10	133.444	70.594	154.622	110.627	3199.59	2793.69	2647.115	0.048	0.055	0.058
	S3	252.656	278.231	336.125	354.028	2367.99	2141.19	2059.29	0.150	0.165	0.172
	S11	28.557	230.136	97.598	238.703	3465.882	3023.082	2863.182	0.069	0.079	0.083
	S4	74.511	217.986	139.906	240.339	2210.94	1996.056	1918.459	0.109	0.120	0.125
	S12	116.499	174.225	168.766	209.175	2731.437	2386.287	2261.6495	0.077	0.088	0.092
3	S10	140.783	87.343	166.986	129.578	3555.1	3104.1	3002.625	0.047	0.054	0.056
	S3	268.334	307.661	360.633	388.161	2631.1	2379.1	2322.4	0.148	0.163	0.167
	S11	29.815	259.599	107.695	268.543	3850.98	3358.98	3248.28	0.070	0.080	0.083
	S4	84.855	241.503	157.305	266.959	2456.6	2217.84	2164.119	0.109	0.120	0.123
	S12	128.816	200.545	188.980	239.190	3034.93	2651.43	2565.1425	0.079	0.090	0.093
2	S10	146.295	102.726	177.113	146.615	3910.61	3414.51	3358.135	0.045	0.052	0.053
	S3	279.464	331.336	378.865	415.176	2894.21	2617.01	2585.51	0.143	0.159	0.161
	S11	30.605	284.157	115.852	293.338	4236.078	3694.878	3633.378	0.069	0.079	0.081

1	S4	93.527	260.984	171.822	289.041	2702.26	2439.624	2409.779	0.107	0.118	0.120
	S12	139.347	223.588	206.424	265.393	3338.423	2916.573	2868.6355	0.079	0.091	0.093
	S10	149.593	114.472	183.935	159.350	4266.12	3724.92	3713.645	0.043	0.049	0.050
	S3	284.399	347.066	388.519	432.386	3157.32	2854.92	2848.62	0.137	0.151	0.152
	S11	30.937	300.240	121.009	309.521	4621.176	4030.776	4018.476	0.067	0.077	0.077
	S4	100.596	274.437	182.927	304.615	2947.92	2661.408	2655.439	0.103	0.114	0.115
	S12	146.684	238.622	218.271	282.627	3641.916	3181.716	3172.1285	0.078	0.089	0.089

Çizelge B.128: 6 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	10.09	5.2527	11.666	8.280	355.51	332.96	287.86	0.033	0.035	0.041
	S3	20.5334	15.3508	25.139	21.511	263.11	250.51	225.31	0.096	0.100	0.112
	S11	1.2552	9.4971	4.104	9.874	385.098	360.498	311.298	0.026	0.027	0.032
	S4	5.8344	9.5103	8.687	11.261	245.66	233.722	209.846	0.046	0.048	0.054
	S12	5.6782	4.4691	7.019	6.173	303.493	284.318	245.968	0.023	0.025	0.029
5	S10	24.9312	5.5624	26.600	13.042	711.02	665.92	598.27	0.037	0.040	0.044
	S3	40.1672	35.6618	50.866	47.712	526.22	501.02	463.22	0.097	0.102	0.110
	S11	2.7014	26.2097	10.564	27.020	770.196	720.996	647.196	0.035	0.037	0.042
	S4	11.7271	26.7306	19.746	30.249	491.32	467.444	431.63	0.062	0.065	0.070
	S12	14.5876	16.5925	19.565	20.969	606.986	568.636	511.111	0.035	0.037	0.041
4	S10	39.8059	6.3154	41.701	18.257	1066.53	998.88	931.23	0.039	0.042	0.045
	S3	59.5888	55.776	76.322	73.653	789.33	751.53	713.73	0.097	0.102	0.107
	S11	3.8704	43.0921	16.798	44.253	1155.294	1081.494	1007.694	0.038	0.041	0.044
	S4	18.0707	44.0333	31.281	49.455	736.98	701.166	665.352	0.067	0.071	0.074
	S12	23.353	29.003	32.054	36.009	910.479	852.954	795.429	0.040	0.042	0.045
3	S10	52.9118	2.8876	53.778	18.761	1422.04	1331.84	1286.74	0.038	0.040	0.042
	S3	77.145	75.1727	99.697	98.316	1052.44	1002.04	976.84	0.095	0.099	0.102
	S11	4.9091	63.1967	23.868	64.669	1540.392	1441.992	1392.792	0.042	0.045	0.046
	S4	24.7776	61.985	43.373	69.418	982.64	934.888	911.012	0.071	0.074	0.076
	S12	32.3619	44.493	45.710	54.202	1213.972	1137.272	1098.922	0.045	0.048	0.049
2	S10	63.2892	3.7602	64.417	22.747	1777.55	1664.8	1642.25	0.036	0.039	0.039
	S3	91.1799	92.3085	118.872	119.662	1315.55	1252.55	1239.95	0.091	0.096	0.097
	S11	5.6692	84.0849	30.895	85.786	1925.49	1802.49	1777.89	0.045	0.048	0.048
	S4	31.3436	79.1754	55.096	88.578	1228.3	1168.61	1156.672	0.072	0.076	0.077
	S12	40.7376	61.0312	59.047	73.252	1517.465	1421.59	1402.415	0.048	0.052	0.052
1	S10	70.0058	11.8224	73.553	32.824	2133.06	1997.76	1997.76	0.034	0.037	0.037
	S3	99.7456	105.3323	131.345	135.256	1578.66	1503.06	1503.06	0.086	0.090	0.090
	S11	6.0233	101.3926	36.441	103.200	2310.588	2162.988	2162.988	0.045	0.048	0.048
	S4	35.0276	92.5331	62.788	103.041	1473.96	1402.332	1402.332	0.070	0.073	0.073
	S12	47.1597	75.4103	69.783	89.558	1820.958	1705.908	1705.908	0.049	0.052	0.052

Çizelge B.129: 9 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	14.131	6.453	16.067	10.692	355.51	310.41	254.035	0.045	0.052	0.063
	S3	30.398	20.228	36.467	29.347	263.11	237.91	206.41	0.139	0.153	0.177
	S11	2.828	10.392	5.945	11.240	385.098	335.898	274.398	0.029	0.033	0.041
	S4	6.917	12.014	10.521	14.089	245.66	221.784	191.939	0.057	0.064	0.073
	S12	7.850	4.093	9.077	6.448	303.493	265.143	217.2055	0.030	0.034	0.042
8	S10	35.159	6.434	37.089	16.981	711.02	620.82	519.345	0.052	0.060	0.071
	S3	61.444	48.466	75.984	66.899	526.22	475.82	419.12	0.144	0.160	0.181
	S11	6.337	29.402	15.158	31.303	770.196	671.796	561.096	0.041	0.047	0.056
	S4	14.308	33.321	24.305	37.613	491.32	443.568	389.847	0.077	0.085	0.096
	S12	20.854	17.115	25.989	23.371	606.986	530.286	443.9985	0.043	0.049	0.059
7	S10	56.832	7.358	59.039	24.408	1066.53	931.23	987.605	0.055	0.063	0.060
	S3	93.167	76.876	116.230	104.827	789.33	713.73	745.23	0.147	0.163	0.156
	S11	9.454	48.836	24.104	51.672	1155.294	1007.694	1069.194	0.045	0.051	0.048
	S4	22.643	54.827	39.092	61.620	736.98	665.352	695.197	0.084	0.093	0.089
	S12	33.966	30.525	43.123	40.714	910.479	795.429	843.3665	0.047	0.054	0.051
6	S10	76.671	2.952	77.557	25.953	1422.04	1241.64	1275.465	0.055	0.062	0.061
	S3	124.222	105.966	156.012	143.233	1052.44	951.64	970.54	0.148	0.164	0.161
	S11	12.435	73.734	34.555	77.465	1540.392	1343.592	1380.492	0.050	0.058	0.056
	S4	32.507	78.305	55.998	88.057	982.64	887.136	905.043	0.090	0.099	0.097
	S12	48.437	48.776	63.070	63.307	1213.972	1060.572	1089.3345	0.052	0.060	0.058
5	S10	94.672	5.521	96.328	33.922	1777.55	1552.05	1585.875	0.054	0.062	0.061
	S3	153.782	135.036	194.293	181.171	1315.55	1189.55	1208.45	0.148	0.163	0.161
	S11	15.022	102.649	45.816	107.155	1925.49	1679.49	1716.39	0.056	0.064	0.062
	S4	44.112	103.272	75.093	116.506	1228.3	1108.92	1126.827	0.095	0.105	0.103
	S12	63.699	70.391	84.816	89.501	1517.465	1325.715	1354.4775	0.059	0.068	0.066
4	S10	110.878	17.037	115.989	50.301	2133.06	1862.46	1918.835	0.054	0.062	0.060
	S3	181.366	163.159	230.313	217.568	1578.66	1427.46	1458.96	0.146	0.161	0.158
	S11	17.102	133.292	57.090	138.423	2310.588	2015.388	2076.888	0.060	0.069	0.067
	S4	52.461	127.689	90.768	143.427	1473.96	1330.704	1360.549	0.097	0.108	0.105
	S12	79.212	95.744	107.935	119.508	1820.958	1590.858	1638.7955	0.066	0.075	0.073
3	S10	121.433	30.476	130.576	66.906	2488.57	2172.87	2274.345	0.052	0.060	0.057
	S3	203.362	190.458	260.500	251.466	1841.77	1665.37	1722.07	0.141	0.156	0.151
	S11	18.741	165.228	68.309	170.850	2695.686	2351.286	2461.986	0.063	0.073	0.069
	S4	61.056	151.010	106.359	169.327	1719.62	1552.488	1606.209	0.098	0.109	0.105
	S12	90.768	120.747	126.992	147.978	2124.451	1856.001	1942.2885	0.070	0.080	0.076
2	S10	128.811	43.086	141.737	81.729	2844.08	2483.28	2629.855	0.050	0.057	0.054
	S3	218.721	214.073	282.943	279.689	2104.88	1903.28	1985.18	0.134	0.149	0.143
	S11	19.767	192.532	77.526	198.462	3080.784	2687.184	2847.084	0.064	0.074	0.070
	S4	69.684	171.385	121.100	192.291	1965.28	1774.272	1851.869	0.098	0.108	0.104
	S12	99.632	142.305	142.324	172.195	2427.944	2121.144	2245.7815	0.071	0.081	0.077
1	S10	133.606	55.472	150.248	95.554	3199.59	2793.69	2985.365	0.047	0.054	0.050
	S3	226.843	230.504	295.995	298.557	2367.99	2141.19	2248.29	0.126	0.139	0.133
	S11	20.282	211.609	83.765	217.694	3465.882	3023.082	3232.182	0.063	0.072	0.067
	S4	75.282	186.137	131.123	208.721	2210.94	1996.056	2097.529	0.094	0.105	0.100
	S12	107.667	159.652	155.563	191.952	2731.437	2386.287	2549.2745	0.070	0.080	0.075

Çizelge B.130: 12 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q0$, $k_{E\gamma} = N_E / N_G + \gamma Q0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	18.097	8.610	20.680	14.039	355.51	310.41	310.41	0.058	0.067	0.067
	S3	40.135	28.606	48.717	40.647	263.11	237.91	237.91	0.185	0.205	0.205
	S11	4.737	12.219	8.402	13.640	385.098	335.898	335.898	0.035	0.041	0.041
	S4	6.855	17.535	12.116	19.592	245.66	221.784	221.784	0.080	0.088	0.088
	S12	9.476	3.933	10.656	6.775	303.493	265.143	265.143	0.035	0.040	0.040
11	S10	45.379	8.002	47.780	21.616	711.02	620.82	620.82	0.067	0.077	0.077
	S3	81.819	69.417	102.644	93.963	526.22	475.82	475.82	0.195	0.216	0.216
	S11	10.710	36.087	21.536	39.300	770.196	671.796	671.796	0.051	0.058	0.058
	S4	14.581	48.025	28.989	52.400	491.32	443.568	443.568	0.107	0.118	0.118
	S12	26.216	19.902	32.187	27.767	606.986	530.286	530.286	0.053	0.061	0.061
10	S10	73.832	8.867	76.492	31.017	1066.53	931.23	931.23	0.072	0.082	0.082
	S3	124.888	110.656	158.085	148.123	789.33	713.73	713.73	0.200	0.221	0.221
	S11	16.151	60.567	34.321	65.412	1155.294	1007.694	1007.694	0.057	0.065	0.065
	S4	23.687	78.783	47.321	85.889	736.98	665.352	665.352	0.117	0.129	0.129
	S12	43.248	36.386	54.164	49.360	910.479	795.429	795.429	0.059	0.068	0.068
9	S10	99.867	2.224	100.534	32.184	1422.04	1241.64	1185.265	0.071	0.081	0.085
	S3	167.934	153.610	214.017	203.990	1052.44	951.64	920.14	0.203	0.225	0.233
	S11	21.461	93.037	49.372	99.475	1540.392	1343.592	1282.092	0.065	0.074	0.078
	S4	35.305	112.722	69.122	123.313	982.64	887.136	857.291	0.125	0.139	0.144
	S12	62.559	59.848	80.513	78.615	1213.972	1060.572	1012.6345	0.066	0.076	0.080
8	S10	123.959	10.137	127.000	47.324	1777.55	1552.05	1450.575	0.071	0.082	0.088
	S3	210.592	197.973	269.984	261.150	1315.55	1189.55	1132.85	0.205	0.227	0.238
	S11	26.273	132.032	65.883	139.914	1925.49	1679.49	1568.79	0.073	0.083	0.089
	S4	50.195	149.575	95.068	164.634	1228.3	1108.92	1055.199	0.134	0.148	0.156
	S12	83.670	88.565	110.239	113.666	1517.465	1325.715	1239.4275	0.075	0.086	0.092
7	S10	146.551	27.879	154.914	71.844	2133.06	1862.46	1715.885	0.073	0.083	0.090
	S3	253.258	243.463	326.297	319.441	1578.66	1427.46	1345.56	0.207	0.229	0.242
	S11	30.487	175.824	83.235	184.970	2310.588	2015.388	1855.488	0.080	0.092	0.100
	S4	60.712	187.290	116.899	205.503	1473.96	1330.704	1253.107	0.139	0.154	0.164
	S12	106.895	124.822	144.341	156.891	1820.958	1590.858	1466.2205	0.086	0.099	0.107
6	S10	161.137	49.329	175.936	97.670	2488.57	2172.87	2003.745	0.071	0.081	0.088
	S3	290.861	292.100	378.491	379.358	1841.77	1665.37	1570.87	0.206	0.228	0.241
	S11	34.213	225.878	101.976	236.142	2695.686	2351.286	2166.786	0.088	0.100	0.109
	S4	73.830	226.483	141.775	248.632	1719.62	1552.488	1462.953	0.145	0.160	0.170
	S12	124.698	162.940	173.580	200.349	2124.451	1856.001	1712.1885	0.094	0.108	0.117
5	S10	173.167	73.000	195.067	124.950	2844.08	2483.28	2314.155	0.069	0.079	0.084
	S3	323.348	340.781	425.583	437.785	2104.88	1903.28	1808.78	0.208	0.230	0.242
	S11	37.265	274.877	119.729	286.057	3080.784	2687.184	2502.684	0.093	0.106	0.114
	S4	88.801	265.825	168.548	292.465	1965.28	1774.272	1684.737	0.149	0.165	0.174
	S12	142.107	202.018	202.712	244.650	2427.944	2121.144	1977.3315	0.101	0.115	0.124
4	S10	185.398	98.079	214.822	153.698	3199.59	2793.69	2647.115	0.067	0.077	0.081
	S3	351.023	386.556	466.990	491.863	2367.99	2141.19	2059.29	0.208	0.230	0.239
	S11	39.675	319.736	135.596	331.638	3465.882	3023.082	2863.182	0.096	0.110	0.116
	S4	103.520	302.855	194.377	333.911	2210.94	1996.056	1918.459	0.151	0.167	0.174
	S12	161.856	242.057	234.473	290.614	2731.437	2386.287	2261.6495	0.106	0.122	0.128
3	S10	195.595	121.349	232.000	180.027	3555.1	3104.1	3002.625	0.065	0.075	0.077
	S3	372.806	427.444	501.039	539.286	2631.1	2379.1	2322.4	0.205	0.227	0.232
	S11	41.424	360.669	149.624	373.096	3850.98	3358.98	3248.28	0.097	0.111	0.115
	S4	117.891	335.528	218.550	370.896	2456.6	2217.84	2164.119	0.151	0.167	0.171
	S12	178.969	278.624	262.556	332.315	3034.93	2651.43	2565.1425	0.109	0.125	0.130
2	S10	203.252	142.721	246.069	203.697	3910.61	3414.51	3358.135	0.063	0.072	0.073
	S3	388.269	460.337	526.370	576.817	2894.21	2617.01	2585.51	0.199	0.220	0.223
	S11	42.520	394.789	160.957	407.545	4236.078	3694.878	3633.378	0.096	0.110	0.112

1	S4	129.940	362.593	238.718	401.575	2702.26	2439.624	2409.779	0.149	0.165	0.167
	S12	193.600	310.639	286.792	368.719	3338.423	2916.573	2868.6355	0.110	0.126	0.129
	S10	207.835	159.040	255.547	221.390	4266.12	3724.92	3713.645	0.060	0.069	0.069
	S3	395.125	482.190	539.782	600.728	3157.32	2854.92	2848.62	0.190	0.210	0.211
	S11	42.982	417.133	168.122	430.028	4621.176	4030.776	4018.476	0.093	0.107	0.107
	S4	139.762	381.284	254.147	423.212	2947.92	2661.408	2655.439	0.144	0.159	0.159
	S12	203.793	331.526	303.251	392.664	3641.916	3181.716	3172.1285	0.108	0.123	0.124

Çizelge B.131: 6 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S10	12.9097	6.1633	14.759	10.036	355.51	332.96	287.86	0.042	0.044	0.051
	S3	26.2714	18.0118	31.675	25.893	263.11	250.51	225.31	0.120	0.126	0.141
	S11	1.606	11.1435	4.949	11.625	385.098	360.498	311.298	0.030	0.032	0.037
	S4	7.4649	11.159	10.813	13.398	245.66	233.722	209.846	0.055	0.057	0.064
	S12	7.265	5.2438	8.838	7.423	303.493	284.318	245.968	0.029	0.031	0.036
5	S10	31.8982	6.5266	33.856	16.096	711.02	665.92	598.27	0.048	0.051	0.057
	S3	51.392	41.8437	63.945	57.261	526.22	501.02	463.22	0.122	0.128	0.138
	S11	3.4563	30.7531	12.682	31.790	770.196	720.996	647.196	0.041	0.044	0.049
	S4	15.0043	31.3643	24.414	35.866	491.32	467.444	431.63	0.073	0.077	0.083
	S12	18.6641	19.4688	24.505	25.068	606.986	568.636	511.111	0.041	0.044	0.049
4	S10	50.9297	7.4102	53.153	22.689	1066.53	998.88	931.23	0.050	0.053	0.057
	S3	76.241	65.4447	95.874	88.317	789.33	751.53	713.73	0.121	0.128	0.134
	S11	4.9519	50.5621	20.121	52.048	1155.294	1081.494	1007.694	0.045	0.048	0.052
	S4	23.1206	51.6665	38.621	58.603	736.98	701.166	665.352	0.080	0.084	0.088
	S12	29.879	34.0307	40.088	42.994	910.479	852.954	795.429	0.047	0.050	0.054
3	S10	67.6981	3.3882	68.715	23.698	1422.04	1331.84	1286.74	0.048	0.052	0.053
	S3	98.7033	88.2038	125.164	117.815	1052.44	1002.04	976.84	0.119	0.125	0.128
	S11	6.2809	74.1518	28.526	76.036	1540.392	1441.992	1392.792	0.049	0.053	0.055
	S4	31.7017	72.7301	53.521	82.241	982.64	934.888	911.012	0.084	0.088	0.090
	S12	41.4055	52.2058	57.067	64.627	1213.972	1137.272	1098.922	0.053	0.057	0.059
2	S10	80.9755	4.4121	82.299	28.705	1777.55	1664.8	1642.25	0.046	0.049	0.050
	S3	116.6603	108.3101	149.153	143.308	1315.55	1252.55	1239.95	0.113	0.119	0.120
	S11	7.2534	98.6609	36.852	100.837	1925.49	1802.49	1777.89	0.052	0.056	0.057
	S4	40.1026	92.9004	67.973	104.931	1228.3	1168.61	1156.672	0.085	0.090	0.091
	S12	52.1218	71.6109	73.605	87.247	1517.465	1421.59	1402.415	0.057	0.061	0.062
1	S10	89.5691	13.8718	93.731	40.743	2133.06	1997.76	1997.76	0.044	0.047	0.047
	S3	127.6196	123.5916	164.697	161.877	1578.66	1503.06	1503.06	0.104	0.110	0.110
	S11	7.7065	118.969	43.397	121.281	2310.588	2162.988	2162.988	0.052	0.056	0.056
	S4	44.8161	108.5737	77.388	122.019	1473.96	1402.332	1402.332	0.083	0.087	0.087
	S12	60.3385	88.4826	86.883	106.584	1820.958	1705.908	1705.908	0.059	0.062	0.062

Çizelge B.132: 9 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S10	20.410	9.320	23.206	15.443	355.51	310.41	254.035	0.065	0.075	0.091
	S3	43.905	29.216	52.670	42.388	263.11	237.91	206.41	0.200	0.221	0.255
	S11	4.084	15.009	8.587	16.234	385.098	335.898	274.398	0.042	0.048	0.059
	S4	9.991	17.352	15.196	20.349	245.66	221.784	191.939	0.083	0.092	0.106
	S12	11.337	5.911	13.111	9.313	303.493	265.143	217.2055	0.043	0.049	0.060
8	S10	50.781	9.292	53.569	24.526	711.02	620.82	519.345	0.075	0.086	0.103
	S3	88.746	70.001	109.747	96.625	526.22	475.82	419.12	0.209	0.231	0.262
	S11	9.153	42.467	21.893	45.213	770.196	671.796	561.096	0.059	0.067	0.081
	S4	20.666	48.126	35.104	54.326	491.32	443.568	389.847	0.111	0.122	0.139
	S12	30.121	24.719	37.536	33.755	606.986	530.286	443.9985	0.062	0.071	0.085
7	S10	82.084	10.628	85.273	35.253	1066.53	931.23	987.605	0.080	0.092	0.086
	S3	134.565	111.035	167.876	151.405	789.33	713.73	745.23	0.213	0.235	0.225
	S11	13.654	70.536	34.815	74.632	1155.294	1007.694	1069.194	0.065	0.074	0.070
	S4	32.705	79.189	56.462	89.001	736.98	665.352	695.197	0.121	0.134	0.128
	S12	49.058	44.088	62.285	58.805	910.479	795.429	843.3665	0.068	0.078	0.074
6	S10	110.739	4.264	112.018	37.485	1422.04	1241.64	1275.465	0.079	0.090	0.088
	S3	179.419	153.051	225.334	206.876	1052.44	951.64	970.54	0.214	0.237	0.232
	S11	17.960	106.497	49.909	111.885	1540.392	1343.592	1380.492	0.073	0.083	0.081
	S4	46.951	113.099	80.881	127.184	982.64	887.136	905.043	0.129	0.143	0.141
	S12	69.959	70.449	91.094	91.437	1213.972	1060.572	1089.3345	0.075	0.086	0.084
5	S10	136.738	7.974	139.130	48.995	1777.55	1552.05	1585.875	0.078	0.090	0.088
	S3	222.114	195.038	280.625	261.672	1315.55	1189.55	1208.45	0.213	0.236	0.232
	S11	21.696	148.260	66.174	154.769	1925.49	1679.49	1716.39	0.080	0.092	0.090
	S4	63.712	149.160	108.460	168.274	1228.3	1108.92	1126.827	0.137	0.152	0.149
	S12	92.002	101.669	122.503	129.269	1517.465	1325.715	1354.4775	0.085	0.098	0.095
4	S10	160.146	24.608	167.528	72.651	2133.06	1862.46	1918.835	0.079	0.090	0.087
	S3	261.953	235.656	332.650	314.242	1578.66	1427.46	1458.96	0.211	0.233	0.228
	S11	24.701	192.519	82.457	199.929	2310.588	2015.388	2076.888	0.087	0.099	0.096
	S4	75.772	184.426	131.100	207.158	1473.96	1330.704	1360.549	0.141	0.156	0.152
	S12	114.409	138.287	155.895	172.610	1820.958	1590.858	1638.7955	0.095	0.109	0.105
3	S10	175.391	44.018	188.596	96.635	2488.57	2172.87	2274.345	0.076	0.087	0.083
	S3	293.724	275.085	376.249	363.202	1841.77	1665.37	1722.07	0.204	0.226	0.218
	S11	27.068	238.645	98.661	246.765	2695.686	2351.286	2461.986	0.092	0.105	0.100
	S4	88.185	218.110	153.618	244.565	1719.62	1552.488	1606.209	0.142	0.158	0.152
	S12	131.100	174.400	183.420	213.730	2124.451	1856.001	1942.2885	0.101	0.115	0.110
2	S10	186.047	62.230	204.716	118.044	2844.08	2483.28	2629.855	0.072	0.082	0.078
	S3	315.907	309.194	408.665	403.966	2104.88	1903.28	1985.18	0.194	0.215	0.206
	S11	28.550	278.081	111.974	286.646	3080.784	2687.184	2847.084	0.093	0.107	0.101
	S4	100.647	247.538	174.909	277.732	1965.28	1774.272	1851.869	0.141	0.157	0.150
	S12	143.903	205.536	205.564	248.707	2427.944	2121.144	2245.7815	0.102	0.117	0.111
1	S10	192.973	80.120	217.009	138.012	3199.59	2793.69	2985.365	0.068	0.078	0.073
	S3	327.639	332.926	427.516	431.217	2367.99	2141.19	2248.29	0.182	0.201	0.192
	S11	29.295	305.635	120.985	314.423	3465.882	3023.082	3232.182	0.091	0.104	0.097
	S4	108.732	268.844	189.385	301.464	2210.94	1996.056	2097.529	0.136	0.151	0.144
	S12	155.508	230.592	224.686	277.244	2731.437	2386.287	2549.2745	0.102	0.116	0.109

Çizelge B.133: 12 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S10	26.139	12.436	29.869	20.277	355.51	310.41	310.41	0.084	0.096	0.096
	S3	57.969	41.317	70.364	58.708	263.11	237.91	237.91	0.267	0.296	0.296
	S11	6.841	17.648	12.136	19.700	385.098	335.898	335.898	0.051	0.059	0.059
	S4	9.901	25.327	17.499	28.297	245.66	221.784	221.784	0.115	0.128	0.128
	S12	13.687	5.680	15.391	9.786	303.493	265.143	265.143	0.051	0.058	0.058
11	S10	65.543	11.558	69.010	31.221	711.02	620.82	620.82	0.097	0.111	0.111
	S3	118.175	100.262	148.253	135.714	526.22	475.82	475.82	0.282	0.312	0.312
	S11	15.469	52.122	31.106	56.762	770.196	671.796	671.796	0.074	0.084	0.084
	S4	21.060	69.365	41.870	75.683	491.32	443.568	443.568	0.154	0.171	0.171
	S12	37.865	28.746	46.489	40.105	606.986	530.286	530.286	0.077	0.088	0.088
10	S10	106.639	12.807	110.481	44.798	1066.53	931.23	931.23	0.104	0.119	0.119
	S3	180.380	159.825	228.328	213.939	789.33	713.73	713.73	0.289	0.320	0.320
	S11	23.328	87.479	49.571	94.478	1155.294	1007.694	1007.694	0.082	0.094	0.094
	S4	34.211	113.790	68.348	124.053	736.98	665.352	665.352	0.168	0.186	0.186
	S12	62.465	52.554	78.231	71.293	910.479	795.429	795.429	0.086	0.098	0.098
9	S10	144.241	3.213	145.205	46.485	1422.04	1241.64	1185.265	0.102	0.117	0.123
	S3	242.553	221.864	309.113	294.630	1052.44	951.64	920.14	0.294	0.325	0.336
	S11	30.997	134.377	71.310	143.676	1540.392	1343.592	1282.092	0.093	0.107	0.112
	S4	50.993	162.808	99.835	178.106	982.64	887.136	857.291	0.181	0.201	0.208
	S12	90.356	86.440	116.288	113.547	1213.972	1060.572	1012.6345	0.096	0.110	0.115
8	S10	179.039	14.641	183.431	68.352	1777.55	1552.05	1450.575	0.103	0.118	0.126
	S3	304.166	285.940	389.948	377.189	1315.55	1189.55	1132.85	0.296	0.328	0.344
	S11	37.947	190.699	95.157	202.083	1925.49	1679.49	1568.79	0.105	0.120	0.129
	S4	72.499	216.037	137.310	237.787	1228.3	1108.92	1055.199	0.194	0.214	0.225
	S12	120.848	127.917	159.223	164.171	1517.465	1325.715	1239.4275	0.108	0.124	0.132
7	S10	211.669	40.267	223.749	103.768	2133.06	1862.46	1715.885	0.105	0.120	0.130
	S3	365.789	351.643	471.282	461.380	1578.66	1427.46	1345.56	0.299	0.330	0.350
	S11	44.034	253.949	120.219	267.159	2310.588	2015.388	1855.488	0.116	0.133	0.144
	S4	87.688	270.510	168.841	296.816	1473.96	1330.704	1253.107	0.201	0.223	0.237
	S12	154.392	180.285	208.478	226.603	1820.958	1590.858	1466.2205	0.124	0.142	0.155
6	S10	232.736	71.247	254.110	141.068	2488.57	2172.87	2003.745	0.102	0.117	0.127
	S3	420.102	421.890	546.669	547.921	1841.77	1665.37	1570.87	0.297	0.329	0.349
	S11	49.415	326.244	147.288	341.068	2695.686	2351.286	2166.786	0.127	0.145	0.157
	S4	106.635	327.117	204.771	359.108	1719.62	1552.488	1462.953	0.209	0.231	0.245
	S12	180.106	235.340	250.708	289.372	2124.451	1856.001	1712.1885	0.136	0.156	0.169
5	S10	250.112	105.437	281.743	180.470	2844.08	2483.28	2314.155	0.099	0.113	0.122
	S3	467.024	492.203	614.685	632.310	2104.88	1903.28	1808.78	0.300	0.332	0.350
	S11	53.824	397.015	172.928	413.162	3080.784	2687.184	2502.684	0.134	0.154	0.165
	S4	128.258	383.941	243.440	422.418	1965.28	1774.272	1684.737	0.215	0.238	0.251
	S12	205.250	291.782	292.784	353.357	2427.944	2121.144	1977.3315	0.146	0.167	0.179
4	S10	267.778	141.659	310.275	221.992	3199.59	2793.69	2647.115	0.097	0.111	0.117
	S3	506.996	558.317	674.491	710.416	2367.99	2141.19	2059.29	0.300	0.332	0.345
	S11	57.304	461.806	195.846	478.997	3465.882	3023.082	2863.182	0.138	0.158	0.167
	S4	149.518	437.425	280.746	482.280	2210.94	1996.056	1918.459	0.218	0.242	0.251
	S12	233.774	349.612	338.658	419.744	2731.437	2386.287	2261.6495	0.154	0.176	0.186
3	S10	282.505	175.269	335.086	260.020	3555.1	3104.1	3002.625	0.094	0.108	0.112
	S3	538.457	617.374	723.669	778.911	2631.1	2379.1	2322.4	0.296	0.327	0.335
	S11	59.830	520.928	216.108	538.877	3850.98	3358.98	3248.28	0.140	0.160	0.166
	S4	170.275	484.616	315.660	535.699	2456.6	2217.84	2164.119	0.218	0.242	0.248
	S12	258.491	402.427	379.219	479.974	3034.93	2651.43	2565.1425	0.158	0.181	0.187
2	S10	293.565	206.137	355.406	294.207	3910.61	3414.51	3358.135	0.091	0.104	0.106
	S3	560.792	664.882	760.256	833.119	2894.21	2617.01	2585.51	0.288	0.318	0.322
	S11	61.414	570.208	232.476	588.633	4236.078	3694.878	3633.378	0.139	0.159	0.162

1	S4	187.677	523.707	344.789	580.010	2702.26	2439.624	2409.779	0.215	0.238	0.241
	S12	279.624	448.668	414.224	532.555	3338.423	2916.573	2868.6355	0.160	0.183	0.186
	S10	300.184	229.707	369.096	319.762	4266.12	3724.92	3713.645	0.087	0.099	0.099
	S3	570.694	696.445	779.628	867.654	3157.32	2854.92	2848.62	0.275	0.304	0.305
	S11	62.080	602.481	242.825	621.105	4621.176	4030.776	4018.476	0.134	0.154	0.155
	S4	201.863	550.703	367.074	611.261	2947.92	2661.408	2655.439	0.207	0.230	0.230
	S12	294.346	478.835	437.997	567.139	3641.916	3181.716	3172.1285	0.156	0.178	0.179

Model 4

Çizelge B.134: 6 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.169	2.946	9.053	5.397	128.2	122.95	112.45	0.071	0.074	0.081
	S9	11.439	0.670	11.640	4.102	206.21	195.96	175.46	0.056	0.059	0.066
	S2	2.209	3.724	3.326	4.386	244.38	232.83	209.73	0.018	0.019	0.021
	S10	7.536	2.347	8.240	4.607	355.51	332.96	287.86	0.023	0.025	0.029
	S3	1.197	6.645	3.190	7.004	263.11	250.51	225.31	0.027	0.028	0.031
	S11	41.053	4.454	42.389	16.770	354.348	335.898	298.998	0.120	0.126	0.142
5	S1	23.382	8.081	25.806	15.095	256.4	245.9	230.15	0.101	0.105	0.112
	S9	31.553	3.018	32.458	12.484	412.42	391.92	361.17	0.079	0.083	0.090
	S2	6.261	10.746	9.484	12.624	488.76	465.66	431.01	0.026	0.027	0.029
	S10	17.998	7.422	20.225	12.822	711.02	665.92	598.27	0.028	0.030	0.034
	S3	2.048	16.659	7.046	17.274	526.22	501.02	463.22	0.033	0.034	0.037
	S11	100.825	7.290	103.012	37.538	708.696	671.796	616.446	0.145	0.153	0.167
4	S1	39.232	13.373	43.243	25.142	384.6	368.85	353.1	0.112	0.117	0.122
	S9	52.469	5.564	54.139	21.305	618.63	587.88	557.13	0.088	0.092	0.097
	S2	10.322	18.001	15.722	21.097	733.14	698.49	663.84	0.029	0.030	0.032
	S10	29.455	12.746	33.279	21.582	1066.53	998.88	931.23	0.031	0.033	0.036
	S3	2.864	26.694	10.872	27.553	789.33	751.53	713.73	0.035	0.037	0.039
	S11	163.498	10.101	166.529	59.151	1063.044	1007.694	952.344	0.157	0.165	0.175
3	S1	55.035	18.369	60.546	34.879	512.8	491.8	481.3	0.118	0.123	0.126
	S9	74.273	8.003	76.674	30.285	824.84	783.84	763.34	0.093	0.098	0.100
	S2	14.170	25.654	21.866	29.905	977.52	931.32	908.22	0.031	0.032	0.033
	S10	39.332	19.237	45.103	31.037	1422.04	1331.84	1286.74	0.032	0.034	0.035
	S3	3.817	36.484	14.763	37.629	1052.44	1002.04	976.84	0.036	0.038	0.039
	S11	227.982	11.047	231.296	79.441	1417.392	1343.592	1306.692	0.163	0.172	0.177
2	S1	69.167	22.729	75.985	43.479	641	614.75	609.5	0.119	0.124	0.125
	S9	94.373	10.200	97.433	38.512	1031.05	979.8	969.55	0.094	0.099	0.100
	S2	17.517	33.023	27.424	38.278	1221.9	1164.15	1152.6	0.031	0.033	0.033
	S10	46.929	25.993	54.727	40.072	1777.55	1664.8	1642.25	0.031	0.033	0.033
	S3	4.773	45.158	18.320	46.590	1315.55	1252.55	1239.95	0.035	0.037	0.038
	S11	285.987	9.975	288.980	95.771	1771.74	1679.49	1661.04	0.163	0.172	0.174
1	S1	79.098	26.065	86.918	49.794	769.2	737.7	737.7	0.113	0.118	0.118
	S9	109.210	11.891	112.777	44.654	1237.26	1175.76	1175.76	0.091	0.096	0.096
	S2	19.421	38.968	31.112	44.794	1466.28	1396.98	1396.98	0.031	0.032	0.032
	S10	51.892	31.999	61.491	47.566	2133.06	1997.76	1997.76	0.029	0.031	0.031
	S3	5.392	51.686	20.898	53.304	1578.66	1503.06	1503.06	0.034	0.035	0.035
	S11	325.906	7.246	328.080	105.018	2126.088	2015.388	2015.388	0.154	0.163	0.163

Çizelge B.135: 9 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	9.900	4.510	11.253	7.480	128.2	117.7	104.575	0.088	0.096	0.108
	S9	13.387	1.060	13.705	5.076	206.21	185.71	160.085	0.066	0.074	0.086
	S2	0.984	5.338	2.586	5.633	244.38	221.28	192.405	0.023	0.025	0.029
	S10	5.370	2.392	6.087	4.003	355.51	310.41	254.035	0.017	0.020	0.024
	S3	1.649	11.198	5.008	11.692	263.11	237.91	206.41	0.044	0.049	0.057
	S11	44.837	5.476	46.480	18.927	354.348	317.448	271.323	0.131	0.146	0.171
8	S1	28.782	12.269	32.462	20.903	256.4	235.4	207.05	0.127	0.138	0.157
	S9	37.974	4.609	39.357	16.001	412.42	371.42	316.07	0.095	0.106	0.125
	S2	3.838	15.445	8.471	16.596	488.76	442.56	380.19	0.034	0.038	0.044
	S10	14.028	8.499	16.577	12.708	711.02	620.82	499.05	0.023	0.027	0.033
	S3	2.323	27.334	10.523	28.031	526.22	475.82	407.78	0.053	0.059	0.069
	S11	113.576	8.766	116.206	42.839	708.696	634.896	535.266	0.164	0.183	0.217
7	S1	48.931	20.268	55.011	34.947	384.6	353.1	314.25	0.143	0.156	0.175
	S9	64.194	8.428	66.722	27.686	618.63	557.13	481.28	0.108	0.120	0.139
	S2	7.077	25.831	14.826	27.954	733.14	663.84	578.37	0.038	0.042	0.048
	S10	24.576	14.994	29.074	22.367	1066.53	931.23	764.36	0.027	0.031	0.038
	S3	3.177	43.636	16.268	44.589	789.33	713.73	620.49	0.056	0.062	0.072
	S11	188.811	12.689	192.618	69.332	1063.044	952.344	815.814	0.181	0.202	0.236
6	S1	70.523	28.187	78.979	49.344	512.8	470.8	426.7	0.154	0.168	0.185
	S9	93.863	12.267	97.543	40.425	824.84	742.84	656.74	0.118	0.131	0.149
	S2	10.643	37.376	21.856	40.569	977.52	885.12	788.1	0.042	0.046	0.051
	S10	34.190	23.732	41.310	33.989	1422.04	1241.64	1052.22	0.029	0.033	0.039
	S3	4.570	60.421	22.696	61.792	1052.44	951.64	845.8	0.059	0.065	0.073
	S11	274.116	14.628	278.504	96.863	1417.392	1269.792	1114.812	0.196	0.219	0.250
5	S1	93.044	35.864	103.803	63.777	641	588.5	544.4	0.162	0.176	0.191
	S9	125.822	16.013	130.625	53.759	1031.05	928.55	842.45	0.127	0.141	0.155
	S2	14.702	49.752	29.628	54.162	1221.9	1106.4	1009.38	0.044	0.049	0.054
	S10	43.232	33.987	53.428	46.956	1777.55	1552.05	1362.63	0.030	0.034	0.039
	S3	6.531	77.141	29.673	79.101	1315.55	1189.55	1083.71	0.060	0.066	0.073
	S11	366.150	14.992	370.647	124.837	1771.74	1587.24	1432.26	0.209	0.234	0.259
4	S1	114.822	43.043	127.735	77.490	769.2	706.2	667.35	0.166	0.181	0.191
	S9	158.614	19.626	164.502	67.211	1237.26	1114.26	1038.41	0.133	0.148	0.158
	S2	17.802	62.008	36.404	67.349	1466.28	1327.68	1242.21	0.046	0.051	0.054
	S10	51.534	45.999	65.333	61.459	2133.06	1862.46	1695.59	0.031	0.035	0.039
	S3	8.405	93.211	36.368	95.732	1578.66	1427.46	1334.22	0.061	0.067	0.072
	S11	460.387	14.285	464.673	152.401	2126.088	1904.688	1768.158	0.219	0.244	0.263
3	S1	136.244	49.328	151.043	90.201	897.4	823.9	795.55	0.168	0.183	0.190
	S9	190.917	23.170	197.868	80.445	1443.47	1299.97	1244.62	0.137	0.152	0.159
	S2	19.737	73.863	41.896	79.785	1710.66	1548.96	1486.59	0.047	0.052	0.054
	S10	56.591	57.590	73.868	74.567	2488.57	2172.87	2051.1	0.030	0.034	0.036
	S3	11.493	108.620	44.079	112.068	1841.77	1665.37	1597.33	0.061	0.067	0.070
	S11	556.058	11.933	559.638	178.751	2480.436	2222.136	2122.506	0.226	0.252	0.264
2	S1	155.420	54.781	171.854	101.407	1025.6	941.6	923.75	0.168	0.183	0.186
	S9	220.117	27.747	228.441	93.782	1649.68	1485.68	1450.83	0.138	0.154	0.157
	S2	21.024	84.168	46.275	90.476	1955.04	1770.24	1730.97	0.046	0.051	0.052
	S10	61.393	67.494	81.641	85.912	2844.08	2483.28	2406.61	0.030	0.035	0.036
	S3	15.044	121.734	51.565	126.247	2104.88	1903.28	1860.44	0.060	0.066	0.068
	S11	637.658	8.910	640.331	200.208	2834.784	2539.584	2476.854	0.226	0.252	0.259
1	S1	168.911	58.792	186.549	109.466	1153.8	1059.3	1051.95	0.162	0.176	0.177
	S9	241.710	32.162	251.359	104.675	1855.89	1671.39	1657.04	0.135	0.150	0.152
	S2	21.385	91.821	48.931	98.236	2199.42	1991.52	1975.35	0.045	0.049	0.050
	S10	65.575	75.739	88.297	95.412	3199.59	2793.69	2762.12	0.030	0.034	0.035
	S3	17.860	130.826	57.107	136.184	2367.99	2141.19	2123.55	0.058	0.064	0.064
	S11	689.357	5.322	690.954	212.129	3189.132	2857.032	2831.202	0.217	0.242	0.244

Çizelge B.136: 12 Kat, İstanbul, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	10.623	7.049	12.738	10.236	128.2	117.7	117.7	0.099	0.108	0.108
	S9	13.957	1.316	14.351	5.503	206.21	185.71	185.71	0.070	0.077	0.077
	S2	0.701	8.350	3.206	8.560	244.38	221.28	221.28	0.035	0.039	0.039
	S10	1.491	2.424	2.218	2.871	355.51	310.41	310.41	0.008	0.009	0.009
	S3	1.728	18.190	7.185	18.709	263.11	237.91	237.91	0.071	0.079	0.079
	S11	41.979	6.370	43.890	18.964	354.348	317.448	317.448	0.124	0.138	0.138
11	S1	31.383	19.077	37.106	28.492	256.4	235.4	235.4	0.145	0.158	0.158
	S9	40.715	6.390	42.632	18.605	412.42	371.42	371.42	0.103	0.115	0.115
	S2	0.198	24.065	7.418	24.125	488.76	442.56	442.56	0.049	0.055	0.055
	S10	6.270	10.299	9.360	12.180	711.02	620.82	620.82	0.017	0.020	0.020
	S3	1.740	43.849	14.894	44.371	526.22	475.82	475.82	0.084	0.093	0.093
	S11	109.862	9.258	112.640	42.217	708.696	634.896	634.896	0.159	0.177	0.177
10	S1	53.659	31.451	63.094	47.549	384.6	353.1	353.1	0.164	0.179	0.179
	S9	69.371	11.870	72.932	32.682	618.63	557.13	557.13	0.118	0.131	0.131
	S2	1.580	40.074	13.603	40.548	733.14	663.84	663.84	0.055	0.061	0.061
	S10	13.189	18.671	18.790	22.627	1066.53	931.23	931.23	0.021	0.024	0.024
	S3	2.027	69.812	22.970	70.420	789.33	713.73	713.73	0.089	0.099	0.099
	S11	185.551	13.335	189.551	69.001	1063.044	952.344	952.344	0.178	0.199	0.199
9	S1	77.990	43.865	91.150	67.262	512.8	470.8	457.675	0.178	0.194	0.199
	S9	102.603	17.477	107.846	48.258	824.84	742.84	717.215	0.131	0.145	0.150
	S2	3.355	57.940	20.737	58.946	977.52	885.12	856.245	0.060	0.067	0.069
	S10	19.077	30.468	28.217	36.191	1422.04	1241.64	1185.265	0.025	0.029	0.031
	S3	2.961	96.941	32.043	97.829	1052.44	951.64	920.14	0.093	0.103	0.106
	S11	274.412	14.561	278.780	96.884	1417.392	1269.792	1223.667	0.197	0.220	0.228
8	S1	104.298	56.290	121.185	87.579	641	588.5	564.875	0.189	0.206	0.215
	S9	139.752	23.136	146.693	65.061	1031.05	928.55	882.425	0.142	0.158	0.166
	S2	5.890	77.433	29.119	79.200	1221.9	1106.4	1054.425	0.065	0.072	0.075
	S10	24.765	44.827	38.213	52.257	1777.55	1552.05	1450.575	0.029	0.034	0.036
	S3	4.691	124.842	42.143	126.249	1315.55	1189.55	1132.85	0.096	0.106	0.111
	S11	375.084	13.769	379.215	126.294	1771.74	1587.24	1504.215	0.214	0.239	0.252
7	S1	131.224	68.553	151.790	107.920	769.2	706.2	672.075	0.197	0.215	0.226
	S9	180.370	28.940	189.052	83.051	1237.26	1114.26	1047.635	0.153	0.170	0.180
	S2	7.516	97.732	36.835	99.987	1466.28	1327.68	1252.605	0.068	0.075	0.080
	S10	30.203	63.126	49.140	72.186	2133.06	1862.46	1715.885	0.034	0.039	0.042
	S3	6.530	153.257	52.508	155.216	1578.66	1427.46	1345.56	0.098	0.109	0.115
	S11	485.558	11.526	489.016	157.193	2126.088	1904.688	1784.763	0.230	0.257	0.274
6	S1	160.681	80.382	184.796	128.586	897.4	823.9	784.525	0.206	0.224	0.236
	S9	224.424	35.128	234.962	102.455	1443.47	1299.97	1223.095	0.163	0.181	0.192
	S2	8.227	119.254	44.003	121.722	1710.66	1548.96	1462.335	0.071	0.079	0.083
	S10	32.397	82.084	57.022	91.803	2488.57	2172.87	2003.745	0.037	0.042	0.046
	S3	10.583	183.207	65.545	186.381	1841.77	1665.37	1570.87	0.101	0.112	0.119
	S11	611.857	6.898	613.926	190.455	2480.436	2222.136	2083.761	0.248	0.276	0.295
5	S1	191.710	92.256	219.387	149.769	1025.6	941.6	902.225	0.214	0.233	0.243
	S9	272.135	44.518	285.490	126.159	1649.68	1485.68	1408.805	0.173	0.192	0.203
	S2	8.538	140.846	50.792	143.407	1955.04	1770.24	1683.615	0.073	0.081	0.085
	S10	36.329	101.524	66.786	112.423	2844.08	2483.28	2314.155	0.040	0.045	0.049
	S3	16.297	212.703	80.108	217.592	2104.88	1903.28	1808.78	0.103	0.114	0.120
	S11	741.161	2.364	741.870	224.712	2834.784	2539.584	2401.209	0.262	0.292	0.309
4	S1	222.539	103.456	253.576	170.217	1153.8	1059.3	1025.175	0.220	0.239	0.247
	S9	319.726	55.594	336.404	151.512	1855.89	1671.39	1604.765	0.181	0.201	0.210
	S2	8.246	161.271	56.627	163.745	2199.42	1991.52	1916.445	0.074	0.082	0.085
	S10	42.117	121.772	78.648	134.407	3199.59	2793.69	2647.115	0.042	0.048	0.051
	S3	23.102	240.190	95.159	247.121	2367.99	2141.19	2059.29	0.104	0.115	0.120

	S11	864.070	1.592	864.547	260.813	3189.132	2857.032	2737.107	0.271	0.303	0.316
3	S1	254.119	114.300	288.409	190.535	1282	1177	1153.375	0.225	0.245	0.250
	S9	364.841	66.132	384.681	175.584	2062.1	1857.1	1810.975	0.187	0.207	0.212
	S2	10.487	179.173	64.238	182.319	2443.8	2212.8	2160.825	0.075	0.082	0.084
	S10	48.951	140.028	90.960	154.713	3555.1	3104.1	3002.625	0.044	0.050	0.052
	S3	29.999	264.465	109.338	273.464	2631.1	2379.1	2322.4	0.104	0.115	0.118
	S11	977.866	5.872	979.628	299.232	3543.48	3174.48	3091.455	0.276	0.309	0.317
2	S1	282.976	123.995	320.174	208.888	1410.2	1294.7	1281.575	0.227	0.247	0.250
	S9	404.336	75.857	427.093	197.158	2268.31	2042.81	2017.185	0.188	0.209	0.212
	S2	14.211	194.000	72.411	198.263	2688.18	2434.08	2405.205	0.074	0.081	0.082
	S10	56.164	155.869	102.925	172.719	3910.61	3414.51	3358.135	0.044	0.051	0.051
	S3	36.089	283.736	121.210	294.563	2894.21	2617.01	2585.51	0.102	0.113	0.114
	S11	1071.419	10.699	1074.628	332.124	3897.828	3491.928	3445.803	0.276	0.308	0.312
1	S1	303.357	130.439	342.489	221.446	1538.4	1412.4	1409.775	0.223	0.242	0.243
	S9	431.455	82.539	456.217	211.976	2474.52	2228.52	2223.395	0.184	0.205	0.205
	S2	16.506	204.634	77.896	209.586	2932.56	2655.36	2649.585	0.071	0.079	0.079
	S10	61.564	166.804	111.606	185.274	4266.12	3724.92	3713.645	0.043	0.050	0.050
	S3	41.233	296.638	130.224	309.008	3157.32	2854.92	2848.62	0.098	0.108	0.108
	S11	1131.107	15.293	1135.695	354.625	4252.176	3809.376	3800.151	0.267	0.298	0.299

Çizelge B.137: 6 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.169	2.946	9.053	5.397	128.2	122.95	112.45	0.071	0.074	0.081
	S9	11.439	0.670	11.640	4.102	206.21	195.96	175.46	0.056	0.059	0.066
	S2	2.209	3.724	3.326	4.386	244.38	232.83	209.73	0.018	0.019	0.021
	S10	7.536	2.347	8.240	4.607	355.51	332.96	287.86	0.023	0.025	0.029
	S3	1.197	6.645	3.190	7.004	263.11	250.51	225.31	0.027	0.028	0.031
	S11	41.053	4.454	42.389	16.770	354.348	335.898	298.998	0.120	0.126	0.142
5	S1	23.382	8.081	25.806	15.095	256.4	245.9	230.15	0.101	0.105	0.112
	S9	31.553	3.018	32.458	12.484	412.42	391.92	361.17	0.079	0.083	0.090
	S2	6.261	10.746	9.484	12.624	488.76	465.66	431.01	0.026	0.027	0.029
	S10	17.998	7.422	20.225	12.822	711.02	665.92	598.27	0.028	0.030	0.034
	S3	2.048	16.659	7.046	17.274	526.22	501.02	463.22	0.033	0.034	0.037
	S11	100.825	7.290	103.012	37.538	708.696	671.796	616.446	0.145	0.153	0.167
4	S1	39.232	13.373	43.243	25.142	384.6	368.85	353.1	0.112	0.117	0.122
	S9	52.469	5.564	54.139	21.305	618.63	587.88	557.13	0.088	0.092	0.097
	S2	10.322	18.001	15.722	21.097	733.14	698.49	663.84	0.029	0.030	0.032
	S10	29.455	12.746	33.279	21.582	1066.53	998.88	931.23	0.031	0.033	0.036
	S3	2.864	26.694	10.872	27.553	789.33	751.53	713.73	0.035	0.037	0.039
	S11	163.498	10.101	166.529	59.151	1063.044	1007.694	952.344	0.157	0.165	0.175
3	S1	55.035	18.369	60.546	34.879	512.8	491.8	481.3	0.118	0.123	0.126
	S9	74.273	8.003	76.674	30.285	824.84	783.84	763.34	0.093	0.098	0.100
	S2	14.170	25.654	21.866	29.905	977.52	931.32	908.22	0.031	0.032	0.033
	S10	39.332	19.237	45.103	31.037	1422.04	1331.84	1286.74	0.032	0.034	0.035
	S3	3.817	36.484	14.763	37.629	1052.44	1002.04	976.84	0.036	0.038	0.039
	S11	227.982	11.047	231.296	79.441	1417.392	1343.592	1306.692	0.163	0.172	0.177
2	S1	69.167	22.729	75.985	43.479	641	614.75	609.5	0.119	0.124	0.125
	S9	94.373	10.200	97.433	38.512	1031.05	979.8	969.55	0.094	0.099	0.100
	S2	17.517	33.023	27.424	38.278	1221.9	1164.15	1152.6	0.031	0.033	0.033
	S10	46.929	25.993	54.727	40.072	1777.55	1664.8	1642.25	0.031	0.033	0.033
	S3	4.773	45.158	18.320	46.590	1315.55	1252.55	1239.95	0.035	0.037	0.038
	S11	285.987	9.975	288.980	95.771	1771.74	1679.49	1661.04	0.163	0.172	0.174
1	S1	79.098	26.065	86.918	49.794	769.2	737.7	737.7	0.113	0.118	0.118
	S9	109.210	11.891	112.777	44.654	1237.26	1175.76	1175.76	0.091	0.096	0.096
	S2	19.421	38.968	31.112	44.794	1466.28	1396.98	1396.98	0.031	0.032	0.032
	S10	51.892	31.999	61.491	47.566	2133.06	1997.76	1997.76	0.029	0.031	0.031
	S3	5.392	51.686	20.898	53.304	1578.66	1503.06	1503.06	0.034	0.035	0.035
	S11	325.906	7.246	328.080	105.018	2126.088	2015.388	2015.388	0.154	0.163	0.163

Çizelge B.138: 9 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	9.900	4.510	11.253	7.480	128.2	117.7	104.575	0.088	0.096	0.108
	S9	13.387	1.060	13.705	5.076	206.21	185.71	160.085	0.066	0.074	0.086
	S2	0.984	5.338	2.586	5.633	244.38	221.28	192.405	0.023	0.025	0.029
	S10	5.370	2.392	6.087	4.003	355.51	310.41	254.035	0.017	0.020	0.024
	S3	1.649	11.198	5.008	11.692	263.11	237.91	206.41	0.044	0.049	0.057
	S11	44.837	5.476	46.480	18.927	354.348	317.448	271.323	0.131	0.146	0.171
8	S1	28.782	12.269	32.462	20.903	256.4	235.4	207.05	0.127	0.138	0.157
	S9	37.974	4.609	39.357	16.001	412.42	371.42	316.07	0.095	0.106	0.125
	S2	3.838	15.445	8.471	16.596	488.76	442.56	380.19	0.034	0.038	0.044
	S10	14.028	8.499	16.577	12.708	711.02	620.82	499.05	0.023	0.027	0.033
	S3	2.323	27.334	10.523	28.031	526.22	475.82	407.78	0.053	0.059	0.069
	S11	113.576	8.766	116.206	42.839	708.696	634.896	535.266	0.164	0.183	0.217
7	S1	48.931	20.268	55.011	34.947	384.6	353.1	314.25	0.143	0.156	0.175
	S9	64.194	8.428	66.722	27.686	618.63	557.13	481.28	0.108	0.120	0.139
	S2	7.077	25.831	14.826	27.954	733.14	663.84	578.37	0.038	0.042	0.048
	S10	24.576	14.994	29.074	22.367	1066.53	931.23	764.36	0.027	0.031	0.038
	S3	3.177	43.636	16.268	44.589	789.33	713.73	620.49	0.056	0.062	0.072
	S11	188.811	12.689	192.618	69.332	1063.044	952.344	815.814	0.181	0.202	0.236
6	S1	70.523	28.187	78.979	49.344	512.8	470.8	426.7	0.154	0.168	0.185
	S9	93.863	12.267	97.543	40.425	824.84	742.84	656.74	0.118	0.131	0.149
	S2	10.643	37.376	21.856	40.569	977.52	885.12	788.1	0.042	0.046	0.051
	S10	34.190	23.732	41.310	33.989	1422.04	1241.64	1052.22	0.029	0.033	0.039
	S3	4.570	60.421	22.696	61.792	1052.44	951.64	845.8	0.059	0.065	0.073
	S11	274.116	14.628	278.504	96.863	1417.392	1269.792	1114.812	0.196	0.219	0.250
5	S1	93.044	35.864	103.803	63.777	641	588.5	544.4	0.162	0.176	0.191
	S9	125.822	16.013	130.625	53.759	1031.05	928.55	842.45	0.127	0.141	0.155
	S2	14.702	49.752	29.628	54.162	1221.9	1106.4	1009.38	0.044	0.049	0.054
	S10	43.232	33.987	53.428	46.956	1777.55	1552.05	1362.63	0.030	0.034	0.039
	S3	6.531	77.141	29.673	79.101	1315.55	1189.55	1083.71	0.060	0.066	0.073
	S11	366.150	14.992	370.647	124.837	1771.74	1587.24	1432.26	0.209	0.234	0.259
4	S1	114.822	43.043	127.735	77.490	769.2	706.2	667.35	0.166	0.181	0.191
	S9	158.614	19.626	164.502	67.211	1237.26	1114.26	1038.41	0.133	0.148	0.158
	S2	17.802	62.008	36.404	67.349	1466.28	1327.68	1242.21	0.046	0.051	0.054
	S10	51.534	45.999	65.333	61.459	2133.06	1862.46	1695.59	0.031	0.035	0.039
	S3	8.405	93.211	36.368	95.732	1578.66	1427.46	1334.22	0.061	0.067	0.072
	S11	460.387	14.285	464.673	152.401	2126.088	1904.688	1768.158	0.219	0.244	0.263
3	S1	136.244	49.328	151.043	90.201	897.4	823.9	795.55	0.168	0.183	0.190
	S9	190.917	23.170	197.868	80.445	1443.47	1299.97	1244.62	0.137	0.152	0.159
	S2	19.737	73.863	41.896	79.785	1710.66	1548.96	1486.59	0.047	0.052	0.054
	S10	56.591	57.590	73.868	74.567	2488.57	2172.87	2051.1	0.030	0.034	0.036
	S3	11.493	108.620	44.079	112.068	1841.77	1665.37	1597.33	0.061	0.067	0.070
	S11	556.058	11.933	559.638	178.751	2480.436	2222.136	2122.506	0.226	0.252	0.264
2	S1	155.420	54.781	171.854	101.407	1025.6	941.6	923.75	0.168	0.183	0.186
	S9	220.117	27.747	228.441	93.782	1649.68	1485.68	1450.83	0.138	0.154	0.157
	S2	21.024	84.168	46.275	90.476	1955.04	1770.24	1730.97	0.046	0.051	0.052
	S10	61.393	67.494	81.641	85.912	2844.08	2483.28	2406.61	0.030	0.035	0.036
	S3	15.044	121.734	51.565	126.247	2104.88	1903.28	1860.44	0.060	0.066	0.068
	S11	637.658	8.910	640.331	200.208	2834.784	2539.584	2476.854	0.226	0.252	0.259
1	S1	168.911	58.792	186.549	109.466	1153.8	1059.3	1051.95	0.162	0.176	0.177
	S9	241.710	32.162	251.359	104.675	1855.89	1671.39	1657.04	0.135	0.150	0.152
	S2	21.385	91.821	48.931	98.236	2199.42	1991.52	1975.35	0.045	0.049	0.050
	S10	65.575	75.739	88.297	95.412	3199.59	2793.69	2762.12	0.030	0.034	0.035
	S3	17.860	130.826	57.107	136.184	2367.99	2141.19	2123.55	0.058	0.064	0.064
	S11	689.357	5.322	690.954	212.129	3189.132	2857.032	2831.202	0.217	0.242	0.244

Çizelge B.139: 12 Kat, İstanbul, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_{G+\beta Q_0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q_0}$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	11.951	7.931	14.330	11.516	128.2	117.7	117.7	0.112	0.122	0.122
	S9	15.701	1.480	16.145	6.191	206.21	185.71	185.71	0.078	0.087	0.087
	S2	0.789	9.393	3.607	9.630	244.38	221.28	221.28	0.039	0.044	0.044
	S10	1.677	2.727	2.495	3.230	355.51	310.41	310.41	0.009	0.010	0.010
	S3	1.944	20.464	8.083	21.047	263.11	237.91	237.91	0.080	0.088	0.088
	S11	47.226	7.166	49.376	21.334	354.348	317.448	317.448	0.139	0.156	0.156
11	S1	35.306	21.462	41.744	32.053	256.4	235.4	235.4	0.163	0.177	0.177
	S9	45.805	7.189	47.961	20.931	412.42	371.42	371.42	0.116	0.129	0.129
	S2	0.223	27.074	8.345	27.140	488.76	442.56	442.56	0.056	0.061	0.061
	S10	7.054	11.587	10.530	13.703	711.02	620.82	620.82	0.019	0.022	0.022
	S3	1.957	49.330	16.756	49.918	526.22	475.82	475.82	0.095	0.105	0.105
	S11	123.595	10.415	126.720	47.494	708.696	634.896	634.896	0.179	0.200	0.200
10	S1	60.366	35.383	70.981	53.492	384.6	353.1	353.1	0.185	0.201	0.201
	S9	78.042	13.354	82.048	36.767	618.63	557.13	557.13	0.133	0.147	0.147
	S2	1.778	45.084	15.303	45.617	733.14	663.84	663.84	0.062	0.069	0.069
	S10	14.837	21.004	21.139	25.456	1066.53	931.23	931.23	0.024	0.027	0.027
	S3	2.280	78.539	25.842	79.223	789.33	713.73	713.73	0.100	0.111	0.111
	S11	208.745	15.002	213.245	77.626	1063.044	952.344	952.344	0.201	0.224	0.224
9	S1	87.739	49.348	102.543	75.670	512.8	470.8	457.675	0.200	0.218	0.224
	S9	115.428	19.662	121.327	54.290	824.84	742.84	717.215	0.147	0.163	0.169
	S2	3.775	65.182	23.329	66.315	977.52	885.12	856.245	0.068	0.075	0.077
	S10	21.462	34.277	31.745	40.715	1422.04	1241.64	1185.265	0.029	0.033	0.034
	S3	3.331	109.058	36.049	110.057	1052.44	951.64	920.14	0.105	0.116	0.120
	S11	308.714	16.381	313.628	108.995	1417.392	1269.792	1223.667	0.221	0.247	0.256
8	S1	117.335	63.326	136.333	98.527	641	588.5	564.875	0.213	0.232	0.241
	S9	157.221	26.028	165.029	73.194	1031.05	928.55	882.425	0.160	0.178	0.187
	S2	6.626	87.113	32.759	89.100	1221.9	1106.4	1054.425	0.073	0.081	0.085
	S10	27.861	50.431	42.990	58.789	1777.55	1552.05	1450.575	0.033	0.038	0.041
	S3	5.277	140.447	47.411	142.030	1315.55	1189.55	1132.85	0.108	0.119	0.125
	S11	421.969	15.490	426.616	142.081	1771.74	1587.24	1504.215	0.241	0.269	0.284
7	S1	147.627	77.122	170.764	121.411	769.2	706.2	672.075	0.222	0.242	0.254
	S9	202.916	32.557	212.684	93.432	1237.26	1114.26	1047.635	0.172	0.191	0.203
	S2	8.455	109.949	41.439	112.485	1466.28	1327.68	1252.605	0.077	0.085	0.090
	S10	33.978	71.016	55.283	81.210	2133.06	1862.46	1715.885	0.038	0.044	0.047
	S3	7.347	172.415	59.071	174.619	1578.66	1427.46	1345.56	0.111	0.122	0.130
	S11	546.253	12.966	550.143	176.842	2126.088	1904.688	1784.763	0.259	0.289	0.308
6	S1	180.766	90.429	207.895	144.659	897.4	823.9	784.525	0.232	0.252	0.265
	S9	252.477	39.519	264.333	115.262	1443.47	1299.97	1223.095	0.183	0.203	0.216
	S2	9.255	134.161	49.504	136.938	1710.66	1548.96	1462.335	0.080	0.088	0.094
	S10	36.446	92.345	64.150	103.278	2488.57	2172.87	2003.745	0.042	0.048	0.052
	S3	11.906	206.107	73.738	209.679	1841.77	1665.37	1570.87	0.114	0.126	0.133
	S11	688.339	7.760	690.667	214.262	2480.436	2222.136	2083.761	0.278	0.311	0.331
5	S1	215.674	103.788	246.810	168.490	1025.6	941.6	902.225	0.241	0.262	0.274
	S9	306.152	50.083	321.177	141.929	1649.68	1485.68	1408.805	0.195	0.216	0.228
	S2	9.605	158.451	57.141	161.333	1955.04	1770.24	1683.615	0.083	0.091	0.096
	S10	40.870	114.215	75.135	126.476	2844.08	2483.28	2314.155	0.044	0.051	0.055
	S3	18.334	239.291	90.121	244.791	2104.88	1903.28	1808.78	0.116	0.129	0.135
	S11	833.806	2.659	834.604	252.801	2834.784	2539.584	2401.209	0.294	0.329	0.348
4	S1	250.357	116.387	285.273	191.494	1153.8	1059.3	1025.175	0.247	0.269	0.278
	S9	359.691	62.544	378.454	170.451	1855.89	1671.39	1604.765	0.204	0.226	0.236
	S2	9.277	181.430	63.705	184.213	2199.42	1991.52	1916.445	0.084	0.092	0.096

	S10	47.382	136.993	88.479	151.208	3199.59	2793.69	2647.115	0.047	0.054	0.057
	S3	25.990	270.214	107.054	278.011	2367.99	2141.19	2059.29	0.117	0.130	0.135
	S11	972.078	1.791	972.616	293.414	3189.132	2857.032	2737.107	0.305	0.340	0.355
3	S1	285.883	128.587	324.460	214.352	1282	1177	1153.375	0.253	0.276	0.281
	S9	410.446	74.398	432.766	197.532	2062.1	1857.1	1810.975	0.210	0.233	0.239
	S2	11.797	201.570	72.268	205.109	2443.8	2212.8	2160.825	0.084	0.093	0.095
	S10	55.070	157.531	102.330	174.052	3555.1	3104.1	3002.625	0.049	0.056	0.058
	S3	33.749	297.523	123.005	307.647	2631.1	2379.1	2322.4	0.117	0.129	0.132
	S11	1100.099	6.606	1102.081	336.636	3543.48	3174.48	3091.455	0.311	0.347	0.356
2	S1	318.347	139.495	360.196	234.999	1410.2	1294.7	1281.575	0.255	0.278	0.281
	S9	454.878	85.339	480.480	221.802	2268.31	2042.81	2017.185	0.212	0.235	0.238
	S2	15.987	218.250	81.462	223.046	2688.18	2434.08	2405.205	0.083	0.092	0.093
	S10	63.185	175.353	115.791	194.308	3910.61	3414.51	3358.135	0.050	0.057	0.058
	S3	40.600	319.203	136.361	331.383	2894.21	2617.01	2585.51	0.114	0.127	0.128
	S11	1205.346	12.036	1208.957	373.640	3897.828	3491.928	3445.803	0.310	0.346	0.351
1	S1	341.277	146.744	385.300	249.127	1538.4	1412.4	1409.775	0.250	0.273	0.273
	S9	485.387	92.856	513.244	238.472	2474.52	2228.52	2223.395	0.207	0.230	0.231
	S2	18.569	230.213	87.633	235.784	2932.56	2655.36	2649.585	0.080	0.089	0.089
	S10	69.260	187.655	125.556	208.433	4266.12	3724.92	3713.645	0.049	0.056	0.056
	S3	46.387	333.718	146.502	347.634	3157.32	2854.92	2848.62	0.110	0.122	0.122
	S11	1272.495	17.205	1277.657	398.953	4252.176	3809.376	3800.151	0.300	0.335	0.336

Çizelge B.140: 6 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	15.317	5.524	16.975	10.120	128.2	122.95	112.45	0.132	0.138	0.151
	S9	21.448	1.256	21.825	7.691	206.21	195.96	175.46	0.106	0.111	0.124
	S2	4.141	6.982	6.236	8.224	244.38	232.83	209.73	0.034	0.035	0.039
	S10	14.129	4.400	15.449	8.639	355.51	332.96	287.86	0.043	0.046	0.054
	S3	2.244	12.460	5.982	13.133	263.11	250.51	225.31	0.050	0.052	0.058
	S11	76.974	8.352	79.479	31.444	354.348	335.898	298.998	0.224	0.237	0.266
5	S1	43.841	15.151	48.386	28.304	256.4	245.9	230.15	0.189	0.197	0.210
	S9	59.161	5.659	60.859	23.407	412.42	391.92	361.17	0.148	0.155	0.169
	S2	11.739	20.148	17.783	23.669	488.76	465.66	431.01	0.048	0.051	0.055
	S10	33.747	13.916	37.922	24.040	711.02	665.92	598.27	0.053	0.057	0.063
	S3	3.841	31.236	13.212	32.388	526.22	501.02	463.22	0.062	0.065	0.070
	S11	189.046	13.669	193.147	70.383	708.696	671.796	616.446	0.273	0.288	0.313
4	S1	73.559	25.074	81.081	47.141	384.6	368.85	353.1	0.211	0.220	0.230
	S9	98.380	10.433	101.510	39.947	618.63	587.88	557.13	0.164	0.173	0.182
	S2	19.354	33.751	29.479	39.557	733.14	698.49	663.84	0.054	0.057	0.060
	S10	55.229	23.898	62.398	40.467	1066.53	998.88	931.23	0.059	0.062	0.067
	S3	5.369	50.051	20.385	51.662	789.33	751.53	713.73	0.065	0.069	0.072
	S11	306.559	18.940	312.241	110.908	1063.044	1007.694	952.344	0.294	0.310	0.328
3	S1	103.191	34.442	113.524	65.399	512.8	491.8	481.3	0.221	0.231	0.236
	S9	139.262	15.006	143.764	56.784	824.84	783.84	763.34	0.174	0.183	0.188
	S2	26.569	48.101	40.999	56.071	977.52	931.32	908.22	0.057	0.060	0.062
	S10	73.748	36.070	84.569	58.194	1422.04	1331.84	1286.74	0.059	0.063	0.066
	S3	7.157	68.407	27.680	70.555	1052.44	1002.04	976.84	0.067	0.070	0.072
	S11	427.466	20.713	433.680	148.952	1417.392	1343.592	1306.692	0.306	0.323	0.332
2	S1	129.688	42.617	142.473	81.523	641	614.75	609.5	0.222	0.232	0.234
	S9	176.949	19.126	182.687	72.210	1031.05	979.8	969.55	0.177	0.186	0.188
	S2	32.844	61.919	51.420	71.772	1221.9	1164.15	1152.6	0.059	0.062	0.062
	S10	87.992	48.737	102.613	75.135	1777.55	1664.8	1642.25	0.058	0.062	0.062
	S3	8.949	84.672	34.350	87.356	1315.55	1252.55	1239.95	0.066	0.070	0.070
	S11	536.226	18.703	541.837	179.571	1771.74	1679.49	1661.04	0.306	0.323	0.326
1	S1	148.309	48.872	162.971	93.364	769.2	737.7	737.7	0.212	0.221	0.221
	S9	204.769	22.295	211.457	83.725	1237.26	1175.76	1175.76	0.171	0.180	0.180
	S2	36.415	73.065	58.334	83.989	1466.28	1396.98	1396.98	0.057	0.060	0.060
	S10	97.297	59.998	115.296	89.187	2133.06	1997.76	1997.76	0.054	0.058	0.058
	S3	10.110	96.911	39.183	99.944	1578.66	1503.06	1503.06	0.063	0.066	0.066
	S11	611.074	13.587	615.150	196.909	2126.088	2015.388	2015.388	0.289	0.305	0.305

Çizelge B.141: 9 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	18.563	8.456	21.100	14.025	128.2	117.7	104.575	0.165	0.179	0.202
	S9	25.101	1.988	25.697	9.518	206.21	185.71	160.085	0.125	0.138	0.161
	S2	1.846	10.008	4.848	10.562	244.38	221.28	192.405	0.043	0.048	0.055
	S10	10.068	4.485	11.413	7.505	355.51	310.41	254.035	0.032	0.037	0.045
	S3	3.091	20.995	9.390	21.923	263.11	237.91	206.41	0.083	0.092	0.106
	S11	84.070	10.268	87.150	35.489	354.348	317.448	271.323	0.246	0.275	0.321
8	S1	53.965	23.004	60.867	39.193	256.4	235.4	207.05	0.237	0.259	0.294
	S9	71.202	8.641	73.794	30.002	412.42	371.42	316.07	0.179	0.199	0.233
	S2	7.196	28.959	15.884	31.118	488.76	442.56	380.19	0.064	0.070	0.082
	S10	26.302	15.936	31.083	23.827	711.02	620.82	499.05	0.044	0.050	0.062
	S3	4.355	51.252	19.731	52.558	526.22	475.82	407.78	0.100	0.110	0.129
	S11	212.955	16.437	217.886	80.323	708.696	634.896	535.266	0.307	0.343	0.407
7	S1	91.745	38.003	103.146	65.526	384.6	353.1	314.25	0.268	0.292	0.328
	S9	120.364	15.802	125.104	51.911	618.63	557.13	481.28	0.202	0.225	0.260
	S2	13.269	48.434	27.799	52.414	733.14	663.84	578.37	0.071	0.079	0.091
	S10	46.080	28.113	54.514	41.937	1066.53	931.23	764.36	0.051	0.059	0.071
	S3	5.957	81.817	30.502	83.604	789.33	713.73	620.49	0.106	0.117	0.135
	S11	354.021	23.792	361.159	129.998	1063.044	952.344	815.814	0.340	0.379	0.443
6	S1	132.231	52.850	148.086	92.519	512.8	470.8	426.7	0.289	0.315	0.347
	S9	175.993	23.000	182.893	75.798	824.84	742.84	656.74	0.222	0.246	0.278
	S2	19.956	70.079	40.979	76.066	977.52	885.12	788.1	0.078	0.086	0.097
	S10	64.106	44.498	77.456	63.730	1422.04	1241.64	1052.22	0.054	0.062	0.074
	S3	8.569	113.289	42.556	115.860	1052.44	951.64	845.8	0.110	0.122	0.137
	S11	513.967	27.427	522.196	181.617	1417.392	1269.792	1114.812	0.368	0.411	0.468
5	S1	174.458	67.244	194.631	119.581	641	588.5	544.4	0.304	0.331	0.358
	S9	235.916	30.023	244.923	100.798	1031.05	928.55	842.45	0.238	0.264	0.291
	S2	27.567	93.284	55.552	101.554	1221.9	1106.4	1009.38	0.083	0.092	0.101
	S10	81.059	63.725	100.177	88.042	1777.55	1552.05	1362.63	0.056	0.065	0.074
	S3	12.245	144.640	55.637	148.314	1315.55	1189.55	1083.71	0.113	0.125	0.137
	S11	686.530	28.110	694.963	234.069	1771.74	1587.24	1432.26	0.392	0.438	0.485
4	S1	215.291	80.706	239.503	145.293	769.2	706.2	667.35	0.311	0.339	0.359
	S9	297.401	36.800	308.441	126.020	1237.26	1114.26	1038.41	0.249	0.277	0.297
	S2	33.379	116.266	68.258	126.279	1466.28	1327.68	1242.21	0.086	0.095	0.102
	S10	96.625	86.248	122.500	115.235	2133.06	1862.46	1695.59	0.057	0.066	0.072
	S3	15.759	174.770	68.190	179.497	1578.66	1427.46	1334.22	0.114	0.126	0.135
	S11	863.226	26.784	871.261	285.752	2126.088	1904.688	1768.158	0.410	0.457	0.493
3	S1	255.458	92.490	283.205	169.127	897.4	823.9	795.55	0.316	0.344	0.356
	S9	357.970	43.444	371.003	150.835	1443.47	1299.97	1244.62	0.257	0.285	0.298
	S2	37.007	138.494	78.555	149.596	1710.66	1548.96	1486.59	0.087	0.097	0.101
	S10	106.108	107.981	138.502	139.813	2488.57	2172.87	2051.1	0.056	0.064	0.068
	S3	21.549	203.663	82.648	210.128	1841.77	1665.37	1597.33	0.114	0.126	0.132
	S11	1042.609	22.375	1049.321	335.158	2480.436	2222.136	2122.506	0.423	0.472	0.494
2	S1	291.412	102.715	322.227	190.139	1025.6	941.6	923.75	0.314	0.342	0.349
	S9	412.720	52.026	428.327	175.842	1649.68	1485.68	1450.83	0.260	0.288	0.295
	S2	39.421	157.816	86.765	169.642	1955.04	1770.24	1730.97	0.087	0.096	0.098
	S10	115.112	126.552	153.077	161.086	2844.08	2483.28	2406.61	0.057	0.065	0.067
	S3	28.208	228.251	96.683	236.713	2104.88	1903.28	1860.44	0.112	0.124	0.127
	S11	1195.609	16.707	1200.621	375.390	2834.784	2539.584	2476.854	0.424	0.473	0.485
1	S1	316.708	110.236	349.779	205.248	1153.8	1059.3	1051.95	0.303	0.330	0.333
	S9	453.207	60.304	471.298	196.266	1855.89	1671.39	1657.04	0.254	0.282	0.284
	S2	40.098	172.163	91.747	184.193	2199.42	1991.52	1975.35	0.084	0.092	0.093
	S10	122.953	142.011	165.556	178.897	3199.59	2793.69	2762.12	0.056	0.064	0.065
	S3	33.487	245.300	107.077	255.346	2367.99	2141.19	2123.55	0.108	0.119	0.120
	S11	1292.544	9.979	1295.538	397.742	3189.132	2857.032	2831.202	0.406	0.453	0.458

Çizelge B.142: 12 Kat, İstanbul, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	18.800	12.476	22.543	18.116	128.2	117.7	117.7	0.176	0.192	0.192
	S9	24.701	2.329	25.399	9.739	206.21	185.71	185.71	0.123	0.137	0.137
	S2	1.241	14.777	5.674	15.149	244.38	221.28	221.28	0.062	0.068	0.068
	S10	2.639	4.290	3.926	5.081	355.51	310.41	310.41	0.014	0.016	0.016
	S3	3.058	32.194	12.716	33.111	263.11	237.91	237.91	0.126	0.139	0.139
	S11	74.295	11.274	77.677	33.562	354.348	317.448	317.448	0.219	0.245	0.245
11	S1	55.542	33.763	65.671	50.425	256.4	235.4	235.4	0.256	0.279	0.279
	S9	72.059	11.310	75.452	32.927	412.42	371.42	371.42	0.183	0.203	0.203
	S2	0.350	42.591	13.128	42.696	488.76	442.56	442.56	0.087	0.096	0.096
	S10	11.097	18.228	16.565	21.557	711.02	620.82	620.82	0.030	0.035	0.035
	S3	3.079	77.605	26.360	78.529	526.22	475.82	475.82	0.149	0.165	0.165
	S11	194.437	16.385	199.352	74.716	708.696	634.896	634.896	0.281	0.314	0.314
10	S1	94.966	55.663	111.665	84.153	384.6	353.1	353.1	0.290	0.316	0.316
	S9	122.773	21.008	129.076	57.840	618.63	557.13	557.13	0.209	0.232	0.232
	S2	2.797	70.924	24.074	71.763	733.14	663.84	663.84	0.098	0.108	0.108
	S10	23.342	33.044	33.255	40.046	1066.53	931.23	931.23	0.038	0.043	0.043
	S3	3.587	123.555	40.654	124.631	789.33	713.73	713.73	0.158	0.175	0.175
	S11	328.392	23.601	335.472	122.119	1063.044	952.344	952.344	0.316	0.352	0.352
9	S1	138.029	77.633	161.319	119.042	512.8	470.8	457.675	0.315	0.343	0.352
	S9	181.589	30.931	190.869	85.408	824.84	742.84	717.215	0.231	0.257	0.266
	S2	5.938	102.543	36.701	104.325	977.52	885.12	856.245	0.107	0.118	0.122
	S10	33.763	53.923	49.940	64.052	1422.04	1241.64	1185.265	0.045	0.052	0.054
	S3	5.241	171.568	56.711	173.140	1052.44	951.64	920.14	0.165	0.182	0.188
	S11	485.661	25.770	493.392	171.468	1417.392	1269.792	1223.667	0.348	0.389	0.403
8	S1	184.589	99.624	214.476	155.000	641	588.5	564.875	0.335	0.364	0.380
	S9	247.336	40.946	259.620	115.147	1031.05	928.55	882.425	0.252	0.280	0.294
	S2	10.423	137.043	51.536	140.170	1221.9	1106.4	1054.425	0.115	0.127	0.133
	S10	43.830	79.336	67.631	92.485	1777.55	1552.05	1450.575	0.052	0.060	0.064
	S3	8.302	220.948	74.586	223.439	1315.55	1189.55	1132.85	0.170	0.188	0.197
	S11	663.832	24.369	671.143	223.518	1771.74	1587.24	1504.215	0.379	0.423	0.446
7	S1	232.244	121.327	268.642	191.000	769.2	706.2	672.075	0.349	0.380	0.400
	S9	319.223	51.218	334.589	146.985	1237.26	1114.26	1047.635	0.270	0.300	0.319
	S2	13.301	172.969	65.192	176.959	1466.28	1327.68	1252.605	0.121	0.133	0.141
	S10	53.453	111.721	86.969	127.757	2133.06	1862.46	1715.885	0.060	0.069	0.074
	S3	11.557	271.238	92.929	274.706	1578.66	1427.46	1345.56	0.174	0.192	0.204
	S11	859.352	20.398	865.472	278.204	2126.088	1904.688	1784.763	0.407	0.454	0.485
6	S1	284.377	142.261	327.056	227.575	897.4	823.9	784.525	0.364	0.397	0.417
	S9	397.191	62.171	415.842	181.328	1443.47	1299.97	1223.095	0.288	0.320	0.340
	S2	14.560	211.059	77.878	215.427	1710.66	1548.96	1462.335	0.126	0.139	0.147
	S10	57.337	145.274	100.919	162.475	2488.57	2172.87	2003.745	0.065	0.075	0.081
	S3	18.730	324.243	116.003	329.862	1841.77	1665.37	1570.87	0.179	0.198	0.210
	S11	1082.878	12.208	1086.540	337.071	2480.436	2222.136	2083.761	0.438	0.489	0.521
5	S1	339.293	163.277	388.276	265.065	1025.6	941.6	902.225	0.379	0.412	0.430
	S9	481.630	78.790	505.267	223.279	1649.68	1485.68	1408.805	0.306	0.340	0.359
	S2	15.111	249.272	89.892	253.805	1955.04	1770.24	1683.615	0.130	0.143	0.151
	S10	64.296	179.680	118.200	198.968	2844.08	2483.28	2314.155	0.070	0.080	0.086
	S3	28.842	376.447	141.776	385.100	2104.88	1903.28	1808.78	0.183	0.202	0.213
	S11	1311.724	4.183	1312.979	397.700	2834.784	2539.584	2401.209	0.463	0.517	0.547
4	S1	393.855	183.098	448.784	301.254	1153.8	1059.3	1025.175	0.389	0.424	0.438
	S9	565.857	98.392	595.375	268.149	1855.89	1671.39	1604.765	0.321	0.356	0.371
	S2	14.594	285.421	100.220	289.799	2199.42	1991.52	1916.445	0.132	0.146	0.151
	S10	74.540	215.514	139.194	237.876	3199.59	2793.69	2647.115	0.074	0.085	0.090
	S3	40.886	425.094	168.415	437.360	2367.99	2141.19	2059.29	0.185	0.204	0.212

	S11	1529.250	2.817	1530.095	461.592	3189.132	2857.032	2737.107	0.480	0.536	0.559
3	S1	449.745	202.291	510.432	337.214	1282	1177	1153.375	0.398	0.434	0.443
	S9	645.704	117.042	680.816	310.753	2062.1	1857.1	1810.975	0.330	0.367	0.376
	S2	18.559	317.105	113.691	322.672	2443.8	2212.8	2160.825	0.132	0.146	0.149
	S10	86.635	247.825	160.982	273.815	3555.1	3104.1	3002.625	0.077	0.088	0.091
	S3	53.093	468.055	193.509	483.983	2631.1	2379.1	2322.4	0.184	0.203	0.208
	S11	1730.649	10.393	1733.767	529.588	3543.48	3174.48	3091.455	0.489	0.546	0.561
2	S1	500.816	219.449	566.651	369.694	1410.2	1294.7	1281.575	0.402	0.438	0.442
	S9	715.603	134.253	755.879	348.934	2268.31	2042.81	2017.185	0.333	0.370	0.375
	S2	25.150	343.346	128.154	350.891	2688.18	2434.08	2405.205	0.131	0.144	0.146
	S10	99.401	275.861	182.159	305.681	3910.61	3414.51	3358.135	0.078	0.090	0.091
	S3	63.871	502.163	214.520	521.324	2894.21	2617.01	2585.51	0.180	0.199	0.202
	S11	1896.221	18.935	1901.901	587.801	3897.828	3491.928	3445.803	0.488	0.545	0.552
1	S1	536.888	230.854	606.144	391.920	1538.4	1412.4	1409.775	0.394	0.429	0.430
	S9	763.599	146.080	807.422	375.159	2474.52	2228.52	2223.395	0.326	0.362	0.363
	S2	29.212	362.166	137.862	370.930	2932.56	2655.36	2649.585	0.126	0.140	0.140
	S10	108.958	295.214	197.522	327.902	4266.12	3724.92	3713.645	0.077	0.088	0.088
	S3	72.975	524.997	230.474	546.890	3157.32	2854.92	2848.62	0.173	0.192	0.192
	S11	2001.858	27.066	2009.978	627.624	4252.176	3809.376	3800.151	0.473	0.528	0.529

Çizelge B.143: 6 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	21.240	7.661	23.538	14.033	128.2	122.95	112.45	0.184	0.191	0.209
	S9	29.742	1.742	30.264	10.664	206.21	195.96	175.46	0.147	0.154	0.172
	S2	5.743	9.682	8.647	11.404	244.38	232.83	209.73	0.047	0.049	0.054
	S10	19.593	6.101	21.423	11.979	355.51	332.96	287.86	0.060	0.064	0.074
	S3	3.112	17.278	8.295	18.212	263.11	250.51	225.31	0.069	0.073	0.081
	S11	106.737	11.581	110.211	43.602	354.348	335.898	298.998	0.311	0.328	0.369
5	S1	60.793	21.010	67.096	39.248	256.4	245.9	230.15	0.262	0.273	0.292
	S9	82.037	7.847	84.391	32.458	412.42	391.92	361.17	0.205	0.215	0.234
	S2	16.278	27.938	24.659	32.822	488.76	465.66	431.01	0.067	0.070	0.076
	S10	46.796	19.297	52.585	33.336	711.02	665.92	598.27	0.074	0.079	0.088
	S3	5.326	43.314	18.320	44.912	526.22	501.02	463.22	0.085	0.090	0.097
	S11	262.144	18.955	267.830	97.598	708.696	671.796	616.446	0.378	0.399	0.434
4	S1	102.002	34.769	112.433	65.369	384.6	368.85	353.1	0.292	0.305	0.318
	S9	136.420	14.468	140.761	55.394	618.63	587.88	557.13	0.228	0.239	0.253
	S2	26.837	46.801	40.877	54.852	733.14	698.49	663.84	0.075	0.079	0.083
	S10	76.584	33.138	86.525	56.114	1066.53	998.88	931.23	0.081	0.087	0.093
	S3	7.446	69.404	28.267	71.638	789.33	751.53	713.73	0.091	0.095	0.100
	S11	425.096	26.264	432.975	153.792	1063.044	1007.694	952.344	0.407	0.430	0.455
3	S1	143.092	47.759	157.420	90.687	512.8	491.8	481.3	0.307	0.320	0.327
	S9	193.110	20.808	199.353	78.741	824.84	783.84	763.34	0.242	0.254	0.261
	S2	36.843	66.700	56.853	77.752	977.52	931.32	908.22	0.080	0.083	0.086
	S10	102.264	50.017	117.269	80.696	1422.04	1331.84	1286.74	0.082	0.088	0.091
	S3	9.925	94.858	38.382	97.836	1052.44	1002.04	976.84	0.093	0.098	0.100
	S11	592.753	28.722	601.369	206.547	1417.392	1343.592	1306.692	0.424	0.448	0.460
2	S1	179.833	59.095	197.562	113.045	641	614.75	609.5	0.308	0.321	0.324
	S9	245.370	26.521	253.326	100.132	1031.05	979.8	969.55	0.246	0.259	0.261
	S2	45.544	85.861	71.302	99.524	1221.9	1164.15	1152.6	0.081	0.085	0.086
	S10	122.016	67.582	142.290	104.187	1777.55	1664.8	1642.25	0.080	0.085	0.087
	S3	12.409	117.411	47.633	121.134	1315.55	1252.55	1239.95	0.092	0.097	0.098
	S11	743.567	25.935	751.348	249.005	1771.74	1679.49	1661.04	0.424	0.447	0.452
1	S1	205.656	67.769	225.986	129.465	769.2	737.7	737.7	0.294	0.306	0.306
	S9	283.946	30.915	293.221	116.099	1237.26	1175.76	1175.76	0.237	0.249	0.249
	S2	50.495	101.317	80.890	116.465	1466.28	1396.98	1396.98	0.079	0.083	0.083
	S10	134.918	83.197	159.877	123.672	2133.06	1997.76	1997.76	0.075	0.080	0.080
	S3	14.019	134.384	54.334	138.589	1578.66	1503.06	1503.06	0.088	0.092	0.092
	S11	847.356	18.841	853.008	273.047	2126.088	2015.388	2015.388	0.401	0.423	0.423

Çizelge B.144: 9 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	25.740	11.726	29.258	19.448	128.2	117.7	104.575	0.228	0.249	0.280
	S9	34.807	2.757	35.634	13.199	206.21	185.71	160.085	0.173	0.192	0.223
	S2	2.559	13.878	6.722	14.645	244.38	221.28	192.405	0.060	0.066	0.076
	S10	13.961	6.219	15.827	10.407	355.51	310.41	254.035	0.045	0.051	0.062
	S3	4.286	29.114	13.020	30.399	263.11	237.91	206.41	0.116	0.128	0.147
	S11	116.577	14.238	120.848	49.211	354.348	317.448	271.323	0.341	0.381	0.445
8	S1	74.832	31.899	84.402	54.348	256.4	235.4	207.05	0.329	0.359	0.408
	S9	98.734	11.982	102.328	41.602	412.42	371.42	316.07	0.248	0.276	0.324
	S2	9.979	40.157	22.026	43.150	488.76	442.56	380.19	0.088	0.098	0.113
	S10	36.472	22.098	43.101	33.040	711.02	620.82	499.05	0.061	0.069	0.086
	S3	6.040	71.069	27.360	72.881	526.22	475.82	407.78	0.138	0.153	0.179
	S11	295.298	22.792	302.135	111.381	708.696	634.896	535.266	0.426	0.476	0.564
7	S1	127.220	52.698	143.029	90.863	384.6	353.1	314.25	0.372	0.405	0.455
	S9	166.905	21.912	173.478	71.983	618.63	557.13	481.28	0.280	0.311	0.360
	S2	18.400	67.161	38.548	72.681	733.14	663.84	578.37	0.099	0.109	0.126
	S10	63.898	38.984	75.593	58.153	1066.53	931.23	764.36	0.071	0.081	0.099
	S3	8.260	113.453	42.296	115.931	789.33	713.73	620.49	0.147	0.162	0.187
	S11	490.909	32.992	500.807	180.264	1063.044	952.344	815.814	0.471	0.526	0.614
6	S1	183.361	73.285	205.346	128.294	512.8	470.8	426.7	0.400	0.436	0.481
	S9	244.043	31.893	253.611	105.106	824.84	742.84	656.74	0.307	0.341	0.386
	S2	27.672	97.177	56.825	105.478	977.52	885.12	788.1	0.108	0.119	0.134
	S10	88.894	61.704	107.405	88.372	1422.04	1241.64	1052.22	0.076	0.087	0.102
	S3	11.882	157.094	59.010	160.659	1052.44	951.64	845.8	0.153	0.169	0.190
	S11	712.702	38.032	724.111	251.843	1417.392	1269.792	1114.812	0.511	0.570	0.650
5	S1	241.914	93.245	269.888	165.820	641	588.5	544.4	0.421	0.459	0.496
	S9	327.136	41.633	339.626	139.773	1031.05	928.55	842.45	0.329	0.366	0.403
	S2	38.226	129.354	77.032	140.822	1221.9	1106.4	1009.38	0.115	0.127	0.140
	S10	112.402	88.365	138.912	122.086	1777.55	1552.05	1362.63	0.078	0.090	0.102
	S3	16.980	200.568	77.150	205.662	1315.55	1189.55	1083.71	0.156	0.173	0.190
	S11	951.989	38.979	963.683	324.576	1771.74	1587.24	1432.26	0.544	0.607	0.673
4	S1	298.537	111.912	332.110	201.473	769.2	706.2	667.35	0.432	0.470	0.498
	S9	412.397	51.029	427.705	174.748	1237.26	1114.26	1038.41	0.346	0.384	0.412
	S2	46.285	161.222	94.651	175.107	1466.28	1327.68	1242.21	0.119	0.132	0.141
	S10	133.987	119.597	169.866	159.793	2133.06	1862.46	1695.59	0.080	0.091	0.100
	S3	21.852	242.347	94.556	248.903	1578.66	1427.46	1334.22	0.158	0.174	0.187
	S11	1197.007	37.140	1208.149	396.242	2126.088	1904.688	1768.158	0.568	0.634	0.683
3	S1	354.235	128.252	392.711	234.523	897.4	823.9	795.55	0.438	0.477	0.494
	S9	496.385	60.243	514.458	209.158	1443.47	1299.97	1244.62	0.356	0.396	0.413
	S2	51.317	192.045	108.930	207.440	1710.66	1548.96	1486.59	0.121	0.134	0.140
	S10	147.136	149.733	192.056	193.874	2488.57	2172.87	2051.1	0.078	0.089	0.095
	S3	29.881	282.413	114.605	291.377	1841.77	1665.37	1597.33	0.158	0.175	0.182
	S11	1445.751	31.027	1455.059	464.752	2480.436	2222.136	2122.506	0.587	0.655	0.686
2	S1	404.092	142.432	446.821	263.659	1025.6	941.6	923.75	0.436	0.475	0.484
	S9	572.305	72.142	593.947	243.834	1649.68	1485.68	1450.83	0.360	0.400	0.409
	S2	54.663	218.838	120.315	235.237	1955.04	1770.24	1730.97	0.120	0.133	0.136
	S10	159.621	175.486	212.267	223.372	2844.08	2483.28	2406.61	0.079	0.090	0.093
	S3	39.115	316.508	134.068	328.242	2104.88	1903.28	1860.44	0.156	0.172	0.176
	S11	1657.912	23.167	1664.862	520.540	2834.784	2539.584	2476.854	0.587	0.656	0.672
1	S1	439.169	152.860	485.027	284.611	1153.8	1059.3	1051.95	0.420	0.458	0.461
	S9	628.447	83.621	653.533	272.155	1855.89	1671.39	1657.04	0.352	0.391	0.394
	S2	55.602	238.733	127.222	255.414	2199.42	1991.52	1975.35	0.116	0.128	0.129
	S10	170.495	196.922	229.572	248.071	3199.59	2793.69	2762.12	0.078	0.089	0.090
	S3	46.435	340.149	148.479	354.079	2367.99	2141.19	2123.55	0.150	0.165	0.167
	S11	1792.328	13.838	1796.479	551.536	3189.132	2857.032	2831.202	0.563	0.629	0.635

Çizelge B.145: 12 Kat, İstanbul, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	26.070	17.300	31.260	25.121	128.2	117.7	117.7	0.244	0.266	0.266
	S9	34.252	3.229	35.221	13.505	206.21	185.71	185.71	0.171	0.190	0.190
	S2	1.720	20.491	7.868	21.007	244.38	221.28	221.28	0.086	0.095	0.095
	S10	3.659	5.948	5.444	7.046	355.51	310.41	310.41	0.020	0.023	0.023
	S3	4.241	44.642	17.633	45.914	263.11	237.91	237.91	0.175	0.193	0.193
	S11	103.023	15.633	107.712	46.540	354.348	317.448	317.448	0.304	0.339	0.339
11	S1	77.018	46.818	91.063	69.923	256.4	235.4	235.4	0.355	0.387	0.387
	S9	99.922	15.683	104.627	45.659	412.42	371.42	371.42	0.254	0.282	0.282
	S2	0.486	59.060	18.204	59.206	488.76	442.56	442.56	0.121	0.134	0.134
	S10	15.387	25.276	22.970	29.892	711.02	620.82	620.82	0.042	0.048	0.048
	S3	4.269	107.613	36.553	108.894	526.22	475.82	475.82	0.207	0.229	0.229
	S11	269.619	22.721	276.435	103.607	708.696	634.896	634.896	0.390	0.435	0.435
10	S1	131.686	77.186	154.842	116.692	384.6	353.1	353.1	0.403	0.439	0.439
	S9	170.246	29.132	178.985	80.205	618.63	557.13	557.13	0.289	0.321	0.321
	S2	3.878	98.348	33.383	99.512	733.14	663.84	663.84	0.136	0.150	0.150
	S10	32.367	45.821	46.113	55.531	1066.53	931.23	931.23	0.052	0.060	0.060
	S3	4.974	171.330	56.373	172.822	789.33	713.73	713.73	0.219	0.242	0.242
	S11	455.370	32.727	465.188	169.338	1063.044	952.344	952.344	0.438	0.488	0.488
9	S1	191.400	107.651	223.695	165.071	512.8	470.8	457.675	0.436	0.475	0.489
	S9	251.804	42.891	264.671	118.432	824.84	742.84	717.215	0.321	0.356	0.369
	S2	8.234	142.193	50.892	144.663	977.52	885.12	856.245	0.148	0.163	0.169
	S10	46.818	74.774	69.250	88.819	1422.04	1241.64	1185.265	0.062	0.072	0.075
	S3	7.267	237.907	78.639	240.087	1052.44	951.64	920.14	0.228	0.252	0.261
	S11	673.449	35.735	684.170	237.769	1417.392	1269.792	1223.667	0.483	0.539	0.559
8	S1	255.963	138.145	297.406	214.933	641	588.5	564.875	0.464	0.505	0.526
	S9	342.973	56.779	360.006	159.670	1031.05	928.55	882.425	0.349	0.388	0.408
	S2	14.454	190.033	71.464	194.369	1221.9	1106.4	1054.425	0.159	0.176	0.184
	S10	60.778	110.013	93.782	128.246	1777.55	1552.05	1450.575	0.072	0.083	0.088
	S3	11.512	306.381	103.426	309.835	1315.55	1189.55	1132.85	0.236	0.260	0.274
	S11	920.514	33.791	930.651	309.945	1771.74	1587.24	1504.215	0.525	0.586	0.619
7	S1	322.045	168.240	372.517	264.853	769.2	706.2	672.075	0.484	0.527	0.554
	S9	442.656	71.023	463.963	203.819	1237.26	1114.26	1047.635	0.375	0.416	0.443
	S2	18.444	239.850	90.399	245.383	1466.28	1327.68	1252.605	0.167	0.185	0.196
	S10	74.122	154.920	120.598	177.156	2133.06	1862.46	1715.885	0.083	0.095	0.103
	S3	16.026	376.117	128.861	380.925	1578.66	1427.46	1345.56	0.241	0.267	0.283
	S11	1191.635	28.286	1200.121	385.776	2126.088	1904.688	1784.763	0.564	0.630	0.672
6	S1	394.337	197.269	453.517	315.570	897.4	823.9	784.525	0.505	0.550	0.578
	S9	550.771	86.210	576.634	251.441	1443.47	1299.97	1223.095	0.399	0.444	0.471
	S2	20.190	292.669	107.991	298.726	1710.66	1548.96	1462.335	0.175	0.193	0.204
	S10	79.507	201.447	139.941	225.299	2488.57	2172.87	2003.745	0.091	0.104	0.112
	S3	25.973	449.617	160.858	457.409	1841.77	1665.37	1570.87	0.248	0.275	0.291
	S11	1501.591	16.928	1506.669	467.405	2480.436	2222.136	2083.761	0.607	0.678	0.723
5	S1	470.486	226.410	538.409	367.556	1025.6	941.6	902.225	0.525	0.572	0.597
	S9	667.861	109.255	700.637	309.613	1649.68	1485.68	1408.805	0.425	0.472	0.497
	S2	20.953	345.657	124.650	351.943	1955.04	1770.24	1683.615	0.180	0.199	0.209
	S10	89.158	249.156	163.904	275.903	2844.08	2483.28	2314.155	0.097	0.111	0.119
	S3	39.994	522.007	196.596	534.005	2104.88	1903.28	1808.78	0.254	0.281	0.295
	S11	1818.923	5.801	1820.664	551.478	2834.784	2539.584	2401.209	0.642	0.717	0.758
4	S1	546.145	253.896	622.314	417.739	1153.8	1059.3	1025.175	0.539	0.587	0.607
	S9	784.656	136.437	825.587	371.834	1855.89	1671.39	1604.765	0.445	0.494	0.514
	S2	20.237	395.783	138.971	401.854	2199.42	1991.52	1916.445	0.183	0.202	0.210
	S10	103.361	298.847	193.015	329.855	3199.59	2793.69	2647.115	0.103	0.118	0.125
	S3	56.696	589.464	233.535	606.472	2367.99	2141.19	2059.29	0.256	0.283	0.295

	S11	2120.560	3.906	2121.732	640.074	3189.132	2857.032	2737.107	0.665	0.743	0.775
3	S1	623.646	280.510	707.799	467.603	1282	1177	1153.375	0.552	0.601	0.614
	S9	895.376	162.298	944.065	430.910	2062.1	1857.1	1810.975	0.458	0.508	0.521
	S2	25.736	439.718	157.651	447.439	2443.8	2212.8	2160.825	0.183	0.202	0.207
	S10	120.134	343.650	223.229	379.690	3555.1	3104.1	3002.625	0.107	0.122	0.126
	S3	73.622	649.036	268.333	671.123	2631.1	2379.1	2322.4	0.255	0.282	0.289
	S11	2399.833	14.412	2404.157	734.362	3543.48	3174.48	3091.455	0.678	0.757	0.778
2	S1	694.465	304.303	785.756	512.643	1410.2	1294.7	1281.575	0.557	0.607	0.613
	S9	992.303	186.164	1048.152	483.855	2268.31	2042.81	2017.185	0.462	0.513	0.520
	S2	34.875	476.106	177.707	486.569	2688.18	2434.08	2405.205	0.181	0.200	0.202
	S10	137.836	382.527	252.594	423.878	3910.61	3414.51	3358.135	0.108	0.124	0.126
	S3	88.568	696.332	297.468	722.903	2894.21	2617.01	2585.51	0.250	0.276	0.280
	S11	2629.426	26.256	2637.303	815.084	3897.828	3491.928	3445.803	0.677	0.755	0.765
1	S1	744.485	320.117	840.520	543.463	1538.4	1412.4	1409.775	0.546	0.595	0.596
	S9	1058.857	202.564	1119.626	520.220	2474.52	2228.52	2223.395	0.452	0.502	0.504
	S2	40.507	502.204	191.168	514.356	2932.56	2655.36	2649.585	0.175	0.194	0.194
	S10	151.088	409.364	273.897	454.690	4266.12	3724.92	3713.645	0.107	0.122	0.122
	S3	101.192	727.996	319.591	758.354	3157.32	2854.92	2848.62	0.240	0.266	0.266
	S11	2775.910	37.532	2787.170	870.305	4252.176	3809.376	3800.151	0.655	0.732	0.733

Çizelge B.146: 6 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0} + Q_0$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				$N_{G0} + Q_0$ (kN)	$N_{G0} + \beta Q_0$ (kN)	$N_{G0} + \gamma Q_0$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	28.273	9.209	31.036	17.691	128.2	122.95	112.45	0.242	0.252	0.276
	S9	39.590	2.094	40.218	13.971	206.21	195.96	175.46	0.195	0.205	0.229
	S2	7.644	11.639	11.136	13.932	244.38	232.83	209.73	0.057	0.060	0.066
	S10	26.080	7.334	28.281	15.158	355.51	332.96	287.86	0.080	0.085	0.098
	S3	4.142	20.771	10.373	22.013	263.11	250.51	225.31	0.084	0.088	0.098
	S11	142.080	13.922	146.257	56.546	354.348	335.898	298.998	0.413	0.435	0.489
5	S1	80.923	25.257	88.500	49.534	256.4	245.9	230.15	0.345	0.360	0.385
	S9	109.201	9.433	112.031	42.194	412.42	391.92	361.17	0.272	0.286	0.310
	S2	21.668	33.586	31.744	40.086	488.76	465.66	431.01	0.082	0.086	0.093
	S10	62.291	23.198	69.250	41.885	711.02	665.92	598.27	0.097	0.104	0.116
	S3	7.089	52.070	22.710	54.197	526.22	501.02	463.22	0.103	0.108	0.117
	S11	348.947	22.786	355.783	127.470	708.696	671.796	616.446	0.502	0.530	0.577
4	S1	135.778	41.797	148.317	82.530	384.6	368.85	353.1	0.386	0.402	0.420
	S9	181.593	17.392	186.810	71.870	618.63	587.88	557.13	0.302	0.318	0.335
	S2	35.724	56.262	52.602	66.979	733.14	698.49	663.84	0.091	0.096	0.101
	S10	101.943	39.837	113.894	70.420	1066.53	998.88	931.23	0.107	0.114	0.122
	S3	9.911	83.434	34.941	86.407	789.33	751.53	713.73	0.109	0.115	0.121
	S11	565.856	31.573	575.328	201.329	1063.044	1007.694	952.344	0.541	0.571	0.604
3	S1	190.473	57.413	207.697	114.555	512.8	491.8	481.3	0.405	0.422	0.432
	S9	257.054	25.014	264.558	102.130	824.84	783.84	763.34	0.321	0.338	0.347
	S2	49.042	80.182	73.097	94.895	977.52	931.32	908.22	0.097	0.102	0.104
	S10	136.126	60.127	154.164	100.965	1422.04	1331.84	1286.74	0.108	0.116	0.120
	S3	13.211	114.033	47.421	117.996	1052.44	1002.04	976.84	0.112	0.118	0.121
	S11	789.028	34.527	799.386	271.236	1417.392	1343.592	1306.692	0.564	0.595	0.612
2	S1	239.381	71.041	260.693	142.855	641	614.75	609.5	0.407	0.424	0.428
	S9	326.618	31.882	336.182	129.867	1031.05	979.8	969.55	0.326	0.343	0.347
	S2	60.625	103.216	91.590	121.404	1221.9	1164.15	1152.6	0.099	0.104	0.105
	S10	162.418	81.243	186.791	129.968	1777.55	1664.8	1642.25	0.105	0.112	0.114
	S3	16.518	141.145	58.862	146.100	1315.55	1252.55	1239.95	0.111	0.117	0.118
	S11	989.782	31.177	999.135	328.112	1771.74	1679.49	1661.04	0.564	0.595	0.602
1	S1	273.753	81.467	298.194	163.593	769.2	737.7	737.7	0.388	0.404	0.404
	S9	377.968	37.164	389.118	150.555	1237.26	1175.76	1175.76	0.314	0.331	0.331
	S2	67.215	121.797	103.754	141.961	1466.28	1396.98	1396.98	0.097	0.102	0.102
	S10	179.593	100.014	209.597	153.892	2133.06	1997.76	1997.76	0.098	0.105	0.105
	S3	18.661	161.548	67.125	167.146	1578.66	1503.06	1503.06	0.106	0.111	0.111
	S11	1127.938	22.649	1134.732	361.030	2126.088	2015.388	2015.388	0.534	0.563	0.563

Çizelge B.147: 9 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	37.125	16.912	42.199	28.050	128.2	117.7	104.575	0.329	0.359	0.404
	S9	50.202	3.976	51.395	19.037	206.21	185.71	160.085	0.249	0.277	0.321
	S2	3.691	20.016	9.696	21.123	244.38	221.28	192.405	0.086	0.095	0.110
	S10	20.136	8.969	22.827	15.010	355.51	310.41	254.035	0.064	0.074	0.090
	S3	6.182	41.991	18.779	43.845	263.11	237.91	206.41	0.167	0.184	0.212
	S11	168.140	20.536	174.301	70.978	354.348	317.448	271.323	0.492	0.549	0.642
8	S1	107.931	46.008	121.733	78.387	256.4	235.4	207.05	0.475	0.517	0.588
	S9	142.404	17.282	147.589	60.003	412.42	371.42	316.07	0.358	0.397	0.467
	S2	14.392	57.918	31.768	62.236	488.76	442.56	380.19	0.127	0.141	0.164
	S10	52.603	31.872	62.165	47.653	711.02	620.82	499.05	0.087	0.100	0.125
	S3	8.711	102.504	39.462	105.117	526.22	475.82	407.78	0.200	0.221	0.258
	S11	425.910	32.873	435.772	160.646	708.696	634.896	535.266	0.615	0.686	0.814
7	S1	183.490	76.006	206.292	131.053	384.6	353.1	314.25	0.536	0.584	0.656
	S9	240.728	31.604	250.209	103.822	618.63	557.13	481.28	0.404	0.449	0.520
	S2	26.538	96.867	55.598	104.829	733.14	663.84	578.37	0.143	0.158	0.181
	S10	92.160	56.227	109.028	83.875	1066.53	931.23	764.36	0.102	0.117	0.143
	S3	11.913	163.634	61.004	167.208	789.33	713.73	620.49	0.212	0.234	0.269
	S11	708.042	47.584	722.317	259.996	1063.044	952.344	815.814	0.679	0.758	0.885
6	S1	264.462	105.700	296.172	185.039	512.8	470.8	426.7	0.578	0.629	0.694
	S9	351.986	45.999	365.785	151.595	824.84	742.84	656.74	0.443	0.492	0.557
	S2	39.911	140.159	81.959	152.132	977.52	885.12	788.1	0.156	0.172	0.193
	S10	128.213	88.996	154.911	127.460	1422.04	1241.64	1052.22	0.109	0.125	0.147
	S3	17.138	226.578	85.111	231.719	1052.44	951.64	845.8	0.220	0.243	0.274
	S11	1027.935	54.854	1044.391	363.235	1417.392	1269.792	1114.812	0.737	0.822	0.937
5	S1	348.915	134.488	389.262	239.163	641	588.5	544.4	0.607	0.661	0.715
	S9	471.831	60.047	489.845	201.596	1031.05	928.55	842.45	0.475	0.528	0.581
	S2	55.133	186.569	111.104	203.108	1221.9	1106.4	1009.38	0.166	0.184	0.201
	S10	162.119	127.449	200.353	176.085	1777.55	1552.05	1362.63	0.113	0.129	0.147
	S3	24.490	289.280	111.274	296.627	1315.55	1189.55	1083.71	0.225	0.249	0.274
	S11	1373.061	56.220	1389.927	468.139	1771.74	1587.24	1432.26	0.784	0.876	0.970
4	S1	430.582	161.412	479.005	290.586	769.2	706.2	667.35	0.623	0.678	0.718
	S9	594.803	73.599	616.883	252.040	1237.26	1114.26	1038.41	0.499	0.554	0.594
	S2	66.757	232.532	136.517	252.559	1466.28	1327.68	1242.21	0.172	0.190	0.203
	S10	193.251	172.495	244.999	230.470	2133.06	1862.46	1695.59	0.115	0.132	0.144
	S3	31.518	349.539	136.380	358.995	1578.66	1427.46	1334.22	0.227	0.251	0.269
	S11	1726.453	53.568	1742.523	571.504	2126.088	1904.688	1768.158	0.820	0.915	0.986
3	S1	510.916	184.979	566.410	338.254	897.4	823.9	795.55	0.631	0.687	0.712
	S9	715.940	86.888	742.007	301.670	1443.47	1299.97	1244.62	0.514	0.571	0.596
	S2	74.014	276.988	157.111	299.192	1710.66	1548.96	1486.59	0.175	0.193	0.201
	S10	212.215	215.962	277.003	279.626	2488.57	2172.87	2051.1	0.112	0.129	0.136
	S3	43.097	407.326	165.295	420.255	1841.77	1665.37	1597.33	0.228	0.252	0.263
	S11	2085.217	44.750	2098.642	670.315	2480.436	2222.136	2122.506	0.846	0.944	0.989
2	S1	582.825	205.430	644.454	380.278	1025.6	941.6	923.75	0.628	0.684	0.698
	S9	825.439	104.051	856.655	351.683	1649.68	1485.68	1450.83	0.519	0.577	0.590
	S2	78.841	315.632	173.531	339.284	1955.04	1770.24	1730.97	0.174	0.192	0.196
	S10	230.223	253.104	306.154	322.171	2844.08	2483.28	2406.61	0.113	0.130	0.134
	S3	56.416	456.502	193.367	473.427	2104.88	1903.28	1860.44	0.225	0.249	0.254
	S11	2391.219	33.413	2401.243	750.779	2834.784	2539.584	2476.854	0.847	0.946	0.969
1	S1	633.417	220.471	699.558	410.496	1153.8	1059.3	1051.95	0.606	0.660	0.665
	S9	906.414	120.607	942.596	392.531	1855.89	1671.39	1657.04	0.508	0.564	0.569
	S2	80.195	344.327	183.493	368.385	2199.42	1991.52	1975.35	0.167	0.185	0.186
	S10	245.906	284.022	331.113	357.794	3199.59	2793.69	2762.12	0.112	0.128	0.130
	S3	66.973	490.599	214.153	510.691	2367.99	2141.19	2123.55	0.216	0.239	0.240
	S11	2585.089	19.958	2591.076	795.485	3189.132	2857.032	2831.202	0.812	0.907	0.915

Çizelge B.148: 12 Kat, İstanbul, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	37.601	24.952	45.087	36.232	128.2	117.7	117.7	0.352	0.383	0.383
	S9	49.402	4.657	50.799	19.478	206.21	185.71	185.71	0.246	0.274	0.274
	S2	2.481	29.554	11.347	30.298	244.38	221.28	221.28	0.124	0.137	0.137
	S10	5.278	8.579	7.851	10.163	355.51	310.41	310.41	0.029	0.033	0.033
	S3	6.117	64.387	25.433	66.222	263.11	237.91	237.91	0.252	0.278	0.278
	S11	148.590	22.547	155.354	67.124	354.348	317.448	317.448	0.438	0.489	0.489
11	S1	111.084	67.526	131.341	100.851	256.4	235.4	235.4	0.512	0.558	0.558
	S9	144.118	22.619	150.904	65.855	412.42	371.42	371.42	0.366	0.406	0.406
	S2	0.701	85.183	26.255	85.393	488.76	442.56	442.56	0.175	0.193	0.193
	S10	22.193	36.456	33.130	43.114	711.02	620.82	620.82	0.061	0.069	0.069
	S3	6.158	155.211	52.721	157.058	526.22	475.82	475.82	0.298	0.330	0.330
	S11	388.873	32.771	398.704	149.433	708.696	634.896	634.896	0.563	0.628	0.628
10	S1	189.932	111.326	223.330	168.306	384.6	353.1	353.1	0.581	0.632	0.632
	S9	245.547	42.017	258.152	115.681	618.63	557.13	557.13	0.417	0.463	0.463
	S2	5.594	141.849	48.148	143.527	733.14	663.84	663.84	0.196	0.216	0.216
	S10	46.684	66.087	66.510	80.092	1066.53	931.23	931.23	0.075	0.086	0.086
	S3	7.174	247.111	81.307	249.263	789.33	713.73	713.73	0.316	0.349	0.349
	S11	656.784	47.202	670.945	244.238	1063.044	952.344	952.344	0.631	0.705	0.705
9	S1	276.057	155.266	322.637	238.083	512.8	470.8	457.675	0.629	0.685	0.705
	S9	363.178	61.862	381.737	170.816	824.84	742.84	717.215	0.463	0.514	0.532
	S2	11.876	205.086	73.402	208.649	977.52	885.12	856.245	0.213	0.236	0.244
	S10	67.526	107.847	99.880	128.104	1422.04	1241.64	1185.265	0.090	0.103	0.108
	S3	10.481	343.135	113.422	346.280	1052.44	951.64	920.14	0.329	0.364	0.376
	S11	971.321	51.540	986.783	342.937	1417.392	1269.792	1223.667	0.696	0.777	0.806
8	S1	369.177	199.247	428.951	310.000	641	588.5	564.875	0.669	0.729	0.759
	S9	494.672	81.892	519.240	230.294	1031.05	928.55	882.425	0.504	0.559	0.588
	S2	20.847	274.087	103.073	280.340	1221.9	1106.4	1054.425	0.229	0.253	0.266
	S10	87.660	158.673	135.262	184.971	1777.55	1552.05	1450.575	0.104	0.119	0.128
	S3	16.604	441.896	149.173	446.877	1315.55	1189.55	1132.85	0.340	0.376	0.394
	S11	1327.664	48.737	1342.285	447.037	1771.74	1587.24	1504.215	0.758	0.846	0.892
7	S1	464.488	242.654	537.284	382.000	769.2	706.2	672.075	0.698	0.761	0.799
	S9	638.446	102.436	669.177	293.970	1237.26	1114.26	1047.635	0.541	0.601	0.639
	S2	26.602	345.937	130.383	353.918	1466.28	1327.68	1252.605	0.241	0.267	0.283
	S10	106.906	223.442	173.939	255.514	2133.06	1862.46	1715.885	0.120	0.137	0.149
	S3	23.115	542.477	185.858	549.411	1578.66	1427.46	1345.56	0.348	0.385	0.408
	S11	1718.704	40.797	1730.943	556.408	2126.088	1904.688	1784.763	0.814	0.909	0.970
6	S1	568.755	284.523	654.111	455.149	897.4	823.9	784.525	0.729	0.794	0.834
	S9	794.381	124.341	831.683	362.656	1443.47	1299.97	1223.095	0.576	0.640	0.680
	S2	29.120	422.118	155.756	430.854	1710.66	1548.96	1462.335	0.252	0.278	0.295
	S10	114.673	290.548	201.837	324.950	2488.57	2172.87	2003.745	0.131	0.150	0.162
	S3	37.461	648.486	232.006	659.724	1841.77	1665.37	1570.87	0.358	0.396	0.420
	S11	2165.756	24.415	2173.081	674.142	2480.436	2222.136	2083.761	0.876	0.978	1.043
5	S1	678.585	326.553	776.551	530.129	1025.6	941.6	902.225	0.757	0.825	0.861
	S9	963.261	157.579	1010.534	446.557	1649.68	1485.68	1408.805	0.613	0.680	0.717
	S2	30.221	498.544	179.784	507.610	1955.04	1770.24	1683.615	0.260	0.287	0.302
	S10	128.593	359.359	236.400	397.937	2844.08	2483.28	2314.155	0.140	0.160	0.172
	S3	57.684	752.894	283.553	770.200	2104.88	1903.28	1808.78	0.366	0.405	0.426
	S11	2623.447	8.367	2625.957	795.401	2834.784	2539.584	2401.209	0.926	1.034	1.094
4	S1	787.710	366.196	897.568	602.509	1153.8	1059.3	1025.175	0.778	0.847	0.876
	S9	1131.715	196.784	1190.750	536.299	1855.89	1671.39	1604.765	0.642	0.712	0.742
	S2	29.187	570.841	200.440	579.597	2199.42	1991.52	1916.445	0.264	0.291	0.302
	S10	149.079	431.029	278.387	475.752	3199.59	2793.69	2647.115	0.149	0.170	0.180
	S3	81.773	850.188	336.829	874.720	2367.99	2141.19	2059.29	0.369	0.409	0.425

	S11	3058.500	5.634	3060.190	923.184	3189.132	2857.032	2737.107	0.960	1.071	1.118
3	S1	899.490	404.581	1020.864	674.428	1282	1177	1153.375	0.796	0.867	0.885
	S9	1291.408	234.083	1361.633	621.505	2062.1	1857.1	1810.975	0.660	0.733	0.752
	S2	37.119	634.209	227.381	645.345	2443.8	2212.8	2160.825	0.264	0.292	0.299
	S10	173.270	495.649	321.965	547.630	3555.1	3104.1	3002.625	0.154	0.176	0.182
	S3	106.185	936.110	387.018	967.966	2631.1	2379.1	2322.4	0.368	0.407	0.417
	S11	3461.298	20.786	3467.533	1059.175	3543.48	3174.48	3091.455	0.979	1.092	1.122
2	S1	1001.633	438.899	1133.302	739.389	1410.2	1294.7	1281.575	0.804	0.875	0.884
	S9	1431.206	268.506	1511.758	697.868	2268.31	2042.81	2017.185	0.666	0.740	0.749
	S2	50.301	686.692	256.308	701.782	2688.18	2434.08	2405.205	0.261	0.288	0.292
	S10	198.801	551.722	364.318	611.362	3910.61	3414.51	3358.135	0.156	0.179	0.182
	S3	127.743	1004.325	429.040	1042.648	2894.21	2617.01	2585.51	0.360	0.398	0.403
	S11	3792.441	37.869	3803.802	1175.602	3897.828	3491.928	3445.803	0.976	1.089	1.104
1	S1	1073.776	461.707	1212.289	783.840	1538.4	1412.4	1409.775	0.788	0.858	0.860
	S9	1527.197	292.159	1614.845	750.318	2474.52	2228.52	2223.395	0.653	0.725	0.726
	S2	58.424	724.332	275.723	741.859	2932.56	2655.36	2649.585	0.253	0.279	0.280
	S10	217.916	590.428	395.044	655.803	4266.12	3724.92	3713.645	0.154	0.176	0.177
	S3	145.950	1049.994	460.948	1093.779	3157.32	2854.92	2848.62	0.346	0.383	0.384
	S11	4003.716	54.133	4019.956	1255.247	4252.176	3809.376	3800.151	0.945	1.055	1.058

Çizelge B.149: 6 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	3.865	1.394	4.283	2.553	128.2	122.95	112.45	0.033	0.035	0.038
	S9	5.412	0.317	5.507	1.940	206.21	195.96	175.46	0.027	0.028	0.031
	S2	1.045	1.762	1.573	2.075	244.38	232.83	209.73	0.008	0.009	0.010
	S10	3.565	1.110	3.898	2.180	355.51	332.96	287.86	0.011	0.012	0.014
	S3	0.566	3.144	1.509	3.314	263.11	250.51	225.31	0.013	0.013	0.015
	S11	19.421	2.107	20.053	7.934	354.348	335.898	298.998	0.057	0.060	0.067
5	S1	11.061	3.823	12.208	7.141	256.4	245.9	230.15	0.048	0.050	0.053
	S9	14.927	1.428	15.355	5.906	412.42	391.92	361.17	0.037	0.039	0.043
	S2	2.962	5.083	4.487	5.972	488.76	465.66	431.01	0.012	0.013	0.014
	S10	8.515	3.511	9.568	6.066	711.02	665.92	598.27	0.013	0.014	0.016
	S3	0.969	7.881	3.333	8.172	526.22	501.02	463.22	0.016	0.016	0.018
	S11	47.698	3.449	48.732	17.758	708.696	671.796	616.446	0.069	0.073	0.079
4	S1	18.560	6.326	20.457	11.894	384.6	368.85	353.1	0.053	0.055	0.058
	S9	24.822	2.632	25.612	10.079	618.63	587.88	557.13	0.041	0.044	0.046
	S2	4.883	8.516	7.438	9.981	733.14	698.49	663.84	0.014	0.014	0.015
	S10	13.935	6.030	15.743	10.210	1066.53	998.88	931.23	0.015	0.016	0.017
	S3	1.355	12.628	5.143	13.035	789.33	751.53	713.73	0.017	0.017	0.018
	S11	77.347	4.779	78.781	27.983	1063.044	1007.694	952.344	0.074	0.078	0.083
3	S1	26.036	8.690	28.643	16.501	512.8	491.8	481.3	0.056	0.058	0.060
	S9	35.137	3.786	36.273	14.327	824.84	783.84	763.34	0.044	0.046	0.048
	S2	6.704	12.136	10.344	14.147	977.52	931.32	908.22	0.014	0.015	0.016
	S10	18.607	9.101	21.337	14.683	1422.04	1331.84	1286.74	0.015	0.016	0.017
	S3	1.806	17.260	6.984	17.801	1052.44	1002.04	976.84	0.017	0.018	0.018
	S11	107.853	5.226	109.421	37.582	1417.392	1343.592	1306.692	0.077	0.081	0.084
2	S1	32.721	10.753	35.947	20.569	641	614.75	609.5	0.056	0.058	0.059
	S9	44.646	4.826	46.093	18.219	1031.05	979.8	969.55	0.045	0.047	0.048
	S2	8.287	15.623	12.974	18.109	1221.9	1164.15	1152.6	0.015	0.016	0.016
	S10	22.201	12.297	25.890	18.957	1777.55	1664.8	1642.25	0.015	0.016	0.016
	S3	2.258	21.363	8.667	22.041	1315.55	1252.55	1239.95	0.017	0.018	0.018
	S11	135.294	4.719	136.710	45.307	1771.74	1679.49	1661.04	0.077	0.081	0.082
1	S1	37.420	12.331	41.119	23.557	769.2	737.7	737.7	0.053	0.056	0.056
	S9	51.665	5.625	53.352	21.125	1237.26	1175.76	1175.76	0.043	0.045	0.045
	S2	9.188	18.435	14.718	21.191	1466.28	1396.98	1396.98	0.014	0.015	0.015
	S10	24.549	15.138	29.090	22.502	2133.06	1997.76	1997.76	0.014	0.015	0.015
	S3	2.551	24.452	9.886	25.217	1578.66	1503.06	1503.06	0.016	0.017	0.017
	S11	154.179	3.428	155.207	49.682	2126.088	2015.388	2015.388	0.073	0.077	0.077

Çizelge B.150: 9 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	4.684	2.134	5.324	3.539	128.2	117.7	104.575	0.042	0.045	0.051
	S9	6.333	0.502	6.484	2.402	206.21	185.71	160.085	0.031	0.035	0.041
	S2	0.466	2.525	1.223	2.665	244.38	221.28	192.405	0.011	0.012	0.014
	S10	2.540	1.132	2.880	1.894	355.51	310.41	254.035	0.008	0.009	0.011
	S3	0.780	5.297	2.369	5.531	263.11	237.91	206.41	0.021	0.023	0.027
	S11	21.212	2.591	21.989	8.954	354.348	317.448	271.323	0.062	0.069	0.081
8	S1	13.616	5.804	15.357	9.889	256.4	235.4	207.05	0.060	0.065	0.074
	S9	17.965	2.180	18.619	7.570	412.42	371.42	316.07	0.045	0.050	0.059
	S2	1.816	7.307	4.008	7.851	488.76	442.56	380.19	0.016	0.018	0.021
	S10	6.636	4.021	7.842	6.012	711.02	620.82	499.05	0.011	0.013	0.016
	S3	1.099	12.931	4.978	13.261	526.22	475.82	407.78	0.025	0.028	0.033
	S11	53.730	4.147	54.974	20.266	708.696	634.896	535.266	0.078	0.087	0.103
7	S1	23.148	9.589	26.024	16.533	384.6	353.1	314.25	0.068	0.074	0.083
	S9	30.369	3.987	31.565	13.098	618.63	557.13	481.28	0.051	0.057	0.066
	S2	3.348	12.220	7.014	13.225	733.14	663.84	578.37	0.018	0.020	0.023
	S10	11.626	7.093	13.754	10.581	1066.53	931.23	764.36	0.013	0.015	0.018
	S3	1.503	20.643	7.696	21.094	789.33	713.73	620.49	0.027	0.030	0.034
	S11	89.322	6.003	91.123	32.800	1063.044	952.344	815.814	0.086	0.096	0.112
6	S1	33.363	13.335	37.363	23.343	512.8	470.8	426.7	0.073	0.079	0.088
	S9	44.404	5.803	46.145	19.124	824.84	742.84	656.74	0.056	0.062	0.070
	S2	5.035	17.682	10.339	19.192	977.52	885.12	788.1	0.020	0.022	0.024
	S10	16.175	11.227	19.543	16.080	1422.04	1241.64	1052.22	0.014	0.016	0.019
	S3	2.162	28.584	10.737	29.232	1052.44	951.64	845.8	0.028	0.031	0.035
	S11	129.678	6.920	131.754	45.823	1417.392	1269.792	1114.812	0.093	0.104	0.118
5	S1	44.017	16.966	49.107	30.171	641	588.5	544.4	0.077	0.083	0.090
	S9	59.523	7.575	61.796	25.432	1031.05	928.55	842.45	0.060	0.067	0.073
	S2	6.955	23.536	14.016	25.623	1221.9	1106.4	1009.38	0.021	0.023	0.025
	S10	20.452	16.078	25.275	22.214	1777.55	1552.05	1362.63	0.014	0.016	0.019
	S3	3.090	36.494	14.038	37.421	1315.55	1189.55	1083.71	0.028	0.031	0.035
	S11	173.217	7.092	175.345	59.057	1771.74	1587.24	1432.26	0.099	0.110	0.122
4	S1	54.320	20.363	60.428	36.659	769.2	706.2	667.35	0.079	0.086	0.091
	S9	75.037	9.285	77.822	31.796	1237.26	1114.26	1038.41	0.063	0.070	0.075
	S2	8.422	29.335	17.222	31.861	1466.28	1327.68	1242.21	0.022	0.024	0.026
	S10	24.379	21.761	30.908	29.075	2133.06	1862.46	1695.59	0.014	0.017	0.018
	S3	3.976	44.096	17.205	45.289	1578.66	1427.46	1334.22	0.029	0.032	0.034
	S11	217.799	6.758	219.826	72.097	2126.088	1904.688	1768.158	0.103	0.115	0.124
3	S1	64.454	23.336	71.455	42.672	897.4	823.9	795.55	0.080	0.087	0.090
	S9	90.319	10.961	93.607	38.057	1443.47	1299.97	1244.62	0.065	0.072	0.075
	S2	9.337	34.943	19.820	37.744	1710.66	1548.96	1486.59	0.022	0.024	0.025
	S10	26.772	27.244	34.945	35.276	2488.57	2172.87	2051.1	0.014	0.016	0.017
	S3	5.437	51.386	20.853	53.017	1841.77	1665.37	1597.33	0.029	0.032	0.033
	S11	263.058	5.645	264.752	84.563	2480.436	2222.136	2122.506	0.107	0.119	0.125
2	S1	73.526	25.916	81.300	47.973	1025.6	941.6	923.75	0.079	0.086	0.088
	S9	104.132	13.127	108.070	44.366	1649.68	1485.68	1450.83	0.066	0.073	0.074
	S2	9.946	39.818	21.892	42.802	1955.04	1770.24	1730.97	0.022	0.024	0.025
	S10	29.044	31.930	38.623	40.643	2844.08	2483.28	2406.61	0.014	0.016	0.017
	S3	7.117	57.589	24.394	59.725	2104.88	1903.28	1860.44	0.028	0.031	0.032
	S11	301.662	4.215	302.926	94.714	2834.784	2539.584	2476.854	0.107	0.119	0.122
1	S1	79.908	27.813	88.252	51.786	1153.8	1059.3	1051.95	0.076	0.083	0.084
	S9	114.348	15.215	118.912	49.519	1855.89	1671.39	1657.04	0.064	0.071	0.072
	S2	10.117	43.438	23.148	46.473	2199.42	1991.52	1975.35	0.021	0.023	0.024
	S10	31.022	35.831	41.771	45.137	3199.59	2793.69	2762.12	0.014	0.016	0.016
	S3	8.449	61.891	27.016	64.426	2367.99	2141.19	2123.55	0.027	0.030	0.030
	S11	326.119	2.518	326.874	100.353	3189.132	2857.032	2831.202	0.102	0.114	0.115

Çizelge B.151: 12 Kat, Ankara, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	4.744	3.148	5.688	4.571	128.2	117.7	117.7	0.044	0.048	0.048
	S9	6.232	0.588	6.408	2.457	206.21	185.71	185.71	0.031	0.035	0.035
	S2	0.313	3.728	1.432	3.822	244.38	221.28	221.28	0.016	0.017	0.017
	S10	0.666	1.082	0.990	1.282	355.51	310.41	310.41	0.004	0.004	0.004
	S3	0.772	8.123	3.208	8.354	263.11	237.91	237.91	0.032	0.035	0.035
	S11	18.745	2.844	19.599	8.468	354.348	317.448	317.448	0.055	0.062	0.062
11	S1	14.014	8.519	16.569	12.723	256.4	235.4	235.4	0.065	0.070	0.070
	S9	18.181	2.854	19.037	8.308	412.42	371.42	371.42	0.046	0.051	0.051
	S2	0.088	10.746	3.312	10.773	488.76	442.56	442.56	0.022	0.024	0.024
	S10	2.800	4.599	4.179	5.439	711.02	620.82	620.82	0.008	0.009	0.009
	S3	0.777	19.580	6.651	19.813	526.22	475.82	475.82	0.038	0.042	0.042
	S11	49.058	4.134	50.298	18.851	708.696	634.896	634.896	0.071	0.079	0.079
10	S1	23.961	14.044	28.174	21.232	384.6	353.1	353.1	0.073	0.080	0.080
	S9	30.977	5.301	32.567	14.594	618.63	557.13	557.13	0.053	0.058	0.058
	S2	0.706	17.895	6.074	18.106	733.14	663.84	663.84	0.025	0.027	0.027
	S10	5.889	8.337	8.390	10.104	1066.53	931.23	931.23	0.009	0.011	0.011
	S3	0.905	31.174	10.257	31.446	789.33	713.73	713.73	0.040	0.044	0.044
	S11	82.856	5.955	84.642	30.811	1063.044	952.344	952.344	0.080	0.089	0.089
9	S1	34.826	19.587	40.702	30.035	512.8	470.8	457.675	0.079	0.086	0.089
	S9	45.816	7.804	48.158	21.549	824.84	742.84	717.215	0.058	0.065	0.067
	S2	1.498	25.872	9.260	26.322	977.52	885.12	856.245	0.027	0.030	0.031
	S10	8.519	13.605	12.600	16.161	1422.04	1241.64	1185.265	0.011	0.013	0.014
	S3	1.322	43.288	14.309	43.684	1052.44	951.64	920.14	0.042	0.046	0.047
	S11	122.536	6.502	124.487	43.263	1417.392	1269.792	1223.667	0.088	0.098	0.102
8	S1	46.573	25.136	54.114	39.108	641	588.5	564.875	0.084	0.092	0.096
	S9	62.405	10.331	65.504	29.052	1031.05	928.55	882.425	0.064	0.071	0.074
	S2	2.630	34.577	13.003	35.366	1221.9	1106.4	1054.425	0.029	0.032	0.034
	S10	11.059	20.017	17.064	23.335	1777.55	1552.05	1450.575	0.013	0.015	0.016
	S3	2.095	55.747	18.819	56.375	1315.55	1189.55	1132.85	0.043	0.047	0.050
	S11	167.490	6.148	169.334	56.395	1771.74	1587.24	1504.215	0.096	0.107	0.113
7	S1	58.597	30.612	67.780	48.191	769.2	706.2	672.075	0.088	0.096	0.101
	S9	80.542	12.923	84.419	37.085	1237.26	1114.26	1047.635	0.068	0.076	0.081
	S2	3.356	43.641	16.448	44.648	1466.28	1327.68	1252.605	0.030	0.034	0.036
	S10	13.487	28.188	21.943	32.234	2133.06	1862.46	1715.885	0.015	0.017	0.019
	S3	2.916	68.436	23.447	69.310	1578.66	1427.46	1345.56	0.044	0.049	0.052
	S11	216.821	5.147	218.365	70.193	2126.088	1904.688	1784.763	0.103	0.115	0.122
6	S1	71.751	35.894	82.519	57.419	897.4	823.9	784.525	0.092	0.100	0.105
	S9	100.214	15.686	104.920	45.750	1443.47	1299.97	1223.095	0.073	0.081	0.086
	S2	3.674	53.252	19.649	54.354	1710.66	1548.96	1462.335	0.032	0.035	0.037
	S10	14.466	36.654	25.463	40.994	2488.57	2172.87	2003.745	0.016	0.019	0.020
	S3	4.726	81.809	29.269	83.227	1841.77	1665.37	1570.87	0.045	0.050	0.053
	S11	273.219	3.080	274.143	85.046	2480.436	2222.136	2083.761	0.111	0.123	0.132
5	S1	85.606	41.196	97.965	66.878	1025.6	941.6	902.225	0.096	0.104	0.109
	S9	121.519	19.879	127.483	56.335	1649.68	1485.68	1408.805	0.077	0.086	0.090
	S2	3.813	62.893	22.680	64.037	1955.04	1770.24	1683.615	0.033	0.036	0.038
	S10	16.222	45.335	29.823	50.201	2844.08	2483.28	2314.155	0.018	0.020	0.022
	S3	7.277	94.981	35.771	97.164	2104.88	1903.28	1808.78	0.046	0.051	0.054
	S11	330.958	1.056	331.275	100.343	2834.784	2539.584	2401.209	0.117	0.130	0.138
4	S1	99.373	46.197	113.232	76.009	1153.8	1059.3	1025.175	0.098	0.107	0.110
	S9	142.770	24.825	150.218	67.656	1855.89	1671.39	1604.765	0.081	0.090	0.094
	S2	3.682	72.014	25.286	73.118	2199.42	1991.52	1916.445	0.033	0.037	0.038
	S10	18.807	54.376	35.120	60.018	3199.59	2793.69	2647.115	0.019	0.021	0.023
	S3	10.316	107.255	42.492	110.349	2367.99	2141.19	2059.29	0.047	0.052	0.054

	S11	385.842	0.711	386.055	116.463	3189.132	2857.032	2737.107	0.121	0.135	0.141
3	S1	113.474	51.039	128.786	85.082	1282	1177	1153.375	0.100	0.109	0.112
	S9	162.916	29.531	171.775	78.405	2062.1	1857.1	1810.975	0.083	0.092	0.095
	S2	4.683	80.008	28.685	81.413	2443.8	2212.8	2160.825	0.033	0.037	0.038
	S10	21.859	62.528	40.617	69.086	3555.1	3104.1	3002.625	0.019	0.022	0.023
	S3	13.396	118.094	48.824	122.113	2631.1	2379.1	2322.4	0.046	0.051	0.053
	S11	436.656	2.622	437.443	133.619	3543.48	3174.48	3091.455	0.123	0.138	0.142
2	S1	126.360	55.369	142.970	93.277	1410.2	1294.7	1281.575	0.101	0.110	0.112
	S9	180.552	33.873	190.714	88.039	2268.31	2042.81	2017.185	0.084	0.093	0.095
	S2	6.346	86.629	32.334	88.532	2688.18	2434.08	2405.205	0.033	0.036	0.037
	S10	25.080	69.602	45.960	77.126	3910.61	3414.51	3358.135	0.020	0.023	0.023
	S3	16.115	126.700	54.125	131.534	2894.21	2617.01	2585.51	0.045	0.050	0.051
	S11	478.431	4.777	479.864	148.307	3897.828	3491.928	3445.803	0.123	0.137	0.139
1	S1	135.461	58.246	152.935	98.885	1538.4	1412.4	1409.775	0.099	0.108	0.108
	S9	192.662	36.857	203.719	94.656	2474.52	2228.52	2223.395	0.082	0.091	0.092
	S2	7.370	91.377	34.784	93.588	2932.56	2655.36	2649.585	0.032	0.035	0.035
	S10	27.491	74.485	49.836	82.732	4266.12	3724.92	3713.645	0.019	0.022	0.022
	S3	18.412	132.461	58.150	137.984	3157.32	2854.92	2848.62	0.044	0.048	0.048
	S11	505.084	6.829	507.133	158.354	4252.176	3809.376	3800.151	0.119	0.133	0.133

Çizelge B.152: 6 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	3.865	1.394	4.283	2.553	128.2	122.95	112.45	0.033	0.035	0.038
	S9	5.412	0.317	5.507	1.940	206.21	195.96	175.46	0.027	0.028	0.031
	S2	1.045	1.762	1.573	2.075	244.38	232.83	209.73	0.008	0.009	0.010
	S10	3.565	1.110	3.898	2.180	355.51	332.96	287.86	0.011	0.012	0.014
	S3	0.566	3.144	1.509	3.314	263.11	250.51	225.31	0.013	0.013	0.015
	S11	19.421	2.107	20.053	7.934	354.348	335.898	298.998	0.057	0.060	0.067
5	S1	11.061	3.823	12.208	7.141	256.4	245.9	230.15	0.048	0.050	0.053
	S9	14.927	1.428	15.355	5.906	412.42	391.92	361.17	0.037	0.039	0.043
	S2	2.962	5.083	4.487	5.972	488.76	465.66	431.01	0.012	0.013	0.014
	S10	8.515	3.511	9.568	6.066	711.02	665.92	598.27	0.013	0.014	0.016
	S3	0.969	7.881	3.333	8.172	526.22	501.02	463.22	0.016	0.016	0.018
	S11	47.698	3.449	48.732	17.758	708.696	671.796	616.446	0.069	0.073	0.079
4	S1	18.560	6.326	20.457	11.894	384.6	368.85	353.1	0.053	0.055	0.058
	S9	24.822	2.632	25.612	10.079	618.63	587.88	557.13	0.041	0.044	0.046
	S2	4.883	8.516	7.438	9.981	733.14	698.49	663.84	0.014	0.014	0.015
	S10	13.935	6.030	15.743	10.210	1066.53	998.88	931.23	0.015	0.016	0.017
	S3	1.355	12.628	5.143	13.035	789.33	751.53	713.73	0.017	0.017	0.018
	S11	77.347	4.779	78.781	27.983	1063.044	1007.694	952.344	0.074	0.078	0.083
3	S1	26.036	8.690	28.643	16.501	512.8	491.8	481.3	0.056	0.058	0.060
	S9	35.137	3.786	36.273	14.327	824.84	783.84	763.34	0.044	0.046	0.048
	S2	6.704	12.136	10.344	14.147	977.52	931.32	908.22	0.014	0.015	0.016
	S10	18.607	9.101	21.337	14.683	1422.04	1331.84	1286.74	0.015	0.016	0.017
	S3	1.806	17.260	6.984	17.801	1052.44	1002.04	976.84	0.017	0.018	0.018
	S11	107.853	5.226	109.421	37.582	1417.392	1343.592	1306.692	0.077	0.081	0.084
2	S1	32.721	10.753	35.947	20.569	641	614.75	609.5	0.056	0.058	0.059
	S9	44.646	4.826	46.093	18.219	1031.05	979.8	969.55	0.045	0.047	0.048
	S2	8.287	15.623	12.974	18.109	1221.9	1164.15	1152.6	0.015	0.016	0.016
	S10	22.201	12.297	25.890	18.957	1777.55	1664.8	1642.25	0.015	0.016	0.016
	S3	2.258	21.363	8.667	22.041	1315.55	1252.55	1239.95	0.017	0.018	0.018
	S11	135.294	4.719	136.710	45.307	1771.74	1679.49	1661.04	0.077	0.081	0.082
1	S1	37.420	12.331	41.119	23.557	769.2	737.7	737.7	0.053	0.056	0.056
	S9	51.665	5.625	53.352	21.125	1237.26	1175.76	1175.76	0.043	0.045	0.045
	S2	9.188	18.435	14.718	21.191	1466.28	1396.98	1396.98	0.014	0.015	0.015
	S10	24.549	15.138	29.090	22.502	2133.06	1997.76	1997.76	0.014	0.015	0.015
	S3	2.551	24.452	9.886	25.217	1578.66	1503.06	1503.06	0.016	0.017	0.017
	S11	154.179	3.428	155.207	49.682	2126.088	2015.388	2015.388	0.073	0.077	0.077

Çizelge B.153: 9 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	4.684	2.134	5.324	3.539	128.2	117.7	104.575	0.042	0.045	0.051
	S9	6.333	0.502	6.484	2.402	206.21	185.71	160.085	0.031	0.035	0.041
	S2	0.466	2.525	1.223	2.665	244.38	221.28	192.405	0.011	0.012	0.014
	S10	2.540	1.132	2.880	1.894	355.51	310.41	254.035	0.008	0.009	0.011
	S3	0.780	5.297	2.369	5.531	263.11	237.91	206.41	0.021	0.023	0.027
	S11	21.212	2.591	21.989	8.954	354.348	317.448	271.323	0.062	0.069	0.081
8	S1	13.616	5.804	15.357	9.889	256.4	235.4	207.05	0.060	0.065	0.074
	S9	17.965	2.180	18.619	7.570	412.42	371.42	316.07	0.045	0.050	0.059
	S2	1.816	7.307	4.008	7.851	488.76	442.56	380.19	0.016	0.018	0.021
	S10	6.636	4.021	7.842	6.012	711.02	620.82	499.05	0.011	0.013	0.016
	S3	1.099	12.931	4.978	13.261	526.22	475.82	407.78	0.025	0.028	0.033
	S11	53.730	4.147	54.974	20.266	708.696	634.896	535.266	0.078	0.087	0.103
7	S1	23.148	9.589	26.024	16.533	384.6	353.1	314.25	0.068	0.074	0.083
	S9	30.369	3.987	31.565	13.098	618.63	557.13	481.28	0.051	0.057	0.066
	S2	3.348	12.220	7.014	13.225	733.14	663.84	578.37	0.018	0.020	0.023
	S10	11.626	7.093	13.754	10.581	1066.53	931.23	764.36	0.013	0.015	0.018
	S3	1.503	20.643	7.696	21.094	789.33	713.73	620.49	0.027	0.030	0.034
	S11	89.322	6.003	91.123	32.800	1063.044	952.344	815.814	0.086	0.096	0.112
6	S1	33.363	13.335	37.363	23.343	512.8	470.8	426.7	0.073	0.079	0.088
	S9	44.404	5.803	46.145	19.124	824.84	742.84	656.74	0.056	0.062	0.070
	S2	5.035	17.682	10.339	19.192	977.52	885.12	788.1	0.020	0.022	0.024
	S10	16.175	11.227	19.543	16.080	1422.04	1241.64	1052.22	0.014	0.016	0.019
	S3	2.162	28.584	10.737	29.232	1052.44	951.64	845.8	0.028	0.031	0.035
	S11	129.678	6.920	131.754	45.823	1417.392	1269.792	1114.812	0.093	0.104	0.118
5	S1	44.017	16.966	49.107	30.171	641	588.5	544.4	0.077	0.083	0.090
	S9	59.523	7.575	61.796	25.432	1031.05	928.55	842.45	0.060	0.067	0.073
	S2	6.955	23.536	14.016	25.623	1221.9	1106.4	1009.38	0.021	0.023	0.025
	S10	20.452	16.078	25.275	22.214	1777.55	1552.05	1362.63	0.014	0.016	0.019
	S3	3.090	36.494	14.038	37.421	1315.55	1189.55	1083.71	0.028	0.031	0.035
	S11	173.217	7.092	175.345	59.057	1771.74	1587.24	1432.26	0.099	0.110	0.122
4	S1	54.320	20.363	60.428	36.659	769.2	706.2	667.35	0.079	0.086	0.091
	S9	75.037	9.285	77.822	31.796	1237.26	1114.26	1038.41	0.063	0.070	0.075
	S2	8.422	29.335	17.222	31.861	1466.28	1327.68	1242.21	0.022	0.024	0.026
	S10	24.379	21.761	30.908	29.075	2133.06	1862.46	1695.59	0.014	0.017	0.018
	S3	3.976	44.096	17.205	45.289	1578.66	1427.46	1334.22	0.029	0.032	0.034
	S11	217.799	6.758	219.826	72.097	2126.088	1904.688	1768.158	0.103	0.115	0.124
3	S1	64.454	23.336	71.455	42.672	897.4	823.9	795.55	0.080	0.087	0.090
	S9	90.319	10.961	93.607	38.057	1443.47	1299.97	1244.62	0.065	0.072	0.075
	S2	9.337	34.943	19.820	37.744	1710.66	1548.96	1486.59	0.022	0.024	0.025
	S10	26.772	27.244	34.945	35.276	2488.57	2172.87	2051.1	0.014	0.016	0.017
	S3	5.437	51.386	20.853	53.017	1841.77	1665.37	1597.33	0.029	0.032	0.033
	S11	263.058	5.645	264.752	84.563	2480.436	2222.136	2122.506	0.107	0.119	0.125
2	S1	73.526	25.916	81.300	47.973	1025.6	941.6	923.75	0.079	0.086	0.088
	S9	104.132	13.127	108.070	44.366	1649.68	1485.68	1450.83	0.066	0.073	0.074
	S2	9.946	39.818	21.892	42.802	1955.04	1770.24	1730.97	0.022	0.024	0.025
	S10	29.044	31.930	38.623	40.643	2844.08	2483.28	2406.61	0.014	0.016	0.017
	S3	7.117	57.589	24.394	59.725	2104.88	1903.28	1860.44	0.028	0.031	0.032
	S11	301.662	4.215	302.926	94.714	2834.784	2539.584	2476.854	0.107	0.119	0.122
1	S1	79.908	27.813	88.252	51.786	1153.8	1059.3	1051.95	0.076	0.083	0.084
	S9	114.348	15.215	118.912	49.519	1855.89	1671.39	1657.04	0.064	0.071	0.072
	S2	10.117	43.438	23.148	46.473	2199.42	1991.52	1975.35	0.021	0.023	0.024
	S10	31.022	35.831	41.771	45.137	3199.59	2793.69	2762.12	0.014	0.016	0.016
	S3	8.449	61.891	27.016	64.426	2367.99	2141.19	2123.55	0.027	0.030	0.030
	S11	326.119	2.518	326.874	100.353	3189.132	2857.032	2831.202	0.102	0.114	0.115

Çizelge B.154: 12 Kat, Ankara, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	4.744	3.148	5.688	4.571	128.2	117.7	117.7	0.044	0.048	0.048
	S9	6.232	0.588	6.408	2.457	206.21	185.71	185.71	0.031	0.035	0.035
	S2	0.313	3.728	1.432	3.822	244.38	221.28	221.28	0.016	0.017	0.017
	S10	0.666	1.082	0.990	1.282	355.51	310.41	310.41	0.004	0.004	0.004
	S3	0.772	8.123	3.208	8.354	263.11	237.91	237.91	0.032	0.035	0.035
	S11	18.745	2.844	19.599	8.468	354.348	317.448	317.448	0.055	0.062	0.062
11	S1	14.014	8.519	16.569	12.723	256.4	235.4	235.4	0.065	0.070	0.070
	S9	18.181	2.854	19.037	8.308	412.42	371.42	371.42	0.046	0.051	0.051
	S2	0.088	10.746	3.312	10.773	488.76	442.56	442.56	0.022	0.024	0.024
	S10	2.800	4.599	4.179	5.439	711.02	620.82	620.82	0.008	0.009	0.009
	S3	0.777	19.580	6.651	19.813	526.22	475.82	475.82	0.038	0.042	0.042
	S11	49.058	4.134	50.298	18.851	708.696	634.896	634.896	0.071	0.079	0.079
10	S1	23.961	14.044	28.174	21.232	384.6	353.1	353.1	0.073	0.080	0.080
	S9	30.977	5.301	32.567	14.594	618.63	557.13	557.13	0.053	0.058	0.058
	S2	0.706	17.895	6.074	18.106	733.14	663.84	663.84	0.025	0.027	0.027
	S10	5.889	8.337	8.390	10.104	1066.53	931.23	931.23	0.009	0.011	0.011
	S3	0.905	31.174	10.257	31.446	789.33	713.73	713.73	0.040	0.044	0.044
	S11	82.856	5.955	84.642	30.811	1063.044	952.344	952.344	0.080	0.089	0.089
9	S1	34.826	19.587	40.702	30.035	512.8	470.8	457.675	0.079	0.086	0.089
	S9	45.816	7.804	48.158	21.549	824.84	742.84	717.215	0.058	0.065	0.067
	S2	1.498	25.872	9.260	26.322	977.52	885.12	856.245	0.027	0.030	0.031
	S10	8.519	13.605	12.600	16.161	1422.04	1241.64	1185.265	0.011	0.013	0.014
	S3	1.322	43.288	14.309	43.684	1052.44	951.64	920.14	0.042	0.046	0.047
	S11	122.536	6.502	124.487	43.263	1417.392	1269.792	1223.667	0.088	0.098	0.102
8	S1	46.573	25.136	54.114	39.108	641	588.5	564.875	0.084	0.092	0.096
	S9	62.405	10.331	65.504	29.052	1031.05	928.55	882.425	0.064	0.071	0.074
	S2	2.630	34.577	13.003	35.366	1221.9	1106.4	1054.425	0.029	0.032	0.034
	S10	11.059	20.017	17.064	23.335	1777.55	1552.05	1450.575	0.013	0.015	0.016
	S3	2.095	55.747	18.819	56.375	1315.55	1189.55	1132.85	0.043	0.047	0.050
	S11	167.490	6.148	169.334	56.395	1771.74	1587.24	1504.215	0.096	0.107	0.113
7	S1	58.597	30.612	67.780	48.191	769.2	706.2	672.075	0.088	0.096	0.101
	S9	80.542	12.923	84.419	37.085	1237.26	1114.26	1047.635	0.068	0.076	0.081
	S2	3.356	43.641	16.448	44.648	1466.28	1327.68	1252.605	0.030	0.034	0.036
	S10	13.487	28.188	21.943	32.234	2133.06	1862.46	1715.885	0.015	0.017	0.019
	S3	2.916	68.436	23.447	69.310	1578.66	1427.46	1345.56	0.044	0.049	0.052
	S11	216.821	5.147	218.365	70.193	2126.088	1904.688	1784.763	0.103	0.115	0.122
6	S1	71.751	35.894	82.519	57.419	897.4	823.9	784.525	0.092	0.100	0.105
	S9	100.214	15.686	104.920	45.750	1443.47	1299.97	1223.095	0.073	0.081	0.086
	S2	3.674	53.252	19.649	54.354	1710.66	1548.96	1462.335	0.032	0.035	0.037
	S10	14.466	36.654	25.463	40.994	2488.57	2172.87	2003.745	0.016	0.019	0.020
	S3	4.726	81.809	29.269	83.227	1841.77	1665.37	1570.87	0.045	0.050	0.053
	S11	273.219	3.080	274.143	85.046	2480.436	2222.136	2083.761	0.111	0.123	0.132
5	S1	85.606	41.196	97.965	66.878	1025.6	941.6	902.225	0.096	0.104	0.109
	S9	121.519	19.879	127.483	56.335	1649.68	1485.68	1408.805	0.077	0.086	0.090
	S2	3.813	62.893	22.680	64.037	1955.04	1770.24	1683.615	0.033	0.036	0.038
	S10	16.222	45.335	29.823	50.201	2844.08	2483.28	2314.155	0.018	0.020	0.022
	S3	7.277	94.981	35.771	97.164	2104.88	1903.28	1808.78	0.046	0.051	0.054
	S11	330.958	1.056	331.275	100.343	2834.784	2539.584	2401.209	0.117	0.130	0.138
4	S1	99.373	46.197	113.232	76.009	1153.8	1059.3	1025.175	0.098	0.107	0.110
	S9	142.770	24.825	150.218	67.656	1855.89	1671.39	1604.765	0.081	0.090	0.094
	S2	3.682	72.014	25.286	73.118	2199.42	1991.52	1916.445	0.033	0.037	0.038
	S10	18.807	54.376	35.120	60.018	3199.59	2793.69	2647.115	0.019	0.021	0.023
	S3	10.316	107.255	42.492	110.349	2367.99	2141.19	2059.29	0.047	0.052	0.054

	S11	385.842	0.711	386.055	116.463	3189.132	2857.032	2737.107	0.121	0.135	0.141
3	S1	113.474	51.039	128.786	85.082	1282	1177	1153.375	0.100	0.109	0.112
	S9	162.916	29.531	171.775	78.405	2062.1	1857.1	1810.975	0.083	0.092	0.095
	S2	4.683	80.008	28.685	81.413	2443.8	2212.8	2160.825	0.033	0.037	0.038
	S10	21.859	62.528	40.617	69.086	3555.1	3104.1	3002.625	0.019	0.022	0.023
	S3	13.396	118.094	48.824	122.113	2631.1	2379.1	2322.4	0.046	0.051	0.053
	S11	436.656	2.622	437.443	133.619	3543.48	3174.48	3091.455	0.123	0.138	0.142
2	S1	126.360	55.369	142.970	93.277	1410.2	1294.7	1281.575	0.101	0.110	0.112
	S9	180.552	33.873	190.714	88.039	2268.31	2042.81	2017.185	0.084	0.093	0.095
	S2	6.346	86.629	32.334	88.532	2688.18	2434.08	2405.205	0.033	0.036	0.037
	S10	25.080	69.602	45.960	77.126	3910.61	3414.51	3358.135	0.020	0.023	0.023
	S3	16.115	126.700	54.125	131.534	2894.21	2617.01	2585.51	0.045	0.050	0.051
	S11	478.431	4.777	479.864	148.307	3897.828	3491.928	3445.803	0.123	0.137	0.139
1	S1	135.461	58.246	152.935	98.885	1538.4	1412.4	1409.775	0.099	0.108	0.108
	S9	192.662	36.857	203.719	94.656	2474.52	2228.52	2223.395	0.082	0.091	0.092
	S2	7.370	91.377	34.784	93.588	2932.56	2655.36	2649.585	0.032	0.035	0.035
	S10	27.491	74.485	49.836	82.732	4266.12	3724.92	3713.645	0.019	0.022	0.022
	S3	18.412	132.461	58.150	137.984	3157.32	2854.92	2848.62	0.044	0.048	0.048
	S11	505.084	6.829	507.133	158.354	4252.176	3809.376	3800.151	0.119	0.133	0.133

Çizelge B.155: 6 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	7.246	2.614	8.030	4.787	128.2	122.95	112.45	0.063	0.065	0.071
	S9	10.147	0.594	10.325	3.638	206.21	195.96	175.46	0.050	0.053	0.059
	S2	1.959	3.303	2.950	3.891	244.38	232.83	209.73	0.016	0.017	0.019
	S10	6.684	2.081	7.309	4.087	355.51	332.96	287.86	0.021	0.022	0.025
	S3	1.062	5.895	2.830	6.213	263.11	250.51	225.31	0.024	0.025	0.028
	S11	36.415	3.951	37.600	14.875	354.348	335.898	298.998	0.106	0.112	0.126
5	S1	20.740	7.168	22.891	13.390	256.4	245.9	230.15	0.089	0.093	0.099
	S9	27.988	2.677	28.791	11.073	412.42	391.92	361.17	0.070	0.073	0.080
	S2	5.553	9.532	8.413	11.198	488.76	465.66	431.01	0.023	0.024	0.026
	S10	15.965	6.583	17.940	11.373	711.02	665.92	598.27	0.025	0.027	0.030
	S3	1.817	14.777	6.250	15.322	526.22	501.02	463.22	0.029	0.031	0.033
	S11	89.433	6.467	91.373	33.297	708.696	671.796	616.446	0.129	0.136	0.148
4	S1	34.799	11.862	38.358	22.301	384.6	368.85	353.1	0.100	0.104	0.109
	S9	46.541	4.936	48.022	18.898	618.63	587.88	557.13	0.078	0.082	0.086
	S2	9.156	15.967	13.946	18.714	733.14	698.49	663.84	0.026	0.027	0.028
	S10	26.127	11.306	29.519	19.144	1066.53	998.88	931.23	0.028	0.030	0.032
	S3	2.540	23.678	9.644	24.440	789.33	751.53	713.73	0.031	0.033	0.034
	S11	145.026	8.960	147.714	52.468	1063.044	1007.694	952.344	0.139	0.147	0.155
3	S1	48.817	16.294	53.705	30.939	512.8	491.8	481.3	0.105	0.109	0.112
	S9	65.882	7.099	68.011	26.863	824.84	783.84	763.34	0.082	0.087	0.089
	S2	12.569	22.755	19.396	26.526	977.52	931.32	908.22	0.027	0.028	0.029
	S10	34.888	17.064	40.008	27.530	1422.04	1331.84	1286.74	0.028	0.030	0.031
	S3	3.386	32.362	13.095	33.378	1052.44	1002.04	976.84	0.032	0.033	0.034
	S11	202.224	9.799	205.164	70.466	1417.392	1343.592	1306.692	0.145	0.153	0.157
2	S1	61.352	20.161	67.401	38.567	641	614.75	609.5	0.105	0.110	0.111
	S9	83.711	9.048	86.425	34.161	1031.05	979.8	969.55	0.084	0.088	0.089
	S2	15.538	29.292	24.326	33.954	1221.9	1164.15	1152.6	0.028	0.029	0.029
	S10	41.627	23.056	48.544	35.544	1777.55	1664.8	1642.25	0.027	0.029	0.030
	S3	4.234	40.056	16.250	41.326	1315.55	1252.55	1239.95	0.031	0.033	0.033
	S11	253.676	8.848	256.331	84.951	1771.74	1679.49	1661.04	0.145	0.153	0.154
1	S1	70.162	23.120	77.098	44.169	769.2	737.7	737.7	0.100	0.105	0.105
	S9	96.872	10.547	100.036	39.609	1237.26	1175.76	1175.76	0.081	0.085	0.085
	S2	17.227	34.565	27.597	39.733	1466.28	1396.98	1396.98	0.027	0.028	0.028
	S10	46.029	28.384	54.544	42.192	2133.06	1997.76	1997.76	0.026	0.027	0.027
	S3	4.783	45.847	18.537	47.281	1578.66	1503.06	1503.06	0.030	0.031	0.031
	S11	289.085	6.428	291.013	93.153	2126.088	2015.388	2015.388	0.137	0.144	0.144

Çizelge B.156: 9 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	8.782	4.000	9.982	6.635	128.2	117.7	104.575	0.078	0.085	0.095
	S9	11.875	0.941	12.157	4.503	206.21	185.71	160.085	0.059	0.065	0.076
	S2	0.873	4.735	2.293	4.996	244.38	221.28	192.405	0.020	0.023	0.026
	S10	4.763	2.122	5.399	3.550	355.51	310.41	254.035	0.015	0.017	0.021
	S3	1.462	9.932	4.442	10.371	263.11	237.91	206.41	0.039	0.044	0.050
	S11	39.772	4.858	41.229	16.789	354.348	317.448	271.323	0.116	0.130	0.152
8	S1	25.530	10.883	28.795	18.542	256.4	235.4	207.05	0.112	0.122	0.139
	S9	33.684	4.088	34.910	14.193	412.42	371.42	316.07	0.085	0.094	0.110
	S2	3.404	13.700	7.514	14.721	488.76	442.56	380.19	0.030	0.033	0.039
	S10	12.443	7.539	14.704	11.272	711.02	620.82	499.05	0.021	0.024	0.029
	S3	2.060	24.246	9.334	24.864	526.22	475.82	407.78	0.047	0.052	0.061
	S11	100.744	7.776	103.077	37.999	708.696	634.896	535.266	0.145	0.162	0.193
7	S1	43.402	17.978	48.796	30.999	384.6	353.1	314.25	0.127	0.138	0.155
	S9	56.941	7.476	59.184	24.558	618.63	557.13	481.28	0.096	0.106	0.123
	S2	6.277	22.913	13.151	24.796	733.14	663.84	578.37	0.034	0.037	0.043
	S10	21.799	13.300	25.789	19.840	1066.53	931.23	764.36	0.024	0.028	0.034
	S3	2.818	38.706	14.430	39.551	789.33	713.73	620.49	0.050	0.055	0.064
	S11	167.479	11.255	170.856	61.499	1063.044	952.344	815.814	0.161	0.179	0.209
6	S1	62.556	25.002	70.056	43.769	512.8	470.8	426.7	0.137	0.149	0.164
	S9	83.258	10.881	86.522	35.858	824.84	742.84	656.74	0.105	0.116	0.132
	S2	9.441	33.153	19.386	35.985	977.52	885.12	788.1	0.037	0.041	0.046
	S10	30.327	21.051	36.642	30.149	1422.04	1241.64	1052.22	0.026	0.030	0.035
	S3	4.054	53.594	20.132	54.811	1052.44	951.64	845.8	0.052	0.058	0.065
	S11	243.146	12.975	247.039	85.919	1417.392	1269.792	1114.812	0.174	0.195	0.222
5	S1	82.532	31.812	92.075	56.571	641	588.5	544.4	0.144	0.156	0.169
	S9	111.606	14.203	115.867	47.685	1031.05	928.55	842.45	0.112	0.125	0.138
	S2	13.041	44.131	26.280	48.043	1221.9	1106.4	1009.38	0.039	0.043	0.048
	S10	38.347	30.147	47.391	41.651	1777.55	1552.05	1362.63	0.027	0.031	0.035
	S3	5.793	68.426	26.321	70.164	1315.55	1189.55	1083.71	0.053	0.059	0.065
	S11	324.782	13.298	328.771	110.733	1771.74	1587.24	1432.26	0.186	0.207	0.230
4	S1	101.849	38.180	113.303	68.735	769.2	706.2	667.35	0.147	0.160	0.170
	S9	140.694	17.409	145.917	59.617	1237.26	1114.26	1038.41	0.118	0.131	0.141
	S2	15.791	55.003	32.291	59.740	1466.28	1327.68	1242.21	0.041	0.045	0.048
	S10	45.711	40.802	57.952	54.515	2133.06	1862.46	1695.59	0.027	0.031	0.034
	S3	7.455	82.680	32.259	84.916	1578.66	1427.46	1334.22	0.054	0.059	0.064
	S11	408.372	12.671	412.174	135.183	2126.088	1904.688	1768.158	0.194	0.216	0.233
3	S1	120.851	43.755	133.978	80.010	897.4	823.9	795.55	0.149	0.163	0.168
	S9	169.347	20.552	175.513	71.357	1443.47	1299.97	1244.62	0.122	0.135	0.141
	S2	17.507	65.518	37.163	70.770	1710.66	1548.96	1486.59	0.041	0.046	0.048
	S10	50.197	51.083	65.522	66.142	2488.57	2172.87	2051.1	0.027	0.030	0.032
	S3	10.194	96.348	39.099	99.407	1841.77	1665.37	1597.33	0.054	0.060	0.062
	S11	493.234	10.585	496.410	158.555	2480.436	2222.136	2122.506	0.200	0.223	0.234
2	S1	137.861	48.592	152.438	89.950	1025.6	941.6	923.75	0.149	0.162	0.165
	S9	195.248	24.612	202.632	83.187	1649.68	1485.68	1450.83	0.123	0.136	0.140
	S2	18.649	74.659	41.047	80.254	1955.04	1770.24	1730.97	0.041	0.045	0.046
	S10	54.457	59.869	72.417	76.206	2844.08	2483.28	2406.61	0.027	0.031	0.032
	S3	13.345	107.980	45.739	111.984	2104.88	1903.28	1860.44	0.053	0.059	0.060
	S11	565.615	7.904	567.986	177.588	2834.784	2539.584	2476.854	0.200	0.224	0.229
1	S1	149.827	52.150	165.472	97.098	1153.8	1059.3	1051.95	0.143	0.156	0.157
	S9	214.402	28.528	222.960	92.849	1855.89	1671.39	1657.04	0.120	0.133	0.135
	S2	18.969	81.447	43.403	87.137	2199.42	1991.52	1975.35	0.040	0.044	0.044
	S10	58.166	67.182	78.321	84.632	3199.59	2793.69	2762.12	0.026	0.030	0.031
	S3	15.842	116.046	50.655	120.798	2367.99	2141.19	2123.55	0.051	0.056	0.057
	S11	611.473	4.721	612.889	188.163	3189.132	2857.032	2831.202	0.192	0.215	0.216

Çizelge B.157: 12 Kat, Ankara, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	8.894	5.902	10.665	8.570	128.2	117.7	117.7	0.083	0.091	0.091
	S9	11.685	1.102	12.016	4.607	206.21	185.71	185.71	0.058	0.065	0.065
	S2	0.587	6.991	2.684	7.167	244.38	221.28	221.28	0.029	0.032	0.032
	S10	1.248	2.029	1.857	2.404	355.51	310.41	310.41	0.007	0.008	0.008
	S3	1.447	15.230	6.016	15.664	263.11	237.91	237.91	0.060	0.066	0.066
	S11	35.147	5.333	36.747	15.877	354.348	317.448	317.448	0.104	0.116	0.116
11	S1	26.276	15.972	31.067	23.855	256.4	235.4	235.4	0.121	0.132	0.132
	S9	34.089	5.350	35.695	15.577	412.42	371.42	371.42	0.087	0.096	0.096
	S2	0.166	20.149	6.210	20.199	488.76	442.56	442.56	0.041	0.046	0.046
	S10	5.250	8.623	7.836	10.198	711.02	620.82	620.82	0.014	0.016	0.016
	S3	1.457	36.713	12.470	37.150	526.22	475.82	475.82	0.071	0.078	0.078
	S11	91.984	7.752	94.309	35.347	708.696	634.896	634.896	0.133	0.149	0.149
10	S1	44.926	26.333	52.826	39.811	384.6	353.1	353.1	0.137	0.150	0.150
	S9	58.081	9.939	61.063	27.363	618.63	557.13	557.13	0.099	0.110	0.110
	S2	1.323	33.553	11.389	33.950	733.14	663.84	663.84	0.046	0.051	0.051
	S10	11.042	15.632	15.732	18.945	1066.53	931.23	931.23	0.018	0.020	0.020
	S3	1.697	58.451	19.232	58.960	789.33	713.73	713.73	0.075	0.083	0.083
	S11	155.355	11.165	158.704	57.772	1063.044	952.344	952.344	0.149	0.167	0.167
9	S1	65.298	36.726	76.316	56.316	512.8	470.8	457.675	0.149	0.162	0.167
	S9	85.906	14.633	90.295	40.404	824.84	742.84	717.215	0.109	0.122	0.126
	S2	2.809	48.511	17.362	49.354	977.52	885.12	856.245	0.050	0.056	0.058
	S10	15.973	25.510	23.625	30.302	1422.04	1241.64	1185.265	0.021	0.024	0.026
	S3	2.479	81.165	26.829	81.908	1052.44	951.64	920.14	0.078	0.086	0.089
	S11	229.755	12.191	233.412	81.118	1417.392	1269.792	1223.667	0.165	0.184	0.191
8	S1	87.325	47.130	101.463	73.327	641	588.5	564.875	0.158	0.172	0.180
	S9	117.009	19.371	122.820	54.473	1031.05	928.55	882.425	0.119	0.132	0.139
	S2	4.931	64.832	24.381	66.311	1221.9	1106.4	1054.425	0.054	0.060	0.063
	S10	20.735	37.532	31.995	43.753	1777.55	1552.05	1450.575	0.025	0.028	0.030
	S3	3.928	104.525	35.285	105.704	1315.55	1189.55	1132.85	0.080	0.089	0.093
	S11	314.044	11.528	317.502	105.741	1771.74	1587.24	1504.215	0.179	0.200	0.211
7	S1	109.869	57.397	127.088	90.358	769.2	706.2	672.075	0.165	0.180	0.189
	S9	151.017	24.230	158.286	69.535	1237.26	1114.26	1047.635	0.128	0.142	0.151
	S2	6.292	81.827	30.841	83.715	1466.28	1327.68	1252.605	0.057	0.063	0.067
	S10	25.287	52.853	41.143	60.439	2133.06	1862.46	1715.885	0.028	0.032	0.035
	S3	5.468	128.317	43.962	129.957	1578.66	1427.46	1345.56	0.082	0.091	0.097
	S11	406.540	9.650	409.435	131.612	2126.088	1904.688	1784.763	0.193	0.215	0.229
6	S1	134.532	67.301	154.722	107.660	897.4	823.9	784.525	0.172	0.188	0.197
	S9	187.902	29.412	196.725	85.782	1443.47	1299.97	1223.095	0.136	0.151	0.161
	S2	6.888	99.847	36.842	101.914	1710.66	1548.96	1462.335	0.060	0.066	0.070
	S10	27.125	68.726	47.742	76.863	2488.57	2172.87	2003.745	0.031	0.035	0.038
	S3	8.861	153.392	54.878	156.050	1841.77	1665.37	1570.87	0.085	0.094	0.099
	S11	512.285	5.775	514.017	159.461	2480.436	2222.136	2083.761	0.207	0.231	0.247
5	S1	160.512	77.242	183.684	125.396	1025.6	941.6	902.225	0.179	0.195	0.204
	S9	227.848	37.274	239.030	105.628	1649.68	1485.68	1408.805	0.145	0.161	0.170
	S2	7.149	117.925	42.526	120.069	1955.04	1770.24	1683.615	0.061	0.068	0.071
	S10	30.417	85.002	55.918	94.127	2844.08	2483.28	2314.155	0.033	0.038	0.041
	S3	13.645	178.089	67.071	182.182	2104.88	1903.28	1808.78	0.087	0.096	0.101
	S11	620.546	1.979	621.140	188.143	2834.784	2539.584	2401.209	0.219	0.245	0.259
4	S1	186.324	86.619	212.309	142.516	1153.8	1059.3	1025.175	0.184	0.200	0.207
	S9	267.694	46.547	281.658	126.855	1855.89	1671.39	1604.765	0.152	0.169	0.176
	S2	6.904	135.026	47.412	137.097	2199.42	1991.52	1916.445	0.062	0.069	0.072
	S10	35.263	101.955	65.849	112.534	3199.59	2793.69	2647.115	0.035	0.040	0.043
	S3	19.342	201.102	79.673	206.905	2367.99	2141.19	2059.29	0.087	0.097	0.100

	S11	723.453	1.333	723.853	218.368	3189.132	2857.032	2737.107	0.227	0.253	0.264
3	S1	212.764	95.699	241.474	159.528	1282	1177	1153.375	0.188	0.205	0.209
	S9	305.468	55.370	322.079	147.010	2062.1	1857.1	1810.975	0.156	0.173	0.178
	S2	8.780	150.015	53.784	152.649	2443.8	2212.8	2160.825	0.062	0.069	0.071
	S10	40.985	117.240	76.157	129.536	3555.1	3104.1	3002.625	0.036	0.042	0.043
	S3	25.117	221.426	91.545	228.961	2631.1	2379.1	2322.4	0.087	0.096	0.099
	S11	818.730	4.917	820.205	250.536	3543.48	3174.48	3091.455	0.231	0.258	0.265
2	S1	236.925	103.816	268.070	174.894	1410.2	1294.7	1281.575	0.190	0.207	0.209
	S9	338.535	63.512	357.589	165.073	2268.31	2042.81	2017.185	0.158	0.175	0.177
	S2	11.898	162.429	60.627	165.998	2688.18	2434.08	2405.205	0.062	0.068	0.069
	S10	47.024	130.504	86.175	144.611	3910.61	3414.51	3358.135	0.037	0.042	0.043
	S3	30.216	237.562	101.485	246.626	2894.21	2617.01	2585.51	0.085	0.094	0.095
	S11	897.058	8.958	899.745	278.075	3897.828	3491.928	3445.803	0.231	0.258	0.261
1	S1	253.989	109.212	286.753	185.408	1538.4	1412.4	1409.775	0.186	0.203	0.203
	S9	361.241	69.107	381.973	177.479	2474.52	2228.52	2223.395	0.154	0.171	0.172
	S2	13.820	171.332	65.219	175.478	2932.56	2655.36	2649.585	0.060	0.066	0.066
	S10	51.546	139.659	93.443	155.123	4266.12	3724.92	3713.645	0.036	0.042	0.042
	S3	34.523	248.364	109.032	258.721	3157.32	2854.92	2848.62	0.082	0.091	0.091
	S11	947.033	12.804	950.874	296.914	4252.176	3809.376	3800.151	0.224	0.250	0.250

Çizelge B.158: 6 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	11.372	4.039	12.584	7.451	128.2	122.95	112.45	0.098	0.102	0.112
	S9	15.924	0.919	16.199	5.696	206.21	195.96	175.46	0.079	0.083	0.092
	S2	3.075	5.105	4.606	6.027	244.38	232.83	209.73	0.025	0.026	0.029
	S10	10.490	3.217	11.455	6.364	355.51	332.96	287.86	0.032	0.034	0.040
	S3	1.666	9.111	4.399	9.610	263.11	250.51	225.31	0.037	0.038	0.043
	S11	57.146	6.107	58.978	23.250	354.348	335.898	298.998	0.166	0.176	0.197
5	S1	32.548	11.078	35.872	20.843	256.4	245.9	230.15	0.140	0.146	0.156
	S9	43.922	4.138	45.163	17.314	412.42	391.92	361.17	0.110	0.115	0.125
	S2	8.715	14.732	13.135	17.346	488.76	465.66	431.01	0.035	0.037	0.040
	S10	25.054	10.175	28.107	17.692	711.02	665.92	598.27	0.040	0.042	0.047
	S3	2.851	22.839	9.703	23.695	526.22	501.02	463.22	0.045	0.047	0.051
	S11	140.351	9.995	143.349	52.100	708.696	671.796	616.446	0.202	0.213	0.233
4	S1	54.612	18.333	60.112	34.717	384.6	368.85	353.1	0.156	0.163	0.170
	S9	73.039	7.629	75.327	29.540	618.63	587.88	557.13	0.122	0.128	0.135
	S2	14.368	24.678	21.772	28.989	733.14	698.49	663.84	0.040	0.042	0.044
	S10	41.003	17.474	46.245	29.775	1066.53	998.88	931.23	0.043	0.046	0.050
	S3	3.986	36.597	14.965	37.792	789.33	751.53	713.73	0.048	0.050	0.053
	S11	227.594	13.849	231.749	82.127	1063.044	1007.694	952.344	0.218	0.230	0.243
3	S1	76.611	25.183	84.166	48.166	512.8	491.8	481.3	0.164	0.171	0.175
	S9	103.390	10.972	106.682	41.989	824.84	783.84	763.34	0.129	0.136	0.140
	S2	19.725	35.170	30.277	41.088	977.52	931.32	908.22	0.042	0.044	0.045
	S10	54.752	26.374	62.664	42.799	1422.04	1331.84	1286.74	0.044	0.047	0.049
	S3	5.314	50.018	20.319	51.612	1052.44	1002.04	976.84	0.049	0.052	0.053
	S11	317.357	15.145	321.901	110.352	1417.392	1343.592	1306.692	0.227	0.240	0.246
2	S1	96.282	31.161	105.630	60.045	641	614.75	609.5	0.165	0.172	0.173
	S9	131.370	13.984	135.565	53.395	1031.05	979.8	969.55	0.131	0.138	0.140
	S2	24.384	45.274	37.966	52.589	1221.9	1164.15	1152.6	0.043	0.045	0.046
	S10	65.327	35.636	76.017	55.234	1777.55	1664.8	1642.25	0.043	0.046	0.046
	S3	6.644	61.910	25.217	63.903	1315.55	1252.55	1239.95	0.049	0.051	0.052
	S11	398.103	13.675	402.205	133.106	1771.74	1679.49	1661.04	0.227	0.239	0.242
1	S1	110.107	35.734	120.827	68.766	769.2	737.7	737.7	0.157	0.164	0.164
	S9	152.024	16.301	156.914	61.908	1237.26	1175.76	1175.76	0.127	0.133	0.133
	S2	27.035	53.424	43.062	61.534	1466.28	1396.98	1396.98	0.042	0.044	0.044
	S10	72.235	43.869	85.395	65.539	2133.06	1997.76	1997.76	0.040	0.043	0.043
	S3	7.506	70.860	28.764	73.111	1578.66	1503.06	1503.06	0.046	0.049	0.049
	S11	453.671	9.935	456.651	146.036	2126.088	2015.388	2015.388	0.215	0.227	0.227

Çizelge B.159: 9 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	13.781	6.278	15.665	10.412	128.2	117.7	104.575	0.122	0.133	0.150
	S9	18.635	1.476	19.078	7.067	206.21	185.71	160.085	0.093	0.103	0.119
	S2	1.370	7.430	3.599	7.841	244.38	221.28	192.405	0.032	0.035	0.041
	S10	7.475	3.330	8.473	5.572	355.51	310.41	254.035	0.024	0.027	0.033
	S3	2.295	15.587	6.971	16.276	263.11	237.91	206.41	0.062	0.068	0.079
	S11	62.415	7.623	64.702	26.348	354.348	317.448	271.323	0.183	0.204	0.238
8	S1	40.065	17.078	45.188	29.098	256.4	235.4	207.05	0.176	0.192	0.218
	S9	52.862	6.415	54.786	22.274	412.42	371.42	316.07	0.133	0.148	0.173
	S2	5.343	21.500	11.792	23.103	488.76	442.56	380.19	0.047	0.052	0.061
	S10	19.527	11.831	23.076	17.689	711.02	620.82	499.05	0.032	0.037	0.046
	S3	3.234	38.050	14.649	39.020	526.22	475.82	407.78	0.074	0.082	0.096
	S11	158.101	12.203	161.762	59.633	708.696	634.896	535.266	0.228	0.255	0.302
7	S1	68.113	28.214	76.577	48.648	384.6	353.1	314.25	0.199	0.217	0.244
	S9	89.360	11.732	92.879	38.540	618.63	557.13	481.28	0.150	0.167	0.193
	S2	9.851	35.958	20.639	38.913	733.14	663.84	578.37	0.053	0.059	0.067
	S10	34.211	20.872	40.472	31.135	1066.53	931.23	764.36	0.038	0.043	0.053
	S3	4.422	60.742	22.645	62.069	789.33	713.73	620.49	0.079	0.087	0.100
	S11	262.831	17.664	268.130	96.513	1063.044	952.344	815.814	0.252	0.282	0.329
6	S1	98.171	39.237	109.942	68.688	512.8	470.8	426.7	0.214	0.234	0.258
	S9	130.660	17.075	135.782	56.273	824.84	742.84	656.74	0.165	0.183	0.207
	S2	14.815	52.028	30.424	56.473	977.52	885.12	788.1	0.058	0.064	0.072
	S10	47.594	33.036	57.504	47.314	1422.04	1241.64	1052.22	0.040	0.046	0.055
	S3	6.362	84.108	31.594	86.016	1052.44	951.64	845.8	0.082	0.090	0.102
	S11	381.577	20.362	387.686	134.836	1417.392	1269.792	1114.812	0.274	0.305	0.348
5	S1	129.520	49.923	144.497	88.779	641	588.5	544.4	0.225	0.246	0.265
	S9	175.147	22.290	181.834	74.834	1031.05	928.55	842.45	0.176	0.196	0.216
	S2	20.466	69.256	41.242	75.395	1221.9	1106.4	1009.38	0.062	0.068	0.075
	S10	60.180	47.310	74.373	65.364	1777.55	1552.05	1362.63	0.042	0.048	0.055
	S3	9.091	107.383	41.306	110.110	1315.55	1189.55	1083.71	0.084	0.093	0.102
	S11	509.691	20.869	515.952	173.777	1771.74	1587.24	1432.26	0.291	0.325	0.360
4	S1	159.835	59.917	177.810	107.868	769.2	706.2	667.35	0.231	0.252	0.266
	S9	220.795	27.321	228.992	93.559	1237.26	1114.26	1038.41	0.185	0.206	0.221
	S2	24.781	86.318	50.676	93.752	1466.28	1327.68	1242.21	0.064	0.071	0.075
	S10	71.736	64.032	90.946	85.552	2133.06	1862.46	1695.59	0.043	0.049	0.054
	S3	11.700	129.752	50.625	133.261	1578.66	1427.46	1334.22	0.084	0.093	0.100
	S11	640.873	19.885	646.838	212.147	2126.088	1904.688	1768.158	0.304	0.340	0.366
3	S1	189.656	68.666	210.256	125.563	897.4	823.9	795.55	0.234	0.255	0.264
	S9	265.763	32.254	275.439	111.982	1443.47	1299.97	1244.62	0.191	0.212	0.221
	S2	27.475	102.820	58.321	111.062	1710.66	1548.96	1486.59	0.065	0.072	0.075
	S10	78.776	80.167	102.826	103.799	2488.57	2172.87	2051.1	0.042	0.048	0.051
	S3	15.998	151.203	61.359	156.002	1841.77	1665.37	1597.33	0.085	0.094	0.098
	S11	774.049	16.612	779.032	248.826	2480.436	2222.136	2122.506	0.314	0.351	0.367
2	S1	216.349	76.257	239.226	141.162	1025.6	941.6	923.75	0.233	0.254	0.259
	S9	306.410	38.625	317.997	130.548	1649.68	1485.68	1450.83	0.193	0.214	0.219
	S2	29.267	117.165	64.416	125.945	1955.04	1770.24	1730.97	0.064	0.071	0.073
	S10	85.461	93.954	113.647	119.592	2844.08	2483.28	2406.61	0.042	0.048	0.050
	S3	20.942	169.457	71.779	175.740	2104.88	1903.28	1860.44	0.083	0.092	0.094
	S11	887.639	12.403	891.360	278.695	2834.784	2539.584	2476.854	0.314	0.351	0.360
1	S1	235.129	81.841	259.681	152.379	1153.8	1059.3	1051.95	0.225	0.245	0.247
	S9	336.468	44.770	349.899	145.711	1855.89	1671.39	1657.04	0.189	0.209	0.211
	S2	29.769	127.817	68.114	136.748	2199.42	1991.52	1975.35	0.062	0.069	0.069
	S10	91.282	105.431	122.912	132.816	3199.59	2793.69	2762.12	0.042	0.048	0.048
	S3	24.861	182.114	79.495	189.573	2367.99	2141.19	2123.55	0.080	0.089	0.089
	S11	959.605	7.409	961.827	295.290	3189.132	2857.032	2831.202	0.302	0.337	0.340

Çizelge B.160: 12 Kat, Ankara, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	13.958	9.262	16.736	13.450	128.2	117.7	117.7	0.131	0.142	0.142
	S9	18.338	1.729	18.857	7.230	206.21	185.71	185.71	0.091	0.102	0.102
	S2	0.921	10.971	4.212	11.247	244.38	221.28	221.28	0.046	0.051	0.051
	S10	1.959	3.185	2.915	3.772	355.51	310.41	310.41	0.011	0.012	0.012
	S3	2.271	23.901	9.441	24.582	263.11	237.91	237.91	0.093	0.103	0.103
	S11	55.158	8.370	57.669	24.917	354.348	317.448	317.448	0.163	0.182	0.182
11	S1	41.235	25.066	48.755	37.437	256.4	235.4	235.4	0.190	0.207	0.207
	S9	53.498	8.397	56.017	24.446	412.42	371.42	371.42	0.136	0.151	0.151
	S2	0.260	31.621	9.746	31.699	488.76	442.56	442.56	0.065	0.072	0.072
	S10	8.238	13.533	12.298	16.004	711.02	620.82	620.82	0.023	0.026	0.026
	S3	2.286	57.616	19.570	58.301	526.22	475.82	475.82	0.111	0.123	0.123
	S11	144.353	12.165	148.002	55.471	708.696	634.896	634.896	0.209	0.233	0.233
10	S1	70.504	41.325	82.902	62.476	384.6	353.1	353.1	0.216	0.235	0.235
	S9	91.149	15.597	95.828	42.942	618.63	557.13	557.13	0.155	0.172	0.172
	S2	2.076	52.655	17.873	53.278	733.14	663.84	663.84	0.073	0.080	0.080
	S10	17.329	24.532	24.689	29.731	1066.53	931.23	931.23	0.028	0.032	0.032
	S3	2.663	91.729	30.182	92.528	789.33	713.73	713.73	0.117	0.130	0.130
	S11	243.803	17.522	249.060	90.663	1063.044	952.344	952.344	0.234	0.262	0.262
9	S1	102.475	57.636	119.765	88.378	512.8	470.8	457.675	0.234	0.254	0.262
	S9	134.815	22.964	141.704	63.408	824.84	742.84	717.215	0.172	0.191	0.198
	S2	4.409	76.130	27.247	77.452	977.52	885.12	856.245	0.079	0.088	0.090
	S10	25.066	40.034	37.076	47.553	1422.04	1241.64	1185.265	0.033	0.038	0.040
	S3	3.891	127.374	42.103	128.542	1052.44	951.64	920.14	0.122	0.135	0.140
	S11	360.562	19.132	366.302	127.301	1417.392	1269.792	1223.667	0.258	0.288	0.299
8	S1	137.041	73.962	159.230	115.074	641	588.5	564.875	0.248	0.271	0.282
	S9	183.626	30.399	192.746	85.487	1031.05	928.55	882.425	0.187	0.208	0.218
	S2	7.738	101.743	38.261	104.065	1221.9	1106.4	1054.425	0.085	0.094	0.099
	S10	32.540	58.901	50.210	68.663	1777.55	1552.05	1450.575	0.039	0.044	0.047
	S3	6.164	164.035	55.374	165.884	1315.55	1189.55	1132.85	0.126	0.139	0.146
	S11	492.839	18.092	498.267	165.943	1771.74	1587.24	1504.215	0.281	0.314	0.331
7	S1	172.421	90.075	199.444	141.801	769.2	706.2	672.075	0.259	0.282	0.297
	S9	236.996	38.025	248.404	109.124	1237.26	1114.26	1047.635	0.201	0.223	0.237
	S2	9.875	128.415	48.399	131.377	1466.28	1327.68	1252.605	0.090	0.099	0.105
	S10	39.684	82.944	64.567	94.849	2133.06	1862.46	1715.885	0.044	0.051	0.055
	S3	8.580	201.372	68.992	203.946	1578.66	1427.46	1345.56	0.129	0.143	0.152
	S11	637.996	15.144	642.540	206.543	2126.088	1904.688	1784.763	0.302	0.337	0.360
6	S1	211.126	105.617	242.811	168.955	897.4	823.9	784.525	0.271	0.295	0.310
	S9	294.880	46.157	308.727	134.621	1443.47	1299.97	1223.095	0.214	0.237	0.252
	S2	10.810	156.694	57.818	159.936	1710.66	1548.96	1462.335	0.093	0.103	0.109
	S10	42.568	107.854	74.924	120.624	2488.57	2172.87	2003.745	0.048	0.056	0.060
	S3	13.906	240.723	86.123	244.895	1841.77	1665.37	1570.87	0.133	0.147	0.156
	S11	803.945	9.063	806.664	250.247	2480.436	2222.136	2083.761	0.325	0.363	0.387
5	S1	251.896	121.219	288.262	196.788	1025.6	941.6	902.225	0.281	0.306	0.320
	S9	357.570	58.495	375.118	165.766	1649.68	1485.68	1408.805	0.227	0.252	0.266
	S2	11.218	185.063	66.737	188.429	1955.04	1770.24	1683.615	0.096	0.106	0.112
	S10	47.735	133.397	87.754	147.717	2844.08	2483.28	2314.155	0.052	0.059	0.064
	S3	21.413	279.480	105.257	285.904	2104.88	1903.28	1808.78	0.136	0.150	0.158
	S11	973.844	3.106	974.776	295.259	2834.784	2539.584	2401.209	0.344	0.384	0.406
4	S1	292.404	135.935	333.184	223.656	1153.8	1059.3	1025.175	0.289	0.315	0.325
	S9	420.101	73.048	442.016	199.078	1855.89	1671.39	1604.765	0.238	0.264	0.275
	S2	10.835	211.901	74.405	215.151	2199.42	1991.52	1916.445	0.098	0.108	0.112
	S10	55.339	160.001	103.340	176.603	3199.59	2793.69	2647.115	0.055	0.063	0.067
	S3	30.355	315.596	125.034	324.703	2367.99	2141.19	2059.29	0.137	0.152	0.158

	S11	1135.339	2.091	1135.966	342.693	3189.132	2857.032	2737.107	0.356	0.398	0.415
3	S1	333.898	150.184	378.953	250.353	1282	1177	1153.375	0.296	0.322	0.329
	S9	479.381	86.893	505.449	230.708	2062.1	1857.1	1810.975	0.245	0.272	0.279
	S2	13.779	235.423	84.406	239.557	2443.8	2212.8	2160.825	0.098	0.108	0.111
	S10	64.319	183.989	119.516	203.284	3555.1	3104.1	3002.625	0.057	0.065	0.068
	S3	39.417	347.491	143.664	359.316	2631.1	2379.1	2322.4	0.137	0.151	0.155
	S11	1284.860	7.716	1287.175	393.174	3543.48	3174.48	3091.455	0.363	0.405	0.416
2	S1	371.814	162.923	420.691	274.467	1410.2	1294.7	1281.575	0.298	0.325	0.328
	S9	531.275	99.672	561.176	259.054	2268.31	2042.81	2017.185	0.247	0.275	0.278
	S2	18.672	254.905	95.144	260.507	2688.18	2434.08	2405.205	0.097	0.107	0.108
	S10	73.797	204.803	135.238	226.942	3910.61	3414.51	3358.135	0.058	0.066	0.068
	S3	47.419	372.813	159.263	387.039	2894.21	2617.01	2585.51	0.134	0.148	0.150
	S11	1407.783	14.057	1412.001	436.392	3897.828	3491.928	3445.803	0.362	0.404	0.410
1	S1	398.594	171.389	450.011	290.968	1538.4	1412.4	1409.775	0.293	0.319	0.319
	S9	566.907	108.452	599.443	278.524	2474.52	2228.52	2223.395	0.242	0.269	0.270
	S2	21.687	268.878	102.351	275.384	2932.56	2655.36	2649.585	0.094	0.104	0.104
	S10	80.892	219.172	146.644	243.439	4266.12	3724.92	3713.645	0.057	0.065	0.066
	S3	54.178	389.766	171.108	406.019	3157.32	2854.92	2848.62	0.129	0.142	0.143
	S11	1486.210	20.094	1492.239	465.957	4252.176	3809.376	3800.151	0.351	0.392	0.393

Çizelge B.161: 6 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	18.746	6.129	20.585	11.753	128.2	122.95	112.45	0.161	0.167	0.183
	S9	26.249	1.394	26.667	9.268	206.21	195.96	175.46	0.129	0.136	0.152
	S2	5.068	7.747	7.392	9.267	244.38	232.83	209.73	0.038	0.040	0.044
	S10	17.292	4.882	18.756	10.069	355.51	332.96	287.86	0.053	0.056	0.065
	S3	2.746	13.825	6.894	14.649	263.11	250.51	225.31	0.056	0.058	0.065
	S11	94.203	9.266	96.982	37.527	354.348	335.898	298.998	0.274	0.289	0.324
5	S1	53.654	16.811	58.697	32.907	256.4	245.9	230.15	0.229	0.239	0.255
	S9	72.403	6.279	74.286	28.000	412.42	391.92	361.17	0.180	0.190	0.206
	S2	14.366	22.354	21.073	26.664	488.76	465.66	431.01	0.055	0.057	0.062
	S10	41.301	15.440	45.933	27.830	711.02	665.92	598.27	0.065	0.069	0.077
	S3	4.700	34.657	15.097	36.067	526.22	501.02	463.22	0.069	0.072	0.078
	S11	231.360	15.166	235.910	84.574	708.696	671.796	616.446	0.333	0.351	0.383
4	S1	90.024	27.819	98.370	54.827	384.6	368.85	353.1	0.256	0.267	0.279
	S9	120.400	11.576	123.873	47.696	618.63	587.88	557.13	0.200	0.211	0.222
	S2	23.686	37.447	34.920	44.553	733.14	698.49	663.84	0.061	0.064	0.067
	S10	67.591	26.515	75.545	46.792	1066.53	998.88	931.23	0.071	0.076	0.081
	S3	6.571	55.532	23.231	57.504	789.33	751.53	713.73	0.073	0.077	0.081
	S11	375.176	21.014	381.480	133.567	1063.044	1007.694	952.344	0.359	0.379	0.401
3	S1	126.288	38.213	137.752	76.100	512.8	491.8	481.3	0.269	0.280	0.286
	S9	170.433	16.649	175.428	67.779	824.84	783.84	763.34	0.213	0.224	0.230
	S2	32.516	53.368	48.527	63.123	977.52	931.32	908.22	0.065	0.068	0.070
	S10	90.255	40.020	102.261	67.096	1422.04	1331.84	1286.74	0.072	0.077	0.079
	S3	8.759	75.899	31.529	78.527	1052.44	1002.04	976.84	0.075	0.078	0.080
	S11	523.145	22.981	530.039	179.924	1417.392	1343.592	1306.692	0.374	0.394	0.406
2	S1	158.715	47.284	172.900	94.898	641	614.75	609.5	0.270	0.281	0.284
	S9	216.555	21.220	222.921	86.187	1031.05	979.8	969.55	0.216	0.228	0.230
	S2	40.196	68.699	60.806	80.758	1221.9	1164.15	1152.6	0.066	0.069	0.070
	S10	107.687	54.074	123.909	86.380	1777.55	1664.8	1642.25	0.070	0.074	0.075
	S3	10.952	93.944	39.135	97.230	1315.55	1252.55	1239.95	0.074	0.078	0.078
	S11	656.249	20.751	662.474	217.626	1771.74	1679.49	1661.04	0.374	0.394	0.399
1	S1	181.505	54.224	197.772	108.675	769.2	737.7	737.7	0.257	0.268	0.268
	S9	250.602	24.736	258.023	99.917	1237.26	1175.76	1175.76	0.209	0.219	0.219
	S2	44.565	81.066	68.885	94.436	1466.28	1396.98	1396.98	0.064	0.068	0.068
	S10	119.075	66.568	139.045	102.290	2133.06	1997.76	1997.76	0.065	0.070	0.070
	S3	12.373	107.524	44.630	111.236	1578.66	1503.06	1503.06	0.070	0.074	0.074
	S11	747.850	15.075	752.372	239.430	2126.088	2015.388	2015.388	0.354	0.373	0.373

Çizelge B.162: 9 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	23.385	10.658	26.582	17.674	128.2	117.7	104.575	0.207	0.226	0.254
	S9	31.629	2.506	32.380	11.994	206.21	185.71	160.085	0.157	0.174	0.202
	S2	2.335	12.615	6.120	13.315	244.38	221.28	192.405	0.054	0.060	0.069
	S10	12.689	5.652	14.384	9.459	355.51	310.41	254.035	0.040	0.046	0.057
	S3	3.906	26.462	11.844	27.633	263.11	237.91	206.41	0.105	0.116	0.134
	S11	105.940	12.940	109.822	44.722	354.348	317.448	271.323	0.310	0.346	0.405
8	S1	67.985	28.994	76.684	49.390	256.4	235.4	207.05	0.299	0.326	0.370
	S9	89.714	10.892	92.982	37.806	412.42	371.42	316.07	0.225	0.250	0.294
	S2	9.098	36.505	20.050	39.234	488.76	442.56	380.19	0.080	0.089	0.103
	S10	33.155	20.087	39.181	30.033	711.02	620.82	499.05	0.055	0.063	0.079
	S3	5.516	64.596	24.894	66.251	526.22	475.82	407.78	0.126	0.139	0.162
	S11	268.350	20.715	274.565	101.220	708.696	634.896	535.266	0.387	0.432	0.513
7	S1	115.578	47.901	129.948	82.574	384.6	353.1	314.25	0.338	0.368	0.414
	S9	151.654	19.919	157.630	65.415	618.63	557.13	481.28	0.255	0.283	0.328
	S2	16.778	61.057	35.095	66.090	733.14	663.84	578.37	0.090	0.100	0.114
	S10	58.092	35.438	68.723	52.865	1066.53	931.23	764.36	0.064	0.074	0.090
	S3	7.553	103.121	38.489	105.387	789.33	713.73	620.49	0.134	0.148	0.170
	S11	446.110	29.986	455.105	163.819	1063.044	952.344	815.814	0.428	0.478	0.558
6	S1	166.581	66.615	186.565	116.590	512.8	470.8	426.7	0.364	0.396	0.437
	S9	221.742	28.993	230.440	95.516	824.84	742.84	656.74	0.279	0.310	0.351
	S2	25.237	88.348	51.741	95.919	977.52	885.12	788.1	0.098	0.108	0.122
	S10	80.829	56.094	97.657	80.343	1422.04	1241.64	1052.22	0.069	0.079	0.093
	S3	10.868	142.790	53.705	146.050	1052.44	951.64	845.8	0.139	0.153	0.173
	S11	647.657	34.568	658.028	228.866	1417.392	1269.792	1114.812	0.464	0.518	0.590
5	S1	219.776	84.760	245.203	150.692	641	588.5	544.4	0.383	0.417	0.450
	S9	297.240	37.848	308.594	127.020	1031.05	928.55	842.45	0.299	0.332	0.366
	S2	34.866	117.607	70.147	128.066	1221.9	1106.4	1009.38	0.105	0.116	0.127
	S10	102.219	80.335	126.320	111.001	1777.55	1552.05	1362.63	0.071	0.081	0.093
	S3	15.526	182.307	70.218	186.965	1315.55	1189.55	1083.71	0.142	0.157	0.173
	S11	865.101	35.430	875.729	294.960	1771.74	1587.24	1432.26	0.494	0.552	0.611
4	S1	271.215	101.729	301.734	183.093	769.2	706.2	667.35	0.392	0.427	0.452
	S9	374.706	46.391	388.624	158.803	1237.26	1114.26	1038.41	0.314	0.349	0.374
	S2	42.229	146.584	86.205	159.253	1466.28	1327.68	1242.21	0.109	0.120	0.128
	S10	121.870	108.733	154.490	145.294	2133.06	1862.46	1695.59	0.072	0.083	0.091
	S3	19.981	220.286	86.066	226.280	1578.66	1427.46	1334.22	0.143	0.159	0.170
	S11	1087.750	33.758	1097.877	360.083	2126.088	1904.688	1768.158	0.516	0.576	0.621
3	S1	321.817	116.583	356.791	213.128	897.4	823.9	795.55	0.398	0.433	0.448
	S9	451.017	54.769	467.447	190.074	1443.47	1299.97	1244.62	0.324	0.360	0.376
	S2	46.843	174.612	99.226	188.665	1710.66	1548.96	1486.59	0.110	0.122	0.127
	S10	133.856	136.136	174.697	176.293	2488.57	2172.87	2051.1	0.071	0.081	0.086
	S3	27.306	256.709	104.318	264.900	1841.77	1665.37	1597.33	0.144	0.159	0.166
	S11	1313.781	28.202	1322.242	422.336	2480.436	2222.136	2122.506	0.533	0.595	0.623
2	S1	367.110	129.473	405.952	239.606	1025.6	941.6	923.75	0.396	0.431	0.439
	S9	519.987	65.591	539.665	221.587	1649.68	1485.68	1450.83	0.327	0.363	0.372
	S2	49.923	198.978	109.616	213.954	1955.04	1770.24	1730.97	0.109	0.121	0.124
	S10	145.239	159.555	193.106	203.127	2844.08	2483.28	2406.61	0.071	0.082	0.084
	S3	35.727	287.705	122.038	298.423	2104.88	1903.28	1860.44	0.142	0.157	0.160
	S11	1506.569	21.057	1512.886	473.028	2834.784	2539.584	2476.854	0.534	0.596	0.611
1	S1	398.975	138.954	440.662	258.647	1153.8	1059.3	1051.95	0.382	0.416	0.419
	S9	570.985	76.031	593.794	247.326	1855.89	1671.39	1657.04	0.320	0.355	0.358
	S2	50.808	217.072	115.929	232.314	2199.42	1991.52	1975.35	0.106	0.117	0.118
	S10	155.155	179.051	208.870	225.597	3199.59	2793.69	2762.12	0.071	0.081	0.082
	S3	42.403	309.200	135.162	321.920	2367.99	2141.19	2123.55	0.136	0.150	0.152
	S11	1628.707	12.577	1632.480	501.189	3189.132	2857.032	2831.202	0.512	0.571	0.577

Çizelge B.163: 12 Kat, Ankara, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	23.676	15.7114	28.38942	22.8142	128.2	117.7	117.7	0.221	0.241	0.241
	S9	31.1066	2.9325	31.98635	12.26448	206.21	185.71	185.71	0.155	0.172	0.172
	S2	1.5623	18.6092	7.14506	19.07789	244.38	221.28	221.28	0.078	0.086	0.086
	S10	3.3231	5.4021	4.94373	6.39903	355.51	310.41	310.41	0.018	0.021	0.021
	S3	3.8515	40.5424	16.01422	41.69785	263.11	237.91	237.91	0.158	0.175	0.175
	S11	93.5621	14.1973	97.82129	42.26593	354.348	317.448	317.448	0.276	0.308	0.308
11	S1	69.9456	42.5185	82.70115	63.50218	256.4	235.4	235.4	0.323	0.351	0.351
	S9	90.746	14.2427	95.01881	41.4665	412.42	371.42	371.42	0.230	0.256	0.256
	S2	0.4411	53.6367	16.53211	53.76903	488.76	442.56	442.56	0.110	0.121	0.121
	S10	13.9742	22.9548	20.86064	27.14706	711.02	620.82	620.82	0.038	0.044	0.044
	S3	3.8773	97.7309	33.19657	98.89409	526.22	475.82	475.82	0.188	0.208	0.208
	S11	244.86	20.6345	251.05035	94.0925	708.696	634.896	634.896	0.354	0.395	0.395
10	S1	119.5935	70.0983	140.62299	105.97635	384.6	353.1	353.1	0.366	0.398	0.398
	S9	154.6123	26.4565	162.54925	72.84019	618.63	557.13	557.13	0.263	0.292	0.292
	S2	3.5221	89.3172	30.31726	90.37383	733.14	663.84	663.84	0.123	0.136	0.136
	S10	29.395	41.6129	41.87887	50.4314	1066.53	931.23	931.23	0.047	0.054	0.054
	S3	4.5173	155.597	51.1964	156.95219	789.33	713.73	713.73	0.199	0.220	0.220
	S11	413.5542	29.7216	422.47068	153.78786	1063.044	952.344	952.344	0.397	0.444	0.444
9	S1	173.8238	97.7656	203.15348	149.91274	512.8	470.8	457.675	0.396	0.432	0.444
	S9	228.6808	38.9525	240.36655	107.55674	824.84	742.84	717.215	0.291	0.324	0.335
	S2	7.4779	129.1358	46.21864	131.37917	977.52	885.12	856.245	0.134	0.148	0.153
	S10	42.5187	67.9074	62.89092	80.66301	1422.04	1241.64	1185.265	0.057	0.065	0.068
	S3	6.5996	216.0604	71.41772	218.04028	1052.44	951.64	920.14	0.207	0.229	0.237
	S11	611.6074	32.4531	621.34333	215.93532	1417.392	1269.792	1223.667	0.438	0.489	0.508
8	S1	232.4581	125.4589	270.09577	195.19633	641	588.5	564.875	0.421	0.459	0.478
	S9	311.4779	51.5646	326.94728	145.00797	1031.05	928.55	882.425	0.317	0.352	0.371
	S2	13.1264	172.5828	64.90124	176.52072	1221.9	1106.4	1054.425	0.144	0.160	0.167
	S10	55.1966	99.9107	85.16981	116.46968	1777.55	1552.05	1450.575	0.066	0.075	0.080
	S3	10.4549	278.2466	93.92888	281.38307	1315.55	1189.55	1132.85	0.214	0.237	0.248
	S11	835.9839	30.6882	845.19036	281.48337	1771.74	1587.24	1504.215	0.477	0.532	0.562
7	S1	292.4718	152.7907	338.30901	240.53224	769.2	706.2	672.075	0.440	0.479	0.503
	S9	402.0075	64.5006	421.35768	185.10285	1237.26	1114.26	1047.635	0.341	0.378	0.402
	S2	16.7504	217.8246	82.09778	222.84972	1466.28	1327.68	1252.605	0.152	0.168	0.178
	S10	67.3152	140.6938	109.52334	160.88836	2133.06	1862.46	1715.885	0.075	0.086	0.094
	S3	14.5546	341.5789	117.02827	345.94528	1578.66	1427.46	1345.56	0.219	0.242	0.257
	S11	1082.2087	25.6881	1089.91513	350.35071	2126.088	1904.688	1784.763	0.513	0.572	0.611
6	S1	358.1251	179.1541	411.87133	286.59163	897.4	823.9	784.525	0.459	0.500	0.525
	S9	500.1943	78.2934	523.68232	228.35169	1443.47	1299.97	1223.095	0.363	0.403	0.428
	S2	18.336	265.7931	98.07393	271.2939	1710.66	1548.96	1462.335	0.159	0.175	0.186
	S10	72.2056	182.9481	127.09003	204.60978	2488.57	2172.87	2003.745	0.082	0.094	0.102
	S3	23.5877	408.3291	146.08643	415.40541	1841.77	1665.37	1570.87	0.226	0.249	0.264
	S11	1363.7017	15.3735	1368.31375	424.48401	2480.436	2222.136	2083.761	0.552	0.616	0.657
5	S1	427.2817	205.6194	488.96752	333.80391	1025.6	941.6	902.225	0.477	0.519	0.542
	S9	606.5318	99.2221	636.29843	281.18164	1649.68	1485.68	1408.805	0.386	0.428	0.452
	S2	19.0292	313.9157	113.20391	319.62446	1955.04	1770.24	1683.615	0.163	0.181	0.190
	S10	80.9703	226.2761	148.85313	250.56719	2844.08	2483.28	2314.155	0.088	0.101	0.108
	S3	36.3218	474.0715	178.54325	484.96804	2104.88	1903.28	1808.78	0.230	0.255	0.268
	S11	1651.8939	5.2683	1653.47439	500.83647	2834.784	2539.584	2401.209	0.583	0.651	0.689
4	S1	495.9935	230.5808	565.16774	379.37885	1153.8	1059.3	1025.175	0.490	0.534	0.551
	S9	712.6016	123.9083	749.77409	337.68878	1855.89	1671.39	1604.765	0.404	0.449	0.467
	S2	18.3782	359.439	126.2099	364.95246	2199.42	1991.52	1916.445	0.166	0.183	0.190
	S10	93.8698	271.4038	175.29094	299.56474	3199.59	2793.69	2647.115	0.094	0.107	0.113
	S3	51.4895	535.334	212.0897	550.78085	2367.99	2141.19	2059.29	0.233	0.257	0.267

	S11	1925.8314	3.5475	1926.89565	581.29692	3189.132	2857.032	2737.107	0.604	0.674	0.704
3	S1	566.3775	254.7506	642.80268	424.66385	1282	1177	1153.375	0.501	0.546	0.557
	S9	813.1547	147.394	857.3729	391.34041	2062.1	1857.1	1810.975	0.416	0.462	0.473
	S2	23.3723	399.3396	143.17418	406.35129	2443.8	2212.8	2160.825	0.166	0.184	0.188
	S10	109.1021	312.093	202.73	344.82363	3555.1	3104.1	3002.625	0.097	0.111	0.115
	S3	66.8612	589.4362	243.69206	609.49456	2631.1	2379.1	2322.4	0.232	0.256	0.262
	S11	2179.4593	13.0883	2183.38579	666.92609	3543.48	3174.48	3091.455	0.616	0.688	0.706
2	S1	630.6935	276.3594	713.60132	465.56745	1410.2	1294.7	1281.575	0.506	0.551	0.557
	S9	901.181	169.0689	951.90167	439.4232	2268.31	2042.81	2017.185	0.420	0.466	0.472
	S2	31.6727	432.3859	161.38847	441.88771	2688.18	2434.08	2405.205	0.164	0.182	0.184
	S10	125.1782	347.4002	229.39826	384.95366	3910.61	3414.51	3358.135	0.098	0.113	0.115
	S3	80.4352	632.3888	270.15184	656.51936	2894.21	2617.01	2585.51	0.227	0.251	0.254
	S11	2387.969	23.845	2395.1225	740.2357	3897.828	3491.928	3445.803	0.614	0.686	0.695
1	S1	676.1198	290.7211	763.33613	493.55704	1538.4	1412.4	1409.775	0.496	0.540	0.541
	S9	961.623	183.9624	1016.81172	472.4493	2474.52	2228.52	2223.395	0.411	0.456	0.457
	S2	36.7874	456.0869	173.61347	467.12312	2932.56	2655.36	2649.585	0.159	0.176	0.176
	S10	137.2141	371.7722	248.74576	412.93643	4266.12	3724.92	3713.645	0.097	0.111	0.111
	S3	91.8995	661.1451	290.24303	688.71495	3157.32	2854.92	2848.62	0.218	0.241	0.242
	S11	2521.0016	34.0854	2531.22722	790.38588	4252.176	3809.376	3800.151	0.595	0.664	0.666

Çizelge B.164: 6 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.106	2.924	8.984	5.356	128.2	122.95	112.45	0.070	0.073	0.080
	S9	11.351	0.665	11.551	4.070	206.21	195.96	175.46	0.056	0.059	0.066
	S2	2.192	3.695	3.300	4.353	244.38	232.83	209.73	0.018	0.019	0.021
	S10	7.478	2.329	8.176	4.572	355.51	332.96	287.86	0.023	0.025	0.028
	S3	1.188	6.594	3.166	6.951	263.11	250.51	225.31	0.026	0.028	0.031
	S11	40.737	4.420	42.063	16.641	354.348	335.898	298.998	0.119	0.125	0.141
5	S1	23.202	8.019	25.608	14.979	256.4	245.9	230.15	0.100	0.104	0.111
	S9	31.310	2.995	32.208	12.388	412.42	391.92	361.17	0.078	0.082	0.089
	S2	6.213	10.663	9.411	12.527	488.76	465.66	431.01	0.026	0.027	0.029
	S10	17.860	7.365	20.069	12.723	711.02	665.92	598.27	0.028	0.030	0.034
	S3	2.033	16.531	6.992	17.141	526.22	501.02	463.22	0.033	0.034	0.037
	S11	100.049	7.234	102.219	37.249	708.696	671.796	616.446	0.144	0.152	0.166
4	S1	38.930	13.270	42.911	24.949	384.6	368.85	353.1	0.112	0.116	0.122
	S9	52.066	5.522	53.722	21.141	618.63	587.88	557.13	0.087	0.091	0.096
	S2	10.243	17.862	15.601	20.935	733.14	698.49	663.84	0.029	0.030	0.032
	S10	29.229	12.648	33.023	21.416	1066.53	998.88	931.23	0.031	0.033	0.035
	S3	2.842	26.489	10.788	27.341	789.33	751.53	713.73	0.035	0.036	0.038
	S11	162.241	10.024	165.248	58.696	1063.044	1007.694	952.344	0.155	0.164	0.174
3	S1	54.612	18.228	60.080	34.611	512.8	491.8	481.3	0.117	0.122	0.125
	S9	73.702	7.942	76.084	30.052	824.84	783.84	763.34	0.092	0.097	0.100
	S2	14.061	25.456	21.698	29.675	977.52	931.32	908.22	0.030	0.032	0.033
	S10	39.030	19.089	44.756	30.798	1422.04	1331.84	1286.74	0.031	0.034	0.035
	S3	3.788	36.203	14.649	37.340	1052.44	1002.04	976.84	0.035	0.037	0.038
	S11	226.228	10.962	229.517	78.830	1417.392	1343.592	1306.692	0.162	0.171	0.176
2	S1	68.635	22.554	75.401	43.144	641	614.75	609.5	0.118	0.123	0.124
	S9	93.647	10.122	96.683	38.216	1031.05	979.8	969.55	0.094	0.099	0.100
	S2	17.382	32.769	27.213	37.984	1221.9	1164.15	1152.6	0.031	0.033	0.033
	S10	46.568	25.793	54.306	39.764	1777.55	1664.8	1642.25	0.031	0.033	0.033
	S3	4.736	44.811	18.179	46.232	1315.55	1252.55	1239.95	0.035	0.037	0.037
	S11	283.788	9.898	286.757	95.034	1771.74	1679.49	1661.04	0.162	0.171	0.173
1	S1	78.490	25.864	86.249	49.411	769.2	737.7	737.7	0.112	0.117	0.117
	S9	108.370	11.799	111.910	44.310	1237.26	1175.76	1175.76	0.090	0.095	0.095
	S2	19.272	38.668	30.872	44.450	1466.28	1396.98	1396.98	0.030	0.032	0.032
	S10	51.492	31.753	61.018	47.200	2133.06	1997.76	1997.76	0.029	0.031	0.031
	S3	5.350	51.289	20.737	52.894	1578.66	1503.06	1503.06	0.034	0.035	0.035
	S11	323.399	7.191	325.556	104.210	2126.088	2015.388	2015.388	0.153	0.162	0.162

Çizelge B.165: 9 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	9.824	4.475	11.167	7.422	128.2	117.7	104.575	0.087	0.095	0.107
	S9	13.284	1.052	13.600	5.037	206.21	185.71	160.085	0.066	0.073	0.085
	S2	0.977	5.297	2.566	5.590	244.38	221.28	192.405	0.023	0.025	0.029
	S10	5.328	2.373	6.040	3.972	355.51	310.41	254.035	0.017	0.019	0.024
	S3	1.636	11.111	4.969	11.602	263.11	237.91	206.41	0.044	0.049	0.056
	S11	44.492	5.434	46.123	18.782	354.348	317.448	271.323	0.130	0.145	0.170
8	S1	28.560	12.174	32.212	20.742	256.4	235.4	207.05	0.126	0.137	0.156
	S9	37.682	4.573	39.054	15.878	412.42	371.42	316.07	0.095	0.105	0.124
	S2	3.808	15.326	8.406	16.469	488.76	442.56	380.19	0.034	0.037	0.043
	S10	13.920	8.434	16.450	12.610	711.02	620.82	499.05	0.023	0.026	0.033
	S3	2.305	27.124	10.442	27.816	526.22	475.82	407.78	0.053	0.058	0.068
	S11	112.702	8.699	115.312	42.510	708.696	634.896	535.266	0.163	0.182	0.215
7	S1	48.554	20.112	54.588	34.679	384.6	353.1	314.25	0.142	0.155	0.174
	S9	63.700	8.363	66.209	27.473	618.63	557.13	481.28	0.107	0.119	0.138
	S2	7.022	25.633	14.712	27.739	733.14	663.84	578.37	0.038	0.042	0.048
	S10	24.387	14.879	28.851	22.195	1066.53	931.23	764.36	0.027	0.031	0.038
	S3	3.153	43.300	16.143	44.246	789.33	713.73	620.49	0.056	0.062	0.071
	S11	187.359	12.591	191.136	68.799	1063.044	952.344	815.814	0.180	0.201	0.234
6	S1	69.981	27.970	78.372	48.964	512.8	470.8	426.7	0.153	0.166	0.184
	S9	93.141	12.172	96.792	40.114	824.84	742.84	656.74	0.117	0.130	0.147
	S2	10.561	37.088	21.687	40.257	977.52	885.12	788.1	0.041	0.045	0.051
	S10	33.927	23.550	40.992	33.728	1422.04	1241.64	1052.22	0.029	0.033	0.039
	S3	4.535	59.956	22.522	61.316	1052.44	951.64	845.8	0.058	0.064	0.072
	S11	272.007	14.515	276.362	96.118	1417.392	1269.792	1114.812	0.195	0.218	0.248
5	S1	92.328	35.588	103.005	63.286	641	588.5	544.4	0.161	0.175	0.189
	S9	124.854	15.889	129.621	53.345	1031.05	928.55	842.45	0.126	0.140	0.154
	S2	14.589	49.369	29.400	53.746	1221.9	1106.4	1009.38	0.044	0.049	0.053
	S10	42.899	33.725	53.017	46.595	1777.55	1552.05	1362.63	0.030	0.034	0.039
	S3	6.480	76.548	29.445	78.492	1315.55	1189.55	1083.71	0.060	0.066	0.072
	S11	363.333	14.877	367.796	123.877	1771.74	1587.24	1432.26	0.208	0.232	0.257
4	S1	113.939	42.712	126.752	76.894	769.2	706.2	667.35	0.165	0.179	0.190
	S9	157.394	19.476	163.237	66.694	1237.26	1114.26	1038.41	0.132	0.146	0.157
	S2	17.665	61.532	36.124	66.831	1466.28	1327.68	1242.21	0.046	0.050	0.054
	S10	51.137	45.645	64.831	60.986	2133.06	1862.46	1695.59	0.030	0.035	0.038
	S3	8.340	92.494	36.088	94.996	1578.66	1427.46	1334.22	0.060	0.067	0.071
	S11	456.846	14.175	461.098	151.229	2126.088	1904.688	1768.158	0.217	0.242	0.261
3	S1	135.196	48.948	149.881	89.507	897.4	823.9	795.55	0.167	0.182	0.188
	S9	189.449	22.992	196.346	79.827	1443.47	1299.97	1244.62	0.136	0.151	0.158
	S2	19.585	73.295	41.574	79.171	1710.66	1548.96	1486.59	0.046	0.051	0.053
	S10	56.155	57.147	73.299	73.993	2488.57	2172.87	2051.1	0.030	0.034	0.036
	S3	11.404	107.785	43.740	111.206	1841.77	1665.37	1597.33	0.060	0.067	0.070
	S11	551.781	11.842	555.333	177.376	2480.436	2222.136	2122.506	0.224	0.250	0.262
2	S1	154.224	54.360	170.532	100.627	1025.6	941.6	923.75	0.166	0.181	0.185
	S9	218.424	27.534	226.684	93.061	1649.68	1485.68	1450.83	0.137	0.153	0.156
	S2	20.863	83.521	45.919	89.780	1955.04	1770.24	1730.97	0.046	0.051	0.052
	S10	60.921	66.975	81.013	85.251	2844.08	2483.28	2406.61	0.030	0.034	0.035
	S3	14.929	120.797	51.168	125.276	2104.88	1903.28	1860.44	0.060	0.066	0.067
	S11	632.753	8.842	635.406	198.668	2834.784	2539.584	2476.854	0.224	0.250	0.257
1	S1	167.612	58.340	185.114	108.624	1153.8	1059.3	1051.95	0.160	0.175	0.176
	S9	239.851	31.915	249.425	103.870	1855.89	1671.39	1657.04	0.134	0.149	0.151
	S2	21.221	91.114	48.555	97.480	2199.42	1991.52	1975.35	0.044	0.049	0.049
	S10	65.071	75.157	87.618	94.678	3199.59	2793.69	2762.12	0.030	0.034	0.034
	S3	17.722	129.820	56.668	135.137	2367.99	2141.19	2123.55	0.057	0.063	0.064
	S11	684.054	5.281	685.639	210.497	3189.132	2857.032	2831.202	0.215	0.240	0.242

Çizelge B.166: 12 Kat, İzmir, ZA Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	12.080	8.016	14.485	11.640	128.2	117.7	117.7	0.113	0.123	0.123
	S9	15.872	1.496	16.320	6.258	206.21	185.71	185.71	0.079	0.088	0.088
	S2	0.797	9.495	3.646	9.734	244.38	221.28	221.28	0.040	0.044	0.044
	S10	1.696	2.756	2.522	3.265	355.51	310.41	310.41	0.009	0.011	0.011
	S3	1.965	20.686	8.171	21.275	263.11	237.91	237.91	0.081	0.089	0.089
	S11	47.738	7.244	49.911	21.565	354.348	317.448	317.448	0.141	0.157	0.157
11	S1	35.688	21.694	42.196	32.401	256.4	235.4	235.4	0.165	0.179	0.179
	S9	46.301	7.267	48.481	21.157	412.42	371.42	371.42	0.118	0.131	0.131
	S2	0.225	27.367	8.435	27.434	488.76	442.56	442.56	0.056	0.062	0.062
	S10	7.130	11.712	10.644	13.851	711.02	620.82	620.82	0.019	0.022	0.022
	S3	1.978	49.865	16.938	50.458	526.22	475.82	475.82	0.096	0.106	0.106
	S11	124.934	10.528	128.093	48.009	708.696	634.896	634.896	0.181	0.202	0.202
10	S1	61.020	35.766	71.750	54.072	384.6	353.1	353.1	0.187	0.203	0.203
	S9	78.888	13.499	82.937	37.165	618.63	557.13	557.13	0.134	0.149	0.149
	S2	1.797	45.572	15.469	46.111	733.14	663.84	663.84	0.063	0.069	0.069
	S10	14.998	21.232	21.368	25.732	1066.53	931.23	931.23	0.024	0.028	0.028
	S3	2.305	79.390	26.122	80.081	789.33	713.73	713.73	0.101	0.112	0.112
	S11	211.007	15.165	215.556	78.467	1063.044	952.344	952.344	0.203	0.226	0.226
9	S1	88.690	49.883	103.655	76.490	512.8	470.8	457.675	0.202	0.220	0.226
	S9	116.679	19.875	122.642	54.878	824.84	742.84	717.215	0.149	0.165	0.171
	S2	3.816	65.889	23.582	67.033	977.52	885.12	856.245	0.069	0.076	0.078
	S10	21.694	34.648	32.089	41.156	1422.04	1241.64	1185.265	0.029	0.033	0.035
	S3	3.367	110.240	36.439	111.250	1052.44	951.64	920.14	0.106	0.117	0.121
	S11	312.059	16.559	317.027	110.176	1417.392	1269.792	1223.667	0.224	0.250	0.259
8	S1	118.607	64.013	137.810	99.595	641	588.5	564.875	0.215	0.234	0.244
	S9	158.925	26.310	166.818	73.987	1031.05	928.55	882.425	0.162	0.180	0.189
	S2	6.698	88.057	33.114	90.066	1221.9	1106.4	1054.425	0.074	0.081	0.085
	S10	28.163	50.977	43.456	59.426	1777.55	1552.05	1450.575	0.033	0.038	0.041
	S3	5.334	141.969	47.925	143.570	1315.55	1189.55	1132.85	0.109	0.121	0.127
	S11	426.542	15.658	431.240	143.621	1771.74	1587.24	1504.215	0.243	0.272	0.287
7	S1	149.227	77.958	172.615	122.726	769.2	706.2	672.075	0.224	0.244	0.257
	S9	205.115	32.910	214.988	94.445	1237.26	1114.26	1047.635	0.174	0.193	0.205
	S2	8.547	111.140	41.889	113.704	1466.28	1327.68	1252.605	0.078	0.086	0.091
	S10	34.346	71.786	55.882	82.090	2133.06	1862.46	1715.885	0.038	0.044	0.048
	S3	7.426	174.283	59.711	176.511	1578.66	1427.46	1345.56	0.112	0.124	0.131
	S11	552.173	13.107	556.105	178.759	2126.088	1904.688	1784.763	0.262	0.292	0.312
6	S1	182.725	91.409	210.148	146.227	897.4	823.9	784.525	0.234	0.255	0.268
	S9	255.213	39.948	267.197	116.511	1443.47	1299.97	1223.095	0.185	0.206	0.218
	S2	9.356	135.615	50.040	138.422	1710.66	1548.96	1462.335	0.081	0.089	0.095
	S10	36.841	93.345	64.845	104.398	2488.57	2172.87	2003.745	0.042	0.048	0.052
	S3	12.035	208.341	74.537	211.951	1841.77	1665.37	1570.87	0.115	0.127	0.135
	S11	695.799	7.844	698.152	216.584	2480.436	2222.136	2083.761	0.281	0.314	0.335
5	S1	218.011	104.913	249.485	170.316	1025.6	941.6	902.225	0.243	0.265	0.277
	S9	309.470	50.626	324.657	143.467	1649.68	1485.68	1408.805	0.197	0.219	0.230
	S2	9.709	160.169	57.760	163.081	1955.04	1770.24	1683.615	0.083	0.092	0.097
	S10	41.313	115.452	75.949	127.846	2844.08	2483.28	2314.155	0.045	0.051	0.055
	S3	18.532	241.885	91.098	247.444	2104.88	1903.28	1808.78	0.118	0.130	0.137
	S11	842.842	2.688	843.649	255.541	2834.784	2539.584	2401.209	0.298	0.332	0.351
4	S1	253.070	117.649	288.364	193.570	1153.8	1059.3	1025.175	0.250	0.272	0.281
	S9	363.589	63.222	382.556	172.298	1855.89	1671.39	1604.765	0.206	0.229	0.238
	S2	9.377	183.396	64.396	186.209	2199.42	1991.52	1916.445	0.085	0.094	0.097
	S10	47.895	138.478	89.438	152.846	3199.59	2793.69	2647.115	0.048	0.055	0.058
	S3	26.271	273.142	108.214	281.024	2367.99	2141.19	2059.29	0.119	0.131	0.136

	S11	982.613	1.810	983.156	296.594	3189.132	2857.032	2737.107	0.308	0.344	0.359
3	S1	288.982	129.981	327.976	216.675	1282	1177	1153.375	0.256	0.279	0.284
	S9	414.894	75.205	437.456	199.673	2062.1	1857.1	1810.975	0.212	0.236	0.242
	S2	11.925	203.754	73.051	207.332	2443.8	2212.8	2160.825	0.085	0.094	0.096
	S10	55.667	159.239	103.438	175.939	3555.1	3104.1	3002.625	0.049	0.057	0.059
	S3	34.114	300.747	124.338	310.981	2631.1	2379.1	2322.4	0.118	0.131	0.134
	S11	1112.021	6.678	1114.024	340.284	3543.48	3174.48	3091.455	0.314	0.351	0.360
2	S1	321.797	141.006	364.099	237.546	1410.2	1294.7	1281.575	0.258	0.281	0.284
	S9	459.808	86.264	485.687	224.206	2268.31	2042.81	2017.185	0.214	0.238	0.241
	S2	16.160	220.615	82.345	225.463	2688.18	2434.08	2405.205	0.084	0.093	0.094
	S10	63.869	177.253	117.045	196.414	3910.61	3414.51	3358.135	0.050	0.058	0.058
	S3	41.040	322.662	137.839	334.974	2894.21	2617.01	2585.51	0.116	0.128	0.130
	S11	1218.409	12.166	1222.058	377.689	3897.828	3491.928	3445.803	0.314	0.350	0.355
1	S1	344.975	148.334	389.475	251.827	1538.4	1412.4	1409.775	0.253	0.276	0.276
	S9	490.647	93.863	518.806	241.057	2474.52	2228.52	2223.395	0.210	0.233	0.233
	S2	18.770	232.708	88.582	238.339	2932.56	2655.36	2649.585	0.081	0.090	0.090
	S10	70.011	189.689	126.917	210.692	4266.12	3724.92	3713.645	0.049	0.057	0.057
	S3	46.890	337.335	148.090	351.402	3157.32	2854.92	2848.62	0.111	0.123	0.123
	S11	1286.285	17.391	1291.503	403.277	4252.176	3809.376	3800.151	0.304	0.339	0.340

Çizelge B.167: 6 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	8.106	2.924	8.984	5.356	128.2	122.95	112.45	0.070	0.073	0.080
	S9	11.351	0.665	11.551	4.070	206.21	195.96	175.46	0.056	0.059	0.066
	S2	2.192	3.695	3.300	4.353	244.38	232.83	209.73	0.018	0.019	0.021
	S10	7.478	2.329	8.176	4.572	355.51	332.96	287.86	0.023	0.025	0.028
	S3	1.188	6.594	3.166	6.951	263.11	250.51	225.31	0.026	0.028	0.031
	S11	40.737	4.420	42.063	16.641	354.348	335.898	298.998	0.119	0.125	0.141
5	S1	23.202	8.019	25.608	14.979	256.4	245.9	230.15	0.100	0.104	0.111
	S9	31.310	2.995	32.208	12.388	412.42	391.92	361.17	0.078	0.082	0.089
	S2	6.213	10.663	9.411	12.527	488.76	465.66	431.01	0.026	0.027	0.029
	S10	17.860	7.365	20.069	12.723	711.02	665.92	598.27	0.028	0.030	0.034
	S3	2.033	16.531	6.992	17.141	526.22	501.02	463.22	0.033	0.034	0.037
	S11	100.049	7.234	102.219	37.249	708.696	671.796	616.446	0.144	0.152	0.166
4	S1	38.930	13.270	42.911	24.949	384.6	368.85	353.1	0.112	0.116	0.122
	S9	52.066	5.522	53.722	21.141	618.63	587.88	557.13	0.087	0.091	0.096
	S2	10.243	17.862	15.601	20.935	733.14	698.49	663.84	0.029	0.030	0.032
	S10	29.229	12.648	33.023	21.416	1066.53	998.88	931.23	0.031	0.033	0.035
	S3	2.842	26.489	10.788	27.341	789.33	751.53	713.73	0.035	0.036	0.038
	S11	162.241	10.024	165.248	58.696	1063.044	1007.694	952.344	0.155	0.164	0.174
3	S1	54.612	18.228	60.080	34.611	512.8	491.8	481.3	0.117	0.122	0.125
	S9	73.702	7.942	76.084	30.052	824.84	783.84	763.34	0.092	0.097	0.100
	S2	14.061	25.456	21.698	29.675	977.52	931.32	908.22	0.030	0.032	0.033
	S10	39.030	19.089	44.756	30.798	1422.04	1331.84	1286.74	0.031	0.034	0.035
	S3	3.788	36.203	14.649	37.340	1052.44	1002.04	976.84	0.035	0.037	0.038
	S11	226.228	10.962	229.517	78.830	1417.392	1343.592	1306.692	0.162	0.171	0.176
2	S1	68.635	22.554	75.401	43.144	641	614.75	609.5	0.118	0.123	0.124
	S9	93.647	10.122	96.683	38.216	1031.05	979.8	969.55	0.094	0.099	0.100
	S2	17.382	32.769	27.213	37.984	1221.9	1164.15	1152.6	0.031	0.033	0.033
	S10	46.568	25.793	54.306	39.764	1777.55	1664.8	1642.25	0.031	0.033	0.033
	S3	4.736	44.811	18.179	46.232	1315.55	1252.55	1239.95	0.035	0.037	0.037
	S11	283.788	9.898	286.757	95.034	1771.74	1679.49	1661.04	0.162	0.171	0.173
1	S1	78.490	25.864	86.249	49.411	769.2	737.7	737.7	0.112	0.117	0.117
	S9	108.370	11.799	111.910	44.310	1237.26	1175.76	1175.76	0.090	0.095	0.095
	S2	19.272	38.668	30.872	44.450	1466.28	1396.98	1396.98	0.030	0.032	0.032
	S10	51.492	31.753	61.018	47.200	2133.06	1997.76	1997.76	0.029	0.031	0.031
	S3	5.350	51.289	20.737	52.894	1578.66	1503.06	1503.06	0.034	0.035	0.035
	S11	323.399	7.191	325.556	104.210	2126.088	2015.388	2015.388	0.153	0.162	0.162

Çizelge B.168: 9 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	10.814	4.926	12.292	8.171	128.2	117.7	104.575	0.096	0.104	0.118
	S9	14.623	1.158	14.971	5.545	206.21	185.71	160.085	0.073	0.081	0.094
	S2	1.075	5.830	2.824	6.153	244.38	221.28	192.405	0.025	0.028	0.032
	S10	5.865	2.613	6.649	4.372	355.51	310.41	254.035	0.019	0.021	0.026
	S3	1.801	12.231	5.470	12.772	263.11	237.91	206.41	0.049	0.054	0.062
	S11	48.977	5.982	50.772	20.675	354.348	317.448	271.323	0.143	0.160	0.187
8	S1	31.439	13.402	35.459	22.833	256.4	235.4	207.05	0.138	0.151	0.171
	S9	41.481	5.034	42.991	17.478	412.42	371.42	316.07	0.104	0.116	0.136
	S2	4.192	16.871	9.254	18.129	488.76	442.56	380.19	0.037	0.041	0.048
	S10	15.323	9.284	18.108	13.881	711.02	620.82	499.05	0.025	0.029	0.036
	S3	2.537	29.858	11.495	30.619	526.22	475.82	407.78	0.058	0.064	0.075
	S11	124.063	9.576	126.935	46.794	708.696	634.896	535.266	0.179	0.200	0.237
7	S1	53.448	22.140	60.090	38.174	384.6	353.1	314.25	0.156	0.170	0.191
	S9	70.121	9.206	72.883	30.242	618.63	557.13	481.28	0.118	0.131	0.151
	S2	7.730	28.216	16.195	30.535	733.14	663.84	578.37	0.042	0.046	0.053
	S10	26.845	16.378	31.759	24.432	1066.53	931.23	764.36	0.030	0.034	0.042
	S3	3.470	47.665	17.770	48.706	789.33	713.73	620.49	0.062	0.068	0.078
	S11	206.244	13.861	210.402	75.734	1063.044	952.344	815.814	0.198	0.221	0.258
6	S1	77.035	30.789	86.271	53.900	512.8	470.8	426.7	0.168	0.183	0.202
	S9	102.529	13.399	106.549	44.158	824.84	742.84	656.74	0.129	0.143	0.162
	S2	11.626	40.827	23.874	44.314	977.52	885.12	788.1	0.045	0.050	0.056
	S10	37.347	25.923	45.124	37.127	1422.04	1241.64	1052.22	0.032	0.036	0.043
	S3	4.992	66.000	24.792	67.497	1052.44	951.64	845.8	0.064	0.071	0.080
	S11	299.425	15.978	304.219	105.806	1417.392	1269.792	1114.812	0.215	0.240	0.273
5	S1	101.635	39.175	113.387	69.665	641	588.5	544.4	0.177	0.193	0.208
	S9	137.439	17.491	142.686	58.723	1031.05	928.55	842.45	0.138	0.154	0.169
	S2	16.060	54.345	32.363	59.163	1221.9	1106.4	1009.38	0.048	0.053	0.059
	S10	47.223	37.125	58.361	51.291	1777.55	1552.05	1362.63	0.033	0.038	0.043
	S3	7.134	84.264	32.413	86.404	1315.55	1189.55	1083.71	0.066	0.073	0.080
	S11	399.956	16.376	404.869	136.363	1771.74	1587.24	1432.26	0.229	0.255	0.283
4	S1	125.423	47.017	139.528	84.644	769.2	706.2	667.35	0.181	0.198	0.209
	S9	173.259	21.439	179.690	73.416	1237.26	1114.26	1038.41	0.145	0.161	0.173
	S2	19.446	67.734	39.766	73.567	1466.28	1327.68	1242.21	0.050	0.055	0.059
	S10	56.292	50.246	71.365	67.133	2133.06	1862.46	1695.59	0.033	0.038	0.042
	S3	9.181	101.817	39.726	104.571	1578.66	1427.46	1334.22	0.066	0.073	0.078
	S11	502.895	15.604	507.576	166.472	2126.088	1904.688	1768.158	0.239	0.266	0.287
3	S1	148.824	53.882	164.988	98.529	897.4	823.9	795.55	0.184	0.200	0.207
	S9	208.545	25.310	216.138	87.873	1443.47	1299.97	1244.62	0.150	0.166	0.174
	S2	21.560	80.683	45.764	87.151	1710.66	1548.96	1486.59	0.051	0.056	0.059
	S10	61.816	62.907	80.688	81.452	2488.57	2172.87	2051.1	0.033	0.037	0.040
	S3	12.554	118.649	48.148	122.415	1841.77	1665.37	1597.33	0.066	0.074	0.077
	S11	607.399	13.035	611.309	195.255	2480.436	2222.136	2122.506	0.246	0.275	0.288
2	S1	169.770	59.839	187.722	110.770	1025.6	941.6	923.75	0.183	0.199	0.203
	S9	240.441	30.309	249.533	102.441	1649.68	1485.68	1450.83	0.151	0.168	0.172
	S2	22.966	91.940	50.547	98.829	1955.04	1770.24	1730.97	0.051	0.056	0.057
	S10	67.061	73.726	89.179	93.845	2844.08	2483.28	2406.61	0.033	0.038	0.039
	S3	16.433	132.973	56.325	137.903	2104.88	1903.28	1860.44	0.066	0.072	0.074
	S11	696.533	9.733	699.453	218.693	2834.784	2539.584	2476.854	0.247	0.275	0.282
1	S1	184.507	64.221	203.773	119.572	1153.8	1059.3	1051.95	0.177	0.192	0.194
	S9	264.027	35.131	274.567	114.340	1855.89	1671.39	1657.04	0.148	0.164	0.166
	S2	23.360	100.298	53.449	107.306	2199.42	1991.52	1975.35	0.049	0.054	0.054
	S10	71.630	82.732	96.449	104.221	3199.59	2793.69	2762.12	0.033	0.037	0.038
	S3	19.509	142.906	62.380	148.758	2367.99	2141.19	2123.55	0.063	0.069	0.070
	S11	753.005	5.814	754.749	231.715	3189.132	2857.032	2831.202	0.237	0.264	0.267

Çizelge B.169: 12 Kat, İzmir, ZB Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	13.590	9.019	16.296	13.096	128.2	117.7	117.7	0.127	0.138	0.138
	S9	17.855	1.683	18.360	7.040	206.21	185.71	185.71	0.089	0.099	0.099
	S2	0.897	10.682	4.101	10.951	244.38	221.28	221.28	0.045	0.049	0.049
	S10	1.908	3.101	2.838	3.673	355.51	310.41	310.41	0.010	0.012	0.012
	S3	2.211	23.272	9.192	23.935	263.11	237.91	237.91	0.091	0.101	0.101
	S11	53.705	8.149	56.150	24.261	354.348	317.448	317.448	0.158	0.177	0.177
11	S1	40.149	24.406	47.471	36.451	256.4	235.4	235.4	0.185	0.202	0.202
	S9	52.089	8.175	54.541	23.802	412.42	371.42	371.42	0.132	0.147	0.147
	S2	0.253	30.788	9.490	30.864	488.76	442.56	442.56	0.063	0.070	0.070
	S10	8.021	13.176	11.974	15.583	711.02	620.82	620.82	0.022	0.025	0.025
	S3	2.226	56.098	19.055	56.766	526.22	475.82	475.82	0.108	0.119	0.119
	S11	140.551	11.844	144.104	54.010	708.696	634.896	634.896	0.203	0.227	0.227
10	S1	68.648	40.237	80.719	60.831	384.6	353.1	353.1	0.210	0.229	0.229
	S9	88.749	15.186	93.304	41.811	618.63	557.13	557.13	0.151	0.167	0.167
	S2	2.022	51.269	17.402	51.875	733.14	663.84	663.84	0.071	0.078	0.078
	S10	16.873	23.886	24.039	28.948	1066.53	931.23	931.23	0.027	0.031	0.031
	S3	2.593	89.314	29.387	90.092	789.33	713.73	713.73	0.114	0.126	0.126
	S11	237.383	17.060	242.501	88.275	1063.044	952.344	952.344	0.228	0.255	0.255
9	S1	99.776	56.118	116.611	86.051	512.8	470.8	457.675	0.227	0.248	0.255
	S9	131.264	22.359	137.972	61.738	824.84	742.84	717.215	0.167	0.186	0.192
	S2	4.292	74.125	26.530	75.413	977.52	885.12	856.245	0.077	0.085	0.088
	S10	24.406	38.979	36.100	46.301	1422.04	1241.64	1185.265	0.033	0.037	0.039
	S3	3.788	124.020	40.994	125.156	1052.44	951.64	920.14	0.119	0.132	0.136
	S11	351.067	18.628	356.655	123.948	1417.392	1269.792	1223.667	0.252	0.281	0.291
8	S1	133.433	72.014	155.037	112.044	641	588.5	564.875	0.242	0.263	0.274
	S9	178.790	29.598	187.670	83.235	1031.05	928.55	882.425	0.182	0.202	0.213
	S2	7.535	99.064	37.254	101.324	1221.9	1106.4	1054.425	0.083	0.092	0.096
	S10	31.683	57.349	48.888	66.854	1777.55	1552.05	1450.575	0.038	0.043	0.046
	S3	6.001	159.715	53.916	161.516	1315.55	1189.55	1132.85	0.123	0.136	0.143
	S11	479.860	17.615	485.145	161.573	1771.74	1587.24	1504.215	0.274	0.306	0.323
7	S1	167.881	87.703	194.192	138.067	769.2	706.2	672.075	0.252	0.275	0.289
	S9	230.755	37.024	241.862	106.250	1237.26	1114.26	1047.635	0.195	0.217	0.231
	S2	9.615	125.033	47.125	127.917	1466.28	1327.68	1252.605	0.087	0.096	0.102
	S10	38.639	80.759	62.867	92.351	2133.06	1862.46	1715.885	0.043	0.050	0.054
	S3	8.354	196.069	67.175	198.575	1578.66	1427.46	1345.56	0.126	0.139	0.148
	S11	621.195	14.745	625.618	201.104	2126.088	1904.688	1784.763	0.294	0.328	0.351
6	S1	205.566	102.836	236.417	164.505	897.4	823.9	784.525	0.263	0.287	0.301
	S9	287.115	44.941	300.597	131.075	1443.47	1299.97	1223.095	0.208	0.231	0.246
	S2	10.525	152.567	56.295	155.725	1710.66	1548.96	1462.335	0.091	0.101	0.106
	S10	41.447	105.013	72.951	117.447	2488.57	2172.87	2003.745	0.047	0.054	0.059
	S3	13.540	234.384	83.855	238.445	1841.77	1665.37	1570.87	0.129	0.143	0.152
	S11	782.774	8.825	785.421	243.657	2480.436	2222.136	2083.761	0.317	0.353	0.377
5	S1	245.262	118.027	280.670	191.606	1025.6	941.6	902.225	0.274	0.298	0.311
	S9	348.153	56.954	365.239	161.400	1649.68	1485.68	1408.805	0.221	0.246	0.259
	S2	10.923	180.190	64.980	183.466	1955.04	1770.24	1683.615	0.094	0.104	0.109
	S10	46.477	129.884	85.443	143.827	2844.08	2483.28	2314.155	0.051	0.058	0.062
	S3	20.849	272.120	102.485	278.375	2104.88	1903.28	1808.78	0.132	0.146	0.154
	S11	948.198	3.024	949.105	287.483	2834.784	2539.584	2401.209	0.335	0.374	0.395
4	S1	284.704	132.355	324.410	217.766	1153.8	1059.3	1025.175	0.281	0.306	0.316
	S9	409.038	71.124	430.375	193.836	1855.89	1671.39	1604.765	0.232	0.257	0.268
	S2	10.549	206.320	72.445	209.485	2199.42	1991.52	1916.445	0.095	0.105	0.109
	S10	53.882	155.788	100.618	171.952	3199.59	2793.69	2647.115	0.054	0.062	0.065
	S3	29.555	307.285	121.741	316.152	2367.99	2141.19	2059.29	0.134	0.148	0.154

	S11	1105.440	2.036	1106.050	333.668	3189.132	2857.032	2737.107	0.347	0.387	0.404
3	S1	325.104	146.229	368.973	243.760	1282	1177	1153.375	0.288	0.313	0.320
	S9	466.756	84.605	492.138	224.632	2062.1	1857.1	1810.975	0.239	0.265	0.272
	S2	13.416	229.224	82.183	233.248	2443.8	2212.8	2160.825	0.095	0.105	0.108
	S10	62.625	179.143	116.368	197.931	3555.1	3104.1	3002.625	0.056	0.064	0.066
	S3	38.379	338.340	139.881	349.854	2631.1	2379.1	2322.4	0.133	0.147	0.151
	S11	1251.024	7.513	1253.277	382.820	3543.48	3174.48	3091.455	0.354	0.395	0.405
2	S1	362.022	158.632	409.612	267.239	1410.2	1294.7	1281.575	0.290	0.316	0.320
	S9	517.284	97.047	546.398	252.232	2268.31	2042.81	2017.185	0.241	0.267	0.271
	S2	18.180	248.192	92.638	253.646	2688.18	2434.08	2405.205	0.094	0.104	0.105
	S10	71.853	199.410	131.676	220.966	3910.61	3414.51	3358.135	0.057	0.065	0.066
	S3	46.170	362.995	155.069	376.846	2894.21	2617.01	2585.51	0.130	0.144	0.146
	S11	1370.710	13.687	1374.816	424.900	3897.828	3491.928	3445.803	0.353	0.394	0.399
1	S1	388.097	166.876	438.160	283.305	1538.4	1412.4	1409.775	0.285	0.310	0.311
	S9	551.978	105.596	583.656	271.189	2474.52	2228.52	2223.395	0.236	0.262	0.263
	S2	21.116	261.797	99.655	268.132	2932.56	2655.36	2649.585	0.091	0.101	0.101
	S10	78.762	213.400	142.782	237.028	4266.12	3724.92	3713.645	0.056	0.064	0.064
	S3	52.751	379.502	166.601	395.327	3157.32	2854.92	2848.62	0.125	0.138	0.139
	S11	1447.071	19.565	1452.941	453.687	4252.176	3809.376	3800.151	0.342	0.381	0.382

Çizelge B.170: 6 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	15.200	5.482	16.844	10.042	128.2	122.95	112.45	0.131	0.137	0.150
	S9	21.283	1.247	21.657	7.632	206.21	195.96	175.46	0.105	0.111	0.123
	S2	4.110	6.928	6.188	8.161	244.38	232.83	209.73	0.033	0.035	0.039
	S10	14.021	4.366	15.330	8.572	355.51	332.96	287.86	0.043	0.046	0.053
	S3	2.227	12.364	5.936	13.032	263.11	250.51	225.31	0.050	0.052	0.058
	S11	76.382	8.287	78.868	31.202	354.348	335.898	298.998	0.223	0.235	0.264
5	S1	43.504	15.035	48.014	28.086	256.4	245.9	230.15	0.187	0.195	0.209
	S9	58.706	5.615	60.390	23.227	412.42	391.92	361.17	0.146	0.154	0.167
	S2	11.649	19.993	17.646	23.487	488.76	465.66	431.01	0.048	0.050	0.054
	S10	33.487	13.809	37.630	23.855	711.02	665.92	598.27	0.053	0.057	0.063
	S3	3.811	30.996	13.110	32.139	526.22	501.02	463.22	0.061	0.064	0.069
	S11	187.592	13.564	191.661	69.842	708.696	671.796	616.446	0.270	0.285	0.311
4	S1	72.994	24.881	80.458	46.779	384.6	368.85	353.1	0.209	0.218	0.228
	S9	97.623	10.353	100.729	39.640	618.63	587.88	557.13	0.163	0.171	0.181
	S2	19.205	33.491	29.252	39.253	733.14	698.49	663.84	0.054	0.056	0.059
	S10	54.804	23.714	61.918	40.155	1066.53	998.88	931.23	0.058	0.062	0.066
	S3	5.328	49.666	20.228	51.265	789.33	751.53	713.73	0.065	0.068	0.072
	S11	304.201	18.795	309.840	110.055	1063.044	1007.694	952.344	0.291	0.307	0.325
3	S1	102.397	34.177	112.650	64.896	512.8	491.8	481.3	0.220	0.229	0.234
	S9	138.191	14.890	142.658	56.348	824.84	783.84	763.34	0.173	0.182	0.187
	S2	26.365	47.731	40.684	55.640	977.52	931.32	908.22	0.057	0.060	0.061
	S10	73.181	35.792	83.918	57.746	1422.04	1331.84	1286.74	0.059	0.063	0.065
	S3	7.102	67.881	27.467	70.012	1052.44	1002.04	976.84	0.067	0.070	0.072
	S11	424.178	20.553	430.344	147.807	1417.392	1343.592	1306.692	0.304	0.320	0.329
2	S1	128.690	42.289	141.377	80.896	641	614.75	609.5	0.221	0.230	0.232
	S9	175.588	18.979	181.282	71.655	1031.05	979.8	969.55	0.176	0.185	0.187
	S2	32.592	61.442	51.024	71.220	1221.9	1164.15	1152.6	0.058	0.061	0.062
	S10	87.315	48.362	101.824	74.557	1777.55	1664.8	1642.25	0.057	0.061	0.062
	S3	8.880	84.020	34.086	86.684	1315.55	1252.55	1239.95	0.066	0.069	0.070
	S11	532.102	18.559	537.669	178.189	1771.74	1679.49	1661.04	0.303	0.320	0.324
1	S1	147.168	48.496	161.717	92.646	769.2	737.7	737.7	0.210	0.219	0.219
	S9	203.194	22.123	209.831	83.081	1237.26	1175.76	1175.76	0.170	0.178	0.178
	S2	36.134	72.503	57.885	83.343	1466.28	1396.98	1396.98	0.057	0.060	0.060
	S10	96.548	59.536	114.409	88.500	2133.06	1997.76	1997.76	0.054	0.057	0.057
	S3	10.032	96.166	38.882	99.175	1578.66	1503.06	1503.06	0.063	0.066	0.066
	S11	606.374	13.482	610.418	195.394	2126.088	2015.388	2015.388	0.287	0.303	0.303

Çizelge B.171: 9 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	18.420	8.391	20.937	13.917	128.2	117.7	104.575	0.163	0.178	0.200
	S9	24.908	1.973	25.500	9.445	206.21	185.71	160.085	0.124	0.137	0.159
	S2	1.831	9.931	4.811	10.480	244.38	221.28	192.405	0.043	0.047	0.054
	S10	9.991	4.450	11.326	7.447	355.51	310.41	254.035	0.032	0.036	0.045
	S3	3.067	20.834	9.317	21.754	263.11	237.91	206.41	0.083	0.091	0.105
	S11	83.423	10.189	86.480	35.216	354.348	317.448	271.323	0.244	0.272	0.319
8	S1	53.550	22.827	60.398	38.892	256.4	235.4	207.05	0.236	0.257	0.292
	S9	70.654	8.575	73.227	29.771	412.42	371.42	316.07	0.178	0.197	0.232
	S2	7.141	28.737	15.762	30.879	488.76	442.56	380.19	0.063	0.070	0.081
	S10	26.099	15.814	30.843	23.643	711.02	620.82	499.05	0.043	0.050	0.062
	S3	4.322	50.858	19.579	52.154	526.22	475.82	407.78	0.099	0.110	0.128
	S11	211.317	16.310	216.210	79.705	708.696	634.896	535.266	0.305	0.341	0.404
7	S1	91.039	37.711	102.352	65.022	384.6	353.1	314.25	0.266	0.290	0.326
	S9	119.438	15.680	124.142	51.512	618.63	557.13	481.28	0.201	0.223	0.258
	S2	13.167	48.061	27.585	52.011	733.14	663.84	578.37	0.071	0.078	0.090
	S10	45.726	27.897	54.095	41.615	1066.53	931.23	764.36	0.051	0.058	0.071
	S3	5.911	81.188	30.267	82.961	789.33	713.73	620.49	0.105	0.116	0.134
	S11	351.298	23.609	358.381	128.998	1063.044	952.344	815.814	0.337	0.376	0.439
6	S1	131.214	52.444	146.947	91.808	512.8	470.8	426.7	0.287	0.312	0.344
	S9	174.639	22.823	181.486	75.214	824.84	742.84	656.74	0.220	0.244	0.276
	S2	19.802	69.540	40.664	75.481	977.52	885.12	788.1	0.077	0.085	0.096
	S10	63.613	44.156	76.860	63.240	1422.04	1241.64	1052.22	0.054	0.062	0.073
	S3	8.503	112.418	42.228	114.968	1052.44	951.64	845.8	0.109	0.121	0.136
	S11	510.014	27.216	518.179	180.220	1417.392	1269.792	1114.812	0.366	0.408	0.465
5	S1	173.116	66.727	193.134	118.662	641	588.5	544.4	0.301	0.328	0.355
	S9	234.101	29.793	243.039	100.023	1031.05	928.55	842.45	0.236	0.262	0.288
	S2	27.354	92.567	55.124	100.773	1221.9	1106.4	1009.38	0.082	0.091	0.100
	S10	80.436	63.235	99.406	87.365	1777.55	1552.05	1362.63	0.056	0.064	0.073
	S3	12.151	143.528	55.209	147.173	1315.55	1189.55	1083.71	0.112	0.124	0.136
	S11	681.249	27.894	689.618	232.269	1771.74	1587.24	1432.26	0.389	0.434	0.481
4	S1	213.635	80.085	237.660	144.175	769.2	706.2	667.35	0.309	0.337	0.356
	S9	295.114	36.517	306.069	125.051	1237.26	1114.26	1038.41	0.247	0.275	0.295
	S2	33.122	115.372	67.733	125.308	1466.28	1327.68	1242.21	0.085	0.094	0.101
	S10	95.882	85.584	121.557	114.349	2133.06	1862.46	1695.59	0.057	0.065	0.072
	S3	15.638	173.425	67.665	178.117	1578.66	1427.46	1334.22	0.113	0.125	0.133
	S11	856.586	26.578	864.559	283.554	2126.088	1904.688	1768.158	0.407	0.454	0.489
3	S1	253.493	91.778	281.026	167.826	897.4	823.9	795.55	0.313	0.341	0.353
	S9	355.216	43.110	368.149	149.675	1443.47	1299.97	1244.62	0.255	0.283	0.296
	S2	36.723	137.429	77.951	148.445	1710.66	1548.96	1486.59	0.087	0.096	0.100
	S10	105.291	107.150	137.436	138.737	2488.57	2172.87	2051.1	0.056	0.064	0.068
	S3	21.383	202.096	82.012	208.511	1841.77	1665.37	1597.33	0.113	0.125	0.131
	S11	1034.589	22.203	1041.249	332.579	2480.436	2222.136	2122.506	0.420	0.469	0.491
2	S1	289.171	101.925	319.748	188.676	1025.6	941.6	923.75	0.312	0.340	0.346
	S9	409.545	51.626	425.033	174.489	1649.68	1485.68	1450.83	0.258	0.286	0.293
	S2	39.118	156.602	86.098	168.337	1955.04	1770.24	1730.97	0.086	0.095	0.097
	S10	114.226	125.579	151.900	159.846	2844.08	2483.28	2406.61	0.056	0.064	0.066
	S3	27.991	226.495	95.940	234.892	2104.88	1903.28	1860.44	0.112	0.123	0.126
	S11	1186.412	16.578	1191.386	372.502	2834.784	2539.584	2476.854	0.420	0.469	0.481
1	S1	314.272	109.388	347.088	203.669	1153.8	1059.3	1051.95	0.301	0.328	0.330
	S9	449.721	59.840	467.672	194.756	1855.89	1671.39	1657.04	0.252	0.280	0.282
	S2	39.789	170.839	91.041	182.776	2199.42	1991.52	1975.35	0.083	0.092	0.093
	S10	122.007	140.919	164.283	177.521	3199.59	2793.69	2762.12	0.055	0.064	0.064
	S3	33.229	243.413	106.253	253.381	2367.99	2141.19	2123.55	0.107	0.118	0.119
	S11	1282.602	9.902	1285.572	394.683	3189.132	2857.032	2831.202	0.403	0.450	0.454

Çizelge B.172: 12 Kat, İzmir, ZC Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	18.656	12.380	22.370	17.977	128.2	117.7	117.7	0.174	0.190	0.190
	S9	24.511	2.311	25.204	9.664	206.21	185.71	185.71	0.122	0.136	0.136
	S2	1.231	14.663	5.630	15.033	244.38	221.28	221.28	0.062	0.068	0.068
	S10	2.619	4.257	3.896	5.042	355.51	310.41	310.41	0.014	0.016	0.016
	S3	3.035	31.946	12.619	32.856	263.11	237.91	237.91	0.125	0.138	0.138
	S11	73.724	11.187	77.080	33.304	354.348	317.448	317.448	0.218	0.243	0.243
11	S1	55.115	33.503	65.166	50.037	256.4	235.4	235.4	0.254	0.277	0.277
	S9	71.505	11.223	74.871	32.674	412.42	371.42	371.42	0.182	0.202	0.202
	S2	0.348	42.264	13.027	42.368	488.76	442.56	442.56	0.087	0.096	0.096
	S10	11.011	18.088	16.437	21.391	711.02	620.82	620.82	0.030	0.034	0.034
	S3	3.055	77.009	26.158	77.925	526.22	475.82	475.82	0.148	0.164	0.164
	S11	192.941	16.259	197.819	74.142	708.696	634.896	634.896	0.279	0.312	0.312
10	S1	94.235	55.235	110.806	83.506	384.6	353.1	353.1	0.288	0.314	0.314
	S9	121.829	20.847	128.083	57.396	618.63	557.13	557.13	0.207	0.230	0.230
	S2	2.775	70.379	23.889	71.211	733.14	663.84	663.84	0.097	0.107	0.107
	S10	23.162	32.790	32.999	39.738	1066.53	931.23	931.23	0.037	0.043	0.043
	S3	3.560	122.605	40.341	123.673	789.33	713.73	713.73	0.157	0.173	0.173
	S11	325.866	23.420	332.892	121.179	1063.044	952.344	952.344	0.313	0.350	0.350
9	S1	136.967	77.036	160.078	118.126	512.8	470.8	457.675	0.312	0.340	0.350
	S9	180.192	30.693	189.400	84.751	824.84	742.84	717.215	0.230	0.255	0.264
	S2	5.892	101.754	36.419	103.522	977.52	885.12	856.245	0.106	0.117	0.121
	S10	33.503	53.509	49.556	63.560	1422.04	1241.64	1185.265	0.045	0.051	0.054
	S3	5.200	170.248	56.275	171.808	1052.44	951.64	920.14	0.163	0.181	0.187
	S11	481.925	25.572	489.596	170.149	1417.392	1269.792	1223.667	0.345	0.386	0.400
8	S1	183.169	98.857	212.826	153.808	641	588.5	564.875	0.332	0.362	0.377
	S9	245.434	40.631	257.623	114.261	1031.05	928.55	882.425	0.250	0.277	0.292
	S2	10.343	135.989	51.140	139.092	1221.9	1106.4	1054.425	0.114	0.126	0.132
	S10	43.493	78.726	67.111	91.774	1777.55	1552.05	1450.575	0.052	0.059	0.063
	S3	8.238	219.248	74.013	221.720	1315.55	1189.55	1132.85	0.169	0.186	0.196
	S11	658.726	24.181	665.980	221.799	1771.74	1587.24	1504.215	0.376	0.420	0.443
7	S1	230.457	120.394	266.575	189.531	769.2	706.2	672.075	0.347	0.377	0.397
	S9	316.768	50.824	332.015	145.854	1237.26	1114.26	1047.635	0.268	0.298	0.317
	S2	13.199	171.638	64.690	175.598	1466.28	1327.68	1252.605	0.120	0.132	0.140
	S10	53.042	110.862	86.301	126.774	2133.06	1862.46	1715.885	0.059	0.068	0.074
	S3	11.469	269.152	92.214	272.593	1578.66	1427.46	1345.56	0.173	0.191	0.203
	S11	852.742	20.241	858.814	276.064	2126.088	1904.688	1784.763	0.404	0.451	0.481
6	S1	282.190	141.167	324.540	225.824	897.4	823.9	784.525	0.362	0.394	0.414
	S9	394.135	61.692	412.643	179.933	1443.47	1299.97	1223.095	0.286	0.317	0.337
	S2	14.448	209.436	77.279	213.770	1710.66	1548.96	1462.335	0.125	0.138	0.146
	S10	56.895	144.157	100.142	161.225	2488.57	2172.87	2003.745	0.065	0.074	0.080
	S3	18.586	321.749	115.111	327.325	1841.77	1665.37	1570.87	0.178	0.197	0.208
	S11	1074.548	12.114	1078.182	334.478	2480.436	2222.136	2083.761	0.435	0.485	0.517
5	S1	336.683	162.021	385.289	263.026	1025.6	941.6	902.225	0.376	0.409	0.427
	S9	477.925	78.184	501.380	221.561	1649.68	1485.68	1408.805	0.304	0.337	0.356
	S2	14.994	247.354	89.201	251.853	1955.04	1770.24	1683.615	0.129	0.142	0.150
	S10	63.802	178.298	117.291	197.438	2844.08	2483.28	2314.155	0.069	0.080	0.085
	S3	28.620	373.551	140.686	382.137	2104.88	1903.28	1808.78	0.182	0.201	0.211
	S11	1301.633	4.151	1302.879	394.641	2834.784	2539.584	2401.209	0.460	0.513	0.543
4	S1	390.825	181.689	445.332	298.937	1153.8	1059.3	1025.175	0.386	0.420	0.434
	S9	561.505	97.635	590.795	266.087	1855.89	1671.39	1604.765	0.318	0.353	0.368
	S2	14.481	283.225	99.449	287.570	2199.42	1991.52	1916.445	0.131	0.144	0.150
	S10	73.966	213.857	138.123	236.046	3199.59	2793.69	2647.115	0.074	0.084	0.089
	S3	40.572	421.824	167.119	433.996	2367.99	2141.19	2059.29	0.183	0.203	0.211

	S11	1517.486	2.795	1518.325	458.041	3189.132	2857.032	2737.107	0.476	0.531	0.555
3	S1	446.285	200.734	506.506	334.620	1282	1177	1153.375	0.395	0.430	0.439
	S9	640.737	116.141	675.579	308.362	2062.1	1857.1	1810.975	0.328	0.364	0.373
	S2	18.417	314.665	112.816	320.190	2443.8	2212.8	2160.825	0.131	0.145	0.148
	S10	85.969	245.918	159.744	271.709	3555.1	3104.1	3002.625	0.076	0.088	0.090
	S3	52.684	464.455	192.021	480.260	2631.1	2379.1	2322.4	0.183	0.202	0.207
	S11	1717.336	10.313	1720.430	525.514	3543.48	3174.48	3091.455	0.486	0.542	0.557
2	S1	496.964	217.761	562.292	366.850	1410.2	1294.7	1281.575	0.399	0.434	0.439
	S9	710.099	133.220	750.065	346.250	2268.31	2042.81	2017.185	0.331	0.367	0.372
	S2	24.957	340.705	127.168	348.192	2688.18	2434.08	2405.205	0.130	0.143	0.145
	S10	98.636	273.739	180.758	303.330	3910.61	3414.51	3358.135	0.078	0.089	0.090
	S3	63.380	498.300	212.870	517.314	2894.21	2617.01	2585.51	0.179	0.198	0.200
	S11	1881.634	18.789	1887.271	583.279	3897.828	3491.928	3445.803	0.484	0.540	0.548
1	S1	532.758	229.078	601.482	388.905	1538.4	1412.4	1409.775	0.391	0.426	0.427
	S9	757.725	144.956	801.211	372.273	2474.52	2228.52	2223.395	0.324	0.360	0.360
	S2	28.987	359.380	136.801	368.076	2932.56	2655.36	2649.585	0.126	0.139	0.139
	S10	108.120	292.943	196.003	325.379	4266.12	3724.92	3713.645	0.076	0.087	0.088
	S3	72.414	520.959	228.701	542.683	3157.32	2854.92	2848.62	0.172	0.190	0.191
	S11	1986.459	26.858	1994.517	622.796	4252.176	3809.376	3800.151	0.469	0.524	0.525

Çizelge B.173: 6 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	21.117	7.616	23.402	13.951	128.2	122.95	112.45	0.183	0.190	0.208
	S9	29.570	1.732	30.089	10.603	206.21	195.96	175.46	0.146	0.154	0.171
	S2	5.709	9.626	8.597	11.339	244.38	232.83	209.73	0.046	0.049	0.054
	S10	19.479	6.066	21.299	11.910	355.51	332.96	287.86	0.060	0.064	0.074
	S3	3.094	17.178	8.247	18.106	263.11	250.51	225.31	0.069	0.072	0.080
	S11	106.119	11.514	109.574	43.350	354.348	335.898	298.998	0.309	0.326	0.366
5	S1	60.441	20.888	66.708	39.021	256.4	245.9	230.15	0.260	0.271	0.290
	S9	81.562	7.802	83.903	32.270	412.42	391.92	361.17	0.203	0.214	0.232
	S2	16.184	27.777	24.517	32.632	488.76	465.66	431.01	0.067	0.070	0.076
	S10	46.525	19.186	52.281	33.143	711.02	665.92	598.27	0.074	0.079	0.087
	S3	5.295	43.064	18.214	44.652	526.22	501.02	463.22	0.085	0.089	0.096
	S11	260.628	18.845	266.281	97.033	708.696	671.796	616.446	0.376	0.396	0.432
4	S1	101.412	34.567	111.783	64.991	384.6	368.85	353.1	0.291	0.303	0.317
	S9	135.631	14.384	139.946	55.073	618.63	587.88	557.13	0.226	0.238	0.251
	S2	26.682	46.531	40.641	54.535	733.14	698.49	663.84	0.074	0.078	0.082
	S10	76.141	32.947	86.025	55.789	1066.53	998.88	931.23	0.081	0.086	0.092
	S3	7.402	69.003	28.103	71.224	789.33	751.53	713.73	0.090	0.095	0.100
	S11	422.637	26.112	430.471	152.903	1063.044	1007.694	952.344	0.405	0.427	0.452
3	S1	142.264	47.483	156.509	90.162	512.8	491.8	481.3	0.305	0.318	0.325
	S9	191.993	20.688	198.200	78.286	824.84	783.84	763.34	0.240	0.253	0.260
	S2	36.630	66.314	56.524	77.303	977.52	931.32	908.22	0.079	0.083	0.085
	S10	101.672	49.727	116.590	80.229	1422.04	1331.84	1286.74	0.082	0.088	0.091
	S3	9.868	94.310	38.160	97.270	1052.44	1002.04	976.84	0.092	0.097	0.100
	S11	589.324	28.555	597.891	205.353	1417.392	1343.592	1306.692	0.422	0.445	0.458
2	S1	178.793	58.753	196.419	112.391	641	614.75	609.5	0.306	0.320	0.322
	S9	243.950	26.368	251.861	99.553	1031.05	979.8	969.55	0.244	0.257	0.260
	S2	45.281	85.364	70.890	98.948	1221.9	1164.15	1152.6	0.081	0.085	0.086
	S10	121.310	67.191	141.467	103.584	1777.55	1664.8	1642.25	0.080	0.085	0.086
	S3	12.338	116.732	47.357	120.433	1315.55	1252.55	1239.95	0.092	0.096	0.097
	S11	739.266	25.785	747.002	247.565	1771.74	1679.49	1661.04	0.422	0.445	0.450
1	S1	204.466	67.377	224.679	128.716	769.2	737.7	737.7	0.292	0.305	0.305
	S9	282.304	30.736	291.525	115.428	1237.26	1175.76	1175.76	0.236	0.248	0.248
	S2	50.203	100.731	80.422	115.792	1466.28	1396.98	1396.98	0.079	0.083	0.083
	S10	134.138	82.715	158.952	122.957	2133.06	1997.76	1997.76	0.075	0.080	0.080
	S3	13.938	133.606	54.020	137.788	1578.66	1503.06	1503.06	0.087	0.092	0.092
	S11	842.455	18.732	848.074	271.468	2126.088	2015.388	2015.388	0.399	0.421	0.421

Çizelge B.174: 9 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	25.591	11.658	29.089	19.335	128.2	117.7	104.575	0.227	0.247	0.278
	S9	34.605	2.741	35.428	13.123	206.21	185.71	160.085	0.172	0.191	0.221
	S2	2.544	13.797	6.684	14.561	244.38	221.28	192.405	0.060	0.066	0.076
	S10	13.880	6.183	15.735	10.347	355.51	310.41	254.035	0.044	0.051	0.062
	S3	4.261	28.945	12.945	30.224	263.11	237.91	206.41	0.115	0.127	0.146
	S11	115.903	14.156	120.149	48.927	354.348	317.448	271.323	0.339	0.378	0.443
8	S1	74.399	31.714	83.913	54.034	256.4	235.4	207.05	0.327	0.356	0.405
	S9	98.163	11.913	101.736	41.362	412.42	371.42	316.07	0.247	0.274	0.322
	S2	9.921	39.925	21.898	42.901	488.76	442.56	380.19	0.088	0.097	0.113
	S10	36.261	21.970	42.852	32.849	711.02	620.82	499.05	0.060	0.069	0.086
	S3	6.005	70.658	27.202	72.459	526.22	475.82	407.78	0.138	0.152	0.178
	S11	293.590	22.660	300.388	110.737	708.696	634.896	535.266	0.424	0.473	0.561
7	S1	126.484	52.393	142.202	90.338	384.6	353.1	314.25	0.370	0.403	0.453
	S9	165.939	21.785	172.475	71.567	618.63	557.13	481.28	0.279	0.310	0.358
	S2	18.293	66.773	38.325	72.261	733.14	663.84	578.37	0.099	0.109	0.125
	S10	63.528	38.758	75.156	57.817	1066.53	931.23	764.36	0.070	0.081	0.098
	S3	8.212	112.797	42.051	115.260	789.33	713.73	620.49	0.146	0.161	0.186
	S11	488.070	32.801	497.910	179.222	1063.044	952.344	815.814	0.468	0.523	0.610
6	S1	182.300	72.862	204.158	127.552	512.8	470.8	426.7	0.398	0.434	0.478
	S9	242.632	31.708	252.144	104.498	824.84	742.84	656.74	0.306	0.339	0.384
	S2	27.512	96.615	56.496	104.868	977.52	885.12	788.1	0.107	0.118	0.133
	S10	88.380	61.347	106.784	87.861	1422.04	1241.64	1052.22	0.075	0.086	0.101
	S3	11.813	156.186	58.669	159.729	1052.44	951.64	845.8	0.152	0.168	0.189
	S11	708.579	37.812	719.923	250.386	1417.392	1269.792	1114.812	0.508	0.567	0.646
5	S1	240.515	92.706	268.327	164.860	641	588.5	544.4	0.419	0.456	0.493
	S9	325.244	41.392	337.662	138.965	1031.05	928.55	842.45	0.327	0.364	0.401
	S2	38.004	128.606	76.586	140.007	1221.9	1106.4	1009.38	0.115	0.127	0.139
	S10	111.752	87.854	138.108	121.379	1777.55	1552.05	1362.63	0.078	0.089	0.101
	S3	16.882	199.408	76.704	204.472	1315.55	1189.55	1083.71	0.155	0.172	0.189
	S11	946.483	38.754	958.109	322.699	1771.74	1587.24	1432.26	0.541	0.604	0.669
4	S1	296.810	111.265	330.189	200.308	769.2	706.2	667.35	0.429	0.468	0.495
	S9	410.011	50.734	425.231	173.737	1237.26	1114.26	1038.41	0.344	0.382	0.410
	S2	46.017	160.289	94.104	174.095	1466.28	1327.68	1242.21	0.119	0.131	0.140
	S10	133.212	118.905	168.884	158.868	2133.06	1862.46	1695.59	0.079	0.091	0.100
	S3	21.726	240.945	94.010	247.463	1578.66	1427.46	1334.22	0.157	0.173	0.185
	S11	1190.084	36.926	1201.161	393.951	2126.088	1904.688	1768.158	0.565	0.631	0.679
3	S1	352.186	127.510	390.439	233.166	897.4	823.9	795.55	0.435	0.474	0.491
	S9	493.514	59.894	511.482	207.948	1443.47	1299.97	1244.62	0.354	0.393	0.411
	S2	51.020	190.934	108.300	206.240	1710.66	1548.96	1486.59	0.121	0.133	0.139
	S10	146.285	148.867	190.945	192.753	2488.57	2172.87	2051.1	0.077	0.089	0.094
	S3	29.708	280.779	113.942	289.692	1841.77	1665.37	1597.33	0.157	0.174	0.181
	S11	1437.388	30.847	1446.642	462.064	2480.436	2222.136	2122.506	0.583	0.651	0.682
2	S1	401.755	141.608	444.237	262.134	1025.6	941.6	923.75	0.433	0.472	0.481
	S9	568.995	71.725	590.512	242.423	1649.68	1485.68	1450.83	0.358	0.397	0.407
	S2	54.347	217.572	119.619	233.876	1955.04	1770.24	1730.97	0.120	0.132	0.135
	S10	158.698	174.471	211.039	222.080	2844.08	2483.28	2406.61	0.078	0.089	0.092
	S3	38.889	314.677	133.292	326.344	2104.88	1903.28	1860.44	0.155	0.171	0.175
	S11	1648.322	23.033	1655.232	517.529	2834.784	2539.584	2476.854	0.584	0.652	0.668
1	S1	436.629	151.976	482.221	282.964	1153.8	1059.3	1051.95	0.418	0.455	0.458
	S9	624.812	83.137	649.753	270.581	1855.89	1671.39	1657.04	0.350	0.389	0.392
	S2	55.280	237.352	126.486	253.936	2199.42	1991.52	1975.35	0.115	0.128	0.129
	S10	169.509	195.783	228.244	246.636	3199.59	2793.69	2762.12	0.077	0.088	0.089
	S3	46.166	338.181	147.621	352.031	2367.99	2141.19	2123.55	0.149	0.164	0.166
	S11	1781.961	13.758	1786.089	548.346	3189.132	2857.032	2831.202	0.560	0.625	0.631

Çizelge B.175: 12 Kat, İzmir, ZD Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	25.919	17.200	31.079	24.976	128.2	117.7	117.7	0.242	0.264	0.264
	S9	34.054	3.210	35.017	13.427	206.21	185.71	185.71	0.170	0.189	0.189
	S2	1.710	20.372	7.822	20.885	244.38	221.28	221.28	0.085	0.094	0.094
	S10	3.638	5.914	5.412	7.005	355.51	310.41	310.41	0.020	0.023	0.023
	S3	4.216	44.384	17.531	45.649	263.11	237.91	237.91	0.173	0.192	0.192
	S11	102.427	15.542	107.089	46.270	354.348	317.448	317.448	0.302	0.337	0.337
11	S1	76.573	46.547	90.537	69.519	256.4	235.4	235.4	0.353	0.385	0.385
	S9	99.344	15.592	104.021	45.395	412.42	371.42	371.42	0.252	0.280	0.280
	S2	0.483	58.719	18.098	58.863	488.76	442.56	442.56	0.120	0.133	0.133
	S10	15.298	25.130	22.837	29.719	711.02	620.82	620.82	0.042	0.048	0.048
	S3	4.245	106.990	36.342	108.264	526.22	475.82	475.82	0.206	0.228	0.228
	S11	268.059	22.590	274.836	103.007	708.696	634.896	634.896	0.388	0.433	0.433
10	S1	130.924	76.740	153.946	116.017	384.6	353.1	353.1	0.400	0.436	0.436
	S9	169.261	28.963	177.950	79.742	618.63	557.13	557.13	0.288	0.319	0.319
	S2	3.856	97.780	33.190	98.936	733.14	663.84	663.84	0.135	0.149	0.149
	S10	32.180	45.556	45.847	55.210	1066.53	931.23	931.23	0.052	0.059	0.059
	S3	4.945	170.339	56.047	171.823	789.33	713.73	713.73	0.218	0.241	0.241
	S11	452.736	32.538	462.498	168.359	1063.044	952.344	952.344	0.435	0.486	0.486
9	S1	190.293	107.028	222.401	164.116	512.8	470.8	457.675	0.434	0.472	0.486
	S9	250.347	42.643	263.140	117.747	824.84	742.84	717.215	0.319	0.354	0.367
	S2	8.186	141.371	50.598	143.827	977.52	885.12	856.245	0.147	0.162	0.168
	S10	46.547	74.341	68.849	88.305	1422.04	1241.64	1185.265	0.062	0.071	0.075
	S3	7.225	236.531	78.184	238.698	1052.44	951.64	920.14	0.227	0.251	0.259
	S11	669.554	35.528	680.213	236.394	1417.392	1269.792	1223.667	0.480	0.536	0.556
8	S1	254.482	137.346	295.686	213.690	641	588.5	564.875	0.461	0.502	0.523
	S9	340.989	56.450	357.924	158.747	1031.05	928.55	882.425	0.347	0.385	0.406
	S2	14.370	188.934	71.050	193.245	1221.9	1106.4	1054.425	0.158	0.175	0.183
	S10	60.426	109.377	93.239	127.505	1777.55	1552.05	1450.575	0.072	0.082	0.088
	S3	11.446	304.609	102.828	308.043	1315.55	1189.55	1132.85	0.234	0.259	0.272
	S11	915.189	33.596	925.268	308.153	1771.74	1587.24	1504.215	0.522	0.583	0.615
7	S1	320.182	167.267	370.362	263.322	769.2	706.2	672.075	0.481	0.524	0.551
	S9	440.096	70.612	461.279	202.640	1237.26	1114.26	1047.635	0.373	0.414	0.440
	S2	18.338	238.462	89.876	243.964	1466.28	1327.68	1252.605	0.166	0.184	0.195
	S10	73.693	154.024	119.900	176.132	2133.06	1862.46	1715.885	0.083	0.095	0.103
	S3	15.934	373.942	128.116	378.722	1578.66	1427.46	1345.56	0.240	0.265	0.281
	S11	1184.743	28.122	1193.179	383.545	2126.088	1904.688	1784.763	0.561	0.626	0.669
6	S1	392.056	196.128	450.894	313.745	897.4	823.9	784.525	0.502	0.547	0.575
	S9	547.585	85.711	573.299	249.987	1443.47	1299.97	1223.095	0.397	0.441	0.469
	S2	20.073	290.976	107.366	296.998	1710.66	1548.96	1462.335	0.174	0.192	0.203
	S10	79.047	200.282	139.131	223.996	2488.57	2172.87	2003.745	0.090	0.103	0.112
	S3	25.823	447.016	159.927	454.763	1841.77	1665.37	1570.87	0.247	0.273	0.289
	S11	1492.906	16.830	1497.955	464.702	2480.436	2222.136	2083.761	0.604	0.674	0.719
5	S1	467.765	225.101	535.295	365.430	1025.6	941.6	902.225	0.522	0.568	0.593
	S9	663.998	108.623	696.585	307.822	1649.68	1485.68	1408.805	0.422	0.469	0.494
	S2	20.832	343.658	123.929	349.907	1955.04	1770.24	1683.615	0.179	0.198	0.208
	S10	88.642	247.715	162.956	274.307	2844.08	2483.28	2314.155	0.096	0.110	0.119
	S3	39.763	518.987	195.459	530.916	2104.88	1903.28	1808.78	0.252	0.279	0.294
	S11	1808.403	5.768	1810.133	548.288	2834.784	2539.584	2401.209	0.639	0.713	0.754
4	S1	542.987	252.427	618.715	415.323	1153.8	1059.3	1025.175	0.536	0.584	0.604
	S9	780.117	135.648	820.812	369.683	1855.89	1671.39	1604.765	0.442	0.491	0.511
	S2	20.120	393.494	138.168	399.530	2199.42	1991.52	1916.445	0.182	0.201	0.208
	S10	102.764	297.118	191.899	327.947	3199.59	2793.69	2647.115	0.102	0.117	0.124
	S3	56.368	586.054	232.184	602.965	2367.99	2141.19	2059.29	0.255	0.282	0.293

	S11	2108.294	3.884	2109.459	636.372	3189.132	2857.032	2737.107	0.661	0.738	0.771
3	S1	620.039	278.887	703.705	464.899	1282	1177	1153.375	0.549	0.598	0.610
	S9	890.197	161.359	938.605	428.418	2062.1	1857.1	1810.975	0.455	0.505	0.518
	S2	25.587	437.175	156.739	444.851	2443.8	2212.8	2160.825	0.182	0.201	0.206
	S10	119.439	341.662	221.938	377.494	3555.1	3104.1	3002.625	0.106	0.122	0.126
	S3	73.196	645.282	266.781	667.241	2631.1	2379.1	2322.4	0.254	0.280	0.287
	S11	2385.952	14.328	2390.251	730.114	3543.48	3174.48	3091.455	0.675	0.753	0.773
2	S1	690.449	302.543	781.212	509.678	1410.2	1294.7	1281.575	0.554	0.603	0.610
	S9	986.564	185.087	1042.090	481.056	2268.31	2042.81	2017.185	0.459	0.510	0.517
	S2	34.674	473.352	176.679	483.754	2688.18	2434.08	2405.205	0.180	0.199	0.201
	S10	137.038	380.315	251.133	421.426	3910.61	3414.51	3358.135	0.108	0.123	0.125
	S3	88.056	692.305	295.747	718.721	2894.21	2617.01	2585.51	0.248	0.275	0.278
	S11	2614.217	26.104	2622.049	810.369	3897.828	3491.928	3445.803	0.673	0.751	0.761
1	S1	740.179	318.266	835.658	540.319	1538.4	1412.4	1409.775	0.543	0.592	0.593
	S9	1052.732	201.392	1113.150	517.212	2474.52	2228.52	2223.395	0.450	0.500	0.501
	S2	40.273	499.299	190.062	511.381	2932.56	2655.36	2649.585	0.174	0.193	0.193
	S10	150.215	406.996	272.313	452.060	4266.12	3724.92	3713.645	0.106	0.121	0.122
	S3	100.607	723.785	317.742	753.967	3157.32	2854.92	2848.62	0.239	0.264	0.265
	S11	2759.854	37.315	2771.049	865.271	4252.176	3809.376	3800.151	0.652	0.727	0.729

Çizelge B.176: 6 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_{G+\beta Q0}$, $k_{E\gamma} = N_E / N_{G+\gamma Q0}$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_{G+Q}$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
6	S1	28.794	9.395	31.613	18.033	128.2	122.95	112.45	0.247	0.257	0.281
	S9	40.320	2.136	40.961	14.232	206.21	195.96	175.46	0.199	0.209	0.233
	S2	7.785	11.873	11.347	14.209	244.38	232.83	209.73	0.058	0.061	0.068
	S10	26.561	7.482	28.806	15.450	355.51	332.96	287.86	0.081	0.087	0.100
	S3	4.218	21.189	10.575	22.454	263.11	250.51	225.31	0.085	0.090	0.100
	S11	144.700	14.202	148.960	57.612	354.348	335.898	298.998	0.420	0.443	0.498
5	S1	82.415	25.765	90.145	50.490	256.4	245.9	230.15	0.352	0.367	0.392
	S9	111.214	9.623	114.101	42.987	412.42	391.92	361.17	0.277	0.291	0.316
	S2	22.067	34.262	32.346	40.882	488.76	465.66	431.01	0.084	0.088	0.095
	S10	63.440	23.665	70.539	42.697	711.02	665.92	598.27	0.099	0.106	0.118
	S3	7.220	53.118	23.156	55.284	526.22	501.02	463.22	0.105	0.110	0.119
	S11	355.381	23.245	362.354	129.859	708.696	671.796	616.446	0.511	0.539	0.588
4	S1	138.281	42.638	151.073	84.123	384.6	368.85	353.1	0.393	0.410	0.428
	S9	184.941	17.742	190.263	73.225	618.63	587.88	557.13	0.308	0.324	0.342
	S2	36.382	57.395	53.601	68.309	733.14	698.49	663.84	0.093	0.098	0.103
	S10	103.822	40.639	116.014	71.786	1066.53	998.88	931.23	0.109	0.116	0.125
	S3	10.094	85.114	35.628	88.142	789.33	751.53	713.73	0.112	0.117	0.123
	S11	576.289	32.208	585.952	205.095	1063.044	1007.694	952.344	0.551	0.581	0.615
3	S1	193.985	58.569	211.556	116.765	512.8	491.8	481.3	0.413	0.430	0.440
	S9	261.794	25.518	269.449	104.056	824.84	783.84	763.34	0.327	0.344	0.353
	S2	49.946	81.797	74.486	96.781	977.52	931.32	908.22	0.099	0.104	0.107
	S10	138.636	61.338	157.037	102.929	1422.04	1331.84	1286.74	0.110	0.118	0.122
	S3	13.455	116.329	48.354	120.366	1052.44	1002.04	976.84	0.114	0.120	0.123
	S11	803.577	35.223	814.143	276.295	1417.392	1343.592	1306.692	0.574	0.606	0.623
2	S1	243.795	72.471	265.536	145.610	641	614.75	609.5	0.414	0.432	0.436
	S9	332.640	32.524	342.397	132.316	1031.05	979.8	969.55	0.332	0.349	0.353
	S2	61.743	105.295	93.331	123.818	1221.9	1164.15	1152.6	0.101	0.106	0.107
	S10	165.413	82.879	190.277	132.503	1777.55	1664.8	1642.25	0.107	0.114	0.116
	S3	16.823	143.987	60.019	149.034	1315.55	1252.55	1239.95	0.113	0.119	0.120
	S11	1008.031	31.805	1017.573	334.214	1771.74	1679.49	1661.04	0.574	0.606	0.613
1	S1	278.801	83.108	303.733	166.748	769.2	737.7	737.7	0.395	0.412	0.412
	S9	384.937	37.913	396.311	153.394	1237.26	1175.76	1175.76	0.320	0.337	0.337
	S2	68.454	124.250	105.729	144.786	1466.28	1396.98	1396.98	0.099	0.104	0.104
	S10	182.905	102.028	213.513	156.899	2133.06	1997.76	1997.76	0.100	0.107	0.107
	S3	19.005	164.801	68.445	170.503	1578.66	1503.06	1503.06	0.108	0.113	0.113
	S11	1148.735	23.105	1155.666	367.726	2126.088	2015.388	2015.388	0.544	0.573	0.573

Çizelge B.177: 9 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
9	S1	36.963	16.838	42.014	27.927	128.2	117.7	104.575	0.328	0.357	0.402
	S9	49.982	3.959	51.169	18.953	206.21	185.71	160.085	0.248	0.276	0.320
	S2	3.675	19.928	9.653	21.031	244.38	221.28	192.405	0.086	0.095	0.109
	S10	20.048	8.930	22.727	14.944	355.51	310.41	254.035	0.064	0.073	0.089
	S3	6.155	41.807	18.697	43.653	263.11	237.91	206.41	0.166	0.183	0.211
	S11	167.403	20.446	173.536	70.667	354.348	317.448	271.323	0.490	0.547	0.640
8	S1	107.458	45.806	121.199	78.043	256.4	235.4	207.05	0.473	0.515	0.585
	S9	141.780	17.206	146.942	59.740	412.42	371.42	316.07	0.356	0.396	0.465
	S2	14.329	57.665	31.629	61.963	488.76	442.56	380.19	0.127	0.140	0.163
	S10	52.373	31.733	61.893	47.444	711.02	620.82	499.05	0.087	0.100	0.124
	S3	8.673	102.054	39.289	104.656	526.22	475.82	407.78	0.199	0.220	0.257
	S11	424.043	32.729	433.861	159.942	708.696	634.896	535.266	0.612	0.683	0.811
7	S1	182.685	75.673	205.387	130.478	384.6	353.1	314.25	0.534	0.582	0.654
	S9	239.672	31.465	249.112	103.367	618.63	557.13	481.28	0.403	0.447	0.518
	S2	26.422	96.442	55.355	104.369	733.14	663.84	578.37	0.142	0.157	0.180
	S10	91.756	55.980	108.550	83.507	1066.53	931.23	764.36	0.102	0.117	0.142
	S3	11.861	162.917	60.736	166.475	789.33	713.73	620.49	0.211	0.233	0.268
	S11	704.938	47.375	719.150	258.857	1063.044	952.344	815.814	0.677	0.755	0.882
6	S1	263.303	105.237	294.874	184.228	512.8	470.8	426.7	0.575	0.626	0.691
	S9	350.442	45.798	364.181	150.930	824.84	742.84	656.74	0.442	0.490	0.555
	S2	39.736	139.544	81.599	151.465	977.52	885.12	788.1	0.155	0.171	0.192
	S10	127.651	88.606	154.232	126.901	1422.04	1241.64	1052.22	0.108	0.124	0.147
	S3	17.062	225.585	84.738	230.703	1052.44	951.64	845.8	0.219	0.242	0.273
	S11	1023.428	54.614	1039.812	361.642	1417.392	1269.792	1114.812	0.734	0.819	0.933
5	S1	347.385	133.899	387.555	238.114	641	588.5	544.4	0.605	0.659	0.712
	S9	469.762	59.784	487.697	200.712	1031.05	928.55	842.45	0.473	0.525	0.579
	S2	54.891	185.750	110.616	202.218	1221.9	1106.4	1009.38	0.165	0.183	0.200
	S10	161.408	126.891	199.475	175.313	1777.55	1552.05	1362.63	0.112	0.129	0.146
	S3	24.383	288.012	110.786	295.327	1315.55	1189.55	1083.71	0.224	0.248	0.273
	S11	1367.041	55.974	1383.833	466.086	1771.74	1587.24	1432.26	0.781	0.872	0.966
4	S1	428.694	160.704	476.905	289.312	769.2	706.2	667.35	0.620	0.675	0.715
	S9	592.195	73.277	614.178	250.935	1237.26	1114.26	1038.41	0.496	0.551	0.591
	S2	66.464	231.512	135.918	251.451	1466.28	1327.68	1242.21	0.171	0.189	0.202
	S10	192.404	171.739	243.925	229.460	2133.06	1862.46	1695.59	0.114	0.131	0.144
	S3	31.380	348.007	135.782	357.420	1578.66	1427.46	1334.22	0.226	0.250	0.268
	S11	1718.883	53.333	1734.883	568.998	2126.088	1904.688	1768.158	0.816	0.911	0.981
3	S1	508.676	184.168	563.926	336.771	897.4	823.9	795.55	0.628	0.684	0.709
	S9	712.801	86.507	738.753	300.348	1443.47	1299.97	1244.62	0.512	0.568	0.594
	S2	73.690	275.773	156.422	297.880	1710.66	1548.96	1486.59	0.174	0.192	0.200
	S10	211.285	215.015	275.789	278.400	2488.57	2172.87	2051.1	0.112	0.128	0.136
	S3	42.908	405.540	164.570	418.413	1841.77	1665.37	1597.33	0.227	0.251	0.262
	S11	2076.074	44.554	2089.440	667.376	2480.436	2222.136	2122.506	0.842	0.940	0.984
2	S1	580.269	204.529	641.628	378.610	1025.6	941.6	923.75	0.626	0.681	0.695
	S9	821.820	103.595	852.899	350.141	1649.68	1485.68	1450.83	0.517	0.574	0.588
	S2	78.496	314.248	172.770	337.796	1955.04	1770.24	1730.97	0.173	0.191	0.195
	S10	229.214	251.994	304.812	320.759	2844.08	2483.28	2406.61	0.113	0.129	0.133
	S3	56.169	454.500	192.519	471.351	2104.88	1903.28	1860.44	0.224	0.248	0.253
	S11	2380.734	33.267	2390.714	747.487	2834.784	2539.584	2476.854	0.843	0.941	0.965
1	S1	630.639	219.504	696.491	408.696	1153.8	1059.3	1051.95	0.604	0.658	0.662
	S9	902.439	120.078	938.463	390.810	1855.89	1671.39	1657.04	0.506	0.561	0.566
	S2	79.843	342.817	182.688	366.770	2199.42	1991.52	1975.35	0.167	0.184	0.186
	S10	244.828	282.777	329.661	356.225	3199.59	2793.69	2762.12	0.111	0.128	0.129
	S3	66.680	488.448	213.214	508.452	2367.99	2141.19	2123.55	0.215	0.237	0.239
	S11	2573.754	19.871	2579.715	791.997	3189.132	2857.032	2831.202	0.809	0.903	0.911

Çizelge B.178: 12 Kat, İzmir, ZE Zemin Sınıfına Ait Deprem Etkisinden Oluşan Eksenel Kuvvetler ve k_E Oranları.

$k_E = N_E / N_{G0+Q0}$, $k_{E\beta} = N_E / N_G + \beta Q_0$, $k_{E\gamma} = N_E / N_G + \gamma Q_0$											
KAT	KOLON	N_E (kN)				N_{G0+Q0} (kN)	$N_{G0+\beta Q0}$ (kN)	$N_{G0+\gamma Q0}$ (kN)	$k_E = N_E / N_G + Q$		
		N_{Ex}	N_{Ey}	$N_{Ex} + 0,3N_{Ey}$	$N_{Ey} + 0,3N_{Ex}$				k_E	$k_{E\beta}$	$k_{E\gamma}$
12	S1	37.436	24.843	44.889	44.889	128.2	117.7	117.7	0.350	0.381	0.381
	S9	49.185	4.637	50.576	50.576	206.21	185.71	185.71	0.245	0.272	0.272
	S2	2.470	29.425	11.298	11.298	244.38	221.28	221.28	0.046	0.051	0.051
	S10	5.254	8.542	7.817	7.817	355.51	310.41	310.41	0.022	0.025	0.025
	S3	6.090	64.105	25.321	25.321	263.11	237.91	237.91	0.096	0.106	0.106
	S11	147.939	22.448	154.673	154.673	354.348	317.448	317.448	0.437	0.487	0.487
11	S1	110.597	67.230	130.766	130.766	256.4	235.4	235.4	0.510	0.556	0.556
	S9	143.486	22.520	150.242	150.242	412.42	371.42	371.42	0.364	0.405	0.405
	S2	0.698	84.809	26.140	26.140	488.76	442.56	442.56	0.053	0.059	0.059
	S10	22.096	36.296	32.984	32.984	711.02	620.82	620.82	0.046	0.053	0.053
	S3	6.131	154.530	52.490	52.490	526.22	475.82	475.82	0.100	0.110	0.110
	S11	387.168	32.627	396.956	396.956	708.696	634.896	634.896	0.560	0.625	0.625
10	S1	189.099	110.838	222.351	222.351	384.6	353.1	353.1	0.578	0.630	0.630
	S9	244.470	41.833	257.020	257.020	618.63	557.13	557.13	0.415	0.461	0.461
	S2	5.569	141.227	47.937	47.937	733.14	663.84	663.84	0.065	0.072	0.072
	S10	46.479	65.798	66.218	66.218	1066.53	931.23	931.23	0.062	0.071	0.071
	S3	7.143	246.027	80.951	80.951	789.33	713.73	713.73	0.103	0.113	0.113
	S11	653.904	46.995	668.003	668.003	1063.044	952.344	952.344	0.628	0.701	0.701
9	S1	274.847	154.585	321.223	321.223	512.8	470.8	457.675	0.626	0.682	0.702
	S9	361.586	61.591	380.063	380.063	824.84	742.84	717.215	0.461	0.512	0.530
	S2	11.824	204.187	73.080	73.080	977.52	885.12	856.245	0.075	0.083	0.085
	S10	67.230	107.374	99.442	99.442	1422.04	1241.64	1185.265	0.070	0.080	0.084
	S3	10.435	341.631	112.924	112.924	1052.44	951.64	920.14	0.107	0.119	0.123
	S11	967.062	51.314	982.457	982.457	1417.392	1269.792	1223.667	0.693	0.774	0.803
8	S1	367.559	198.373	427.071	427.071	641	588.5	564.875	0.666	0.726	0.756
	S9	492.503	81.533	516.963	516.963	1031.05	928.55	882.425	0.501	0.557	0.586
	S2	20.755	272.885	102.621	102.621	1221.9	1106.4	1054.425	0.084	0.093	0.097
	S10	87.276	157.977	134.669	134.669	1777.55	1552.05	1450.575	0.076	0.087	0.093
	S3	16.531	439.958	148.519	148.519	1315.55	1189.55	1132.85	0.113	0.125	0.131
	S11	1321.843	48.524	1336.400	1336.400	1771.74	1587.24	1504.215	0.754	0.842	0.888
7	S1	462.451	241.590	534.928	534.928	769.2	706.2	672.075	0.695	0.757	0.796
	S9	635.647	101.987	666.243	666.243	1237.26	1114.26	1047.635	0.538	0.598	0.636
	S2	26.486	344.420	129.812	129.812	1466.28	1327.68	1252.605	0.089	0.098	0.104
	S10	106.438	222.463	173.176	173.176	2133.06	1862.46	1715.885	0.081	0.093	0.101
	S3	23.013	540.098	185.043	185.043	1578.66	1427.46	1345.56	0.117	0.130	0.138
	S11	1711.169	40.618	1723.354	1723.354	2126.088	1904.688	1784.763	0.811	0.905	0.966
6	S1	566.261	283.275	651.243	651.243	897.4	823.9	784.525	0.726	0.790	0.830
	S9	790.898	123.796	828.037	828.037	1443.47	1299.97	1223.095	0.574	0.637	0.677
	S2	28.993	420.267	155.073	155.073	1710.66	1548.96	1462.335	0.091	0.100	0.106
	S10	114.170	289.274	200.952	200.952	2488.57	2172.87	2003.745	0.081	0.092	0.100
	S3	37.297	645.643	230.989	230.989	1841.77	1665.37	1570.87	0.125	0.139	0.147
	S11	2156.260	24.308	2163.553	2163.553	2480.436	2222.136	2083.761	0.872	0.974	1.038
5	S1	675.610	325.122	773.146	773.146	1025.6	941.6	902.225	0.754	0.821	0.857
	S9	959.037	156.888	1006.103	1006.103	1649.68	1485.68	1408.805	0.610	0.677	0.714
	S2	30.089	496.358	178.996	178.996	1955.04	1770.24	1683.615	0.092	0.101	0.106
	S10	128.029	357.784	235.364	235.364	2844.08	2483.28	2314.155	0.083	0.095	0.102
	S3	57.431	749.593	282.309	282.309	2104.88	1903.28	1808.78	0.134	0.148	0.156
	S11	2611.944	8.330	2614.443	2614.443	2834.784	2539.584	2401.209	0.922	1.029	1.089
4	S1	784.256	364.590	893.633	893.633	1153.8	1059.3	1025.175	0.775	0.844	0.872
	S9	1126.753	195.922	1185.529	1185.529	1855.89	1671.39	1604.765	0.639	0.709	0.739
	S2	29.059	568.338	199.561	199.561	2199.42	1991.52	1916.445	0.091	0.100	0.104
	S10	148.425	429.139	277.167	277.167	3199.59	2793.69	2647.115	0.087	0.099	0.105
	S3	81.414	846.460	335.352	335.352	2367.99	2141.19	2059.29	0.142	0.157	0.163

	S11	3045.089	5.609	3046.772	3046.772	3189.132	2857.032	2737.107	0.955	1.066	1.113
3	S1	895.546	402.807	1016.388	1016.388	1282	1177	1153.375	0.793	0.864	0.881
	S9	1285.745	233.057	1355.662	1355.662	2062.1	1857.1	1810.975	0.657	0.730	0.749
	S2	36.956	631.429	226.384	226.384	2443.8	2212.8	2160.825	0.093	0.102	0.105
	S10	172.510	493.476	320.553	320.553	3555.1	3104.1	3002.625	0.090	0.103	0.107
	S3	105.720	932.006	385.321	385.321	2631.1	2379.1	2322.4	0.146	0.162	0.166
	S11	3446.121	20.695	3452.330	3452.330	3543.48	3174.48	3091.455	0.974	1.088	1.117
2	S1	997.241	436.974	1128.333	1128.333	1410.2	1294.7	1281.575	0.800	0.872	0.880
	S9	1424.931	267.329	1505.129	1505.129	2268.31	2042.81	2017.185	0.664	0.737	0.746
	S2	50.080	683.681	255.185	255.185	2688.18	2434.08	2405.205	0.095	0.105	0.106
	S10	197.930	549.303	362.720	362.720	3910.61	3414.51	3358.135	0.093	0.106	0.108
	S3	127.183	999.922	427.159	427.159	2894.21	2617.01	2585.51	0.148	0.163	0.165
	S11	3775.813	37.703	3787.124	3787.124	3897.828	3491.928	3445.803	0.972	1.085	1.099
1	S1	1069.068	459.683	1206.973	1206.973	1538.4	1412.4	1409.775	0.785	0.855	0.856
	S9	1520.501	290.878	1607.764	1607.764	2474.52	2228.52	2223.395	0.650	0.721	0.723
	S2	58.168	721.156	274.514	274.514	2932.56	2655.36	2649.585	0.094	0.103	0.104
	S10	216.961	587.839	393.312	393.312	4266.12	3724.92	3713.645	0.092	0.106	0.106
	S3	145.310	1045.391	458.927	458.927	3157.32	2854.92	2848.62	0.145	0.161	0.161
	S11	3986.162	53.895	4002.330	4002.330	4252.176	3809.376	3800.151	0.941	1.051	1.053